APPENDIX A

Oregon Water Quality Standards (excerpt)

The Oregon Administrative Rules containing OARs filed through June 13, 2008[1]

DEPARTMENT OF ENVIRONMENTAL QUALITY

WATER POLLUTION

DIVISION 41 (excerpts)

WATER QUALITY STANDARDS: BENEFICIAL USES, POLICIES, AND CRITERIA FOR OREGON

340-041-0009

Bacteria

(6) Sewer Overflows in winter: Domestic waste collection and treatment facilities are prohibited from discharging raw sewage to waters of the State during the period of November 1 through May 21, except during a storm event greater than the one-in-five-year, 24-hour duration storm. However, the following exceptions apply:

(a) The Commission may on a case-by-case basis approve a bacteria control management plan to be prepared by the permittee, for a basin or specified geographic area which describes hydrologic conditions under which the numeric bacteria criteria would be waived. These plans will identify the specific hydrologic conditions, identify the public notification and education processes that will be followed to inform the public about an event and the plan, describe the water quality assessment conducted to determine bacteria sources and loads associated with the specified hydrologic conditions, and describe the bacteria control program that is being implemented in the basin or specified geographic area for the identified sources;

(b) Facilities with separate sanitary and storm sewers existing on January 10, 1996, and which currently experience sanitary sewer overflows due to inflow and infiltration problems, must submit an acceptable plan to the Department at the first permit renewal, which describes actions that will be taken to assure compliance with the discharge prohibition by January 1, 2010. Where discharges occur to a receiving stream with sensitive beneficial uses, the Department may negotiate a more aggressive schedule for discharge elimination;

(c) On a case-by-case basis, the beginning of winter may be defined as October 15, if the permittee so requests and demonstrates to the Department's satisfaction that the risk to beneficial uses, including water contact recreation, will not be increased due to the date change.

(7) Sewer Overflows in summer: Domestic waste collection and treatment facilities are prohibited from discharging raw sewage to waters of the State during the period of May 22

[1] http://arcweb.sos.state.or.us/rules/OARs_300/OAR_340/340_041.html

through October 31, except during a storm event greater than the one-in-ten-year, 24-hour duration storm. The following exceptions apply:

(a) For facilities with combined sanitary and storm sewers, the Commission may on a case-by-case basis approve a bacteria control management plan such as that described in subsection (6)(a) of this rule;

(b) On a case-by-case basis, the beginning of summer may be defined as June 1 if the permittee so requests and demonstrates to the Department's satisfaction that the risk to beneficial uses, including water contact recreation, will not be increased due to the date change;

(c) For discharge sources whose permit identifies the beginning of summer as any date from May 22 through May 31: If the permittee demonstrates to the Department's satisfaction that an exceedance occurred between May 21 and June 1 because of a sewer overflow, and that no increase in risk to beneficial uses, including water contact recreation, occurred because of the exceedance, no violation may be triggered, if the storm associated with the overflow was greater than the one-in-five-year, 24-hour duration storm.

APPENDIX B

City Land Use Categories

Master Metro Plan

PLAN_CLASS	DEFINITION	DESCRIPTION
CC	Central Commercial	Allows a full range of commercial activities typically associated with central business districts. More restrictive than general commercial in the case of large lot and highway oriented uses, but usually allows multi-story development.
CG	General Commercial	Larger scale commercial districts, often with a more regional orientation for providing services. Businesses offering a wide variety of goods and services are permitted and include highway and strip commercial zones.
CN	Neighborhood Commercial	Small scale commercial districts permitting retail and service activities such as grocery stores and laundromats supporting the local residential community. Floor space and/or lot size is usually imited from 5,000 to 10,000 square feet.
CO	Office Commercial	Districts accomodating a range of business, professional and medical office facilities, typically as a buffer between residential areas and more intensive uses.
FF	Agriculture or Forestry	Activities suited to commercial scale agricultural production, typically with lot sizes of 30 acres or more.
IA	Industrial Area	Districts designated exclusively for manufacturing, industrial, warehouse and distribution related operations.
IH	Heavy Industrial	Districts permitting light industrial and more intensive industrial activities such as bottling, limited chemical processing, heavy manufacturing and similar uses.
IL	Light Industrial	Districts permitting warehousing and light processing and fabrication activities. May allow some commercial activities.
IMU	Mixed Use Industrial	Districts accommodating a mix of light manufacturing, office and retail uses.
MFR1	Multi family 1	Housing and or duplex, townhouse and attached single-family structures allowed outright. Maximum net allowable densities range from 2 to 25 units per acre, with height limits usually set at 2 1/2 to 3 stories.
MFR2	Multi family 2	Housing accommodating densities ranging from 25 to 50 units per acre. Buildings may exceed three stories in height.
MFR3	Multi family 3	Housing accomodating densities ranging from 50 to 100 units.
MFR4	Multi family 4	Housing accommodating densities greater than 100 units. This is the densest of the multi-family zones and would require greater use of vertical space and buildings with multiple stories.
MUC1	Mixed Used Center 1	Combines residential and employment uses in town centers, main streets and corridors.
MUC2	Mixed Used Center 2	Combines residential and employment uses in light rail station areas and regional centers.
MUC3	Mixed Used Center 3	Combines residential and employment uses in central city locations. Mixed use is weighted toward residential development.
PF	Public Facilities	Public Facilities
POS	Parks and Open Space	Parks and Open Space
RRFU	Rural or Future Urban	Residential uses permitted on rural lands or areas designated for future urban development, with minimum lot sizes of one acre or more.
SFR1	Single Family 1	Detached housing with minimum lot sizes from 20,000 sq feet and up.
SFR2	Single Family 2	Detached housing with minimum lot sizes ranging from 12,000 to 20,000 sq feet.
SFR3	Single Family 3	Detached housing with minimum lot sizes ranging from 8,500 to 12,000 sq feet.
SFR4	Single Family 4	Detached housing with minimum lot sizes from 6,500 to 8,500 sq feet.
SFR5	Single Family 5	Detached housing with minimum lot sizes ranging from 5,500 to 6,500 sq feet.
SFR6	Single Family 6	Detached housing with minimum lot sizes from 4,000 to 5,500 sq feet.
SFR7	Single Family 7	Detached housing with minimum lot sizes ranging from 0 to 4,000 sq feet.

City of Hillsboro Land Use Codes

CITY CODE	HILLSBORO DESCRIPTION ** to be confirmed	METRO CODE
C	Commercial	CG
FP		POS
IN	Industrial	IMU
MU	Mixed Use	MUC1
OS	Open space	POS
PF	Public Facility	PF
RH	Residential - High Density	MFR1
RL	Residential - Low Density	SFR2
RM	Residential - Medium Density	MFR1
RMR		MFR2
SCPA		MUC2

GIS data received from City?:	Yes
Name of data set used for land use:	COMP.shp
Comments received from City?:	Yes - map markups
Were comments addressed by West Yost?:	Yes
Method used to derive METRO CODE:	Referred to City-Metro mapped codes in the Metro PLAN data set

WEST YOST ASSOCIATES
Consulting Engineers

TECHNICAL MEMORANDUM NO. 1 (DRAFT)

DATE:	April 12, 2007	Project No.:	517-03-06-14
TO:	Andy Braun Clean Water Services	CC:	Distribution (see Attachment 3)
FROM:	Jeff Pelz	Reviewed By:	Lynne Chicoine

SUBJECT: Sanitary Sewer Master Plan Update—Service Area Characteristics

The purpose of this memorandum is to document the land use assumptions to be used for the Clean Water Services (District) Sanitary Sewer Master Plan Update. The land use assumptions are based on input from the various jurisdictions that comprise the District. This memorandum is organized around the following topics:

- Land Use Data Compilation
- Growth Phasing (Existing, 2010, 2020, and Buildout)
- Presentation of the compiled data (land use maps)

Upon approval, the land uses presented herein will be used to generate flows within the sanitary sewer computer model to predict existing and future flows and sewer capacity needs.

LAND USE DATA COMPILATION

Land use information was obtained from the individual cities within the District, as well as from Metro. West Yost Associates (WYA) met with representatives from each of the member agencies, as well as Metro and Washington County planning staff. During these meetings, the jurisdictions reviewed and commented on preliminary land use maps based on zoning, and provided WYA with the most up to date land use planning information available. Some agencies provided graphical files and databases that reflect current planning assumptions for the agency. Others provided verbal comments which were recorded in written notes and mapping annotations. Meeting records are included as Attachment 1.

Land use data for unincorporated areas currently within the District were obtained from Metro's Regional Land Information System (RLIS) and discussions with Washington County Planning Staff. Metro data was used only where data were not available from the interviews with cities' staff. Therefore, future land use assumptions for some potential growth areas are based on the Metro RLIS data. For the remaining areas cities or Washington County provided specific

information based on their own planning process. In many cases, the Metro land use designation for potential urban growth boundary expansion areas is “RRFU” (Rural Residential or Future Urban) or “FF” (Agriculture or Forestry).In many cases, no input regarding future land uses in these areas has been provided to WYA. Additional input from the District and cities is needed to define the basis of planning future wastewater flows for these areas.

Figure 1 summarizes the overall study area based on input received to date. The figure shows two categories of expansion study areas where future sewer service is anticipated. For sewer planning purposes, it will be assumed that the District will ultimately provide service to these areas; however, inclusion of these areas in the master plan study area does not represent a commitment serve the area or entitlement of any kind. The two expansion study area categories shown on Figure 1 are:

District Expansion Study Areas. These areas are inside the UGB but not currently served by the District.

UGB Expansion Study Areas. These areas are outside the UGB, but have been identified as planned growth areas by one or more agencies.

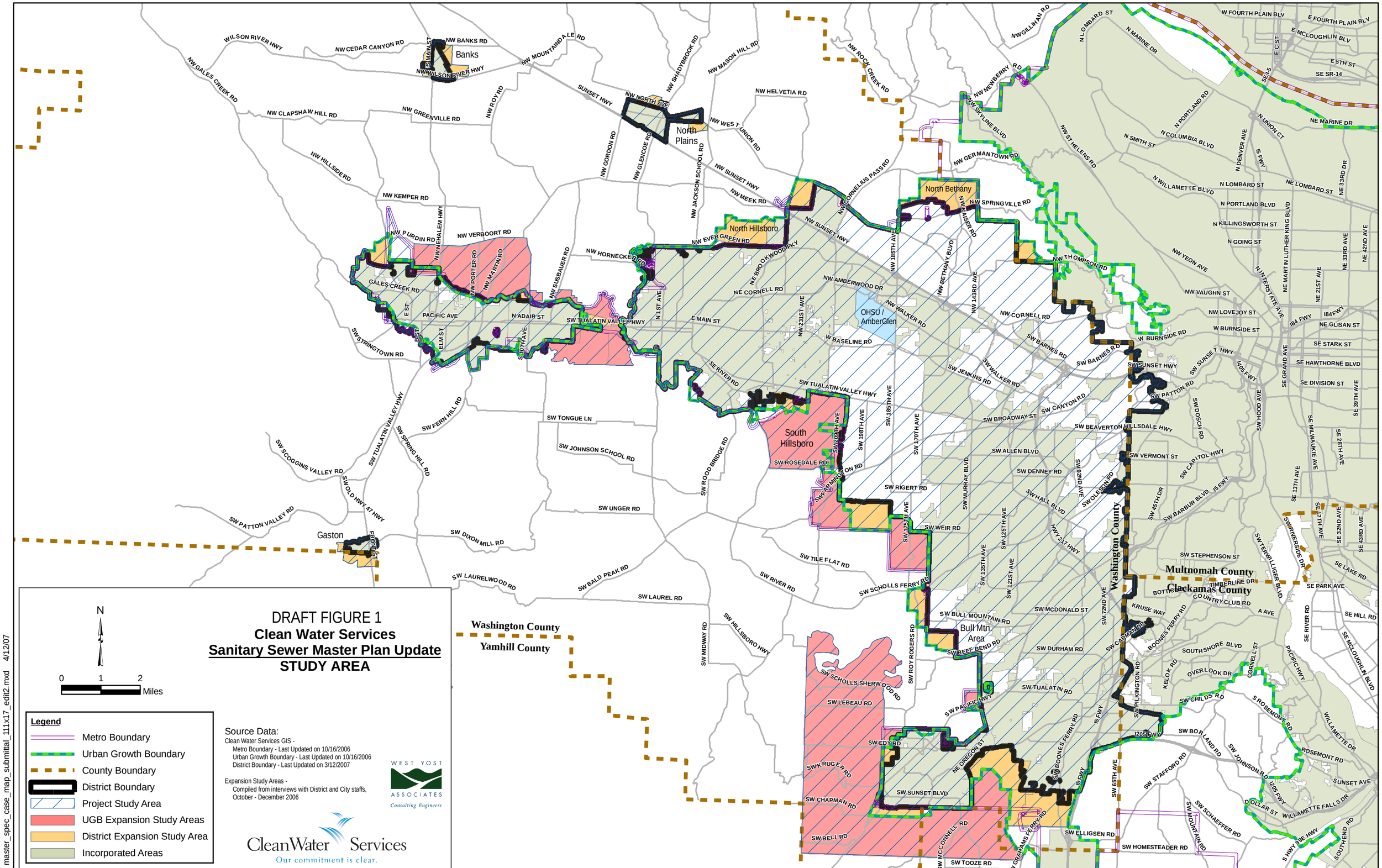
Many jurisdictions within the District use their own unique land use category designations. This creates significant complexity in the process of preparing a unified map and database that will be used to generate flows within the sewer model. The procedures used to compile the comprehensive District land use map are as follows:

1. Use District GIS and Metro RLIS data to prepare a base map of the District service areas, as well as to depict the current Urban Growth Boundary (UGB) and tax lot boundaries. In general, the Metro RLIS data is used for all base mapping underlying the land use designations.
2. Combine into a single map the electronic land use mapping provided to WYA by the following cities in late 2006 and early 2007:

   Beaverton
   Forest Grove
   Hillsboro
   Tigard
   Tualatin

3. Incorporate the land use mapping changes noted by the jurisdictions during WYA’s meetings with staff. In lieu of electronic data, paper maps and/or land use mapping annotations were received during meetings with the following cities:

   Banks
   Cornelius
   Gaston
   North Plains
   Sherwood


DRAFT FIGURE 1
Clean Water Services
Sanitary Sewer Master Plan Update
STUDY AREA
N
0 1 2
Miles
Legend
Metro Boundary
Urban Growth Boundary
County Boundary
District Boundary
Project Study Area
UGB Expansion Study Areas
District Expansion Study Area
Incorporated Areas
Source Data:
Clean Water Services GIS -
Metro Boundary - Last Updated on 10/16/2006
Urban Growth Boundary - Last Updated on 10/16/2006
District Boundary - Last Updated on 3/12/2007
Expansion Study Areas -
Compiled from interviews with District and City staffs, October - December 2006
WEST YOST ASSOCIATES
Consulting Engineers
Clean Water Services
Our commitment is clear.
Banks
North Plains
North Hillsboro
North Bethany
OHSU / AmberGlen
South Hillsboro
Bull Mtn Area
Gaston
Washington County
Yamhill County
Multnomah County
Clackamas County
Washington County
master_spec_case_map_submittal_111x17_edit2.mxd 4/12/07

4. Prepare, for District and city review, tables of the land use codes to be used for wastewater flow projections. The tables will include the land use category code and description. In addition, each residential category will have a predicted density in terms of dwelling units per acre. A single value (in lieu of a range of values) is needed for population and wastewater flow projections. The listed density represents the anticipated average density at buildout for all lands in the given category. The resulting table is provided as Attachment 2. Attachment 2 will also be used in later phases of this project to assign wastewater flow generation factors. Most of the cities have not yet provided residential density values, and WYA requests this important information be forwarded as soon as possible.
5. Identify for District and city review and confirmation those parcels where the land use category from the cities is substantively different from the category reported by Metro. Those parcels requiring confirmation are highlighted in yellow on the maps provided electronically with this memorandum. In each case, the city land use code and Metro land use code are displayed. Unless City staff direct a different course of action for particular locations, the city land use code will supersede the Metro code.

The results of the land use data compilation are presented on a land use map for each listed city. Due to their large size, the maps are posted on WYA's internet ftp site. Recipients of this memorandum will be provided access to the ftp site for downloading one or more of the maps. The maps show the city-assigned land use category for all incorporated areas, and Metro's land use designation for areas where city data was not provided. In addition, tax lots where Metro's land us designation is substantively different from the city's land use designation are highlighted. Attachment 2 provides a list of the category names corresponding to the individual land use category labels used for the mapping.

GROWTH PHASING (EXISTING, 2010, 2020, AND BUILDOUT)

The Sanitary Sewer Master Plan Update includes sewer flow projections and analyses of capacity needs for existing conditions, 2010, 2020, and buildout. The previous Sanitary Sewer Master Plan (Arsenault, 2000) incorporated growth predictions in five year increments. The District has directed WYA to use the previous growth rate predictions to project flows for the updated master plan. The projections were expressed in terms of percentage of acres or residential dwelling units developed within each land use category within each census tract block group.

Development has, of course, occurred subsequent to the previous master planning and can be compared to growth predictions. The degree to which actual development patterns match the previous predictions varies from area to area. In order to use the previous growth projections it was necessary to compare actual existing conditions to those predicted for 2005 and 2010, and to adjust the previous predictions where development occurred at a different rate of growth different than anticipated. Projected growth rates are determined through the following steps:

1. The land use category assigned by the cities, or by Metro in the absence of a City designation, is assumed to be the buildout land use, unless city staff provided information to WYA regarding planned changes in land use.
2. Tax lot acreage is used as the buildout acreage for all uses.

3. For non-residential uses, wastewater flows are projected using gallons per day per acre (gpd/acre) factor, on a gross acreage basis. Residential sanitary flows are projected using a gpd per dwelling unit (gpd/du) factor. Therefore, for residential uses it is necessary to predict the total number of residential dwelling units at each phase of growth.
4. For single family residential categories, it is assumed that each non-vacant lot represents a single dwelling unit. Metro maintains RLIS data that indicates which tax lots are vacant and which are occupied, and this data is used to identify the non-vacant tax lots.
5. For multi-family land use categories, it is assumed that each non-vacant lot is developed at the predicted buildout density (du/acre) for the given multi-family category. The existing number of dwelling units is estimated using the predicted density multiplied by the acreage of each non-vacant tax lot. The buildout dwelling unit count is projected by multiplying the total tax lot acreage for the given land use category by the predicted density for the given category. Attachment 2 lists the predicted dwelling unit density for each land use category.
6. Development conditions for the two intermediate growth phases (2010 and 2020) are based on the growth predictions used in previous modeling for each census tract block group. Within a block group boundary, each land use category had a predicted level of development between zero and 100 percent for each five year increment from 2000 through 2020. The same levels of development as used in the previous model for 2010 and 2020 are assigned to each tax lot with a similar land use designation and located within the same block group boundary. Where existing development exceeds one or more of the predicted future conditions, the existing level of development is used.
7. Buildout is based on the assumptions that 100 percent of the planned development has occurred, and has no specified date.

PRESENTATION OF THE COMPILED DATA (LAND USE MAPS)

Large format maps are provided electronically with this memorandum for review and approval. The maps depict the build out land use categories to be used for predicting sanitary sewer flows within the current and anticipated District service area. The anticipated District service area includes potential UGB and District expansion study areas, which are defined above, and are shown on the large format maps as well as Figure 1.

As noted above, the maps also identify those tax lots within each city where a city's land use designation is substantively different from Metro's land use designation. For sanitary sewer planning purposes, a city's land use designation is used to predict sanitary sewer flows.

The maps will also be used in the future to show the amount of development predicted at each growth phase. Within each major land use area, the growth prediction will be indicated by three numbers representing the percent of build-out development under existing, 2010, and 2020 conditions. The mapping of growth prediction data will be provided for review as it becomes available.

We request that the District, with input from the cities, review and approve or comment on the land uses shown on the maps provided electronically with this memorandum. WYA will use the approved land use predictions in developing the updated sanitary sewer model.

JP:nmp

ATTACHMENT 1

Attachment 1

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: September 20, 2006**

Time: 1:15 pm

Contact Information:

Name: KJ Won	Other Attendees Present:
Agency: KJ Won, AICP Planning Consultant	
Agency/City Represented: City of Banks	
Phone: 503-292-2221	
Fax:	
Email: kjwon@mac.com	

Questions:

1. Current land use data

   The City has been built-out since about 1993. They need to expand their UGB and are in the process of looking at that now. They currently have a population of about 1,450 (last census) and are projected to have 37,339 by 2024. The county has accepted this growth rate (4.1 – 4.2%). The UGB currently coincides with the City limits.

2. Planned extensions/new developments within the City's current boundaries

   None – city is built-out.

3. Planned extensions/new developments beyond the City's current boundaries

   They need approximately 100 acres for residential and another 100 acres for commercial and industrial uses. There is potential land on all sides. North has steep slopes, so may not be

desirable. West and East (currently golf course) both have interested "sellers", but West has some wetland issues and East is across the railroad. South has some exceptions lands but any extensive growth would be across Hwy. 26 and down in elevation. KJ would like our help assessing which direction would be best for sewer development.

4. Land use changes coming - Metro or city

   None known yet. Banks has not been identified by Metro as a "neighboring city" so is not included in their planning.

5. How are they handling Measure 37 claims?

   No claims yet and don't expect many.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   They don't know yet which directions they will grow. Expansions will have to go to a vote.

7. Are there any planned annexations that you already know about?

   Acreage only – not specific areas.

8. Other Stuff:

   KJ gave me a copy of some emailed questions and responses between him and Andy Braun. He will also send a copy of the City's zoning map showing existing land uses and the following docs:

   - Plan Text Amendment to Update Long Term Population/Employment Forecase
   - Banks Comprehensive Plan Text Amendment to Update Housing and Residential Land Needs
   - Banks Comprehensive Plan Text Amendment to Update Commercial and Industrial Land Needs
   - Chapter 4 of the Banks Goal 9 Technical Report – Demand and Supply of Buildable Land in Banks

   He said that there was a sanitary sewer master plan done for Banks in 1997 by David Evans – we should get it from CWS. Dave Monson of LDC is the City Engineer – has been for 1-2 years. They City recorder is Jolynn Becker (503-324-5112) and Mike Lyda is the mayor.

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: November 17, 2006**

Time: 1:00 pm

Contact Information:

Name: KJ Won	Other Attendees Present:
Agency: KJ Won, AICP Planning Consultant	
Agency/City Represented: City of Banks	
Phone: 503-292-2221	
Fax:	
Email: kjwon@mac.com	

Discussion:

KJ showed me some exception lands that are located to the North of town. These are likely candidates to come in to the city, but residents may not want to be annexed. We looked at the topo in that area and I expressed that going to high up the hill could make sewer construction more expensive.

The exception lands to the south are over 50 acres. Each lot has a house and there is some commercial. Exceptions lands are north of Wilkesboro Road west to Aerts Road.

There is currently one Measure 37 claim south of Wilkesboro Road, but KJ did not have the details.

He will get us elevations at potential sewer connection points if available from the city.

WYA Interviewer: Corie Peterson **Date:** 10/17/06

Time: 9:30 am

Contact Information

Name: Hal Bergsma, Principal Planner	Other Attendees Present:
Agency: City of Beaverton	
Agency/City Represented: City of Beaverton	
Phone: 503-350-4037	
Fax: 503-526-3720	
Email: hbergsma@ci.beaverton.or.us	

Questions:

1. Current land use data

   There were many discrepancies between Metro zoning and city of Beaverton zoning. Several are marked on the map. We can get GIS zoning from Beaverton, but may have to pay for it. I will be in contact with Doug Taylor – GIS Specialist to coordinate.

   Metro population numbers are what they use, especially the transportation numbers in the regional centers (those use TAZ boundaries).

2. Planned extensions/new developments within the City's current boundaries

   Not much infill planned. A few areas of note are:

   - Barrows and Barnes – old Tufel nursery site.
   - Some higher density residential infill in community centers and town centers
   - Peterkort area – there is some vacant land near sunset transit center.
   - Area near summerville – developing now.

3. Planned extensions/new developments beyond the City's current boundaries

There is some interest in the area near Cooper Mountain Regional Park, but nothing is planned as of now. (Tile Flat Road and Scholls.)

4. Land use changes coming - Metro or city

   No specific major changes were mentioned, but Hal did mention that the regional centers allow for a very broad range of zoning depending on development demand. Currently they are mostly retail, but could be industrial, multifamily or commercial too.

5. How are they handling Measure 37 claims?

   They have had a couple of claims, but they are very minimal. One auto dealer down town – not sure what he really has planned, and an area East of Cedar Hills Blvd. and South of Hall where the owner wants to deviate from buffer zones. Hal said that this was one CWS was currently looking at.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   Hal sees an annexation west to 170th and 185 North to Highway 26 and South to the Tigard City line as very likely to happen in the next 8ish years. Beyond that, who knows.

7. Are there any planned annexations that you already know about?

   None officially planned.

WYA Interviewer: Bhargavi Ambadkar, Jeff Pelz **Date:** 12/06/06

Time: 3:00 pm

Contact Information

Name: Dave Winship, City Utilities Engineer Mark Boguslawski, ProjectEngineer	Other Attendees Present:
Agency: City of Beaverton	
Agency/City Represented: City of Beaverton	
Phone: 503-526-2424 (Dave) 503-350-4025 (Mark)	
Fax: 503-350-4052	
Email: dwinship@ci.beaverton.or.us mboguslawski@ci.beaverton.or.us	

Notes:

Beaverton manages all sewers 21" or less.

Their primary concerns are –

1. Some sewers that are less than 21" carry flows from areas other than the Beaverton service areas. The City's maintenance crew performs significant services on these flow lines, some of which are probably under sized. Beaverton would al least like to see these lines modeled in the current SSMP. If the lines are undersized, they would request CWS to undertake the replacement if required. Areas of specific concern are –
    - Summer creek Trunk
    - Bull Mountain Area
    - Fanno Creek Sewer
    - Old Beaverton Treatment Plant Site – remnant manholes are complex and have significant drops. This is a potential area to reduce hydraulic losses in the system.
    - Tektronix Pump Station – Pipe plugging
2. The basin boundaries in the previous SSMP were not correct. This was largely due to inaccurate mapping available at that time.
3. Flow metering – Mark does not believe that that we will get accurate measurements from the Flodar operation.
4. Growth areas need to be included in the master plan – Scholls – Barrows area.

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: December 6, 2006**

Time: 9:00 am

Contact Information:

Name: Dick Reynolds	Other Attendees Present:
Agency: City of Cornelius	
Agency/City Represented: City of Cornelius	
Phone: 503-357-3011	
Fax:	
Email:	

Questions:

1. Current land use data

   Cornelius only maintains one zoning map – it is current zoning. The city limits and UGB are about the same. Institutional uses are allowed within current residential zones only.

2. Planned extensions/new developments within the City's current boundaries

   The dashed line near Main Street designates a mixed use redevelopment area. The dotted line near Main Street designates a commercial only redevelopment area.

3. Planned extensions/new developments beyond the City's current boundaries

   There is a URA study happening now between Metro and Washington County to study future growth areas around Forest Grove and Cornelius. The study goes from Susbauer Road

north to Verbort, west to Highway 47, south to the Tualatin River and west to Dairy Creek (on the south side of Cornelius).

4. Land use changes coming - Metro or city

   Over the next 20 years the residential lands will probably stay residential. The rail line has the potential to become a light rail extension or commuter rail line from Hillsboro to Forest Grove. If that happened there would be potential for redevelopment.

5. How are they handling Measure 37 claims?

   They have signed the MOU with Washington County to not provide services to measure 37 claims outside of current boundaries.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   Depends on Metro study.

7. Are there any planned annexations that you already know about?

   Cornelius does not have much room for residential infill, but there is a lot of industrial land to be developed and some commercial infill. Dick will check on what they have for a vacant lands inventory.

WEST YOST ASSOCIATES
CONTACT RECORD

WYA Staff:	Corie Peterson	Date: October 9, 2006	
Contact Name:	Jon Holan	☒ Call ☐ E-mail ☐ Meeting ☐ _____	
Title:	Planner	Copies to:	
Company Name:	City of Forest Grove		
Telephone:	503-992-3224 Fax:		
E-mail:	jholan@ci.forest-grove.or.us	Contract File? ☐ Yes ☐ No	
Project/File No.:	517-03-06-14 **Project Name:**	CWS Sanitary Sewer Master Plan	
Subject:	City of Forest Grove Land Use meeting		

Action Items	Responsibility	Date Promised

NOTES:

Forest Grove uses Metro population estimates.

He is available to review FG land use Thursday, Oct. 19 at 8 am.

His office is on the first floor of City Hall.

Please attach any relevant documentation

P:\Clients\517 CWS\03-06-14 Sanitary Sewer Master Plan\ENGR\Planning\Forest Grove\CR 10-9-06 Holan.doc

WYA Interviewer: Corie Peterson **Date:** 10/19/06

Time: 8:00 am

Contact Information

Name: Jon Holan	Other Attendees Present:
Agency: City of Forest Grove	
Agency/City Represented: City of Forest Grove	
Phone: 503-922-3224	
Fax:	
Email: jholan@ci.forest-grove.or.us	

Questions:

1. Current land use data

   FG will provide WYA with a shapefile (coming from Lou in Engineering) of their comprehensive plan designations. Discrepancies found were mostly areas that Metro had marked as single family, but were actually 2-family – see the map for marked areas. FG does not have a separate designation for schools, they are in residential areas. Several were marked on the map.

   They use Metro population numbers, but have found that they often hit those numbers much sooner than Metro says they will.

2. Planned extensions/new developments within the City's current boundaries

   A list and map was provided of approved units in the last 2-3 years that are currently being built or will soon.

3. Planned extensions/new developments beyond the City's current boundaries

   They currently have none, but they know that Metro is looking at some areas north of town. It will be up to Metro.

4. Land use changes coming - Metro or city

There are no known land use changes coming.

5. How are they handling Measure 37 claims?

   They currently have no claims. They anticipate that if there are any in the future they will be when there is rezoning and then it would just revert back to the old zoning.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   If their boundary changes it is up to Metro. They are not actively expanding their boundary.

7. Are there any planned annexations that you already know about?

   There are some planned annexations to the City limits, but none to the UGB. There are two 11x17 figures showing these areas.

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: December 20, 2006**

Time: 1:30 pm

Contact Information:

Name: Margret Bell	Other Attendees Present:
Agency: City of Gaston	
Agency/City Represented: City of Gaston	
Phone: 503-985-3340	
Fax:	
Email:	

Questions:

1. Current land use data

   Hard copy map attached – ele not available. Above the dotted line is currently within the City Limits. Outside the dotted line is within the UGB. Note 8 (as marked in pencil on map) is made up of lots partly in the city and partly out. They are served by City water – didn't know about sewer. Southern city limit line is also Yamhill/Washington County line.

2. Planned extensions/new developments within the City's current boundaries

   Areas marked in pencil on map:

   1. 6 new lots
   2. No homes yet – this subdivision has been on the books since the 1980s. Had some slide problems in the 90s.

3. Empty Lot
4. School owns this property – they are looking to sell some of it for residential development
5. The owner is looking to develop 15-20 acres
6. Manufactured home park – map may not be quite right there on the lot lines.. The industrial next to it has some commercial business like a welding shop. May be light industry/commercial/industrial mix in the future.
7. There are three lots here with one existing house (original – drawn as box on map)This lot could be further divided.

3. Planned extensions/new developments beyond the City's current boundaries

   They have approx. 650 residents now. They have the potential of being about 2500ish. They are boxed in on the east by flood plain and on the west by the mountains. They are opening bids tomorrow on a new 1 MG water reservoir which will allow them to make new annexations that they have not been doing due to storage shortages. Margret sees developments like the one that happened in Banks in the next 5 to 10 years. Most growth would be residential.

4. Land use changes coming - Metro or city

   None. The green to the north could infill.

5. How are they handling Measure 37 claims?

   They do not have any claims. They were not asked to sign the MOU, but would not provide services beyond the UGB.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   See map. How fast will pop of 2500 occur? – could be in 20 years or less. New water storage will make a difference. The last big subdivision had all the homes sold before they were completed. The council does not actively seek annexations. The latest UBG line was drawn in 2002. They do not currently need more.

7. Are there any planned annexations that you already know about?

   None already planned for. They do not need a vote for annexation – only a public hearing.

8. Other

Green – 10k lots

yellow – 5-7k lots

brown – 1 acre lots

Orange – commercial of single family homes with R-2 standards

MHP – mobile home park

Duplex can be built in R-2 with a minimum lot size of 3k per unit.

The school property has elementary, junior high and high school all at one site.

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: December 6, 2006**

Time: 1:00 pm

Contact Information:

Name: Valarie Counts	Other Attendees Present:
Agency: City of Hillsboro	
Agency/City Represented: City of Hillsboro	
Phone: 503-681-6239	
Fax:	
Email:	

Questions:

1. Current land use data

   Hillsboro maintains a zoning map of existing zoning and a comprehensive map of future zoning. We can get shape files of these maps from Jay Leroux (GIS manager).

   We can get a vacant lands inventory from Karla Antonini (503-681-6181) when she returns from maternity leave in mid June. May be a couple years old – they do not update it very frequently.

2. Planned extensions/new developments within the City's current boundaries

   Areas 69 and 71 had comprehensive planning done in June.

Much of the land in the north part of the city – near the airport – is industrial and has been "land banked". Companies currently own it but are not actively developing, and have no know plans in the works to do so. It is not "available" but it is not developed either.

There are some redevelopment areas within the City:

- The downtown area is a regional center – they will be adding some high density housing.
- Pacific University just opened Phase I of a downtown campus for their grad program. They are starting Phase II now.
- OHSU and the Amber Glen Business Park could have major redevelopment. These areas could allow 20 story towers. Concept planning for this area has been done. If more information is needed on this Wink Brooks is the person heading this project (Planning Director).

3. Planned extensions/new developments beyond the City's current boundaries

The City of Hillsboro does not yet have a firm Urban Planning Area established. They are in talks with Washington County to try to establish one – eventually it may follow the school district boundaries.

They are not actively looking to bring areas to the north into the service area. They are currently more interested in areas south.

Valarie sees their ultimate boundaries as being South and west to the river. McKay Creek provides a permanent separation between Hillsboro and Cornelius.

4. Land use changes coming - Metro or city

OHSU area – See #2.

5. How are they handling Measure 37 claims?

There are some claims north and south. The City's general policy is to prevent extending service outside of the city limits – with some exceptions. They have signed the MOU with Washington County. Steve Kelly in Long Range Planning at Washington County should have a list of the signed MOUs and Cities participating in that.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

See last item on #3.

7. Are there any planned annexations that you already know about?

None mentioned.

WEST YOST ASSOCIATES
CONTACT RECORD

WYA Staff:	Corie Peterson	Date: 9-26-06	
Contact Name:	Malu Wilkinson	☒ Call ☐ E-mail ☐ Meeting ☐ _____	
Title:		Copies to:	
Company Name:	Metro Planning		
Telephone:	503-797-1680 Fax:		
E-mail:		Contract File? ☐ Yes ☐ No	
Project/File No.:	**Project Name:** CWS SSMP		
Subject:	Metro Land Use and Planning Meeting		

Action Items	Responsibility	Date Promised

NOTES:

Would like to set up a meeting to discuss metros new land use designations etc. within the CWS boundary. We are looking at the date Oct 12, early afternoon.

Left msg. 9-26-06

Malu felt that she was not the right person for this meeting and referred me to Tim O'brien 503-797-1840.

I spoke with Tim on 9-27-06 and he agreed. He is available for a meeting at 1:30 on Oct. 12 at CWS facility near Jackson Bottom Wetlands.

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date:** **10/12/06**

Time: **1:30 pm**

Contact Information:

Name: Tim O'Brien	Other Attendees Present: Jeff Pelz, WYA Andy Braun, CWS
Agency: Metro	
Agency/City Represented: Metro	
Phone: 503-797-1840	
Fax: 503-797-1911	
Email: obrien@metro.dst.or.us	

Discussion:

The State of Oregon is currently undergoing the "Big Look" at statewide landuse. Metro is undergoing the "New Look" at their forecasts for 2040. Metro is not changing their overall ideas, but revisiting areas that aren't working as previously planned.

There are three main types of state land use (outside UGB);

1. Resource land – designated for farm or forest. Divided also by soil type – class 1-4
2. Exception land – county has excepted it from agricultural uses. Often 5 acre residential. Divided also by soil type – class 1-4
3. Marginal Land – less than 100 acres total of this designation in Washington County

There is a hierarchy that is required by the state when looking into lands to annex into the UGB:

1. Exception Lands (class 3 and 4 first)
2. Marginal Land

3. Resource Land (class 3 and 4 first)

Metro's new look has 3 components:

1. Look at land designations outside of UGB. Identify "critical" farm lands that will keep the agricultural industry going as lands that should be protected. Identify other lands that maybe designated farmland, but aren't being used in that manner.

2. Look at natural features for protection such as the Tualatin River and Forest Park extensions.

3. Look at lands outside of the hierarchy. What lands make sense to annex outside of agricultural designations? Consider: infrastructure, finance, transportation, topography, other geographic features.

Metro's last UGB decision/annexation took place in 2003 though 2005. Lands brought in to the UGB in 2003 were residential. Lands brought in to the UGB in 2004 were industrial. In 2005 it was decided that the 2003 and 2004 lands were not quite adequate so additional land was brought in to the UGB – mostly industrial. Metro is required to look at their lands every 5 years to maintain a 20 year supply of residential land within the UGB, so their next decision is due in 2008, but they are asking for an extension.

Specific areas that are "targets" for the next annexation are:

1. St. Mary's area – Hillsboro will look at including them in the comprehensive plan

2. Bethany area – this area would likely be served by Beaverton. Washington County is looking at that area now.

3. An area west of Tigard near Beef Bend Road and Roy Rogers – it makes sense to take this area all the way to the Tualatin River flood plain.

4. Other areas should be looked at with each city. Each city should have some areas of their own in mind.

Reports that Metro has and will get to us:

1. Report with dwelling unit numbers on the new areas

2. Running status report on what is happening in new areas

3. Vacant land inventory – this is updated every year. 2005 is almost complete. Dennis Ye can get this for us.

4. Exception lands map

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: December 20, 2006**

Time: 11:00 am

Contact Information:

Name: Don Otterman, City Manager	Other Attendees Present:
Agency: City of North Plains	
Agency/City Represented: City of North Plains	
Phone: 503-647-5555	
Fax: 503-647-2031	
Email: don@northplains.org	

Questions:

1. Current land use data

   Their zoning map is very up to date. They have a one map system for current and comprehensive plan land use. They do not have the map electronically, but we may be able to get it from Murray Smith and Associates – Kyle McTeague was their lead engineer. Their last buildable lands inventory was done 5 years ago, so Don didn't want to share it with me.

2. Planned extensions/new developments within the City's current boundaries

   Numbered notes tied to "City of North Plains Zoning Map":

   1. 55 lot subdivision has been permitted
   2. 40 lot subdivision has been permitted
   3. 22 lot subdivision has been filed

4. 26 lot subdivision is being planned

Schools are in residential areas – shown as hatched areas on the comp plan map. In the East expansion area there are 10 acres that the Hillsboro School District is looking to buy.

3. Planned extensions/new developments beyond the City's current boundaries

The areas shaded yellow on the Comprehensive Plan Map are not yet approved, but will be the next to come in. These lands will provide a 20 year supply and were acknowledged by LCDC in 2003. City Charter requires a vote on annexation of lands into the city limits. There are 24 acres being voted on this spring – it will be their 4th attempt at annexation. Hard copies of plan maps for the two new areas are attached.

The exception lands located south of the city (across hwy. 26) will not be annexed into the city. The city does not want to extend across the highway and got the state land board to agree that they could look at other lands instead. There are several Measure 37 claims over there – will likely be large lot residential with septic tanks.

4. Land use changes coming - Metro or city

None

5. How are they handling Measure 37 claims?

They do not have any claims. They have signed the MOU with Washington County.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

The two yellow areas shown on the comprehensive plan map provide a 20 yr. supply of land.

7. Are there any planned annexations that you already know about?

See #3

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: December 14, 2006**

Time: 9:00 am

Contact Information:

Name: Julia Hadjuk	Other Attendees Present:
Agency: City of Sherwood	
Agency/City Represented: City of Sherwood	
Phone: 503-625-4204	
Fax:	
Email: hajduk@ci.sherwood.or.us	

Questions:

1. Current land use data

   They maintain one zone map. Julia will get me the shapefile. Sherwood is a fairly new City thus the zoning map is pretty accurate to real life zoning.

2. Planned extensions/new developments within the City's current boundaries

   Nothing big planned within the City. Julia will get me the buildable lands inventory. Their commercial zones allow condos above so there may be some unexpected residential infill.

3. Planned extensions/new developments beyond the City's current boundaries

   As a City their tax base is out of balance – they currently are approx. 80% residential. They do not need more residential land so are likely to discourage residential growth and encourage other types of growth.

Area 48 will probably be industrial, but the line between Tualatin and Sherwood is not firm and this area may end up being Tualatin.

They do have some growth constraints – the area to the southeast is swampy and Parrot Mountain is located to the southwest.

4. Land use changes coming - Metro or city

None big coming.

5. How are they handling Measure 37 claims?

The MOU with Washington County has not gone to the council yet.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

See map.

7. Are there any planned annexations that you already know about?

See map.

Other:

Schools are not all in institutional zones, they are mostly in residential zones.

WEST YOST ASSOCIATES
CONTACT RECORD

WYA Staff:	Corie Peterson	Date: April 11, 2007	
Contact Name:	Gene Thomas	☒ Call ☐ E-mail ☐ Meeting ☐ _____	
Title:		Copies to:	
Company Name:	City of Sherwood Engineering		
Telephone:	503-925-2303 Fax:		
E-mail:		Contract File? ☐ Yes ☐ No	
Project/File No.:	517-03-06-14 **Project Name:**	CWS Sanitary Sewer Master Plan	
Subject:	**Sherwood SSMP Study Area**		

Action Items	Responsibility	Date Promised

NOTES:

Julia Hadjuk, City of Sherwood Planner, directed me to speak with Gene regarding additional study areas for the City South and West of their current boundaries.

Gene indicated that for the purposes of their official, approved, master plan they are only planning within their current boundary. When the MP is complete, however, their engineer Murray Smith & Associates will be developing a technical memorandum that will look at potential growth beyond the current boundary for a 50 year planning horizon. They will then see how this growth might impact the recommendations in the MP. Gene could not tell me the specific areas of study and asked me to call Tom Boland at MSA for that information.

Please attach any relevant documentation

WEST YOST ASSOCIATES
CONTACT RECORD

WYA Staff:	Corie Peterson	Date: April 11, 2007	
Contact Name:	Tom Boland	☒ Call ☐ E-mail ☐ Meeting ☐ _____	
Title:	Engineer	Copies to:	
Company Name:	Murray Smith & Associates		
Telephone:	503-225-9010 Fax:		
E-mail:	bolandt@msa-ep.com	Contract File? ☐ Yes ☐ No	
Project/File No.:	517-03-06-14 **Project Name:**	CWS Sanitary Sewer Master Plan	
Subject:	**Sherwood SSMP Study Area**		

Action Items	Responsibility	Date Promised

NOTES:

Gene Thomas, engineering for Sherwood, asked me to call Tom Boland at MSA for specific sanitary sewer study areas beyond the City's current boundaries.

Tom said that the master plan for the City was about 1 month from being completed and the technical memorandum analyzing service areas beyond city boundaries would start after that. He gave me the following areas from their scope of work with the City:

From the City's current boundary west two miles between SW Bell Road and the Tualatin River.

From the City's current boundary south one mile between Highway 99 and Coffee Lake Creek.

Please attach any relevant documentation

WEST YOST ASSOCIATES
CONTACT RECORD

WYA Staff:	Corie Peterson	Date: October 9, 2006	
Contact Name:	Denver Igarta	☒ Call ☐ E-mail ☐ Meeting ☐ _____	
Title:	Planner	Copies to:	
Company Name:	City of Tigard Planning		
Telephone:	503-639-4171 Fax:		
E-mail:	denver@tigard-or.gov	Contract File? ☐ Yes ☐ No	
Project/File No.:	517-03-06-14 **Project Name:**	CWS Sanitary Sewer Master Plan	
Subject:	City of Tigard Land Use meeting		

Action Items	Responsibility	Date Promised

NOTES:

Tigard is currently updating their comprehensive plan.

They have no expansions planned beyond their current UGB.

They recently stopped providing permitting/inspection etc. services to the Bull Mountain area since they are working toward incorporation. Washington County is now providing.

Denver did not feel that he is the appropriate person for my questions. He will have the senior planner contact me – Beth St. Amand. He asked that I send questions ahead of time, so I emailed him the current questions on the planning questionnaire.

Please attach any relevant documentation

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: October 25, 2006**

Time: 3:00 pm

Contact Information:

Name: Denver Igarta, Associate Planner	Other Attendees Present: Beth St. Amand, Senior Planner beth@tigard-or.gov Darren Wyss, Associate Planner/GIS darren@tigard-or.gov
Agency: City of Tigard	
Agency/City Represented: City of Tigard	
Phone: 503-718-2429	
Fax: 503-684-7297	
Email: denver@tigard-or.gov	

Questions:

1. Current land use data

   There were several discrepancies between what is shown on the metro map and City of Tigard zoning. Tigard has zoning that shows that is allowed now and a comprehensive plan that shows what will be allowed in the future. Right now, for Tigard these two are pretty similar. Tigard is fairly built-out and land-locked.

2. Planned extensions/new developments within the City's current boundaries

   There are no major developments pending within the City limits. There are two small developments on Sunrise Lane and a couple of other R-7 areas circled on the map. Downtown may have more housing in the future.

3. Planned extensions/new developments beyond the City's current boundaries

No areas are planned for extensions beyond the current City boundary. There are no plans for annexation of Bull Mountain (vote next week on Bull Mtn. incorporating itself). There was a ballot measure a few years ago to annex Bull Mtn., but it failed. Tigard is fairly land-locked by Beaverton, Tualatin, Portland and Bull Mtn.

4. Land use changes coming - Metro or city

   No specific changes coming.

5. How are they handling Measure 37 claims?

   Only two claims that are very minor.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   Same as now.

7. Are there any planned annexations that you already know about?

   None.

WEST YOST ASSOCIATES
CONTACT RECORD

WYA Staff:	Corie Peterson	Date: December 19, 2006	
Contact Name:	William Harper	☒ Call ☐ E-mail ☐ Meeting ☐ _____	
Title:	Planner	Copies to:	
Company Name:	City of Tualatin		
Telephone:	503-691-3027 Fax:		
E-mail:		Contract File? ☐ Yes ☐ No	
Project/File No.:	517-03-06-14 **Project Name:**	CWS Sanitary Sewer Master Plan	
Subject:	City of Tualatin Planning Discussion		

Action Items	Responsibility	Date Promised

NOTES:

Will can not meet with me this week. We scheduled Bhargavi to meet with him on Thursday December 28 at 1:30 pm.

He does not want us to bring the metro map – doesn't want to spend time correcting their land use. He would rather just look at Tualatin's map and have discussions about specific areas from that map. We likely can get whatever we need electronically too.

Tualatin has a "one map system", so no current and future zoning. He warned me that not much is changing and that he won't have much info on URAs and expansion areas.

Please attach any relevant documentation

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Bhargavi Ambadkar **Date: December 28, 2006**

Time: 1:30 am

Contact Information:

Name: William Harper	Other Attendees Present:
Agency: City of Tualatin	
Agency/City Represented: City of Tualatin	
Phone: 503-691-3027	
Fax:	
Email:	

Questions:

1. Current land use data

   There were several discrepancies between what is shown on the metro map and City of Tualatin zoning. Tualatin has zoning that shows comprehensive plan which illustrates what will be allowed in the future. Existing conditions for Tualatin are shown on the map. Tualatin is fairly built-out, however there are areas that could be incorporated into the City – east towards Stafford Triangle, south towards Wilsonville and west towards Sherwood. Harper thinks that south and east should be discussed with Metro, and east will come into the city limits (either Sherwood or Tualatin) pretty soon. If it comes into Tualatin, they would like it to be Industrial.

2. Planned extensions/new developments within the City's current boundaries

   There are no major developments pending within the City limits. There is only one small developments south of the City (60 acres).

3. Planned extensions/new developments beyond the City's current boundaries

   No areas are planned for extensions beyond the current City boundary.

4. Land use changes coming - Metro or city

   No specific changes coming.

5. How are they handling Measure 37 claims?

   They are participating in it.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   Same as now.

7. Are there any planned annexations that you already know about?

   See Q2.

Clean Water Services

Sanitary Sewer Master Plan

Zoning/Land Use Interview

517-03-06-14

WYA Interviewer: Corie Peterson **Date: 10/19/06**

Time: 1:30 pm

Contact Information:

Name: Andrea Vannelli, Senior Planner	Other Attendees Present: Aisha Willits, Senior Planner Aisha_Willits@co.washington.or.us 503-846-3961
Agency: Washington County Planning	
Agency/City Represented: Washington County	
Phone: 503-846-3970	
Fax: 503-846-4412	
Email: Andrea_Vannelli@co.washington.or.us	

Questions:

1. Current land use data

   Washington County only has comprehensive plan designations. They don't really keep a listing of existing zoning. Churches and schools can be in residential areas. Schools are supposed to request changes to institutional designations, but not all do. Beaverton has been good about this. Just North of Hwy 26 there is a golf course designated as institutional. It maybe used to be "open space".

2. Planned extensions/new developments within the City's current boundaries

   The Bonny Slope area is one of concern. It is in the Metro UGB, in Multnomah County, but the topography runs downhill in to Washington County. The City of Portland is currently not interested in serving this area. There are some areas of septic in Washington County within the Metro Boundary – does CWS know when these will be sewered?

3. Planned extensions/new developments beyond the City's current boundaries

   Only what Metro plans.

4. Land use changes coming - Metro or city

   Bull Mountain incorporation may have some impact on land uses, but for several years the city will likely contract back services to the same agencies that provide them now.

5. How are they handling Measure 37 claims?

   They are not required, and do not allow for extension of services to claim lands.

6. What is the city boundary you see developing by 2020/30? How fast will this occur?

   County boundary will not change. Areas of concern to CWS are Metro driven.

7. Are there any planned annexations that you already know about?

   May be some annexations between Tualatin and Sherwood, but the potential 99 connector would have limited access, so growth there should be minimal. Big growth areas are likely North of Hillsboro – especially for residential.

ATTACHMENT 2

Attachment 2

Banks

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
R5	Single-Family Residential		
R2.5	Multi-Family Residential		
CF	Community Facilities		
C	General Commercial		
I	General Industrial		
H	Historic Resource Overlay		
PD	Planned Development		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Beaverton

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
COR	General Commercial		
EMP	Commercial - Office		
IND	Industrial		
MS	Municipal Services		
NR-HD	Residential - High Density		
NR-LD	Residential - Low Density		
NR-MD	Residential - Medium Density		
NR-SD	Residential		
RC	Mixed Use		
SC	Mixed Use		
TC	Mixed Use		
ROW	Roads and Highways		
Wacnty	County Lands		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Cornelius

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
R-7	Single Family Residential	Average of 5 dwelling units per acre. Standard lots 5,000 to 6,500 sf.	5
A-2	Multi-family Residential	Maximum overall density is 14 dwelling units per acre	14
MHP	Manufactured Home Park	Maximum overall density is 14 dwelling units per acre	14
C-2	Highway Commerical	Range of retail and service commercial	
CE	Core Commercial Employment		
M-1	General Industrial	Light industrial	
MSR	Retail Commercial	Retail commercial	
MSM	Mixed Use		
MSG	General Employment		
MSC	Civic		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Forest Grove

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
CA	Commercial - Administration		
CBD	Commercial Business District		
CH	Highway Commercial		
CN	Neighborhood Commercial		
EXISTING PARK	Park		
GENERAL INDUSTRIAL	Industrial		
HIGH DENSITY	Residential		
A-MEDIUM	Residential		
B-STANDARD	Residential		
B-C	Residential		
C-LOW	Residential		
OPENSPACE	Open Space		
PUBLIC	Public Facility		
SEMI-PUBLIC	Semi-Public Facility		
CPD	Commercial Planned Development		
D-SUBURBAN	Residential		
MEDIUM DENSITY	Residential		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Gaston

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
SR-1	Residential - Suburban Low Density	40,000 sf (1 acre) lots	
R-1	Residential - Urban Low Density	10,000 sf lots	
R-2	Residential - Urban Medium Density	5,000 - 7,000 ft lots	
R-3 or MHP	Residential - Urban high density or Mobile Home Park		
C	Commercial		
I	Industrial		
FP	Flood Plain		
MU	Mixed Use	Commercial or single family homes with R-2 standards	
PF	Public facilities	Schools	
POS	Parks	Parks and open space	

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Hillsboro

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
C	General Commercial		
FP	Park / Open Space		
IN	Industrial		
MU	Mixed Use Commercial		
OS	Open Space		
PF	Public Facility		
RH	Residential - High Density		
RL	Residential - Low Density		
RM	Residential - Medium Density		
RMR	Residential - Multi-Family		
SCPA	Mixed Use Commercial		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

North Plains

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
R 7.5	Single Family Residential		
R 5	Single Family Residential		
R 2.5	Single Family Residential		
C 1	General Commercial		
C 2	Highway Commercial		
M 1	Light Industrial		
M 2	General Industrial		
CS	Community Service		
HO	Historical Overlay District		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Sherwood

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]

(a) Draft, for review and editing by City
(b) Cities to provide values for use in wastewater modeling

Attachment 2

Tigard

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
CBD	Central Business District		
CC	Community Commercial		
CG	General Commercial		
IH	Heavy Industrial		
H	High Density Residential		
IL	Light Industrial		
L	Low Density Residential		
M	Medium Density Residential		
MH	Medium-High Density Residential		
MUC	Mixed Use Commercial		
MUE	Mixed Use Employment		
MUE-1	Mixed Use Employment 1		
MUE-2	Mixed Use Employment 2		
MUR-1	Mixed Use Residential 1		
MUR-2	Mixed Use Residential 2		
CN	Neighborhood Commercial		
OS	Open Space		
CP	Professional Commercial		
PI	Public Institution		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Tualatin

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
CC	Central Commercial		
CG	Commercial General		
CO	Commercial Office		
CR	Commercial Recreational		
MC	Medical Center		
MG	General Manufacturing		
ML	Light Manufacturing		
MP	Manufacturing Park		
RH	Residential high density		
RH/HR	Residential high density/high rise		
RL	Residential low density		
RMH	Residential medium-high density		
RML	Residential medium-low density		

(a) Draft, for review and editing by City

(b) Cities to provide values for use in wastewater modeling

Attachment 2

Metro

Category Label	Land Use Type[a]	Description	Predicted Residential Density (du/acre)[b]
CC	Central Commercial	Central Commercial - allows a full range of commercial typically associated with CBD's and downtowns. More restrictive than general commercial in the case of large lot and highway oriented uses. Encourages higher FAR uses including multi-story development..	NA
CG	General Commercial	General Commercial - larger scale commercial districts, often with a more regional orientation for providing goods and services. Businesses offering a wider variety of goods and services (including large format retailers) are permitted in this district and include mid-rise office buildings, and highway and strip commercial zones.	NA
CN	Neighborhood Commercial	Neighborhood Commercial - small scale commercial districts permitting retail and serice activities such as grocery stores and neighborhood service establishments that support the local residential community. Floor space and/or lot sizes are usually limited to between 5,000 to 10,000 square feet.	NA
CO	Office Commercial	Office Commercial - districts accommodating a range of low-rise offices; supports various community business establishments, professional and medical offices; typically as a buffer between residential areas and more intensive commercial districts.	NA
FF	Agriculture or Forestry	Agriculture or Forestry - activities suited to commercial scale agrricultural production or forestry, typically with lot sizes of 10, 20 or 30 acres or more.	NA
IA	-	-	NA
IH	Heavy Industrial	Heavy Industrial - districts permit light industrial and intensive industrial activity such as bottling, chemical processing, heavy manufacturing and similar uses with noxious externalities.	NA
IL	Light Industrial	Light Industrial - districts permit warehousing and distribution facilities, light manufacturing, processing, fabrication or assembly. May allow limited commercial activities such as retail and service functions that support the businesses and workers in	NA
IMU	-	-	-
MFR1	Multi-family Residential 1	Multi-family - single family, townhouses, row houses permitted outright. Max density permitted is 15 units / net acre.	10
MFR2	Multi-family Residential 2	Multi-family - single family, townhouses, row houses permitted outright. Max density permitted is 20 units / net acre.	18
MFR3	Multi-family Residential 3	Multi-family - single family, townhouses, row houses permitted outright. Max density permitted is 25 units / net acre.	23
MFR4	Multi-family Residential 4	Multi-family - single family, townhouses, row houses permitted outright. Max density permitted is 30 units / net acre.	28
MUC1	-	-	-
MUC2	-	-	-
MUC3	-	-	-
PF	Public Facilities	Public Facilities - allows government building, institutional and cultural uses such as museums.	1
POS	Parks and Open Space	Parks and Open Space	1
RRFU	Rural Residential or Future Urban	Rural Residential or Future Urban - residential uses permitted on rural lands (1 dwelling unit per lot) or areas designated for future urban development, typically lots are 10 or more acres.	1
SFR1	Single family 1	Single family - detached housing with minimum lot size from 35,000 sq. ft.	1
SFR2	Single family 2	Single family - detached housing with minimum lot size from 15,000 sq. ft. to a net acre	2
SFR3	Single family 3	Single family - detached housing with lot sizes from about 10,000 sq. ft. to 15,000 sq. ft.	3
SFR4	Single family 4	Single family - detached housing with lot sizes around 9,000 sq. ft.	4
SFR5	Single family 5	Single family - detached housing with lot sizes around 7,000 sq. ft.	5
SFR6	Single family 6	Single family - detached housing with lot sizes around 6,000 sq. ft.	6
SFR7	Single family 7	Single family - detached housing with lot sizes around 5,000 sq. ft.	7

(a) Draft, for review and editing by Metro
(b) Metro to confirm values for use in wastewater modeling

ATTACHMENT 3

Distribution List -- Clean Water Services Sanitary Sewer Master Plan Update TM 1

(City Committee Membership Plus Additional for Land Use Review)

Added For SSMP Land Use Review	Name	Title	Co	Email
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x	Jolynn Becker	City Recorder	City of Banks	
x	Mike Lyda	Mayor	City of Banks	
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APPENDIX C

Modeling Parameters for Special Case Wet Industries

MODELING PARAMETERS FOR SPECIAL CASE WET INDUSTRIES

Flows from wet industries represent an important component of the flow projections used to predict capacity needs. This document presents the wet industry flow assumptions that were used to predict both existing and future flow conditions. Presented below are the specific modeling parameters used to simulate flows from the wet industries within the collection system model. The data presented includes:

- Average Flow Information
- Daily Flow Patterns (Diurnal Curves)

AVERAGE FLOW INFORMATION

Table C-1 lists the industries modeled as special case dischargers, including the modeled existing flow and their predicted future flows. The table also lists the manhole number into which flow from the industry is injected.

In addition to the flows subject to the industrial dischargers' permits, the model includes a domestic flow component for the lands associated with each discharger. A factor of 500 gpd/acre was adopted to account for non-process sanitary flows generated by domestic uses on the tax lots occupied by the wet industries. This additional factor accounts for flows that are discharged separately from the wet industries' permitted discharges and are therefore not metered or included in the permitted flow records.

A standard flow factor is applied to all other lands assigned uses in the industrial categories (IA, IH, and IL). The factor applied is 1,500 gpd/acre, which reflects District staff experience with industrial dischargers throughout the District. The factor of 1,500 gpd/acre is intended to allow for a variety of industrial uses other than industries considered to be significant dischargers in terms of wastewater volume (wet industries).

Table C-1. Wet Industries Modeled As Point Flows[1]

Industry Name	Average Flow, mgd			Buildout Plus[4]	Injection Manhole
	Existing	2015[2]	Buildout[3]		
Bimbo's Bakeries USA	0.000	0.007	0.014	0.029	12429
Fiskars Group II	0.000	0.005	0.010	0.020	10432
Fujimi America FO Facility	0.227	0.265	0.265	0.265	97183
Maxim Integrated Products	0.418	0.504	0.504	0.504	03050
Novellus Systems,Inc.	0.000	0.005	0.010	0.021	97183
Pacific Foods Functional Ingredients	0.045	0.040	0.040	0.040	20763
Pacific Foods Of Oregon	0.083	0.075	0.075	0.075	96873
Pacific Nutritional Foods	0.054	0.068	0.068	0.076	20761
Resers Fine Foods - Allen Blvd Facility	0.022	0.024	0.024	0.024	20653
Tektronix Inc - Jenkins Rd	0.015	0.019	0.493	0.986	54044
Weyerhaeuser Corporation - Specialty Products Division	0.000	0.006	0.013	0.025	20590
Williams Controls	0.000	0.013	0.025	0.050	10432
Durham Basin Totals	*0.865*	*1.032*	*1.541*	*2.115*	
Gray And Company	0.057	0.071	0.071	0.125	20419
Merix Corporation - Poplar Lane	0.208	0.250	0.250	0.250	12739
New Season Foods Inc	0.000	0.063	0.125	0.250	20470
Westak of Oregon Inc	0.041	0.051	0.051	0.061	20468
Forest Grove Basin Totals	*0.306*	*0.435*	*0.497*	*0.686*	
Genentech[5]	0.000	0.066	0.133	0.265	77438
Hillsboro Landfill Inc	0.037	0.047	0.047	0.080	21305
Integrated Device Technology Inc	0.312	0.390	0.390	0.536	27270
Intel Corporation - Aloha Campus 1	0.042	0.052	0.280	0.560	13094
Intel Corporation - Aloha Campus 2	0.310	0.388	0.388	*0.560*	13094
Intel Corporation - Ronler Acres Campus	2.961	3.153	3.153	3.153	28242
Resers Fine Foods - Jenkins Rd Facility	0.070	0.088	0.088	0.091	09893
SolarWorld Industries America LP	0.007	0.009	0.400	0.800	27275
Soloflex Inc	0.000	0.004	0.008	0.015	19964
Sumitomo Electric Semiconductor Materials, Inc	0.027	0.031	0.031	0.031	20091
Project Tahoe	0.000	1.500	3.000	3.000	77438

Table C-1. Wet Industries Modeled As Point Flows(1), cont'd…

Industry Name	Average Flow, mgd			Buildout Plus(4)	Injection Manhole
	Existing	2015(2)	Buildout(3)		
TOK America	0.039	0.049	0.049	0.055	22402
Tokai Carbon USA Inc	0.023	0.024	0.024	0.024	22397
Triquint Semiconductor	0.084	0.105	0.105	0.109	27062
Rock Creek Basin Totals	*3.961*	*5.959*	*8.149*	*9.334*	

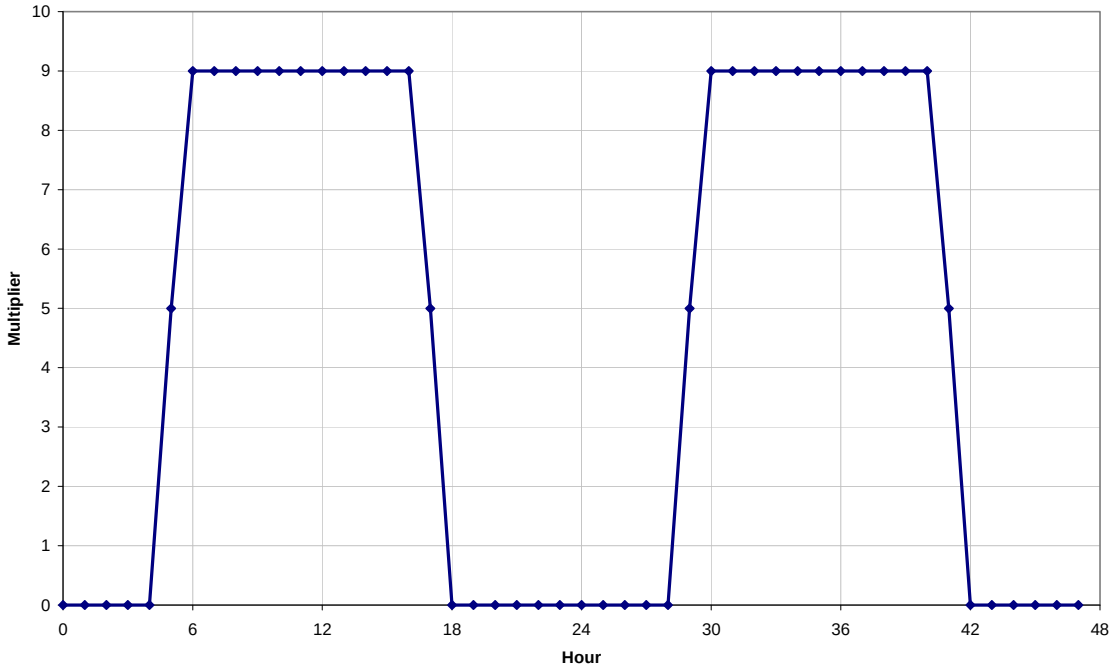
(1) Point flows were used for modeling wet industries with reported average flows of greater than 15,000 gpd. For all other industrial land uses, planning value flow factors were applied to acreage to estimate flows.
(2) 2015 flows were assumed to be the smaller of 125% of existing flows and the permitted flows. For industries with zero existing flow, the 2015 flows were assumed to be 25 % of permitted flows.
(3) Buildout flows were assumed to be the larger of 2015 flows and 50% of the permitted flows.
(4) Permitted flows were assumed for Buildout Plus conditions
(5) Anticipated flow at buildout plus is 0.265 mgd. Current permitted flow is less than this.

DAILY FLOW PATTERNS (DIURNAL CURVES)

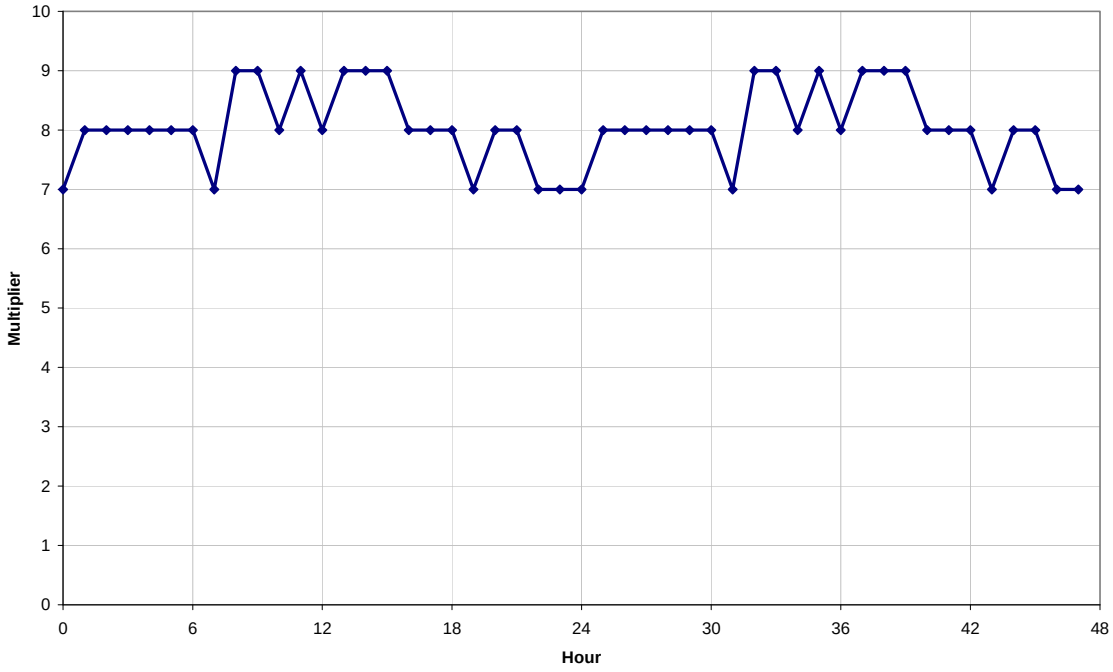
The model input data includes a series of 48 values representing the relative amount of flow from the discharger in each hour over a two day period. For each modeled time period, the modeling software determines what portion of the average flow for the industry would be discharged during the given period, based on the relative magnitude of the 48 values. Therefore, only the relative magnitude of the values, coupled with the defined average flow for the discharger is important. The actual magnitude of the 48 values is not relevant.

Previous modeling which served as the basis for this Master Plan Update included flow patterns from many existing wet industries. These flow patterns were used for the update. A standard flow pattern was used for industries for which metering data defining an hourly pattern was not available. The flow patterns used in the model are presented below.

Fujimi America Fo Fac and Novellus

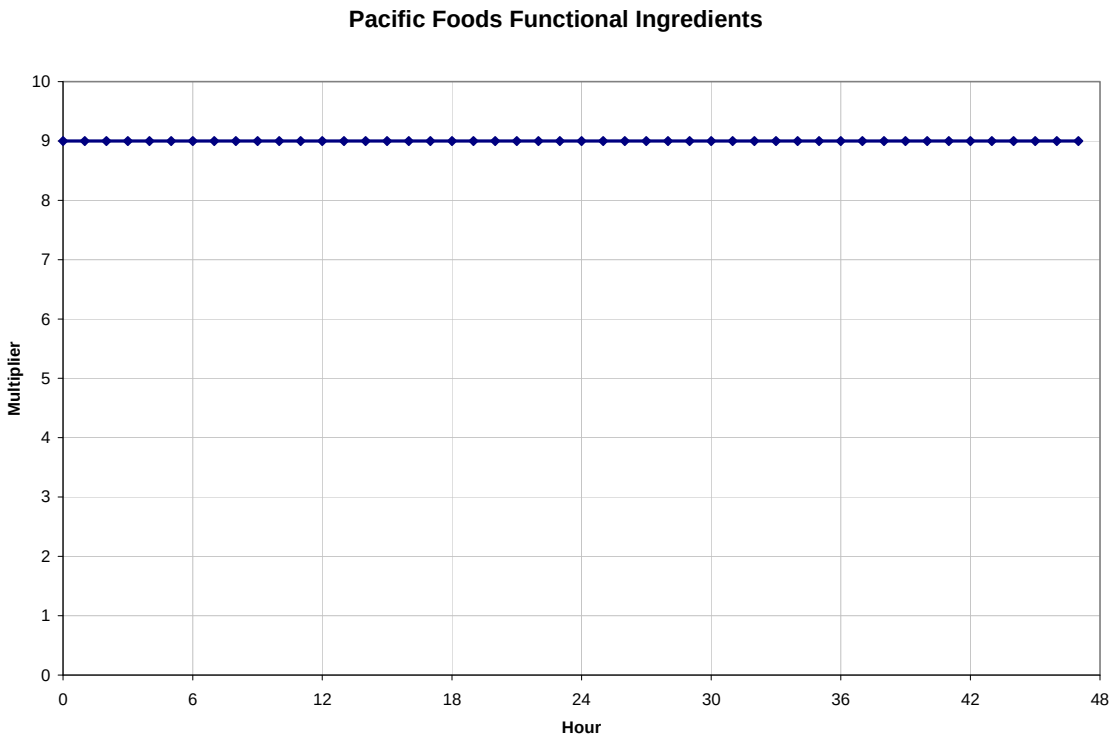


Pacific Nutritional Foods



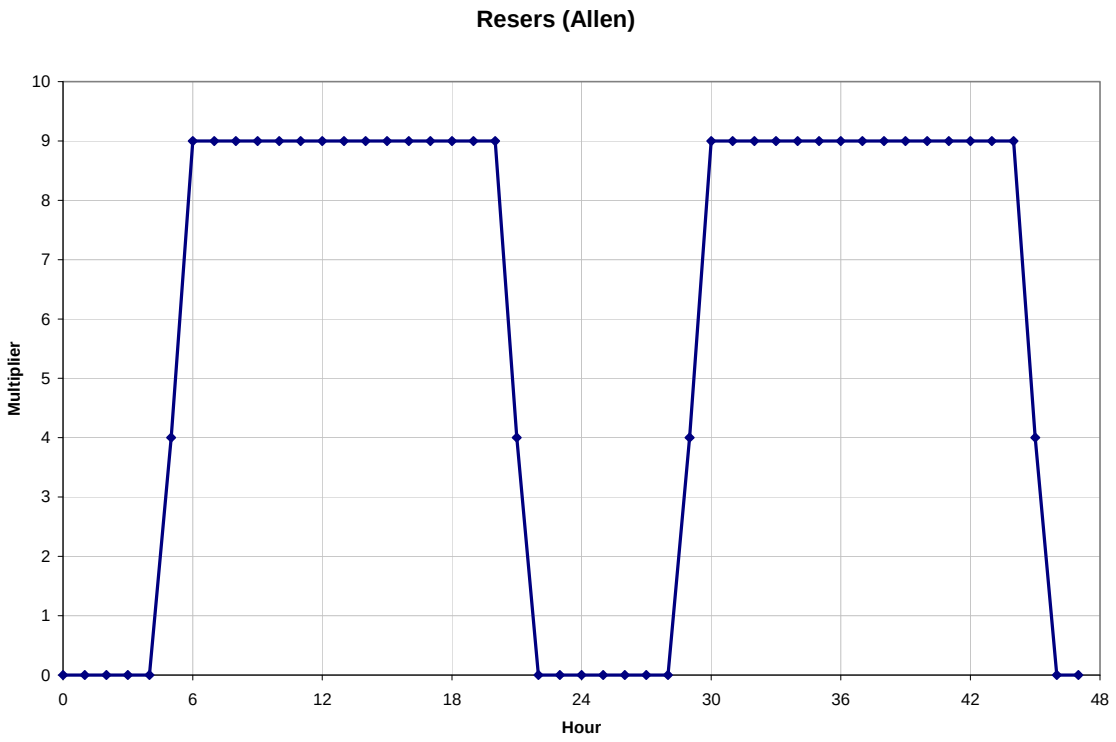
Pacific Nutritional Foods curve also applies to:

1. Bimbos Bakery – Rock Creek Basin
2. Fiskars Group II and Williams Controls – Rock Creek Basin
3. Novellus Systems, Inc. – Rock Creek Basin
4. Weyerhauser Corporation – Specialty Products Division
5. Williams Controls – Rock Creek Basin
6. Intel – Aloha Fab 15 – Rock Creek Basin
7. Integrated Dev Tech, Inc. – Rock Creek Basin
8. Komatsu Silicon America – Rock Creek Basin
9. Maxim Integrated Products – Rock Creek Basin
10. Sumitomo Electric Semiconductor Materials, Inc. – Rock Creek Basin
11. TOK America – Rock Creek Basin
12. Genentech – Rock Creek Basin
13. Pacific Foods or Oregon – Rock Creek Basin
14. SolarWorld Industries America LP – Rock Creek Basin
15. Soloflex, Inc. – Rock Creek Basin
16. Westak – Forest Grove Basin
17. New Season Foods – Forest Grove Basin



Pacific Foods Functional Ingredients curve assumes the permitted flow rate could be discharged at any time during the day. The curve also applies to:

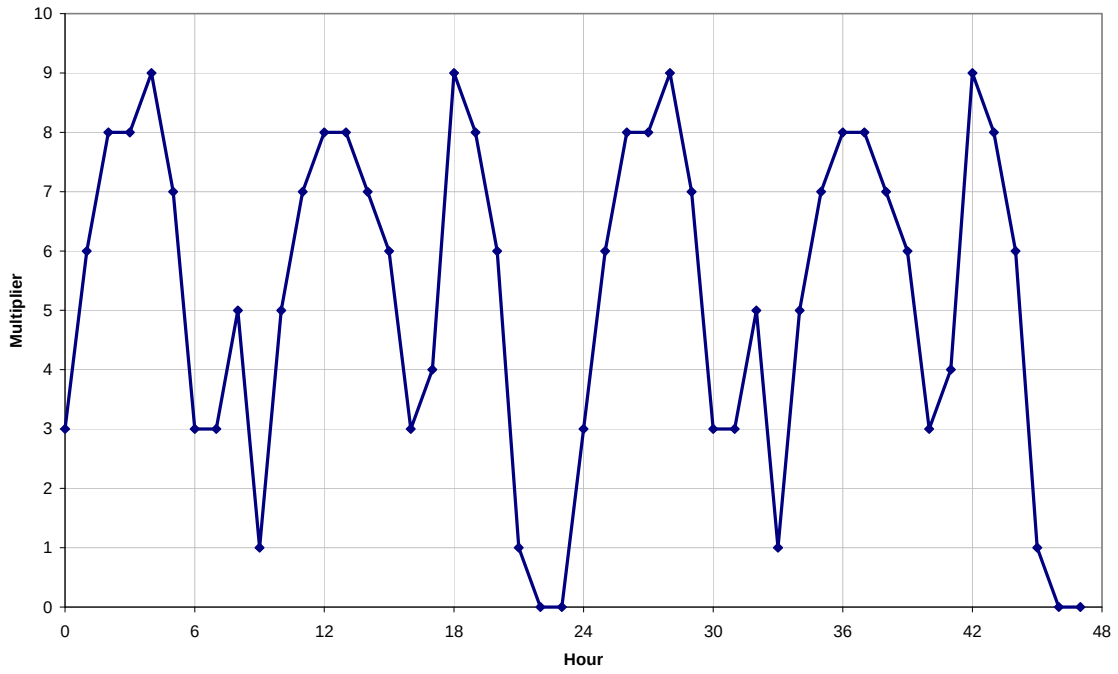
1. Intel Ronler Acres – Rock Creek Basin
2. Triquint Semiconductor – Rock Creek Basin
3. Hillsboro Landfill – Rock Creek Basin
4. Tokai Carbon USA, Inc. – Rock Creek Basin
5. Merix Corporation – Forest Grove Basin



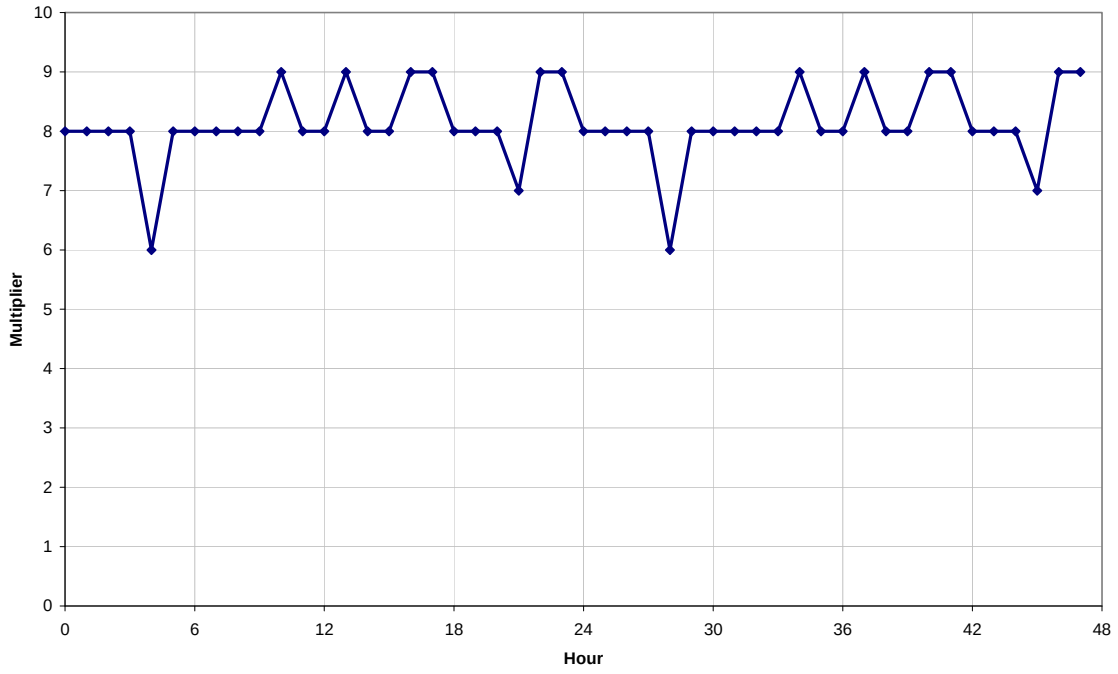
Resers (Allen) curve also applies to:

1. Resers (Jenkins) – Rock Creek Basin

Tektronix-Beaverton



Gray & Co.



APPENDIX D

Detailed Land Use and Development Condition Data (electronic file only)

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.04	-	-	-	-	-	25.9	-	-	-	-
2	-	19.6	-	-	-	-	-	-	-	8.68	-	-	-	-	-	-	-	3.02	-	-	-	2.61	-	0.998	-	32.2	-	-
3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.0	-	-	-	-	-	-	-	-	-
5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
6	13.9	-	-	-	-	-	-	32.7	-	25.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
7	18.1	9.54	-	-	-	-	-	-	-	12.3	-	-	-	-	-	-	4.82	-	0.907	-	22.3	-	-	-	24.7	13.9	-	-
8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.5	-	-	-	-	-	-	-
9	-	-	-	-	28.6	-	-	-	-	-	-	-	-	-	-	-	-	-	3.11	-	-	-	-	-	-	-	-	-
10	-	-	-	-	7.70	-	-	-	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-	-	-	-	-	-	-
11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.66	-	-	-	-	0.0000	-	-	-	-
12	-	-	-	-	0.546	-	9.99	-	-	-	-	-	-	-	-	-	-	-	5.42	-	4.56	-	-	-	-	-	-	-
13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	48.7	-	2.25	-	-	-	-	-	-	-
14	2.31	-	-	-	-	-	2.57	-	-	0.338	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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17	12.1	12.5	-	-	-	-	-	-	-	19.2	-	-	-	-	-	-	60.5	-	0.0001	-	-	22.6	-	-	-	-	-	-
18	-	-	-	-	0.0038	-	12.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
19	-	-	-	-	-	-	-	-	-	6.91	-	-	-	-	-	-	-	17.3	0.0135	-	-	-	-	-	-	-	-	-
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21	-	3.90	-	-	-	-	-	-	1.54	-	-	-	-	-	-	-	0.303	-	-	-	-	-	-	-	-	-	-	-
22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.1	-	-	-	-	-	-	-	-	-
23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	39.4	-	-	-	-	-	-	-	-	-
24	-	-	-	-	-	-	-	-	1.92	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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26	-	-	-	-	2.73	-	-	0.0251	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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28	-	-	-	-	1.71	-	-	-	-	-	-	-	-	-	-	-	-	-	0.159	-	-	-	-	-	-	-	-	-
29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.36	-	-	-	-	-	-	-	-	-
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32	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.66	-	-	-	-	-	-	-	-	-
33	-	-	-	-	0.0004	-	-	-	-	-	-	-	-	-	-	-	-	-	6.78	-	-	-	-	-	-	-	-	-
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36	-	-	-	-	-	-	-	-	1.51	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
37	-	-	-	-	-	-	-	-	3.27	-	-	-	-	-	-	-	417	9.15	-	-	-	-	-	-	-	-	-	-
38	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	-	-	9.81	-	-	-	-	-	-	-	-	-	-	-
39	-	-	-	-	-	-	-	-	34.4	-	-	-	-	-	-	-	0.197	-	-	-	-	-	-	-	-	-	-	-
40	-	0.901	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
41	-	-	-	-	-	-	-	-	30.7	-	-	-	-	-	-	-	-	5.74	-	-	-	-	-	-	-	-	-	-
42	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.297	-	-	-	64.3	-	-	-	-	-	-	-
43	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
44	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.2	-	0.0490	-	-	-	-	-	-	-	-	-
45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.8	-	0.0002	-	-	-	-	-	-	-	-	-
46	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.20	-	-	-	-	-	-	-	-	-
47	-	-	-	-	-	-	-	-	4.77	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
48	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0353	-	199	45.4	-	-	-	-	-	-
49	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.52	1.30	-	-	45.7	-	-	-	-	-	-	-
50	-	1.35	-	-	-	-	-	0.0168	113	5.87	-	-	-	-	-	-	-	-	-	-	-	4.21	-	-	-	-	-	-
51	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.61	34.3	-	-	2.82	-	-	-	-	-	-	-
52	-	-	-	-	-	-	-	-	45.1	-	-	-	-	-	-	-	-	4.08	-	-	-	-	-	-	-	-	-	-
53	-	-	-	-	-	-	-	-	25.2	-	-	-	-	-	-	-	-	0.0120	-	-	-	-	-	-	-	-	-	-
54	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.78	196	-	-	0.686	-	-	-	-	-	-	-
55	1.19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.8	-	-	-	-	-	-	-	-	-
56	65.7	-	-	-	-	48.1	-	-	-	-	-	-	-	-	-	-	-	-	1.71	-	-	-	-	-	-	-	-	-
57	-	-	-	-	3.97	-	-	-	-	17.1	-	-	-	1.20	-	-	16.3	4.05	31.2	-	0.0535	-	-	-	-	-	-	-
58	-	-	-	-	-	-	-	-	0.0065	13.2	-	-	-	-	-	-	-	-	-	-	-	0.304	-	-	-	-	-	-
59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	9.02	-	-	-	-	-	-	-	-	-
60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.8	-	1.84	1.53	-	-	-	-	-	-
61	-	-	-	-	-	-	-	-	5.84	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
62	-	-	-	-	-	-	-	-	28.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
63	-	-	-	-	-	-	-	-	9.04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
64	-	-	-	-	-	-	-	-	5.13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
65	-	-	-	-	-	-	-	-	17.5	-	-	-	-	-	-	-	5.73	-	0.0067	-	-	-	-	-	-	-	-	-
66	-	-	0.921	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0836	-	-	-	83.6	55.5	-	-	-	-	-	-
67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.77	69.8	-	-	-	-	-	-
68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44.1	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
69	-	-	-	-	-	-	-	-	33.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
70	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.98	-	-	-	-	-	-	-	-	-	-	-	-	-
71	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-	-	-	3.59	-	-	30.7	-	-	-	-	-	-	-
72	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.03	-	-	-	2.36	-	-	-	-	-	-	-
73	-	0.0004	-	-	-	-	-	-	-	22.4	-	-	-	-	-	-	-	-	-	-	-	0.0016	27.9	-	-	-	-	-
74	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.80	-	-	-	-	-	-	-
75	-	-	-	-	11.0	-	-	-	-	-	-	-	-	-	-	-	-	-	1.81	-	-	-	-	-	-	-	-	-
76	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.49	-	-	-	-	-	-	-	-	-
77	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	0.0553	-	-	-	-	-	-	-
78	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.46	-	0.0001	0.0395	-	-	-	-	-	-
79	6.80	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
80	-	-	-	-	-	-	-	-	-	0.0847	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
81	-	-	2.37	-	-	-	-	-	-	16.5	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-
82	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.03	-	-	0.330	-	-	-	-	-	-	-	-	-	-
83	-	-	-	-	-	-	-	-	8.92	-	-	-	-	-	-	-	-	0.265	-	-	-	-	-	-	-	-	-	-
84	-	-	-	-	-	-	-	-	-	8.15	-	-	-	-	17.8	-	-	3.84	-	-	14.5	-	-	-	-	-	-	-
85	-	-	-	-	-	-	-	-	41.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
86	-	-	-	-	-	-	-	-	2.89	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
87	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.2	-	-	-	-	-	-	-	-	-
88	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
89	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.66	-	-	-	-	-	-	-	-	-
90	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.0	-	-	-	-	-	-	-	-	-
91	-	-	-	-	0.0018	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0265	-	-	-	-	-	-	-	-	-
92	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.3	-	-	0.0000	-	-	-	-	-	-
93	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.625	-	-	30.9	-	-	-	-	-	-
94	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.36	-	-	-	-	-	-	-	-	-
95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
96	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
97	-	-	-	-	0.151	-	-	-	-	-	-	-	-	-	-	-	-	-	29.6	-	-	-	-	-	-	-	-	-
98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.4	-	-	-	-	-	-	-	-	-
99	-	-	-	-	-	-	-	-	3.06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
100	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.203	-	8.49	-	-	-	-	-	-	-	-	-
101	-	-	-	-	0.997	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
102	-	-	-	-	286	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
103	-	-	-	-	66.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
104	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
105	-	-	-	-	203	-	-	-	-	-	-	-	-	-	-	-	-	-	31.2	-	-	-	-	-	-	-	-	-
106	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.8	-	-	0.0909	-	-	-	-	-	-	-	-	-	-
107	-	0.0001	-	-	-	-	-	-	52.2	0.0024	-	-	-	-	-	-	3.11	0.135	-	-	3.47	-	-	-	-	-	-	-
108	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.34	-	-	4.98	-	-	-	-	-	-	-
109	-	-	-	-	-	-	-	-	86.1	5.52	-	-	-	-	-	-	4.98	-	-	-	12.1	-	-	-	-	-	-	-
110	-	0.0834	-	-	-	-	-	-	-	3.97	-	-	-	-	-	-	-	39.6	-	-	2.96	-	-	-	-	-	-	-
111	-	8.61	-	-	-	-	-	-	-	14.4	-	-	-	-	-	-	-	5.58	-	-	3.85	-	-	-	-	-	-	-
112	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.618	-	-	-	-	-	-	-
113	-	-	-	-	-	-	-	-	-	5.40	-	-	-	-	-	-	-	12.8	-	-	53.7	-	-	-	-	-	-	-
114	-	-	-	-	-	-	-	-	-	0.0013	-	-	-	-	-	-	-	-	-	-	14.5	-	-	-	-	-	-	-
115	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.946	-	-	4.57	-	-	-	-	-	-	-
116	-	-	-	-	-	-	-	-	15.4	14.5	-	-	-	-	-	-	-	6.10	-	-	-	-	-	-	-	-	-	-
117	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.0	-	-	15.4	-	-	-	-	-	-	-
118	-	-	-	-	-	-	-	-	-	13.0	-	-	-	-	-	-	-	8.16	-	-	20.1	-	-	-	-	-	-	-
119	-	-	-	-	-	-	-	-	-	7.41	-	-	-	-	-	-	49.0	-	-	-	65.8	-	-	-	-	-	-	-
120	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.171	-	-	14.6	-	-	-	-	-	-	-
121	-	-	-	-	-	-	-	-	-	17.9	-	-	-	-	-	-	-	-	-	-	13.1	-	-	-	-	-	-	-
122	-	-	-	-	-	-	-	-	18.7	4.12	-	-	-	-	-	-	-	-	-	-	10.8	-	-	-	-	-	-	-
123	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.57	-	-	24.9	-	-	-	-	-	-	-
124	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.796	-	-	30.9	-	-	-	-	-	-	-
125	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.85	-	-	13.1	-	-	-	-	-	-	-
126	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0048	-	-	17.3	-	-	-	-	-	-	-
127	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0835	-	-	31.3	-	-	-	-	-	-	-
128	-	13.6	-	-	-	-	-	-	0.198	11.2	0.497	-	-	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-
129	-	10.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.7	-	-	-	-	-	-	-
130	-	-	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
131	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.2	-	5.38	0.943	-	-	-	-	-	-	-	-	-	-
132	-	-	-	-	-	-	-	-	-	3.97	-	-	-	-	9.49	-	-	1.92	-	-	31.7	-	-	-	-	-	-	-
133	-	-	-	-	-	-	-	-	-	4.48	-	-	-	-	39.0	-	-	1.62	-	-	9.65	-	-	-	-	-	-	-
134	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.997	-	-	11.9	-	-	-	-	-	-	-
135	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.12	-	-	16.2	-	-	-	-	-	-	-
136	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.2	-	-	-	-	-	-	-
137	-	-	-	-	-	-	-	-	-	3.10	-	-	-	-	-	-	-	-	-	-	24.6	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
138	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.51	-	-	18.2	-	-	-	-	-	-	-
139	-	-	-	-	-	-	-	-	0.965	21.6	-	-	-	-	25.2	-	0.0000	5.26	-	-	74.2	-	-	-	-	-	-	-
140	-	-	-	-	-	-	-	-	-	2.34	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-	-	-	-
141	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.63	-	-	-	3.52	-	-	-	-	-	-	-
142	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.7	-	-	-	-	-	-	-
143	-	-	-	-	-	-	-	-	-	7.71	-	-	-	5.21	0.421	-	-	-	-	-	59.3	-	-	-	-	-	-	-
144	-	6.52	-	-	-	-	-	-	-	6.70	-	-	-	-	87.5	-	11.2	-	-	-	8.90	-	-	-	-	-	-	-
145	-	-	-	-	-	-	-	-	-	1.97	-	-	-	1.85	-	-	-	0.390	-	-	24.5	-	-	-	-	-	-	-
146	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.193	-	-	1.50	-	-	10.9	-	-	-	-	-	-	-
147	-	-	-	-	-	-	-	-	-	12.7	-	-	-	5.45	-	-	5.61	4.51	-	-	6.50	-	-	-	-	-	-	-
148	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.32	-	-	1.84	-	-	1.20	-	-	-	-	-	-	-
149	-	-	-	-	-	-	-	-	-	3.93	-	-	-	-	8.60	-	-	1.45	-	-	3.71	-	-	-	-	-	-	-
150	-	-	-	-	-	-	-	-	-	6.12	-	-	-	-	-	-	18.1	-	-	-	7.23	-	-	-	-	-	-	-
151	-	20.5	-	-	-	-	-	-	0.0019	16.9	-	-	-	-	-	-	-	-	-	-	11.1	-	-	-	-	-	-	-
152	-	4.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0014	-	-	-	21.1	-	-	-	-	-	-	-
153	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.13	-	-	-	-	-	-	-
154	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.14	-	-	-	-	-	-	-
155	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.5	-	-	-	-	-	-	-
156	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.6	-	-	-	-	-	-	-
157	-	-	-	-	-	-	-	-	-	1.41	-	-	-	-	7.11	-	-	-	-	-	6.66	-	-	-	-	-	-	-
158	-	-	3.05	-	-	-	-	-	-	-	18.1	-	8.46	0.503	-	-	0.547	-	-	-	19.2	7.27	0.734	-	-	-	-	-
159	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.09	-	-	-	117	8.85	-	-	-	-	-	-
160	-	-	0.592	-	-	-	-	-	-	-	-	-	-	-	-	-	10.7	-	-	-	124	75.1	3.05	0.692	-	-	-	-
161	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.3	0.0007	-	-	-	-	-	-
162	-	-	-	-	-	-	-	-	-	7.97	-	-	-	-	-	-	-	-	2.86	-	40.4	38.4	-	-	-	-	-	-
163	-	-	-	-	-	-	-	-	-	31.5	-	-	-	2.29	-	-	-	3.12	-	-	-	150	-	-	-	-	-	-
164	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	86.3	-	-	-	-	-	-
165	-	-	-	-	-	-	-	-	-	0.107	-	-	-	-	-	-	-	-	-	-	0.0001	63.7	-	-	-	-	-	-
166	-	-	-	-	-	-	-	-	0.0000	5.25	-	-	-	-	-	-	33.7	-	-	-	1.72	83.1	-	-	-	-	-	-
167	-	-	-	-	-	-	-	0.0004	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
168	-	-	-	-	-	-	-	-	31.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
169	-	-	7.40	2.34	-	-	-	-	-	95.6	-	-	-	-	-	-	-	-	-	-	1.26	15.5	-	-	-	-	-	-
170	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	153	-	-	-	-	-	-	-	-	-	-	-
171	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.8	3.88	-	-	-	-	-	-
172	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.6	17.4	-	-	-	-	-	-
173	-	-	-	-	-	-	-	-	-	6.05	-	-	-	-	-	-	-	-	-	-	45.6	24.3	-	-	-	-	-	-
174	-	-	-	-	-	-	-	-	-	2.04	-	-	-	-	-	-	-	-	-	-	-	73.9	-	-	-	-	-	-
175	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.95	-	-	-	4.47	95.6	-	-	-	-	-	-
176	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.7	-	-	-	-	-	-
177	-	-	-	2.27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.6	-	-	-	-	-	-
178	-	8.80	-	8.32	-	-	-	-	3.31	33.5	-	-	-	-	-	-	1.40	-	-	-	-	44.0	-	2.45	-	-	-	-
179	-	-	-	-	-	-	-	-	-	0.0027	-	-	-	-	-	-	-	-	-	-	54.8	5.35	-	-	-	-	-	-
180	-	-	-	-	-	-	-	-	-	5.54	-	-	-	-	-	-	3.88	-	-	-	2.12	35.0	-	-	-	-	-	-
181	-	-	-	9.14	-	-	-	30.3	36.9	47.3	-	-	-	-	-	-	10.2	-	-	-	-	2.52	3.58	-	-	-	-	-
182	-	-	1.86	-	-	-	-	18.3	4.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
183	-	9.39	3.96	5.10	-	-	-	4.20	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-
184	-	-	0.196	-	-	-	-	-	-	13.5	-	-	-	-	-	-	-	-	-	-	-	9.29	-	-	-	-	-	-
185	-	1.50	1.63	-	-	-	-	-	11.1	1.17	-	-	-	-	-	-	-	-	-	-	-	38.6	8.10	-	-	-	-	-
186	-	-	-	-	-	-	-	111	2.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
187	-	-	-	-	-	-	-	1.50	19.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
188	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0235	40.5	-	-	-	-	-
189	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.94	-	-	-	0.0007	-	34.0	-	-	-	-
190	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.22	-	-	-	0.208	26.0	12.6	-	-	-	-
191	-	3.40	-	14.1	-	-	-	-	-	32.3	-	-	-	-	-	-	-	5.29	-	-	-	-	-	-	-	-	-	-
192	-	1.93	-	6.49	-	-	-	22.9	18.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
193	-	-	-	-	-	-	-	-	-	6.08	-	-	-	-	-	-	-	5.72	-	-	-	0.363	-	29.7	-	-	-	-
194	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.11	-	-	-	0.0027	34.8	-	-	-	-	-
195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.91	-	-	-	0.0009	18.5	-	-	-	-	-
196	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.15	-	-	-	0.0428	47.1	0.762	-	-	-	-
197	-	-	-	-	-	-	-	-	-	1.16	-	-	8.55	-	-	-	-	8.37	-	-	-	0.0001	-	21.7	-	-	-	-
198	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.13	0.185	-	2.61	-	-	-	-
199	-	10.2	-	2.64	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
200	-	-	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	-	-	3.09	13.6	-	-	-	-	-	-
201	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	50.6	-	-	-	-	-	-	-
202	-	-	-	-	-	-	-	-	83.7	-	-	-	-	-	-	-	0.0024	0.0050	-	-	-	-	-	-	-	-	-	-
203	-	-	-	-	-	-	-	-	84.9	-	-	-	-	-	-	-	-	2.06	-	-	-	-	-	-	-	-	-	-
204	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.39	-	-	-	-	-	-	-	-	-	-	-	-	-
205	-	-	-	-	-	-	-	-	0.0303	-	-	-	-	-	57.3	-	-	2.81	-	-	-	-	-	-	-	-	-	-
206	-	-	-	-	-	-	-	-	-	-	-	-	-	-	68.2	-	-	11.2	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
207	-	-	-	-	-	-	49.6	-	-	0.146	-	-	-	-	0.146	-	-	0.449	-	-	-	-	-	-	-	-	-	-
208	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.2	-	-	3.79	-	-	-	-	-	-	-	-	-	-
209	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.0	-	-	4.69	-	-	-	-	-	-	-	-	-	-
210	-	0.0009	-	-	-	-	-	-	-	7.41	88.3	-	-	-	4.18	-	-	31.5	-	-	-	-	-	-	-	-	-	-
211	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
212	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98.6	-	-	-	-	-	-	-	-	-	-	-	-	-
213	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.0	-	-	-	-	-	-	-	-	-	-	-	-	-
214	-	4.51	-	-	-	-	-	-	-	10.5	-	-	-	-	17.6	-	-	15.3	-	-	23.5	-	-	-	-	-	-	-
215	-	-	-	-	-	-	-	-	-	-	-	-	-	-	60.3	-	-	2.76	-	-	-	-	-	-	-	-	-	-
216	-	0.0004	-	-	-	-	-	-	-	23.4	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	-	-	-	-	-
217	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93.9	-	-	-	-	23.7	-	-	-	-	-	-
218	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	0.0061	-	-	-	-	-	-	-	0.0058	-	-	-	-	-
219	-	-	-	-	-	-	8.50	-	-	-	-	-	-	-	33.0	-	-	13.2	-	-	5.81	2.77	-	-	-	-	-	-
220	-	-	-	-	-	-	-	-	-	4.34	0.0146	-	-	3.56	46.1	-	-	1.54	-	-	-	-	-	-	-	-	-	-
221	-	7.52	-	-	-	-	-	-	12.2	7.68	20.0	-	-	-	-	-	-	0.0023	-	-	-	-	-	-	-	-	-	-
222	-	51.8	-	-	-	-	-	-	-	18.4	44.9	-	-	24.3	18.7	-	-	0.0433	-	-	-	-	-	-	-	-	-	-
223	-	10.6	-	-	-	-	-	-	-	0.0017	0.276	-	-	0.920	-	-	-	0.783	-	-	-	-	-	-	-	-	-	-
224	-	-	-	-	-	-	-	-	22.5	-	-	-	-	-	-	-	-	10.3	-	-	-	-	-	-	-	-	-	-
225	-	-	-	-	-	-	-	-	-	7.55	-	-	-	-	-	-	0.0003	-	-	-	-	48.0	-	-	-	-	-	-
226	-	-	-	-	-	-	-	-	1.99	0.141	-	-	-	-	-	-	30.2	31.8	-	-	7.18	-	-	-	-	-	-	-
227	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0041	-	-	-	-	-	-	0.0015	18.5	-	-	-	-	-
228	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	10.4	-	2.81	-	-	-	-
229	-	-	-	-	-	-	-	-	-	0.667	-	-	-	-	-	-	-	-	-	-	-	0.0015	-	16.7	-	-	-	-
230	-	-	-	-	-	-	-	-	-	36.5	-	-	-	-	-	-	-	-	-	-	-	0.967	-	22.7	-	-	-	-
231	-	61.6	-	0.0852	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
232	-	0.0073	-	-	-	-	-	-	0.0003	-	-	-	-	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-
233	-	0.0019	3.46	-	-	-	-	-	-	36.1	-	-	-	-	-	-	7.16	-	-	-	-	29.4	-	-	-	-	-	-
234	-	-	-	-	-	-	-	-	0.0445	-	-	-	-	-	-	-	6.56	0.0063	-	-	-	45.0	-	-	-	-	-	-
235	-	-	-	-	-	-	-	-	14.1	-	-	-	-	-	-	-	59.3	-	-	-	-	-	-	-	-	-	-	-
236	-	17.2	-	-	-	-	-	-	37.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
237	-	-	1.45	-	-	-	-	-	-	-	-	-	-	-	-	-	42.7	-	-	-	-	57.7	-	-	-	-	-	-
238	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.262	-	-	-	16.5	35.0	-	-	-	-	-	-
239	-	-	-	-	-	-	-	-	-	8.02	-	-	-	-	-	-	73.0	-	-	-	-	61.8	-	-	-	-	-	-
240	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	60.9	-	-	-	-	-	-
241	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	113	45.4	-	-	-	-	-	-
242	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	139	22.7	-	-	-	-	-	-
243	-	-	2.04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55.8	63.5	-	-	-	-	-	-
244	-	-	-	-	-	-	-	-	-	7.63	-	-	-	-	-	-	-	-	-	-	48.8	131	-	-	-	-	-	-
245	-	-	0.386	-	-	-	-	-	-	3.02	-	-	-	-	-	-	7.93	-	-	-	94.3	96.0	-	-	-	-	-	-
246	-	-	10.2	3.42	-	-	-	-	-	-	0.720	-	-	0.464	-	-	0.110	-	-	-	-	158	-	-	-	-	-	-
247	-	-	1.56	0.794	-	-	-	-	-	-	-	-	-	-	-	-	7.80	-	-	-	102	105	-	-	-	-	-	-
248	-	-	35.4	2.27	-	-	-	-	-	0.0001	23.0	-	-	-	-	-	23.9	-	-	-	2.38	17.0	-	-	-	-	-	-
249	-	-	0.0011	-	-	-	-	-	-	-	31.3	-	-	0.701	-	-	-	-	-	-	-	-	-	-	-	-	-	-
250	-	-	1.37	-	-	-	-	-	-	0.483	15.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
251	-	-	-	-	-	-	-	-	-	-	0.237	-	-	-	-	-	38.6	-	-	-	-	9.51	-	-	-	-	-	-
252	-	-	-	-	-	-	-	0.734	-	8.42	-	-	-	-	-	-	7.56	-	-	-	-	74.9	-	-	-	-	-	-
253	-	-	1.15	1.88	-	-	-	89.7	-	29.1	-	-	-	-	-	-	-	-	-	-	-	11.7	-	-	-	-	-	-
254	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.8	-	-	-	-	33.1	-	-	-	-	-	-
255	-	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	-	19.0	-	-	-	-	23.1	2.84	-	-	-	-	-
256	6.02	-	-	0.444	-	-	-	-	-	11.2	2.79	-	-	-	-	-	-	0.0010	-	-	-	6.94	-	-	-	-	-	-
257	-	-	-	-	-	-	-	-	-	2.09	15.2	-	-	-	-	-	13.3	-	-	-	11.9	29.8	-	-	-	-	-	-
258	-	-	-	-	-	-	-	42.9	-	-	-	-	-	3.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-
259	-	-	-	-	-	-	-	2.24	-	0.0013	-	-	-	-	6.52	-	-	-	-	-	-	-	-	-	-	-	-	-
260	-	-	-	-	-	-	-	-	-	0.0724	-	-	0.0104	-	-	-	-	218	-	-	-	-	-	-	-	-	-	-
261	-	-	-	-	-	-	-	-	-	-	-	-	61.5	-	-	-	-	3.23	-	-	-	-	-	-	-	-	-	-
262	-	3.44	-	-	-	-	-	-	5.93	12.0	4.03	-	-	-	-	-	0.222	-	-	-	-	97.0	-	-	-	-	-	-
263	-	-	-	-	-	-	-	0.518	0.0000	12.8	12.2	-	-	-	-	-	-	-	-	-	0.0001	114	-	-	-	-	-	-
264	-	0.0014	-	-	-	-	-	7.01	-	52.1	17.0	-	-	-	-	-	20.1	-	-	-	-	-	-	-	-	-	-	-
265	-	-	0.423	0.102	-	-	-	-	-	18.9	-	-	-	-	-	-	-	3.28	-	-	-	14.9	-	-	-	-	-	-
266	-	-	-	-	-	-	-	-	-	7.41	-	-	-	-	-	-	-	-	-	-	-	25.5	-	-	-	-	-	-
267	-	0.0205	0.449	-	-	-	-	-	-	34.1	-	-	-	-	-	-	-	0.502	-	-	-	24.2	-	10.4	-	-	-	-
268	-	20.7	-	-	-	-	-	-	-	0.0004	-	-	23.3	-	10.5	-	-	-	-	-	-	-	-	-	-	-	-	-
269	-	30.4	-	-	-	-	-	-	-	35.8	-	-	5.07	-	-	-	3.21	-	-	-	0.0002	5.08	-	-	-	-	-	-
270	-	-	-	-	-	-	-	-	-	-	0.0003	-	14.1	-	-	-	-	2.82	-	-	0.0000	6.83	-	-	-	-	-	-
271	-	0.0711	-	-	-	-	-	-	-	46.3	-	-	-	-	-	-	-	-	-	-	0.0001	5.82	17.4	1.15	-	-	-	-
272	-	17.2	-	-	-	-	-	36.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
273	-	-	-	-	-	-	-	3.14	-	-	-	-	-	-	-	-	-	14.7	-	-	-	-	-	-	-	-	-	-
274	-	-	-	-	-	-	-	49.0	0.0004	0.0008	0.0006	-	39.9	-	-	-	-	4.41	-	-	-	-	-	-	-	-	-	-
275	-	-	-	-	-	-	-	3.42	0.0000	0.0053	-	13.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
276	-	-	12.3	-	-	-	-	0.548	0.0079	0.0842	24.0	-	-	14.1	65.0	-	24.5	-	-	-	-	7.62	-	-	-	-	-	-
277	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.2	-	-	-	-	-	-	-	-	-	-	-	-	-
278	-	-	-	-	-	-	-	8.60	0.0022	-	-	0.0010	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-
279	-	0.0003	-	0.370	-	-	-	-	-	-	-	-	6.43	-	-	-	0.0000	-	-	-	0.0006	44.9	3.26	1.62	-	-	-	-
280	-	-	5.05	-	-	-	-	-	5.86	0.430	-	-	-	-	-	-	3.54	-	-	-	-	88.3	-	-	-	-	-	-
281	-	-	-	-	-	-	-	-	26.4	-	-	-	-	-	-	-	8.69	-	-	-	-	12.2	-	-	-	-	-	-
282	-	-	-	-	-	-	-	-	-	14.4	-	-	-	-	-	-	-	-	-	-	-	14.6	-	-	-	-	-	-
283	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	18.0	-	-	-	0.308	49.7	-	-	-	-	-	-
284	-	20.6	-	-	4.03	-	-	0.0037	5.37	13.5	-	-	-	-	-	-	18.7	-	-	-	5.98	31.2	-	-	-	-	-	-
285	-	-	-	-	-	-	-	-	-	1.08	-	-	-	-	-	-	16.4	-	-	-	13.4	90.2	-	-	-	-	-	-
286	16.2	7.97	-	-	-	-	-	-	3.60	22.4	-	-	-	-	-	-	1.54	-	-	-	-	27.4	-	-	-	-	-	-
287	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.40	-	-	-	-	-	-
288	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.1	-	-	-	3.70	20.9	-	-	-	-	-	-
289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.50	-	-	-	24.6	21.5	-	-	-	-	-	-
290	-	-	-	-	-	-	-	-	-	16.3	-	-	-	-	-	-	0.0003	-	-	-	-	74.9	-	-	-	-	-	-
291	7.16	-	-	-	-	-	-	-	-	33.1	-	-	-	-	-	-	2.62	-	-	-	-	-	-	-	-	-	-	-
292	4.88	-	-	-	-	-	-	-	-	16.8	-	-	-	-	-	-	3.32	-	-	-	-	67.0	-	-	-	-	-	-
293	-	-	-	-	-	-	-	-	38.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
294	19.4	-	-	-	-	-	-	-	-	8.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
295	3.68	-	-	-	-	-	-	-	-	16.6	-	-	-	-	-	-	-	-	-	-	-	14.2	-	-	-	-	-	-
296	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.1	-	-	-	-	12.8	-	-	-	-	-	-
297	0.973	-	0.0637	19.0	-	-	-	-	10.7	11.3	7.14	-	-	-	-	-	13.9	-	-	-	-	87.6	-	-	-	-	-	-
298	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.0	-	-	-	-	-	-
299	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.0	-	-	-	-	41.4	-	-	-	-	-	-
300	17.0	-	-	-	-	-	-	-	-	0.368	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
301	-	-	-	-	-	-	-	-	-	9.62	-	-	-	-	-	-	6.17	-	-	-	5.78	64.0	-	-	-	-	-	-
302	3.45	-	-	-	-	-	-	-	-	31.6	-	-	-	-	-	-	5.67	-	-	-	-	17.6	-	-	-	-	-	-
303	-	-	-	-	-	-	-	-	-	15.7	1.71	-	-	-	-	-	14.3	-	-	-	-	43.7	-	-	-	-	-	-
304	5.70	-	-	-	-	-	-	-	-	19.1	-	-	-	-	-	-	2.71	-	-	-	-	34.8	-	-	-	-	-	-
305	-	-	7.54	-	-	-	-	-	0.731	14.4	19.3	-	-	-	2.40	-	1.43	-	-	-	18.8	44.2	-	-	-	-	-	-
306	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.0	-	-	50.5	7.56	0.378	38.0	-	-	-	-
307	-	10.4	0.996	-	-	-	-	-	-	7.28	-	-	-	-	-	-	-	4.42	-	-	-	0.0163	-	60.6	-	-	-	-
308	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-	-	-	-	-	0.0010	12.5	-	-	-	-	-
309	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.26	24.4	-	-	-	-	-	-
310	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.66	-	-	16.3	0.0008	-	19.7	-	-	-	-
311	-	-	2.43	-	-	-	-	-	-	-	-	-	-	-	-	-	9.05	-	-	-	-	96.7	28.2	7.98	-	-	-	-
312	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0035	54.1	-	-	-	-	-
313	-	-	-	-	-	-	-	-	-	6.81	9.79	-	-	-	-	-	-	-	-	-	-	0.0060	69.8	-	-	-	-	-
314	-	-	0.0000	-	-	-	-	-	-	0.0001	1.58	-	-	-	-	-	-	15.3	-	-	-	0.334	65.6	-	-	-	-	-
315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.2	-	-	0.0017	1.03	61.1	8.63	-	-	-	-
316	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.54	-	-	-	1.02	83.1	16.7	-	-	-	-
317	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	0.726	35.2	55.1	-	-	-	-
318	-	0.0003	-	-	-	-	-	-	-	4.61	-	-	-	-	-	-	-	29.5	-	-	-	0.0073	106	6.28	-	-	-	-
319	-	-	-	-	-	-	-	-	-	6.07	-	-	-	-	-	-	-	-	-	-	-	0.0959	107	5.11	-	-	-	-
320	-	-	-	-	-	-	-	-	-	1.89	-	-	-	-	-	-	-	-	-	-	-	30.1	-	-	-	-	-	-
321	-	-	0.641	-	-	-	-	-	-	26.9	-	-	-	-	-	-	3.02	-	-	-	2.54	78.6	-	-	-	-	-	-
322	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	57.3	1.93	-	-	-	-	-	-
323	-	-	-	-	-	-	-	-	-	23.3	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-
324	-	-	-	-	-	-	-	-	-	1.55	-	-	-	-	-	-	13.9	-	-	-	-	54.9	-	-	-	-	-	-
325	-	-	0.188	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	8.10	-	-	-	99.8	73.1	-	-	-	-	-	-
326	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.05	-	-	-	62.5	55.4	-	-	-	-	-	-
327	-	-	-	-	-	-	-	-	-	8.75	-	-	-	-	-	-	24.6	8.22	-	-	51.8	102	33.8	18.7	-	-	-	-
328	-	-	-	-	-	-	-	-	-	21.9	-	-	-	-	-	-	-	-	-	-	-	92.7	-	-	-	-	-	-
329	-	-	0.618	1.31	-	-	-	-	-	8.27	-	-	-	-	-	-	1.04	-	-	-	0.573	92.8	-	-	-	-	-	-
330	20.1	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	1.01	-	-	-	0.0000	14.7	-	-	-	-	-	-
331	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	4.09	68.2	-	-	-	-	-	-
332	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.49	-	-	-	-	53.9	-	-	-	-	-	-
333	-	-	8.27	-	-	-	-	-	-	24.1	-	-	-	-	-	-	0.0001	-	-	-	5.37	107	-	-	-	-	-	-
334	-	-	2.01	-	-	-	-	-	-	28.1	-	-	-	-	-	-	3.33	-	-	-	-	29.4	-	-	-	-	-	-
335	-	-	0.937	-	-	-	-	-	-	11.6	-	-	-	-	-	-	0.0001	-	-	-	15.2	6.88	-	-	-	-	-	-
336	0.0047	-	-	-	-	-	-	-	-	7.88	-	-	-	-	-	-	6.84	-	-	-	16.9	26.6	-	-	-	-	-	-
337	-	6.11	0.0004	0.762	-	-	-	-	-	4.13	-	-	-	-	-	-	-	0.307	-	-	-	8.36	85.8	26.0	-	-	-	-
338	-	0.0001	-	-	-	-	-	-	-	28.7	-	-	0.284	-	-	-	-	7.23	-	-	0.0003	1.31	34.0	4.36	-	-	-	-
339	-	11.3	0.0349	3.53	-	-	-	-	-	12.5	-	-	-	-	-	-	-	-	-	-	-	0.0010	20.8	-	-	-	-	-
340	-	-	-	-	-	-	-	-	-	1.91	-	-	-	-	-	-	20.9	-	-	-	-	19.8	-	-	-	-	-	-
341	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77.7	-	-	-	-	-	-
342	-	-	-	1.04	-	-	-	-	-	0.234	2.83	-	-	-	-	-	22.7	-	-	-	-	87.6	0.415	-	-	-	-	-
343	-	0.0003	0.572	-	-	-	-	-	-	13.5	0.0000	-	0.927	-	-	1.22	-	-	-	-	-	0.793	5.65	38.4	-	-	-	-
344	-	0.385	4.73	-	-	-	-	-	-	14.8	1.11	-	9.75	-	-	-	-	0.0308	-	-	-	0.0061	58.6	1.16	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
345	-	-	-	-	-	-	-	-	-	20.9	-	-	-	-	44.7	-	0.0059	7.15	-	-	91.4	21.3	-	-	-	-	-	-
346	-	9.45	-	-	-	-	-	-	-	15.9	-	-	-	-	-	-	4.44	4.23	-	-	4.03	-	-	-	-	-	-	-
347	-	0.0075	-	-	-	-	-	-	-	8.10	-	-	-	-	-	-	-	15.6	-	-	90.5	-	-	-	-	-	-	-
348	-	-	1.42	3.53	-	-	-	-	-	-	0.0751	-	17.0	0.0001	-	-	7.49	-	-	-	-	15.4	-	-	-	-	-	-
349	-	-	-	3.79	-	-	-	-	-	-	4.83	-	-	-	-	-	17.5	-	-	-	-	7.54	6.83	-	-	-	-	-
350	-	-	-	3.83	-	-	-	-	-	-	4.48	-	-	-	-	-	0.0004	-	-	-	-	27.1	2.07	-	-	-	-	-
351	-	-	15.6	28.1	-	-	-	-	-	0.151	7.74	-	-	-	5.34	-	-	-	-	-	-	19.8	-	-	-	-	-	-
352	-	-	-	-	-	-	-	-	-	15.1	10.2	-	-	-	-	-	-	-	-	-	-	48.2	5.19	-	-	-	-	-
353	-	-	-	-	-	-	-	-	-	-	0.0952	-	-	-	-	-	-	-	-	-	-	58.5	-	-	-	-	-	-
354	-	-	-	-	-	-	-	-	-	-	1.54	-	-	-	-	-	-	-	-	-	-	64.7	-	-	-	-	-	-
355	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.79	-	-	-	-	169	-	-	-	-	-	-
356	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	29.0	-	-	-	-	-	-
357	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.5	-	-	-	-	-	-
358	-	-	-	-	-	-	-	-	-	5.85	-	-	-	-	-	-	-	-	-	-	-	22.3	-	-	-	-	-	-
359	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	6.32	-	-	-	-	-	-
360	-	-	-	-	-	-	-	-	-	6.57	-	-	-	-	-	-	0.0000	-	-	-	-	50.7	-	-	-	-	-	-
361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.7	-	-	-	-	-	-
362	-	0.839	1.21	-	-	-	-	-	0.0001	15.7	-	-	-	-	-	-	-	-	-	-	-	64.2	-	-	-	-	-	-
363	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.140	64.6	-	-	-	-	-
364	-	24.1	0.0026	6.18	-	-	-	4.93	-	8.28	25.9	-	5.57	-	-	-	-	-	-	-	-	0.0000	-	0.692	-	-	-	-
365	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	64.1	0.0030	-	10.3	-	-	-	-
366	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	9.08	-	-	-	0.0002	24.0	-	-	-	-	-	-
367	-	0.0008	-	17.7	-	-	-	98.7	0.0225	0.0009	5.48	-	-	20.0	29.3	-	-	-	-	-	-	-	-	-	-	-	-	-
368	-	0.0556	-	-	-	-	-	1.06	-	0.0009	17.7	-	15.5	4.65	0.0995	-	-	1.74	-	-	12.3	0.0510	59.9	22.1	-	-	-	-
369	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.28	-	-	1.44	-	-	4.94	5.04	-	-	-	-	-	-
370	-	-	0.888	3.30	-	-	-	-	7.21	4.40	14.1	-	-	-	11.6	-	2.69	1.74	-	-	0.0649	60.5	-	-	-	-	-	-
371	-	-	-	-	14.5	-	-	-	4.11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
372	-	-	-	-	-	-	-	-	24.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
373	-	-	-	-	-	-	-	-	75.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
374	-	4.19	-	-	-	-	-	-	-	23.3	-	-	-	-	-	-	-	-	-	-	13.6	-	-	-	-	-	-	-
375	-	0.453	-	-	-	-	-	-	-	6.74	-	-	-	-	-	-	0.0022	9.12	-	-	35.0	-	-	-	-	-	-	-
376	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.79	-	-	-	12.3	-	-	-	-	-	-	-
377	-	-	-	-	-	-	-	-	-	23.9	-	-	-	-	-	-	-	3.07	-	-	4.34	-	-	-	-	-	-	-
378	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.5	-	-	-	-	-	-	-
379	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	96.7	-	-	-	-	-	-	-	-	-	-	-	-	-
380	-	22.4	-	-	-	-	-	-	12.4	21.3	-	-	-	-	13.2	-	-	0.619	-	-	40.3	-	-	-	-	-	-	-
381	-	-	-	-	-	-	-	-	-	32.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
382	-	-	-	-	-	-	-	-	88.7	0.269	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
383	-	-	-	-	-	-	-	-	-	10.2	-	-	-	-	-	-	4.39	-	-	-	27.7	14.2	-	-	-	-	-	-
384	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.5	56.7	-	-	-	-	-	-
385	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	-	-	9.02	-	-	-	-	-	-	-
386	-	-	-	-	-	-	-	-	-	3.48	-	-	-	-	-	-	19.5	-	-	-	19.1	-	-	-	-	-	-	-
387	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.4	-	-	-	0.367	47.4	-	-	-	-	-	-
388	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.0	-	-	-	-	-	-	-
389	-	55.2	-	-	-	-	-	-	0.0151	-	-	-	-	-	-	-	-	-	-	-	2.14	-	-	-	-	-	-	-
390	-	12.9	0.943	3.35	-	-	-	-	-	1.98	5.61	-	-	-	0.0063	-	-	4.46	-	-	-	0.0008	-	23.5	-	-	-	-
391	-	-	-	-	-	-	-	-	18.1	18.9	-	-	-	-	-	-	15.1	-	-	-	-	-	-	-	-	-	-	-
392	-	0.0017	-	-	-	-	-	-	-	38.4	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-
393	-	-	-	-	-	-	-	-	42.0	11.1	-	-	-	-	-	-	-	1.27	-	-	13.6	-	-	-	-	-	-	-
394	-	6.32	-	-	-	-	-	-	6.76	11.2	-	-	-	-	-	-	0.0002	2.66	-	-	68.0	-	-	-	-	-	-	-
395	-	8.93	-	-	-	-	-	-	-	8.03	-	-	-	-	-	-	8.45	4.62	-	-	82.6	-	-	-	-	-	-	-
396	-	-	-	-	-	-	-	-	2.19	22.2	11.1	-	-	-	-	-	-	0.429	-	-	3.16	-	-	-	-	-	-	-
397	-	-	-	-	0.0138	-	-	-	-	-	-	-	-	-	-	-	-	0.0049	-	-	31.9	0.0197	-	-	-	-	-	-
398	-	-	-	-	0.0029	-	-	-	-	2.51	-	-	-	-	-	-	-	0.0322	-	-	64.3	0.0018	-	-	-	-	-	-
399	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
400	-	-	-	-	-	-	-	-	-	0.684	-	-	-	-	-	-	-	9.19	-	-	35.5	-	-	-	-	-	-	-
401	-	-	-	-	-	-	-	-	-	18.0	-	-	-	-	6.69	-	-	-	-	-	4.76	-	-	-	-	-	-	-
402	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.3	-	-	41.8	-	-	-	-	-	-	-
403	-	-	-	-	-	-	-	-	25.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
404	-	-	-	-	-	-	-	-	32.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
405	-	-	-	-	-	-	-	-	23.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
406	-	17.1	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-	53.3	-	-	-	-	-	-	-
407	-	12.5	-	-	-	-	-	-	-	50.0	-	-	-	-	-	-	0.0134	-	-	-	207	-	-	-	-	-	-	-
408	-	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	-	-	17.2	-	-	96.3	-	-	-	-	-	-	-
409	-	3.76	-	-	-	-	-	-	-	18.5	-	-	-	-	25.3	-	-	4.87	-	-	59.1	-	-	-	-	-	-	-
410	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.2	-	-	-	-	-	-	-	-	-	-	-	-	-
411	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76.9	-	-	-	-	-	28.8	-	-	-	-	-	-	-
412	-	-	-	-	-	-	-	-	255	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
413	-	-	-	-	-	-	-	-	111	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
414	-	15.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
415	-	21.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
416	-	-	-	-	-	-	137	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-	-	-	-	-	-	-	-
417	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	-	-	0.257	-	-	-	-	-	-	-	-	-	-
418	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.31	-	-	-	-	-	-	-	-	-	-	-	-	-
419	-	-	-	-	-	-	-	-	-	2.29	-	-	-	-	47.1	-	-	14.7	-	-	3.26	-	-	-	-	-	-	-
420	-	-	-	-	-	-	-	-	-	16.2	-	-	-	-	10.7	-	-	2.06	-	-	3.95	5.79	-	-	-	-	-	-
421	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.0	-	-	0.299	-	-	-	-	-	-	-	-	-	-
422	-	-	-	-	-	-	-	-	112	-	-	-	-	-	1.63	-	-	14.1	-	-	-	-	-	-	-	-	-	-
423	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.905	-	-	23.6	-	-	-	-	-	-	-
424	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.3	-	-	-	-	-	-	-
425	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-	-	-	-
426	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.9	-	-	-	-	-	-	-
427	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.86	-	-	19.3	-	-	-	-	-	-	-
428	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.0	-	-	-	14.4	-	-	-	-	-	-	-
429	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	-	-	-	-	-	-	-
430	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.101	-	-	6.32	-	-	-	-	-	-	-
431	-	-	-	-	-	-	-	-	0.396	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
432	-	4.21	-	-	-	-	-	-	93.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
433	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	38.5	-	-	6.65	-	-	0.555	8.05	-	-	-	-	-	-
434	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.3	80.5	-	-	-	-	-	-
435	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.116	-	-	-	19.4	74.4	-	-	-	-	-	-
436	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.18	-	-	-	-	-	-
437	-	-	0.240	1.26	-	-	-	-	-	10.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
438	4.25	-	-	-	-	-	-	-	-	22.4	-	-	-	-	-	-	5.74	-	-	-	46.3	66.2	-	-	-	-	-	-
439	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90.1	-	-	-	-	-	-	-
440	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52.8	28.4	-	-	-	-	-	-
441	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	101	13.3	-	-	-	-	-	-
442	-	-	-	-	-	-	-	-	-	12.9	-	-	-	-	-	-	-	-	-	-	20.9	40.3	-	-	-	-	-	-
443	5.64	-	-	-	-	-	-	-	-	96.2	-	-	-	-	-	-	-	-	-	-	5.44	32.8	-	-	-	-	-	-
444	-	-	-	-	-	-	-	-	-	9.01	-	-	-	-	-	-	-	-	-	-	11.8	27.6	-	-	-	-	-	-
445	-	-	-	-	-	-	-	-	-	24.0	-	-	-	-	-	-	-	-	-	-	29.0	24.6	-	-	-	-	-	-
446	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44.4	-	-	-	-	-	-	-	-	-
447	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
448	-	-	-	-	42.2	-	-	-	3.60	-	-	-	-	-	-	-	0.0026	-	54.1	-	0.0000	-	-	-	-	-	-	-
449	-	-	0.932	-	1.58	-	-	-	-	-	-	-	-	-	-	-	-	-	17.4	-	-	-	-	-	-	-	-	-
450	-	-	-	-	-	-	-	-	-	0.854	-	-	-	-	-	-	-	-	2.51	2.03	-	270	-	-	-	-	-	-
451	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	2.48	0.0017	119	-	-	-	-	-	-
452	-	-	-	-	-	-	-	-	-	-	-	-	-	1.71	-	-	0.0254	1.41	-	13.3	-	67.1	-	-	-	-	-	-
453	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.9	14.6	-	-	-	-	-	-
454	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	28.2	-	-	-	-	-	-
455	18.4	-	-	-	-	-	-	-	-	12.2	10.6	-	-	-	-	-	5.69	-	-	-	-	1.60	-	-	-	-	-	-
456	-	-	-	-	-	-	-	-	-	16.6	0.0000	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-	-	-	-
457	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
458	-	-	-	-	-	-	-	-	55.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
459	-	-	-	-	21.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
460	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	-	-	-	-
461	-	-	-	-	3.59	-	-	-	-	-	-	-	-	-	-	-	-	-	69.0	-	-	-	-	-	-	-	-	-
462	-	-	-	-	1.40	-	85.7	-	-	-	-	-	-	-	-	-	-	-	7.80	-	-	-	-	-	-	-	-	-
463	-	-	0.216	-	0.612	-	-	-	-	-	-	-	-	-	-	-	-	-	0.433	0.0000	6.68	-	-	-	-	-	-	-
464	-	-	-	-	0.0338	-	-	-	-	-	-	-	-	-	-	-	-	-	1.19	-	10.8	-	-	-	-	-	-	-
465	-	-	-	-	0.620	-	-	-	-	-	-	-	-	-	-	-	-	-	73.4	-	-	-	-	-	-	-	-	-
466	-	0.0105	-	-	-	-	-	-	1.27	-	-	-	-	-	12.1	-	2.99	-	-	-	-	-	-	-	-	-	-	-
467	-	-	-	-	1.00	-	-	-	-	-	-	-	-	-	-	-	-	4.53	-	-	20.5	0.0017	-	-	-	-	-	-
468	-	-	9.83	-	-	-	32.6	-	-	0.778	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-
469	-	-	0.0001	-	-	-	21.9	-	-	16.8	-	-	-	-	-	-	13.1	-	-	0.0000	21.7	9.32	-	-	-	-	-	-
470	-	-	-	-	-	-	-	-	-	1.81	-	-	-	-	-	-	-	2.16	-	-	2.04	-	-	-	-	-	-	-
471	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
472	9.85	-	-	-	0.661	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
473	-	-	-	-	2.43	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.94	-	-	-	-	-	-	-	-
474	-	-	-	-	2.38	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.622	-	-	-	-	-	-	-	-
475	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
476	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	10.7	-	-	-	-	-	-	-	-
477	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0229	5.67	-	-	-	-	-	-	-	-
478	-	-	-	-	2.12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
479	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
480	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.31	-	-	-	36.5	-	-	-	-	-	-	-
481	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.25	-	-	-	-	38.6	-	-	-	-	-	-
482	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	12.3	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
483	29.1	-	-	-	-	-	-	-	-	9.46	-	-	-	-	-	-	0.960	-	-	-	-	19.7	-	-	-	-	-	-
484	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0018	-	-	7.23	-	-	-	-	-	-
485	-	-	-	-	-	-	-	-	-	8.81	-	-	-	-	-	-	-	2.02	0.0000	-	-	0.344	-	-	-	-	-	-
486	-	-	-	-	-	-	-	-	-	0.0008	-	-	-	-	-	-	-	0.448	-	-	-	9.85	-	-	-	-	-	-
487	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-
488	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.89	-	-	18.6	-	0.0000	-	-	-	-	-	-
489	-	-	-	-	-	-	-	-	-	0.0004	-	-	-	-	-	-	0.0021	-	-	23.1	-	7.01	-	-	-	-	-	-
490	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	5.96	-	-	-	46.2	-	-	-	-	-	-
491	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.3	-	-	-	-	2.27	-	-	-	-	-	-
492	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.1	0.0001	-	-	0.720	-	-	-	-	-	-
493	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.4	-	-	-	-	-	-
494	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.7	-	-	-	61.4	-	-	-	-	-	-
495	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.49	-	-	-	23.4	-	-	-	-	-	-
496	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0020	-	-	-	-	13.4	-	-	-	-	-	-
497	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.414	-	-	-	13.1	-	-	-	-	-	-
498	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	0.0038	-	-	-	16.5	-	-	-	-	-	-
499	0.0008	5.58	0.591	-	-	-	-	-	-	2.33	-	-	-	-	-	-	0.0270	-	0.0430	-	-	11.0	-	-	-	-	-	-
500	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.6	0.132	-	-	3.71	-	-	-	-	-	-
501	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0398	-	0.154	6.49	-	23.6	-	-	-	-	-	-
502	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0098	-	-	-	-	54.4	-	-	-	-	-	-
503	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	0.549	-	-	-	23.6	-	-	-	-	-	-
504	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	6.48	-	-	-	17.9	-	-	-	-	-	-
505	-	-	-	-	-	-	-	-	-	5.70	-	-	-	-	-	-	-	-	-	-	-	9.40	-	-	-	-	-	-
506	-	-	-	-	-	-	-	-	-	6.71	-	-	-	-	-	-	-	0.0002	0.0284	-	-	7.64	-	-	-	-	-	-
507	-	-	-	-	-	-	-	-	-	16.7	-	-	-	-	-	-	-	-	-	-	-	1.59	-	-	-	-	-	-
508	-	-	0.197	-	-	-	-	-	-	35.9	-	-	-	-	-	-	1.28	4.11	0.0317	-	-	-	-	-	-	-	-	-
509	-	-	-	-	0.0057	-	0.0002	-	-	-	-	-	-	-	-	-	7.27	-	-	-	-	-	-	-	-	-	-	-
510	-	-	-	-	0.0200	-	7.57	-	-	-	-	-	-	-	-	-	-	0.0046	0.256	-	-	-	-	-	-	-	-	-
511	1.71	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.8	-	-	0.0001	-	-	-	-	-	-
512	-	-	-	-	-	-	-	-	115	-	-	-	-	-	-	-	18.7	-	-	-	-	-	-	-	-	-	-	-
513	-	0.442	-	-	-	-	-	-	3.89	1.69	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
514	-	-	-	-	-	-	-	-	-	5.02	-	-	-	-	-	-	-	92.6	-	-	-	-	-	-	-	-	-	-
515	-	-	-	-	-	-	-	-	-	5.46	-	-	-	-	4.82	-	-	14.0	-	-	10.00	-	-	-	-	-	-	-
516	-	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	-	8.04	-	-	20.3	-	-	-	-	-	-	-
517	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0029	9.31	-	-	14.9	-	-	-	-	-	-	-
518	-	-	-	-	-	-	-	-	-	4.92	-	-	-	-	-	-	0.0003	1.92	-	-	12.2	-	-	-	-	-	-	-
519	-	-	-	-	-	-	-	-	-	5.96	-	-	-	-	-	-	9.71	-	-	-	30.9	-	-	-	-	-	-	-
520	-	-	-	-	-	-	-	-	-	3.84	-	-	-	-	-	-	-	-	-	-	20.9	-	-	-	-	-	-	-
521	-	-	-	-	-	-	-	-	-	9.74	-	-	-	-	-	-	0.0065	-	-	-	28.5	-	-	-	-	-	-	-
522	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.1	-	-	-	36.2	-	-	-	-	-	-	-
523	-	-	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	-	-
524	-	-	-	-	-	-	-	-	-	0.339	-	-	-	-	-	-	-	-	-	-	27.7	-	-	-	-	-	-	-
525	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.6	-	-	-	-	-	-	-
526	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.7	-	-	-	-	-	-	-
527	-	-	-	-	-	-	-	-	-	0.0034	-	-	-	-	-	-	-	-	-	-	36.2	-	-	-	-	-	-	-
528	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-	-	0.833	-	-	4.83	-	-	-	-	-	-	-
529	-	-	-	-	-	-	-	-	-	1.76	-	-	-	-	-	-	-	3.67	-	-	36.5	-	-	-	-	-	-	-
530	-	-	-	-	-	-	-	-	-	1.30	-	-	-	-	-	-	-	0.333	-	-	12.0	-	-	-	-	-	-	-
531	-	-	-	-	-	-	-	-	-	3.64	-	-	-	-	-	-	9.51	2.99	-	-	36.2	-	-	-	-	-	-	-
532	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.63	-	-	14.0	-	-	-	-	-	-	-
533	-	-	-	-	-	-	-	-	-	1.32	-	-	-	-	-	-	-	2.62	-	-	10.7	-	-	-	-	-	-	-
534	-	-	-	-	0.110	-	-	-	-	5.34	-	-	-	-	-	-	-	24.7	-	-	-	-	-	-	-	-	-	-
535	-	2.36	-	-	-	-	-	-	22.6	-	-	-	-	-	4.71	-	-	-	-	-	-	-	-	-	-	-	-	-
536	-	-	-	-	-	-	-	-	28.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
537	-	23.2	-	-	-	-	-	-	7.67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
538	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.08	-	-	-	-	-	-	-	-	-	-	-	-	-
539	-	-	-	-	-	-	-	-	14.1	6.61	-	-	-	-	-	-	-	0.370	-	-	0.0811	-	-	-	-	-	-	-
540	-	-	-	-	-	-	-	-	-	6.03	-	-	-	-	-	-	-	-	-	-	0.0689	-	-	-	-	-	-	-
541	-	-	-	-	-	-	-	-	-	17.4	-	-	-	-	-	-	-	1.86	-	-	21.3	-	-	-	-	-	-	-
542	-	1.61	-	-	-	-	-	-	-	8.75	-	-	-	-	15.3	-	0.515	-	-	-	1.48	-	-	-	-	-	-	-
543	-	-	-	-	-	-	-	-	5.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
544	-	-	-	-	-	-	-	-	3.89	-	-	-	-	-	10.5	-	-	-	-	-	-	-	-	-	-	-	-	-
545	-	-	-	-	-	-	-	-	3.42	2.62	-	-	-	-	3.70	-	-	-	-	-	-	-	-	-	-	-	-	-
546	-	-	-	-	-	-	-	-	0.555	-	-	-	-	-	22.8	-	-	-	-	-	-	-	-	-	-	-	-	-
547	-	-	-	-	-	-	-	-	1.70	-	-	-	-	-	19.6	-	-	-	-	-	-	-	-	-	-	-	-	-
548	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.6	-	-	-	-	-	-	-	-	-	-	-	-	-
549	-	-	-	-	-	-	-	-	0.708	11.6	-	-	-	-	-	-	5.04	0.362	-	-	-	-	-	-	-	-	-	-
550	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.98	-	-	-	-	-	-	-	-	-	-	-	-	-
551	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
552	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.6	-	-	-	-	-	-	-	-	-	-	-	-	-
553	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.3	-	-	-	-	-	-	-	-	-	-	-	-	-
554	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.27	-	0.0001	-	-	-	6.40	-	-	-	-	-	-	-
555	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.41	-	-	-	-	-	16.1	-	-	-	-	-	-	-
556	-	-	-	-	-	-	-	-	-	0.142	-	-	-	-	9.01	-	-	-	-	-	-	-	-	-	-	-	-	-
557	-	-	-	-	-	-	-	-	-	1.93	-	-	-	-	-	-	0.0038	1.72	-	-	33.3	-	-	-	-	-	-	-
558	-	-	-	-	-	-	-	-	-	6.16	-	-	-	-	-	-	35.8	5.46	-	-	-	-	-	-	-	-	-	-
559	-	-	-	-	-	-	-	-	-	3.56	-	-	-	-	-	-	-	13.8	-	-	59.9	-	-	-	-	-	-	-
560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.98	-	-	-	43.2	-	-	-	-	-	-	-
561	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
562	-	-	-	-	-	-	-	-	-	5.07	-	-	-	-	-	-	-	-	-	-	18.9	-	-	-	-	-	-	-
563	-	-	-	-	-	-	-	-	-	24.9	-	-	-	-	-	-	-	-	-	-	59.0	-	-	-	-	-	-	-
564	-	-	-	-	-	-	-	-	-	3.44	-	-	-	-	-	-	-	4.50	-	-	36.1	-	-	-	-	-	-	-
565	-	-	-	-	0.213	-	-	-	-	0.971	-	-	-	-	-	-	-	3.07	-	-	21.1	0.0803	-	-	-	-	-	-
566	-	-	-	-	-	-	-	-	26.3	8.76	-	-	-	-	-	-	0.0203	-	-	-	44.0	-	-	-	-	-	-	-
567	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
568	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.13	-	-	3.77	-	-	-	-	-	-	-
569	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.5	-	-	-	-	-	-	-	-	-	-	-	-	-
570	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
571	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.152	-	-	5.41	-	-	-	-	-	-
572	-	-	-	-	-	-	1.56	-	-	32.5	-	-	-	-	-	-	-	-	0.0102	-	-	0.493	-	-	-	-	-	-
573	-	-	-	-	-	-	8.56	-	-	43.4	-	-	-	-	-	-	1.05	-	0.0047	-	-	-	-	-	-	-	-	-
574	2.12	-	-	-	-	-	-	-	-	5.28	-	-	-	-	-	-	-	-	10.4	-	-	50.8	-	-	-	-	-	-
575	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.93	-	3.24	-	-	-	-	-	-
576	-	-	-	-	-	-	-	-	-	0.0006	-	-	-	-	-	-	-	0.0004	-	-	-	13.9	-	-	-	-	-	-
577	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0104	-	0.0013	-	-	9.07	-	-	-	-	-	-
578	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.52	-	-	-	-	-	-	-	-	-	-	-	-	-
579	-	-	-	-	0.0014	-	-	-	-	-	-	-	-	-	-	-	-	-	27.2	-	14.3	-	-	-	-	-	-	-
580	-	-	6.58	-	2.01	-	3.80	-	-	20.8	-	-	-	-	-	-	-	-	5.20	-	6.56	24.1	-	-	-	-	-	-
581	-	-	32.5	-	0.699	-	14.9	-	-	35.9	-	-	-	-	-	-	4.23	-	3.45	-	16.0	13.4	-	-	-	-	-	-
582	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0054	0.0000	11.2	-	13.0	-	-	-	-	-	-
583	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.1	-	-	-	-	-	-	-	-	-	-	-	-	-
584	-	-	-	-	-	-	-	-	-	14.7	2.57	-	-	-	17.5	-	-	-	-	-	1.27	-	-	-	-	-	-	-
585	-	-	-	-	-	-	-	-	-	5.89	-	-	-	-	-	-	-	0.0306	-	-	19.2	-	-	-	-	-	-	-
586	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.7	-	-	-	-	-	-	-	-	-	-	-	-	-
587	-	30.8	-	-	0.0000	-	-	-	22.9	-	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-
588	-	-	16.9	-	-	-	7.11	-	-	-	-	-	-	-	-	-	36.9	-	-	-	47.8	-	-	-	-	-	-	-
589	-	-	6.86	-	52.3	-	23.3	-	-	1.74	-	-	-	-	-	-	0.0048	6.23	-	-	37.2	-	-	-	-	-	-	-
590	-	-	-	-	0.610	-	-	-	-	-	-	-	-	-	-	-	-	1.09	-	-	2.24	-	-	-	-	-	-	-
591	-	5.95	-	-	-	-	-	-	-	7.06	-	-	-	-	15.2	-	-	-	-	-	-	-	-	-	-	-	-	-
592	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.2	-	-	-	-	-	-
593	-	-	-	-	3.80	-	-	-	2.21	-	-	-	-	-	-	-	-	0.0045	-	-	-	-	-	-	-	-	-	-
594	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
595	-	-	-	-	3.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
596	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
597	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.59	-	-	-	-	-	-	-	-	-
598	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.05	-	-	-	-	-	-	-	-	-
599	-	-	-	-	0.989	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.94	-	-	-	-	-	-
600	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
601	-	-	-	-	38.4	0.0009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
602	-	-	-	-	27.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
603	-	-	-	-	86.0	-	-	-	-	-	-	-	-	-	-	-	-	3.18	1.24	-	0.350	-	-	-	-	-	-	-
604	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.29	-	-	-	-	-	-	-	-	-
605	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
606	-	-	-	-	1.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0055	-	-	-	-	-	-	-
607	-	-	-	-	3.21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
608	-	-	-	-	2.59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
609	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
610	-	-	-	-	17.4	-	-	-	-	-	-	-	-	-	-	-	-	-	4.18	-	-	-	-	-	-	-	-	-
611	-	-	-	-	30.9	-	-	-	-	-	-	-	-	-	-	-	-	-	5.00	-	-	-	-	-	-	-	-	-
612	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
613	-	-	-	-	0.329	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
614	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
615	-	-	-	-	1.10	-	-	-	-	-	-	-	-	-	-	-	-	-	0.471	-	-	9.11	-	-	-	-	-	-
616	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
617	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
618	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.1	-	-	-	-	-	-	-	-
619	-	11.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0019	-	-	-	-	1.05	-	-	-	-	-	-
620	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.40	-	-	-	-	10.2	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
621	6.68	-	-	-	-	-	2.79	-	-	21.1	-	-	-	3.68	-	-	9.98	-	-	-	-	15.0	-	-	-	-	-	-
622	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.8	-	-	-	-	17.7	-	-	-	-	-	-
623	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.41	-	-	-	-	-	-
624	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.797	-	-	-	-	22.6	-	-	-	-	-	-
625	-	-	-	-	-	-	7.47	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
626	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
627	-	-	-	-	3.68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
628	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
629	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.17	-	-	-	-	-	-
630	-	-	-	-	-	4.49	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
631	1.21	5.56	-	-	-	-	6.69	-	-	3.65	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
632	-	-	-	-	-	-	7.35	-	-	0.924	-	-	-	-	-	-	0.0382	-	-	-	-	1.30	-	-	-	-	-	-
633	-	-	-	-	-	-	-	-	-	2.07	-	-	-	-	-	-	-	-	-	-	-	0.446	-	-	-	-	-	-
634	-	-	-	-	-	-	-	-	-	17.7	-	-	-	-	-	-	0.0001	-	-	-	-	33.0	-	-	-	-	-	-
635	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.8	-	-	-	-	-	-
636	-	-	-	-	6.16	-	10.3	-	-	12.9	-	-	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-
637	5.20	-	-	-	-	-	-	-	-	7.47	-	-	-	-	-	-	0.590	-	-	-	-	22.0	-	-	-	-	-	-
638	-	-	-	-	-	-	6.78	-	-	4.49	-	-	-	-	-	-	-	-	-	-	-	20.8	-	-	-	-	-	-
639	-	-	-	-	0.0000	-	9.32	-	-	7.41	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
640	16.4	-	-	-	-	-	10.6	-	-	30.9	-	-	-	2.39	-	-	-	-	-	-	-	-	-	-	-	-	-	-
641	0.565	-	-	-	-	-	-	-	-	3.57	-	-	-	-	-	-	-	-	-	-	-	15.2	-	-	-	-	-	-
642	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-
643	-	4.19	-	-	-	-	-	-	-	0.664	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
644	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.3	-	-	-	-	-	-
645	-	-	-	-	35.8	1.50	1.86	-	-	-	-	-	-	-	-	-	0.572	5.50	1.33	-	-	2.31	-	-	-	-	-	-
646	-	4.18	-	-	1.08	-	23.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
647	-	1.62	-	-	-	-	-	-	-	6.98	-	-	-	-	-	-	4.45	2.01	-	-	-	57.4	-	-	-	-	-	-
648	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.04	-	-	-	-	-	-
649	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.04	-	-	-	-	-	-
650	-	-	-	-	-	-	8.81	-	-	16.4	-	-	-	-	-	-	4.10	-	-	-	-	-	-	-	-	-	-	-
651	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.294	-	-	-	-	10.9	-	-	-	-	-	-
652	-	3.23	-	-	-	-	-	-	-	17.5	-	-	-	-	-	-	5.18	3.62	-	-	-	2.08	-	-	-	-	-	-
653	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.44	-	-	-	-	25.6	-	-	-	-	-	-
654	-	5.73	-	-	-	-	-	-	-	2.36	-	-	-	-	-	-	-	-	-	-	-	8.99	-	-	-	-	-	-
655	-	11.9	-	-	-	-	43.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
656	-	-	2.12	-	-	-	2.59	-	-	-	-	-	-	-	-	-	-	3.25	-	0.0001	-	3.29	-	26.0	6.90	-	-	-
657	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-	-	-	4.29	0.0035	-	-	16.8	-	12.7	2.89	-	-	-
658	-	6.35	-	-	-	-	-	0.0044	-	-	-	-	-	-	-	-	6.84	-	-	-	-	15.4	-	-	-	-	-	-
659	-	-	5.09	-	1.66	-	9.32	-	-	-	-	-	-	-	-	-	-	12.0	-	-	-	-	-	-	3.79	-	-	-
660	-	42.4	-	-	-	-	-	-	-	50.7	-	-	-	-	-	-	5.36	2.75	-	-	-	1.27	-	-	-	-	-	-
661	-	-	-	-	0.0156	-	0.0026	0.884	-	-	-	-	-	-	-	-	179	-	-	-	-	0.0000	-	-	-	-	-	-
662	-	-	-	-	-	-	-	-	-	4.09	-	-	-	-	-	-	9.28	3.58	-	-	-	29.8	-	-	-	-	-	-
663	-	-	-	-	-	-	8.85	-	-	-	-	-	-	-	-	-	-	0.0421	-	-	-	-	-	-	-	-	-	-
664	8.49	23.0	-	-	-	-	2.04	-	-	8.27	-	-	-	-	-	-	4.35	-	-	-	-	-	-	-	-	-	-	-
665	-	-	-	-	-	-	0.0431	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-
666	-	-	-	-	-	-	8.85	-	-	23.8	-	-	-	-	-	-	6.31	-	0.0033	-	-	-	-	-	-	-	-	-
667	-	-	-	-	-	-	-	-	-	4.10	-	-	-	-	-	-	9.42	1.82	-	-	-	-	-	-	-	-	-	-
668	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.5	-	-	-	-	-	-
669	-	34.7	-	-	-	-	0.121	-	-	24.6	-	-	-	-	-	-	-	-	-	-	-	6.22	-	-	-	-	-	-
670	6.29	1.71	-	-	-	-	-	-	-	49.4	-	-	-	-	-	-	5.35	0.0005	-	-	-	5.11	-	-	-	-	-	-
671	-	6.35	-	-	-	-	11.7	-	-	7.52	-	-	-	-	-	-	31.4	-	-	-	-	-	-	-	-	-	-	-
672	-	-	-	-	-	-	-	-	-	0.679	-	-	-	-	-	-	-	-	0.0000	-	-	0.551	-	-	-	-	-	-
673	-	-	-	-	0.117	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	3.90	-	-	-	-	-	-
674	19.1	-	-	-	-	-	-	-	-	9.93	-	-	-	-	-	-	-	-	-	-	-	87.0	-	-	-	-	-	-
675	24.1	-	-	-	-	-	-	-	-	0.740	-	-	-	6.72	-	-	2.46	-	-	-	-	5.07	-	-	-	-	-	-
676	-	-	-	-	0.103	-	-	25.8	-	-	-	-	-	-	-	-	42.8	-	-	-	-	34.4	-	-	-	-	-	-
677	-	-	-	-	-	-	11.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
678	-	33.3	-	-	-	-	-	-	-	3.59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
679	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	0.0024	-	-	-	-	4.48	-	-	-	-	-	-
680	-	13.1	-	-	-	-	0.0037	1.29	-	8.35	-	-	-	-	-	-	0.0008	-	-	-	-	18.0	-	-	-	-	-	-
681	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.216	-	-
682	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.28	-	-	-	-	-	-	-
683	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	87.9	-	-	-	-	-	-	-	-	-
684	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.7	-	-	-	-	-	-	-	-	-
685	-	-	-	-	0.0506	-	-	-	-	-	-	-	-	-	-	-	-	-	29.3	-	-	-	-	-	-	-	-	-
686	-	-	-	-	0.0004	-	-	-	-	-	-	-	-	-	-	-	-	-	17.3	-	-	-	-	-	-	-	-	-
687	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.4	-	-	-	-	-	-	-	-	-
688	-	-	-	-	0.0483	-	-	-	-	-	-	-	-	-	-	-	-	-	26.7	-	-	-	-	-	-	-	-	-
689	-	-	-	-	0.0078	5.28	-	-	-	-	-	-	-	-	-	-	-	-	30.7	-	0.879	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
690	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	-	34.9	-	7.56	-	-	-	-	-	-	-
691	0.0034	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.15	-	-	-	-	-	-	-	-	-
692	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.91	-	-	-	-	-	-	-	-	-
693	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.517	-	-	-	-	-	-	-	-	-
694	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.90	-	-	-	-	-	-	-	-	-
695	35.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.91	-	-	-	-	-	-	-	-	-	-
696	5.78	-	-	-	-	-	-	-	-	3.94	-	-	0.229	-	-	-	-	10.3	-	-	-	-	-	-	-	-	-	-
697	-	-	-	-	-	-	-	-	-	9.98	-	-	-	-	-	-	-	-	-	-	-	0.0162	12.9	13.9	-	-	-	-
698	-	-	-	-	-	-	-	-	-	4.06	0.0165	-	4.94	0.0250	-	7.06	-	-	-	-	-	0.0016	-	13.8	-	-	-	-
699	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
700	-	-	-	-	0.0521	-	-	3.75	-	-	-	-	-	-	-	-	-	-	62.9	-	-	-	-	-	-	-	-	-
701	-	-	-	-	0.983	-	2.27	-	-	-	-	-	-	-	-	-	-	-	38.2	-	-	-	-	-	-	-	-	-
702	-	-	-	-	28.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
703	-	-	-	-	12.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
704	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.08	-	-	-	-	-	-	-	-	-
705	-	-	-	-	39.5	-	-	-	-	-	-	-	-	-	-	-	-	-	1.78	-	-	-	-	-	-	-	-	-
706	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0570	1.46	-	0.0000	9.79	-	-	22.9	-	-	-
707	-	-	-	-	0.0675	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
708	-	-	-	-	0.0189	-	-	-	-	-	-	-	-	-	-	-	-	-	12.8	-	-	-	-	-	-	-	-	-
709	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.03	-	-	-	-	-	-	-	-	-
710	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-
711	81.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.0	-	-	-	-	-	-	-	-	-	-
712	13.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.120	-	-	48.0	-	-	-	-	-	-	-
713	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.9	5.21	-	-	-	-	-	-
714	-	8.68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	67.4	12.2	-	-	-	-	-	-
715	-	-	-	-	-	-	81.3	1.61	-	-	-	-	-	-	-	-	-	5.31	-	-	-	-	-	1.22	-	-	-	-
716	-	-	-	-	-	-	-	32.5	-	-	-	-	-	-	-	-	-	0.184	-	-	-	-	-	30.4	-	-	-	-
717	-	-	-	5.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
718	-	-	-	4.83	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.7	-	-	-	-	-	-
719	-	-	-	7.79	-	-	-	-	-	-	-	-	-	-	-	-	-	5.73	-	-	-	75.1	1.99	-	-	-	-	-
720	-	-	-	-	-	-	-	-	-	0.260	-	-	-	-	-	-	-	-	-	-	-	30.9	0.311	-	-	-	-	-
721	1.67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.9	19.4	-	-	-	-	-
722	-	1.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.6	-	-	-	-	-	-
723	-	-	-	-	-	-	-	-	-	-	7.44	-	0.415	0.0129	7.17	5.44	-	-	-	-	-	-	-	-	-	-	-	-
724	-	-	-	-	-	-	-	-	-	7.81	-	-	-	-	-	-	-	0.554	-	-	-	0.0001	4.37	2.68	-	-	-	-
725	-	-	-	-	-	-	-	-	-	-	-	-	-	0.367	14.9	-	-	-	-	-	-	-	-	-	-	-	-	-
726	-	-	-	-	-	-	-	-	-	-	-	-	-	0.895	10.2	-	-	-	-	-	-	-	-	-	-	-	-	-
727	-	11.6	-	-	-	-	-	-	-	0.0000	-	-	0.361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
728	-	-	-	-	-	-	-	-	-	-	-	-	12.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
729	-	3.19	-	-	-	-	-	-	-	-	-	-	-	0.0001	21.4	-	-	-	-	-	-	-	-	-	-	-	-	-
730	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	10.6	-	-	-	-	-	-
731	-	-	-	-	-	-	-	-	-	-	0.0000	-	0.501	0.0182	-	14.4	-	-	-	-	-	-	-	-	-	-	-	-
732	-	-	0.187	-	-	-	-	-	-	5.01	4.81	-	-	-	-	-	33.4	-	-	-	-	30.1	-	-	-	-	-	-
733	-	-	-	-	-	-	-	-	-	3.40	-	-	-	-	-	-	33.2	-	-	-	-	25.7	0.120	-	-	-	-	-
734	-	-	7.84	-	-	-	-	-	-	28.4	-	-	-	-	-	-	0.238	-	-	-	-	40.4	-	-	-	-	-	-
735	-	-	0.704	0.646	-	-	-	-	-	3.35	-	-	-	-	-	-	-	-	-	-	-	9.70	-	-	-	-	-	-
736	-	-	-	-	-	-	-	-	-	1.26	-	-	-	-	-	-	-	-	-	-	8.66	99.0	-	-	-	-	-	-
737	0.266	-	-	-	-	-	-	29.4	-	-	-	-	-	-	-	-	-	16.6	-	-	8.49	-	-	-	-	-	-	-
738	6.00	3.14	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-	-	-	-	-	3.25	-	-	-	5.69	0.0302	-	-
739	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.1	-	-	-	54.7	-	-	-	9.86	-	-	-
740	9.94	-	-	-	-	-	-	4.15	-	2.52	-	-	-	-	-	-	45.2	-	-	-	-	-	-	-	24.2	12.0	-	-
741	-	-	-	-	-	-	8.18	8.52	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
742	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.685	-	-	54.1	62.0	-	-	-	3.71	-	-	-
743	-	-	-	-	-	-	-	81.9	-	-	-	-	-	0.0027	-	-	-	85.7	-	-	-	-	-	-	-	-	-	-
744	-	-	-	-	-	-	-	-	-	10.7	-	-	-	-	-	-	-	9.45	-	-	-	0.0872	76.4	-	-	-	-	-
745	-	0.0003	4.00	-	-	-	-	-	-	25.0	-	-	9.86	-	-	-	-	-	-	-	-	0.0008	21.4	-	-	-	-	-
746	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0418	117	12.0	-	-	-	-
747	-	-	-	-	-	-	-	-	-	-	9.74	-	-	-	-	-	-	3.36	-	-	-	0.0054	70.7	6.61	-	-	-	-
748	-	8.85	-	-	-	6.84	-	0.877	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	8.47	-	-	-	-	-
749	-	11.9	-	0.937	-	-	-	-	-	4.17	6.95	-	-	-	-	0.0980	-	-	-	-	-	0.0005	45.7	-	-	-	-	-
750	-	-	6.70	2.00	-	-	-	2.09	-	13.4	12.6	-	-	2.80	7.32	62.4	-	-	-	-	21.6	53.2	-	-	-	-	-	-
751	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	50.3	-	-	-	-	-	-
752	-	-	-	1.37	-	-	-	-	-	2.18	2.53	-	-	-	-	-	-	-	-	-	-	107	15.0	-	-	-	-	-
753	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.3	148	-	-	-	-	-	-	-	-	-	-	-
754	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63.7	28.7	8.39	-	-	-	-
755	-	-	-	-	-	-	-	-	-	-	-	-	-	0.257	-	-	-	-	-	-	-	39.5	31.4	5.03	-	-	-	-
756	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.26	14.0	8.42	-	-	-	-
757	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.77	-	-	-	-	54.7	-	-	-	-	-	-
758	-	-	-	1.93	-	-	-	-	-	0.171	0.921	-	-	-	-	-	-	-	-	-	-	52.6	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
759	-	-	-	-	-	-	12.7	49.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
760	-	-	-	-	-	-	-	79.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
761	-	5.76	-	-	-	-	7.94	9.06	-	9.42	-	-	-	-	-	-	-	1.85	-	-	0.447	1.05	-	36.8	-	3.48	-	-
762	-	-	-	-	-	-	134	18.3	-	-	-	-	-	-	-	-	-	4.29	-	-	-	-	-	-	-	-	-	-
763	-	-	-	-	-	-	-	3.69	-	9.54	-	-	-	-	-	-	-	7.32	-	-	-	-	-	-	-	-	-	-
764	1.93	-	-	-	-	-	-	-	-	40.9	-	-	10.6	-	-	-	-	25.8	-	-	-	-	-	-	-	-	-	-
765	-	-	-	0.0000	-	-	40.1	-	-	0.754	-	-	-	-	-	-	-	2.90	-	-	-	-	-	4.41	-	2.27	-	-
766	-	-	-	-	-	-	24.6	13.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
767	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.9	0.340	-	43.3	85.0	-	0.271	-	0.0092	-	-
768	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.91	-	-	-	-	-	117	-	-	-	-
769	-	-	-	-	-	-	2.25	19.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.991	-	-	-	-
770	23.2	-	-	4.20	-	-	1.69	9.35	-	-	-	-	-	-	-	-	-	8.81	-	-	-	-	-	-	-	-	-	-
771	1.49	0.115	-	-	-	-	-	-	-	9.89	-	-	-	-	-	-	0.936	0.0625	-	-	-	-	-	92.3	-	0.404	-	-
772	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.2	-	-	-	-
773	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.554	-	-	-	-	-	20.2	-	-	-	-
774	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	0.964	-	-	-	-	-	91.8	-	-	-	-
775	-	-	-	-	0.211	-	-	3.28	-	-	-	-	-	-	-	-	-	-	-	8.57	23.7	-	-	-	14.7	33.8	-	-
776	10.8	-	-	-	-	-	-	-	-	1.53	-	-	-	-	-	-	8.21	-	0.0440	-	103	-	-	-	42.9	5.29	-	-
777	-	-	-	-	-	-	-	1.87	-	-	-	-	-	-	-	-	-	-	-	-	89.8	-	-	-	3.04	22.9	-	-
778	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-	59.2	-	-	-	14.6	5.33	-	-
779	-	-	-	-	0.0001	-	81.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
780	-	-	1.03	-	-	-	-	-	-	5.19	-	-	-	-	-	-	21.5	-	-	-	-	-	-	-	3.78	-	-	-
781	32.9	25.2	-	0.451	-	-	-	-	-	51.3	-	-	-	-	-	-	7.25	-	-	-	10.2	-	-	-	17.1	4.26	-	-
782	-	14.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.3	-	114	0.117	-	-	-	-	-	-
783	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85.5	-	-	-	-	14.0	-	-
784	-	-	-	-	-	-	12.5	-	-	-	-	-	-	-	-	-	-	7.43	-	-	-	-	-	-	-	-	-	-
785	-	-	-	-	-	-	23.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
786	-	-	-	-	-	-	-	35.1	-	-	-	-	-	-	-	-	-	6.29	-	-	-	-	-	22.6	-	-	-	-
787	-	-	-	-	-	-	74.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
788	-	-	-	-	-	-	17.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
789	-	-	-	-	-	-	13.3	-	-	-	-	-	-	-	-	-	-	0.0010	-	-	-	-	-	-	-	-	-	-
790	-	-	-	-	-	-	40.0	-	-	-	-	-	-	-	-	-	-	0.566	-	-	-	-	-	-	-	-	-	-
791	-	-	-	-	-	-	20.2	-	-	-	-	-	-	-	-	-	-	1.51	-	-	-	-	-	-	-	-	-	-
792	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
793	-	-	-	-	-	1.67	69.2	-	9.56	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
794	-	-	-	-	-	-	32.1	-	-	-	-	-	-	-	-	-	-	1.23	-	-	-	-	-	-	-	-	-	-
795	-	-	-	-	-	-	38.1	2.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
796	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.37	-	-	-	-
797	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.860	-	-	-	-	-	16.3	-	-	-	-
798	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.0	-	-	-	-	-	43.3	-	-	-	-
799	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.00	-	-	-	-	-	25.4	-	-	-	-
800	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.59	-	-	-	-	-	17.7	-	-	-	-
801	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-
802	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.8	-	-	-	-
803	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	43.7	-	-	-	-
804	-	-	-	-	-	-	-	56.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
805	-	-	-	-	-	-	28.1	-	-	-	-	-	-	-	-	-	-	5.05	-	-	-	-	-	-	-	-	-	-
806	-	-	-	-	-	-	17.8	-	-	-	-	-	-	-	-	-	-	13.5	-	-	-	-	-	-	-	-	-	-
807	1.92	0.346	-	-	-	-	-	19.1	-	0.560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
808	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.89	3.58	-	-	-	-	-	65.5	-	25.8	-	-
809	11.6	1.07	-	4.94	-	-	-	-	-	15.2	-	-	-	-	-	-	-	1.32	-	-	-	-	-	-	-	-	-	-
810	28.8	5.96	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.80	-	-	-	-	-	-	-	-	-	-
811	2.22	-	-	29.4	-	-	-	-	-	-	-	-	-	-	-	-	-	0.137	-	-	-	-	-	-	-	-	-	-
812	-	-	-	10.0	-	-	-	-	-	-	-	-	-	-	-	-	-	0.386	-	-	-	-	-	0.741	-	-	-	-
813	-	-	-	7.13	-	-	-	-	-	19.9	-	-	-	-	-	-	-	0.229	-	-	-	-	-	21.7	-	19.0	-	-
814	-	39.4	-	4.98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.09	-	-	-	-
815	-	31.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	51.1	37.0	-	-	-	-	-	-
816	-	-	-	4.71	-	-	-	0.0134	-	-	-	-	-	-	-	4.92	-	2.61	-	-	26.7	29.8	-	-	-	-	-	-
817	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.8	0.159	-	-	-	-	0.0510	2.48	-	-	-	-	-	-
818	-	-	3.13	-	-	-	-	-	-	-	3.73	-	-	-	19.2	-	1.65	-	-	-	11.4	39.6	-	-	-	-	-	-
819	1.58	17.3	-	9.49	-	-	-	22.1	-	5.94	-	-	-	-	-	-	0.199	20.4	-	-	73.5	33.1	-	-	-	-	-	-
820	19.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0269	-	-	40.3	-	-	-	-	-	-	-
821	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.9	21.6	-	-	211	80.3	-	-	-	-	-	-
822	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	0.0377	-	126	-	-	-	-
823	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	82.6	-	-	-	-	-	0.189	-	-	-	-
824	-	-	0.761	-	-	-	-	8.21	-	-	-	-	-	-	-	-	43.7	0.0023	-	-	64.2	57.2	-	-	-	-	-	-
825	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.907	32.9	-	-	9.31	9.26	-	-	-	-	-	-
826	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	110	28.9	-	-	-	-	-	-
827	-	8.00	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0056	-	-	-	122	7.16	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
828	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55.0	109	-	-	-	-	-	-
829	-	0.0000	-	-	-	-	-	-	-	19.1	-	-	-	-	-	-	-	-	5.03	-	33.5	24.6	-	-	-	-	-	-
830	-	-	-	-	-	-	-	-	-	49.4	-	-	-	-	-	-	-	-	-	-	53.0	40.0	-	0.118	-	-	-	-
831	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69.4	-	-	-	-	-	-	-
832	-	16.4	0.177	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0072	-	-	46.9	23.1	-	-	-	-	-	-
833	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.62	47.3	-	-	-	-	-	-
834	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34.5	0.835	-	40.8	21.0	-	8.64	-	-	-	-
835	-	-	-	6.68	-	-	-	-	-	0.786	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
836	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.7	-	-	-	-	-	-	33.5	-	-	-	-
837	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.655	-	-	-	115	18.3	-	-	-	-	-	-
838	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40.6	30.5	-	-	-	-	-	-
839	-	1.46	12.0	-	-	-	-	-	-	26.3	4.18	-	-	-	-	-	20.5	-	-	-	37.6	0.0184	-	-	17.2	-	-	-
840	4.51	-	-	-	-	-	-	-	-	31.4	-	-	-	-	-	-	1.21	2.44	0.301	-	-	41.0	-	-	0.0000	-	-	-
841	-	-	7.76	-	-	-	-	-	-	7.09	-	-	-	-	-	-	17.9	-	-	-	-	-	-	-	27.3	-	-	-
842	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.22	-	30.1	-	-
843	-	3.10	-	-	-	-	-	-	-	11.2	-	-	-	-	-	-	16.3	-	-	-	-	-	-	-	-	-	-	-
844	-	-	-	-	-	-	-	-	-	32.9	-	-	-	-	-	-	0.0001	-	-	-	0.752	30.4	-	-	8.76	-	-	-
845	-	-	-	-	-	-	-	-	-	6.50	-	-	-	-	-	-	-	-	-	-	-	13.9	-	-	-	-	-	-
846	-	-	-	-	-	-	-	-	-	33.8	-	-	-	-	-	-	-	-	0.232	-	-	35.0	-	-	-	-	-	-
847	-	-	-	-	-	-	-	5.87	-	-	-	-	-	-	-	-	-	10.5	-	-	-	-	-	76.2	-	-	-	-
848	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.5	-	-	-	-
849	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.15	-	-	-	-	-	25.4	-	-	-	-
850	-	0.0068	-	-	-	-	-	-	-	17.6	-	-	-	-	-	-	-	3.21	-	-	-	0.0043	7.76	31.2	-	-	-	-
851	-	0.0004	-	-	-	-	-	-	-	4.56	-	-	-	-	-	-	-	-	-	-	-	0.0014	1.67	26.0	-	-	-	-
852	-	19.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.39	-	-	-	0.0020	-	39.3	-	-	-	-
853	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0048	-	57.6	-	-	-	-
854	-	26.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0030	-	38.7	-	-	-	-
855	-	-	-	-	-	-	-	-	-	-	-	3.42	40.9	0.0009	-	-	-	0.0084	-	-	-	-	-	-	-	-	-	-
856	-	-	-	-	-	-	-	-	-	20.7	-	-	-	-	-	-	-	-	-	-	-	0.0045	-	43.9	-	-	-	-
857	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.19	-	-	-	0.0040	-	27.5	-	-	-	-
858	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0008	-	-	-	0.0833	-	26.1	-	-	-	-
859	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.297	-	-	0.0051	-	58.2	-	-	-	-
860	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.38	-	-	0.830	0.0700	-	85.1	-	-	-	-
861	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.6	0.0703	-	-	0.0000	-	22.3	-	-	-	-
862	-	10.9	-	-	-	-	-	-	-	0.0434	-	-	-	-	2.26	-	-	24.8	-	-	61.4	18.9	-	-	-	-	-	-
863	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.181	8.31	-	-	86.8	13.9	-	-	-	-	-	-
864	-	-	-	-	-	-	-	62.7	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-
865	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.3	25.9	-	-	7.04	-	-	-	-	-	-	-
866	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.9	-	-	-	-	-	-	-
867	-	-	-	-	-	-	-	-	-	64.0	-	-	-	7.14	-	-	-	18.5	-	-	6.68	57.9	-	-	-	-	-	-
868	-	-	-	-	-	-	-	-	-	21.4	-	-	-	-	-	-	-	2.23	-	-	61.5	2.40	-	-	-	-	-	-
869	-	2.18	2.04	2.25	-	-	-	-	-	29.8	-	-	-	-	-	-	0.0056	15.4	-	-	27.5	55.9	-	-	-	-	-	-
870	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.5	14.8	-	-	107	3.80	-	-	-	-	-	-
871	-	2.42	-	-	-	-	-	-	-	-	15.5	-	-	-	-	-	-	0.0173	-	-	-	-	-	-	-	-	-	-
872	-	0.0004	-	2.68	-	-	-	-	-	7.87	26.1	-	1.34	-	-	-	-	-	-	-	-	0.0001	26.3	-	-	-	-	-
873	-	-	-	-	-	-	-	-	-	9.27	-	-	3.95	-	-	-	-	-	-	-	-	0.0014	15.8	-	-	-	-	-
874	-	-	2.32	-	-	-	-	-	-	13.2	-	-	-	-	-	-	-	0.0017	-	-	-	0.0063	30.2	-	-	-	-	-
875	-	-	0.508	-	-	-	-	-	-	3.76	-	-	-	-	-	-	-	-	-	-	-	0.864	77.8	1.46	-	-	-	-
876	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0282	35.5	-	-	-	-	-
877	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0054	51.8	11.6	-	-	-	-
878	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0115	55.8	1.43	-	-	-	-
879	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0030	13.7	20.8	-	-	-	-
880	-	0.116	-	-	-	-	-	-	-	20.1	-	-	-	-	-	-	-	5.74	-	-	-	0.0005	-	17.7	-	-	-	-
881	-	0.0010	-	-	-	-	-	-	-	20.6	-	-	-	-	-	-	-	-	-	-	-	-	-	8.15	-	-	-	-
882	-	-	-	-	-	-	-	-	-	25.8	-	11.5	12.1	0.249	-	-	-	-	-	-	-	-	-	-	-	-	-	-
883	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0266	5.31	-	-	44.7	-	-	-	-	-	-	-
884	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.08	34.4	-	28.9	-	-	7.59	3.46	-	-	-	-	-	-
885	-	-	-	-	-	-	-	12.1	-	-	-	-	-	-	-	1.79	-	8.44	-	-	1.55	9.39	-	-	-	-	-	-
886	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.148	-	-	-	-	-	-	-	-	-	-	-	-
887	-	19.4	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	-	-	-	-	-	-	-	-
888	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.9	65.7	-	-	-	-	0.0447	-	-	-	-	-	-	-
889	-	-	-	0.0107	-	-	6.80	34.4	-	-	-	-	-	-	-	-	-	33.1	-	-	4.53	23.9	-	-	-	-	-	-
890	-	-	-	26.8	-	-	45.1	41.7	-	4.72	-	-	-	-	5.17	-	-	0.0172	-	-	9.81	-	-	-	-	-	-	-
891	-	3.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-
892	-	15.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34.1	-	-	-
893	-	3.20	-	-	-	-	-	67.2	-	-	-	-	-	-	-	-	-	-	-	-	0.0031	-	0.120	-	-	-	-	-
894	-	-	-	-	-	-	-	57.2	-	-	-	-	-	-	-	-	-	7.76	-	-	-	-	-	-	-	-	-	-
895	-	55.3	-	21.5	-	-	-	-	20.4	16.3	-	-	-	-	-	-	-	24.2	-	-	72.0	-	8.70	-	0.478	-	-	-
896	-	0.0351	-	1.99	-	-	-	76.3	-	-	-	-	-	-	-	-	-	-	-	-	3.64	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
897	-	-	-	-	-	-	-	0.0212	-	-	-	-	-	-	-	-	-	2.45	-	-	49.2	81.6	-	-	-	-	-	-
898	-	60.0	-	2.75	-	-	-	5.94	-	-	-	-	-	-	-	-	1.94	0.163	-	-	-	-	-	-	-	-	-	-
899	-	0.178	-	6.94	-	-	-	-	-	-	-	-	-	-	-	-	-	3.55	-	-	41.3	-	-	-	-	-	-	-
900	-	-	-	-	-	-	33.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
901	-	16.4	-	4.76	-	-	-	-	-	-	-	-	-	-	-	-	-	16.2	-	-	-	-	-	-	55.7	-	-	-
902	-	-	-	16.2	-	-	-	4.51	-	-	-	-	-	-	-	-	-	7.45	-	-	43.6	-	-	-	-	-	-	-
903	-	7.42	-	2.49	-	-	-	23.3	-	1.90	-	-	-	-	-	7.42	48.4	38.5	-	-	10.2	0.526	-	-	-	-	-	-
904	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	117	4.20	-	-	-	-	-	-
905	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.30	-	-	-	8.89	8.51	-	-	-	-	-	-
906	-	-	-	-	-	-	-	-	-	-	0.0590	-	-	-	-	-	6.61	-	-	-	2.20	38.3	-	-	-	-	-	-
907	-	30.6	-	12.6	-	-	-	-	-	5.95	5.54	-	-	-	12.9	-	-	-	-	-	46.4	43.2	-	-	-	-	-	-
908	-	99.2	-	-	-	-	-	-	-	-	-	-	-	-	58.0	-	-	-	-	-	-	-	-	3.49	-	-	-	-
909	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75.9	-	2.79	-	0.342	-	-	-
910	0.0554	22.6	-	6.69	-	-	-	43.6	-	-	-	-	-	-	-	-	-	10.1	-	-	12.5	-	-	-	-	-	-	-
911	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	49.3	-	-	-	-	-	-
912	-	-	-	-	-	-	-	-	-	0.656	-	-	-	-	-	-	-	21.5	-	-	-	36.5	37.1	-	-	-	-	-
913	-	0.0110	-	1.25	-	-	-	-	-	13.8	-	-	-	-	-	-	-	0.358	-	-	9.99	5.47	110	-	-	-	-	-
914	4.03	-	1.44	8.72	-	-	-	-	-	26.5	-	-	-	2.86	-	-	-	-	-	-	-	0.930	2.10	62.4	-	13.4	-	-
915	-	-	-	44.1	-	-	-	-	-	2.55	-	-	-	2.75	-	-	-	-	-	-	-	32.6	-	5.69	-	-	-	-
916	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.7	-	-	-	-	-	-
917	-	-	-	31.0	-	-	-	-	-	-	0.0172	-	-	-	-	-	-	9.16	-	-	-	106	-	0.0033	-	-	-	-
918	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.428	-	-	-	53.7	-	-	-
919	-	5.40	1.41	0.393	-	-	-	-	-	0.768	-	-	-	-	1.83	-	-	-	-	-	28.4	90.5	-	-	-	-	-	-
920	-	-	0.970	-	-	-	-	-	-	2.60	4.09	-	-	-	-	-	2.69	-	-	-	1.19	89.1	-	-	-	-	-	-
921	0.779	4.09	-	-	-	-	-	-	-	1.12	-	-	-	-	-	-	2.25	-	-	-	-	61.2	-	-	-	-	-	-
922	2.47	17.4	-	1.27	-	-	-	-	-	10.6	-	-	-	-	-	-	12.0	5.05	-	-	-	69.8	0.297	-	-	-	-	-
923	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	123	12.1	-	-	-	-	-
924	-	-	-	-	-	-	-	-	-	4.85	-	-	-	-	-	-	-	-	-	-	-	0.132	34.3	6.16	-	-	-	-
925	-	-	0.0001	-	-	-	-	-	-	23.6	-	-	-	-	-	-	16.3	-	-	-	-	79.9	4.07	0.621	-	-	-	-
926	2.08	9.47	2.43	12.0	-	-	-	-	-	4.94	-	-	-	-	-	-	-	-	-	-	-	56.0	2.21	-	-	-	-	-
927	-	0.0002	-	-	-	-	-	-	-	1.29	-	-	-	-	-	-	0.446	-	-	-	-	59.8	-	-	-	-	-	-
928	-	15.3	-	-	-	10.6	-	5.45	0.0000	-	-	-	6.75	-	-	-	-	1.82	-	-	0.0001	15.7	0.788	-	-	-	-	-
929	-	-	-	-	-	-	-	0.0000	0.236	-	-	-	-	-	-	-	-	-	-	-	0.0001	6.81	50.2	-	-	-	-	-
930	-	-	5.45	-	-	-	-	-	0.0041	3.67	0.0002	-	2.82	-	-	-	-	-	-	-	-	0.475	29.2	-	-	-	-	-
931	-	-	0.0003	-	-	27.8	-	2.70	0.0944	-	2.43	-	-	-	-	-	-	-	-	-	-	0.0935	2.15	4.71	-	-	-	-
932	-	-	-	-	-	-	-	-	-	8.13	-	-	-	-	-	-	-	-	-	-	-	5.29	0.979	-	-	-	-	-
933	3.18	4.98	-	-	-	-	-	-	-	8.01	-	-	-	-	-	-	8.11	-	-	-	-	43.0	-	-	-	-	-	-
934	-	21.4	-	-	-	-	-	-	-	2.58	-	-	-	-	2.93	-	-	-	-	-	-	-	-	-	-	-	-	-
935	-	-	-	-	-	-	-	-	-	14.2	-	-	-	-	-	-	-	0.0001	-	-	-	16.4	-	2.95	-	-	-	-
936	-	36.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
937	-	6.70	-	1.88	-	-	-	-	20.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
938	-	-	-	-	-	-	-	-	-	0.810	-	-	-	0.136	-	30.6	-	-	-	-	-	1.12	1.32	-	-	-	-	-
939	-	-	-	-	-	-	-	-	-	-	0.0006	-	11.9	0.0003	17.7	-	-	-	-	-	-	-	-	-	-	-	-	-
940	-	-	-	-	-	-	-	-	-	1.19	-	-	-	-	-	-	-	-	-	-	-	14.1	-	-	-	-	-	-
941	-	-	-	-	-	-	-	56.2	-	-	-	-	-	0.0002	-	-	-	4.93	-	-	-	-	0.0023	-	-	-	-	-
942	-	13.0	-	-	-	16.8	-	-	4.10	-	-	-	-	-	-	-	-	2.73	-	-	-	-	-	-	-	-	-	-
943	-	0.264	-	1.05	-	1.68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0006	9.36	-	-	-	-	-
944	-	-	-	-	-	53.1	-	4.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
945	-	-	-	-	-	-	-	4.81	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
946	-	-	-	-	-	-	-	6.57	0.0022	2.01	0.0001	-	2.54	-	-	-	-	-	-	-	-	0.0006	8.26	-	-	-	-	-
947	-	-	-	-	-	-	-	30.7	-	-	-	-	-	-	-	-	-	6.05	-	-	-	-	0.0021	-	-	-	-	-
948	-	-	-	-	-	-	-	0.0326	-	-	-	-	-	-	-	-	-	-	-	-	-	0.865	34.0	3.82	-	-	-	-
949	-	0.0000	-	3.61	-	-	-	-	-	5.93	4.48	-	-	-	-	-	-	2.57	-	-	-	0.0122	68.1	5.66	-	-	-	-
950	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-	-	-	-	-	-	-	-
951	-	43.0	1.43	-	-	-	-	-	-	59.4	-	-	-	-	-	-	-	29.7	-	-	58.3	63.9	-	-	-	-	-	-
952	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0031	4.62	10.8	-	-	-	-	-	-	-	-	-	-	-	-
953	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	20.7	1.71	-	-	-	-	-	-	-	-	-	-	-	-
954	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	35.9	-	-	-	-	-	-	-	-	-	-	-	-
955	-	-	0.548	-	-	-	-	2.99	0.0004	13.1	-	-	-	-	-	-	-	-	-	-	-	0.0027	17.9	7.35	-	-	-	-
956	-	-	-	-	-	-	-	2.69	-	-	-	-	6.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
957	-	-	-	-	-	-	-	-	-	0.348	14.0	-	4.57	-	-	-	-	2.44	-	-	-	0.0017	69.2	0.873	-	-	-	-
958	-	-	-	-	-	-	-	-	-	-	-	-	-	0.443	-	26.2	-	-	-	-	-	-	-	-	-	-	-	-
959	-	-	-	-	-	-	-	0.161	-	-	-	-	-	0.0523	-	14.2	-	-	-	-	-	-	-	-	-	-	-	-
960	-	-	0.0160	-	-	-	-	-	-	8.95	0.0001	-	3.09	0.0005	-	9.98	-	-	-	-	-	-	-	0.791	-	-	-	-
961	-	0.164	-	-	-	-	-	-	-	-	-	-	-	0.0801	0.606	6.20	-	-	-	-	-	-	-	-	-	-	-	-
962	-	-	6.53	-	-	-	-	-	-	2.16	0.171	-	20.6	-	-	-	-	-	-	-	-	0.0440	6.86	-	-	-	-	-
963	-	0.0006	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-	0.0145	-	-	-	0.0545	46.6	32.5	-	-	-	-
964	-	-	-	-	-	-	-	19.9	0.0000	-	-	-	-	-	-	-	-	7.16	-	-	-	0.0000	0.0056	-	-	-	-	-
965	-	-	-	-	-	0.168	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.157	31.8	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
966	5.56	7.27	-	0.289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
967	-	20.7	-	0.939	-	11.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	2.99	-	-	-	-	-
968	-	-	-	-	-	35.8	-	57.2	0.0006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
969	-	17.6	-	-	-	46.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
970	-	2.62	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
971	-	0.266	-	-	-	-	-	-	-	18.2	-	-	-	-	-	-	-	-	-	-	-	0.0101	11.1	-	-	-	-	-
972	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.21	-	-	0.721	15.3	-	-	-	-	-	-
973	-	-	-	3.43	-	-	-	-	-	-	8.78	-	-	-	-	-	-	-	-	-	-	69.7	18.8	-	-	-	-	-
974	-	1.27	-	-	-	-	-	-	-	2.66	-	-	-	-	-	-	-	-	-	-	-	115	5.02	-	-	-	-	-
975	-	23.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
976	4.73	23.0	-	0.140	-	-	-	-	-	3.80	-	-	-	-	-	-	0.813	0.0306	-	-	-	7.16	-	-	-	-	-	-
977	-	0.0446	0.170	0.390	-	-	-	-	-	16.0	-	-	-	-	-	-	9.56	-	-	-	-	72.2	41.5	-	-	-	-	-
978	-	0.0000	-	-	-	-	-	-	-	3.22	-	-	-	-	-	-	7.51	-	-	-	-	76.8	9.08	-	-	-	-	-
979	-	-	0.781	30.5	-	-	-	-	-	0.0005	5.45	-	-	-	5.64	-	-	-	-	-	-	10.4	1.27	-	-	-	-	-
980	-	0.0000	-	-	-	-	-	-	-	1.16	-	-	-	-	-	-	2.18	-	-	-	0.0002	97.0	-	-	-	-	-	-
981	-	0.0002	-	-	-	-	-	-	-	2.69	-	-	-	-	-	-	0.0006	-	-	-	-	33.4	-	-	-	-	-	-
982	-	-	-	2.34	-	-	-	-	-	3.07	-	-	-	-	-	-	10.9	-	-	-	-	82.5	-	-	-	-	-	-
983	15.4	0.0001	-	0.230	-	-	-	-	-	12.8	0.726	-	-	-	-	-	10.4	-	-	-	-	28.6	2.68	0.589	-	-	-	-
984	-	32.1	-	32.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
985	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.7	-	-	-	-	-	-
986	-	-	-	-	-	-	-	-	-	3.70	-	-	-	-	-	-	-	-	-	-	-	51.2	-	-	-	-	-	-
987	-	2.19	-	0.236	-	-	-	-	-	8.01	-	-	-	-	-	-	0.0002	5.17	-	-	-	0.0879	117	-	-	-	-	-
988	0.318	-	-	-	-	-	-	-	-	9.71	-	-	-	-	-	-	6.12	-	-	-	-	35.2	6.67	-	-	-	-	-
989	-	-	-	-	-	-	-	-	-	85.5	-	-	-	-	-	-	22.5	-	-	-	-	26.3	6.62	-	-	-	-	-
990	-	-	-	-	-	-	-	-	-	4.95	-	7.19	-	14.1	-	-	-	0.788	-	-	-	0.636	-	72.7	-	-	-	-
991	-	-	-	-	-	-	-	-	-	2.78	-	-	-	-	-	-	-	-	11.2	-	14.7	9.61	-	-	-	-	-	-
992	-	1.22	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-	-	0.284	-	0.0010	0.0023	-	29.0	-	-	-	-
993	-	-	-	-	-	-	-	-	-	-	-	3.99	11.1	10.9	-	-	-	0.499	-	-	-	1.25	-	-	-	-	-	-
994	-	-	-	-	-	-	-	4.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
995	-	-	-	-	-	-	57.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
996	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.41	-	-	-
997	-	-	0.0002	8.80	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58.9	-	-	-	-	2.90	-	-
998	-	1.02	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.7	12.6	-	-
999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.3	-	-	-	-
1000	-	-	-	-	-	-	-	24.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1001	-	-	-	-	-	-	-	57.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1002	-	-	-	-	-	-	45.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1003	-	-	-	-	-	-	23.0	-	-	-	-	-	-	-	-	-	-	0.795	-	-	-	-	-	-	-	-	-	-
1004	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.625	-	-	-	-	-	-	-	-	-	-
1005	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.06	-	-	-	-
1006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.37	0.592	-	-	-	-	5.56	-	-	-	-
1007	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0239	16.7	-	-	-	-	-	-
1008	-	11.6	-	-	-	-	-	-	-	-	-	-	-	-	73.5	-	-	-	-	-	-	-	-	-	-	-	-	-
1009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91.7	-	-	-	-	-	-	-
1010	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.6	-	-	-	-	-	-	-
1011	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.6	-	-	-	-	-	-	-
1012	-	-	-	-	-	-	-	-	-	7.49	-	-	-	-	-	-	-	7.82	-	-	-	1.07	-	-	-	-	-	-
1013	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.73	-	-	-	-	-
1014	-	2.39	-	-	-	-	-	-	-	-	-	-	2.27	0.0064	-	12.0	-	0.0312	-	-	-	0.694	-	-	-	-	-	-
1015	-	4.38	-	-	-	-	-	-	-	9.94	-	-	-	-	-	-	7.24	-	-	-	-	78.6	16.0	-	-	-	-	-
1016	14.6	23.5	-	0.248	-	-	-	-	-	18.1	-	-	-	-	-	-	1.91	-	-	-	-	13.3	0.512	2.40	-	-	-	-
1017	-	11.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1018	-	-	-	-	-	-	-	-	-	-	-	-	5.22	-	4.73	-	-	-	-	-	-	-	-	-	-	-	-	-
1019	-	-	-	-	-	-	-	2.00	42.4	-	-	-	-	-	10.7	-	-	0.190	-	-	-	-	-	-	-	-	-	-
1020	-	2.78	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	2.05	-	-	-	-	-
1021	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1022	1.25	3.38	-	-	-	-	-	-	-	4.74	-	-	-	-	-	-	-	3.06	-	-	-	3.77	-	-	-	-	-	-
1023	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.01	-	-	-	-	-	90.0	-	-	-	-
1024	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.518	-	-	-	-	-	28.0	-	-	-	-
1025	-	-	-	-	-	-	-	2.42	-	-	-	-	-	-	-	-	-	-	0.136	-	-	-	-	-	-	-	-	-
1026	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.06	-	-	-	-	-	2.28	-	-	-	-
1027	-	6.56	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	0.0288	-	-	-	-	-	61.3	-	-	-	-
1028	-	1.04	-	2.43	-	-	-	-	-	-	-	-	-	-	-	-	-	13.2	-	-	-	-	-	0.106	-	-	-	-
1029	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.79	-	0.115	-	-	0.248	-	-	-	-
1030	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.9	-	0.213	-	-	0.386	-	-	-	-
1031	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.7	-	-	-	-	-	45.8	-	-	-	-
1032	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.6	-	-	-	-	-	16.6	-	-	-	-
1033	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.54	-	-	-	-	-	25.3	-	-	-	-
1034	-	-	-	-	-	-	-	-	0.0002	0.0058	-	-	-	-	-	-	-	-	-	-	5.41	25.1	-	-	-	12.5	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
1035	-	20.8	-	-	-	-	-	24.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-
1036	-	19.7	-	-	-	-	21.9	8.49	0.0664	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1037	-	-	1.80	-	-	-	-	-	-	4.60	-	-	-	-	-	-	1.71	-	-	-	2.02	1.89	-	-	24.7	-	-	-
1038	-	-	-	-	-	-	-	24.3	-	-	-	-	-	-	-	-	-	0.721	-	-	-	-	-	-	-	-	-	-
1039	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.6	-	-	-	70.2	0.801	-	-	-	-	-	-
1040	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1041	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.28	-	-	-	-	-	-	-
1042	-	-	-	-	-	-	-	-	-	17.1	-	-	-	-	-	-	-	-	0.0054	-	27.3	-	-	-	-	-	-	-
1043	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.1	-	-	-	-	-	-	-
1044	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.4	13.4	-	-	-	-	-	-
1045	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91.4	-	-	-	-	-	-	-
1046	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	-	-	-	-
1047	-	-	-	-	0.0215	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1048	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	50.3	-	-	-	-	-	-	-
1049	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.69	-	-	-	-	-	-	-	-	-
1050	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41.9	10.2	-	-	-	-	-	-
1051	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.7	-	-	-	-	-	-	-	-	-
1052	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61.7	0.323	12.9	-	20.5	-	-	-	-	-	-
1053	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.11	-	-	-	-	-	-	-	-
1054	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1055	-	0.0002	-	-	-	-	-	-	158	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1056	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.27	-	-	0.0031	-	-	22.2	-	-	-	-
9999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.43	-	-	-	-	-	88.4	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
0																												
1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
2	-	85%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	16%	-	-	-	100%	-	100%	-	100%	-	-
3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
6	100%	-	-	-	-	-	-	36%	-	74%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
7	82%	74%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	38%	-	100%	-	87%	-	-	-	95%	70%	-	-
8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
9	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
10	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19%	-	-	-	-	100%	-	-	-	-
12	-	-	-	-	3%	-	72%	-	-	-	-	-	-	-	-	-	-	-	100%	-	38%	-	-	-	-	-	-	-
13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26%	-	22%	-	-	-	-	-	-	-
14	17%	-	-	-	-	-	36%	-	-	13%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
15	-	-	-	-	77%	-	58%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
16	-	-	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	100%	-	100%	-	-	100%	-	-	-	-	-	-
17	100%	98%	-	-	-	-	-	-	-	68%	-	-	-	-	-	-	100%	-	100%	-	-	100%	-	-	-	-	-	-
18	-	-	-	-	17%	-	36%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
19	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-	-	-	-	-
20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
21	-	61%	-	-	-	-	-	-	12%	-	-	-	-	-	-	-	5%	-	-	-	-	-	-	-	-	-	-	-
22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-	-	-	-
23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	62%	-	-	-	-	-	-	-	-	-
24	-	-	-	-	-	-	-	-	6%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
25	-	-	-	-	15%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
26	-	-	-	-	4%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
28	-	-	-	-	7%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19%	-	-	-	-	-	-	-	-	-
30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8%	-	-	-	-	-	-	-	-	-
31	-	-	-	-	7%	-	-	-	-	-	-	-	-	-	-	-	-	-	16%	-	-	-	-	-	-	-	-	-
32	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12%	-	-	-	-	-	-	-	-	-
33	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	-	-	-	-	-	-	-	-
34	-	-	-	-	45%	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-
35	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
36	-	-	-	-	-	-	-	-	9%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
37	-	-	-	-	-	-	-	-	31%	-	-	-	-	-	-	-	98%	100%	-	-	-	-	-	-	-	-	-	-
38	-	-	-	-	-	-	-	-	16%	-	-	-	-	-	-	-	55%	-	-	-	-	-	-	-	-	-	-	-
39	-	-	-	-	-	-	-	-	76%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
40	-	4%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
41	-	-	-	-	-	-	-	-	61%	-	-	-	-	-	-	-	-	51%	-	-	-	-	-	-	-	-	-	-
42	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	82%	-	-	-	-	-	-	-
43	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
44	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-
45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-
46	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5%	-	-	-	-	-	-	-	-	-
47	-	-	-	-	-	-	-	-	35%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
48	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	77%	91%	-	-	-	-	-	-
49	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	21%	-	-	87%	-	-	-	-	-	-	-
50	-	100%	-	-	-	-	-	61%	61%	91%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
51	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	90%	-	-	28%	-	-	-	-	-	-	-
52	-	-	-	-	-	-	-	-	73%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
53	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-
54	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
55	3%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19%	-	-	-	-	-	-	-	-	-
56	100%	-	-	-	-	63%	-	-	-	-	-	-	-	-	-	-	-	-	9%	-	-	-	-	-	-	-	-	-
57	-	-	-	-	9%	-	-	-	-	29%	-	-	-	25%	-	-	99%	56%	52%	-	1%	-	-	-	-	-	-	-
58	-	-	-	-	-	-	-	-	100%	96%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	75%	-	-	-	-	-	-	-	-	-
60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	73%	-	100%	100%	-	-	-	-	-	-
61	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
62	-	-	-	-	-	-	-	-	41%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
63	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
64	-	-	-	-	-	-	-	-	54%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
65	-	-	-	-	-	-	-	-	16%	-	-	-	-	-	-	-	95%	-	89%	-	-	-	-	-	-	-	-	-
66	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	69%	99%	-	-	-	-	-	-
67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69%	73%	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69%	-	-	-	-	-	-	-
69	-	-	-	-	-	-	-	-	63%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
70	-	-	-	-	-	-	-	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	-	-	-	-	-	-	-
71	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
72	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
73	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
74	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-
75	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
76	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24%	-	-	-	-	-	-	-	-	-
77	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	100%	-	-	-	-	-	-	-
78	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21%	-	100%	18%	-	-	-	-	-	-
79	100%	-	-	-	-	-	-	-	-	51%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
80	-	-	-	-	-	-	-	-	-	2%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
81	-	-	100%	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	-
82	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	4%	-	-	-	-	-	-	-	-	-	-
83	-	-	-	-	-	-	-	-	48%	-	-	-	-	-	-	-	-	7%	-	-	-	-	-	-	-	-	-	-
84	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	48%	-	-	100%	-	-	100%	-	-	-	-	-	-	-
85	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
86	-	-	-	-	-	-	-	-	30%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
87	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	-	-
88	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
89	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19%	-	-	-	-	-	-	-	-	-
90	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15%	-	-	-	-	-	-	-	-	-
91	-	-	-	-	20%	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-
92	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22%	-	-	14%	-	-	-	-	-	-
93	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	30%	-	-	-	-	-	-
94	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17%	-	-	-	-	-	-	-	-	-
95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
96	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
97	-	-	-	-	4%	-	-	-	-	-	-	-	-	-	-	-	-	-	44%	-	-	-	-	-	-	-	-	-
98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	-	-	-	-	-	-	-
99	-	-	-	-	-	-	-	-	2%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
100	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2%	-	34%	-	-	-	-	-	-	-	-	-
101	-	-	-	-	2%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
102	-	-	-	-	50%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
103	-	-	-	-	42%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
104	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
105	-	-	-	-	81%	-	-	-	-	-	-	-	-	-	-	-	-	-	55%	-	-	-	-	-	-	-	-	-
106	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	100%	-	-	-	-	-	-	-	-	-	-
107	-	100%	-	-	-	-	-	-	87%	100%	-	-	-	-	-	-	54%	1%	-	-	100%	-	-	-	-	-	-	-
108	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52%	-	-	100%	-	-	-	-	-	-	-
109	-	-	-	-	-	-	-	-	85%	85%	-	-	-	-	-	-	100%	-	-	-	91%	-	-	-	-	-	-	-
110	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	99%	-	-	100%	-	-	-	-	-	-	-
111	-	85%	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	-	80%	-	-	100%	-	-	-	-	-	-	-
112	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-
113	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	77%	-	-	87%	-	-	-	-	-	-	-
114	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
115	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63%	-	-	62%	-	-	-	-	-	-	-
116	-	-	-	-	-	-	-	-	91%	97%	-	-	-	-	-	-	-	30%	-	-	-	-	-	-	-	-	-	-
117	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
118	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
119	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
120	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	98%	-	-	-	-	-	-	-
121	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
122	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-
123	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	85%	-	-	-	-	-	-	-
124	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33%	-	-	100%	-	-	-	-	-	-	-
125	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	39%	-	-	100%	-	-	-	-	-	-	-
126	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1%	-	-	98%	-	-	-	-	-	-	-
127	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3%	-	-	95%	-	-	-	-	-	-	-
128	-	100%	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-
129	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
130	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
131	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	100%	9%	-	-	-	-	-	-	-	-	-	-
132	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	47%	-	-	100%	-	-	-	-	-	-	-
133	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	69%	-	-	95%	-	-	-	-	-	-	-
134	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52%	-	-	93%	-	-	-	-	-	-	-
135	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
136	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
137	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	-
138	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69%	-	-	86%	-	-	-	-	-	-	-
139	-	-	-	-	-	-	-	-	11%	78%	-	-	-	-	100%	-	%	31%	-	-	75%	-	-	-	-	-	-	-
140	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
141	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
142	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
143	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	96%	-	-	-	-	-	-	-
144	-	92%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	100%	-	-	-	100%	-	-	-	-	-	-	-
145	-	-	-	-	-	-	-	-	-	80%	-	-	-	86%	-	-	-	14%	-	-	88%	-	-	-	-	-	-	-
146	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	46%	-	-	84%	-	-	-	-	-	-	-
147	-	-	-	-	-	-	-	-	-	89%	-	-	-	100%	-	-	100%	100%	-	-	53%	-	-	-	-	-	-	-
148	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	60%	-	-	71%	-	-	-	-	-	-	-
149	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	97%	-	-	60%	-	-	97%	-	-	-	-	-	-	-
150	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
151	-	100%	-	-	-	-	-	-	100%	98%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
152	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
153	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
154	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
155	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
156	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-
157	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	97%	-	-	-	-	-	100%	-	-	-	-	-	-	-
158	-	-	100%	-	-	-	-	-	-	-	89%	-	16%	53%	-	-	100%	-	-	-	78%	92%	100%	-	-	-	-	-
159	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	86%	92%	-	-	-	-	-	-
160	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	80%	81%	100%	100%	-	-	-	-
161	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	%	-	-	-	-	-	-
162	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	14%	-	84%	79%	-	-	-	-	-	-
163	-	-	-	-	-	-	-	-	-	92%	-	-	-	100%	-	-	-	98%	-	-	-	97%	-	-	-	-	-	-
164	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-
165	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	9%	99%	-	-	-	-	-	-
166	-	-	-	-	-	-	-	-	40%	100%	-	-	-	-	-	-	79%	-	-	-	87%	100%	-	-	-	-	-	-
167	-	-	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
168	-	-	-	-	-	-	-	-	60%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
169	-	-	86%	100%	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	35%	83%	-	-	-	-	-	-
170	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
171	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	96%	-	-	-	-	-	-
172	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95%	89%	-	-	-	-	-	-
173	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	100%	97%	-	-	-	-	-	-
174	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
175	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	91%	100%	-	-	-	-	-	-
176	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-
177	-	-	-	94%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	-	-
178	-	81%	-	91%	-	-	-	-	100%	88%	-	-	-	-	-	-	100%	-	-	-	-	89%	-	100%	-	-	-	-
179	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	71%	94%	-	-	-	-	-	-
180	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	100%	-	-	-	100%	99%	-	-	-	-	-	-
181	-	-	-	100%	-	-	-	100%	100%	98%	-	-	-	-	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-
182	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
183	-	100%	100%	100%	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
184	-	-	62%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
185	-	100%	83%	-	-	-	-	-	79%	100%	-	-	-	-	-	-	-	-	-	-	-	89%	81%	-	-	-	-	-
186	-	-	-	-	-	-	-	98%	7%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
187	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
188	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
189	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	99%	-	-	-	-
190	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	98%	-	-	-	-
191	-	100%	-	67%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
192	-	100%	-	100%	-	-	-	75%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
193	-	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	100%	-	-	-	-
194	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-
195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	97%	-	-	-	-	-
196	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47%	-	-	-	55%	95%	100%	-	-	-	-
197	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	100%	-	-	-	100%	-	100%	-	-	-	-
198	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	73%	100%	-	96%	-	-	-	-
199	-	75%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
200	-	-	-	-	-	-	-	-	-	22%	-	-	-	-	-	-	-	-	-	-	54%	100%	-	-	-	-	-	-
201	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
202	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	80%	-	-	-	-	-	-	-	-	-	-
203	-	-	-	-	-	-	-	-	74%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
204	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
205	-	-	-	-	-	-	-	-	4%	-	-	-	-	-	69%	-	-	100%	-	-	-	-	-	-	-	-	-	-
206	-	-	-	-	-	-	-	-	-	-	-	-	-	-	89%	-	-	100%	-	-	-	-	-	-	-	-	-	-
207	-	-	-	-	-	-	85%	-	-	100%	-	-	-	-	100%	-	-	9%	-	-	-	-	-	-	-	-	-	-
208	-	-	-	-	-	-	-	-	-	-	-	-	-	-	67%	-	-	100%	-	-	-	-	-	-	-	-	-	-
209	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75%	-	-	100%	-	-	-	-	-	-	-	-	-	-
210	-	%	-	-	-	-	-	-	-	100%	100%	-	-	-	89%	-	-	97%	-	-	-	-	-	-	-	-	-	-
211	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
212	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-	-	-	-	-	-	-
213	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58%	-	-	-	-	-	-	-	-	-	-	-	-	-
214	-	97%	-	-	-	-	-	-	-	100%	-	-	-	-	62%	-	-	55%	-	-	65%	-	-	-	-	-	-	-
215	-	-	-	-	-	-	-	-	-	-	-	-	-	-	80%	-	-	53%	-	-	-	-	-	-	-	-	-	-
216	-	100%	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
217	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
218	-	-	-	-	-	-	68%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-
219	-	-	-	-	-	-	30%	-	-	-	-	-	-	-	97%	-	-	93%	-	-	100%	100%	-	-	-	-	-	-
220	-	-	-	-	-	-	-	-	-	91%	18%	-	-	57%	98%	-	-	29%	-	-	-	-	-	-	-	-	-	-
221	-	43%	-	-	-	-	-	-	61%	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
222	-	96%	-	-	-	-	-	-	-	100%	91%	-	-	95%	93%	-	-	6%	-	-	-	-	-	-	-	-	-	-
223	-	100%	-	-	-	-	-	-	-	7%	4%	-	-	27%	-	-	-	20%	-	-	-	-	-	-	-	-	-	-
224	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
225	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	94%	-	-	-	-	-	-
226	-	-	-	-	-	-	-	-	72%	100%	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
227	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	99%	-	-	-	-	-
228	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	100%	-	-	-	-
229	-	-	-	-	-	-	-	-	-	57%	-	-	-	-	-	-	-	-	-	-	-	100%	-	81%	-	-	-	-
230	-	-	-	-	-	-	-	-	-	88%	-	-	-	-	-	-	-	-	-	-	-	100%	-	92%	-	-	-	-
231	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
232	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
233	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
234	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	-	-	-	-
235	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
236	-	97%	-	-	-	-	-	-	83%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
237	-	-	93%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
238	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	77%	100%	-	-	-	-	-	-
239	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
240	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
241	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	88%	100%	-	-	-	-	-	-
242	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	72%	62%	-	-	-	-	-	-
243	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41%	78%	-	-	-	-	-	-
244	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	92%	-	-	-	-	-	-
245	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	74%	97%	-	-	-	-	-	-
246	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	100%	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
247	-	-	68%	100%	-	-	-	-	-	-	-	-	-	-	-	-	81%	-	-	-	79%	77%	-	-	-	-	-	-
248	-	-	98%	100%	-	-	-	-	-	100%	98%	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
249	-	-	100%	-	-	-	-	-	-	-	89%	-	-	4%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
250	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
251	-	-	-	-	-	-	-	-	-	-	3%	-	-	-	-	-	100%	-	-	-	-	92%	-	-	-	-	-	-
252	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
253	-	-	100%	100%	-	-	-	100%	-	98%	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-
254	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
255	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	89%	100%	-	-	-	-	-
256	100%	-	-	100%	-	-	-	-	-	88%	100%	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-	-	-	-
257	-	-	-	-	-	-	-	-	-	31%	53%	-	-	-	-	-	100%	-	-	-	89%	88%	-	-	-	-	-	-
258	-	-	-	-	-	-	-	88%	-	-	-	-	-	35%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
259	-	-	-	-	-	-	-	55%	-	100%	-	-	-	-	8%	-	-	-	-	-	-	-	-	-	-	-	-	-
260	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
261	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	27%	-	-	-	-	-	-	-	-	-	-
262	-	100%	-	-	-	-	-	-	100%	94%	91%	-	-	-	-	-	3%	-	-	-	-	94%	-	-	-	-	-	-
263	-	-	-	-	-	-	-	100%	100%	88%	100%	-	-	-	-	-	-	-	-	-	100%	87%	-	-	-	-	-	-
264	-	100%	-	-	-	-	-	97%	-	78%	96%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
265	-	-	10%	5%	-	-	-	-	-	92%	-	-	-	-	-	-	-	100%	-	-	-	58%	-	-	-	-	-	-
266	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
267	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	79%	-	100%	-	-	-	-
268	-	98%	-	-	-	-	-	-	-	100%	-	-	87%	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-
269	-	94%	-	-	-	-	-	-	-	98%	-	-	100%	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
270	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	100%	-	-	100%	100%	-	-	-	-	-	-
271	-	100%	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	100%	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
272	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
273	-	-	-	-	-	-	-	38%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
274	-	-	-	-	-	-	-	98%	100%	100%	100%	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
275	-	-	-	-	-	-	-	100%	100%	100%	-	77%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
276	-	-	100%	-	-	-	-	100%	100%	51%	86%	-	-	75%	99%	-	99%	-	-	-	-	65%	-	-	-	-	-	-
277	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
278	-	-	-	-	-	-	-	33%	100%	-	-	100%	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-
279	-	100%	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	100%	99%	100%	100%	-	-	-	-
280	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	97%	-	-	-	-	-	-
281	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
282	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
283	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	91%	-	-	-	-	-	-
284	-	97%	-	-	100%	-	-	100%	100%	91%	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
285	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	97%	-	-	-	-	-	-
286	84%	100%	-	-	-	-	-	-	100%	94%	-	-	-	-	-	-	64%	-	-	-	-	100%	-	-	-	-	-	-
287	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-
288	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	94%	-	-	-	-	-	-
290	-	-	-	-	-	-	-	-	-	73%	-	-	-	-	-	-	100%	-	-	-	-	82%	-	-	-	-	-	-
291	100%	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
292	100%	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
293	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
294	91%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
295	100%	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-	-	-	67%	-	-	-	-	-	-
296	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
297	100%	-	10%	96%	-	-	-	-	100%	64%	100%	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
298	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
299	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	96%	-	-	-	-	-	-
300	96%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
301	-	-	-	-	-	-	-	-	-	69%	-	-	-	-	-	-	93%	-	-	-	98%	80%	-	-	-	-	-	-
302	81%	-	-	-	-	-	-	-	-	83%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
303	-	-	-	-	-	-	-	-	-	97%	100%	-	-	-	-	-	85%	-	-	-	-	84%	-	-	-	-	-	-
304	100%	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	100%	-	-	-	-	93%	-	-	-	-	-	-
305	-	-	90%	-	-	-	-	-	100%	98%	57%	-	-	-	71%	-	100%	-	-	-	100%	81%	-	-	-	-	-	-
306	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	94%	-	-	72%	100%	100%	65%	-	-	-	-
307	-	100%	100%	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	89%	-	-	-	-
308	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	1%	44%	-	-	-	-	-
309	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	97%	-	-	-	-	-	-
310	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	72%	100%	-	99%	-	-	-	-
311	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	96%	100%	-	-	-	-
312	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	87%	-	-	-	-	-
313	-	-	-	-	-	-	-	-	-	100%	95%	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
314	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	100%	96%	-	-	-	-	-
315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	91%	100%	97%	68%	-	-	-	-
316	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	99%	92%	-	-	-	-
317	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	100%	100%	99%	-	-	-	-
318	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	92%	97%	-	-	-	-
319	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
320	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
321	-	-	60%	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	74%	99%	-	-	-	-	-	-
322	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	53%	100%	-	-	-	-	-	-
323	-	-	-	-	-	-	-	-	-	93%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
324	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
325	-	-	19%	-	-	-	-	-	-	%	-	-	-	-	-	-	100%	-	-	-	73%	94%	-	-	-	-	-	-
326	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	84%	100%	-	-	-	-	-	-
327	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	85%	97%	99%	98%	-	-	-	-
328	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
329	-	-	100%	49%	-	-	-	-	-	88%	-	-	-	-	-	-	100%	-	-	-	100%	91%	-	-	-	-	-	-
330	100%	-	-	-	-	-	-	-	-	83%	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
331	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
332	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
333	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	94%	-	-	-	-	-	-
334	-	-	100%	-	-	-	-	-	-	96%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
335	-	-	100%	-	-	-	-	-	-	75%	-	-	-	-	-	-	100%	-	-	-	100%	61%	-	-	-	-	-	-
336	100%	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-	100%	-	-	-	87%	83%	-	-	-	-	-	-
337	-	100%	100%	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	95%	98%	96%	-	-	-	-
338	-	100%	-	-	-	-	-	-	-	98%	-	-	100%	-	-	-	-	100%	-	-	100%	65%	99%	100%	-	-	-	-
339	-	100%	100%	86%	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
340	-	-	-	-	-	-	-	-	-	10%	-	-	-	-	-	-	100%	-	-	-	-	96%	-	-	-	-	-	-
341	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
342	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-
343	-	100%	100%	-	-	-	-	-	-	94%	100%	-	100%	-	-	86%	-	-	-	-	-	100%	100%	97%	-	-	-	-
344	-	100%	100%	-	-	-	-	-	-	96%	100%	-	95%	-	-	-	-	100%	-	-	-	100%	82%	100%	-	-	-	-
345	-	-	-	-	-	-	-	-	-	81%	-	-	-	-	82%	-	100%	94%	-	-	100%	87%	-	-	-	-	-	-
346	-	100%	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	97%	55%	-	-	44%	-	-	-	-	-	-	-
347	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	56%	-	-	93%	-	-	-	-	-	-	-
348	-	-	11%	90%	-	-	-	-	-	-	%	-	84%	%	-	-	100%	-	-	-	-	92%	-	-	-	-	-	-
349	-	-	-	100%	-	-	-	-	-	-	53%	-	-	-	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-
350	-	-	-	97%	-	-	-	-	-	-	100%	-	-	-	-	-	86%	-	-	-	-	93%	100%	-	-	-	-	-
351	-	-	100%	77%	-	-	-	-	-	100%	11%	-	-	-	100%	-	-	-	-	-	-	89%	-	-	-	-	-	-
352	-	-	-	-	-	-	-	-	-	99%	36%	-	-	-	-	-	-	-	-	-	-	89%	61%	-	-	-	-	-
353	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-
354	-	-	-	-	-	-	-	-	-	-	47%	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-
355	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	95%	-	-	-	-	-	-
356	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
357	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
358	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
359	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
360	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	18%	-	-	-	-	91%	-	-	-	-	-	-
361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
362	-	100%	79%	-	-	-	-	-	77%	73%	-	-	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	-	-
363	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	55%	-	-	-	-	-
364	-	100%	100%	92%	-	-	-	100%	-	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-
365	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93%	96%	-	100%	-	-	-	-
366	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
367	-	100%	-	100%	-	-	-	91%	100%	100%	86%	-	-	79%	98%	-	-	-	-	-	-	-	-	-	-	-	-	-
368	-	100%	-	-	-	-	-	100%	-	100%	100%	-	99%	100%	100%	-	-	37%	-	-	82%	99%	99%	93%	-	-	-	-
369	-	-	-	-	-	-	-	-	-	-	-	-	-	-	68%	-	-	100%	-	-	100%	68%	-	-	-	-	-	-
370	-	-	100%	90%	-	-	-	-	100%	100%	100%	-	-	-	84%	-	100%	99%	-	-	100%	98%	-	-	-	-	-	-
371	-	-	-	-	100%	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
372	-	-	-	-	-	-	-	-	50%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
373	-	-	-	-	-	-	-	-	68%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
374	-	100%	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-
375	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
376	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76%	-	-	-	100%	-	-	-	-	-	-	-
377	-	-	-	-	-	-	-	-	-	67%	-	-	-	-	-	-	-	24%	-	-	83%	-	-	-	-	-	-	-
378	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
379	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	84%	-	-	-	-	-	-	-	-	-	-	-	-	-
380	-	74%	-	-	-	-	-	-	86%	72%	-	-	-	-	100%	-	-	7%	-	-	100%	-	-	-	-	-	-	-
381	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
382	-	-	-	-	-	-	-	-	100%	21%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
383	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	56%	91%	-	-	-	-	-	-
384	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-	-
385	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
386	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
387	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
388	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
389	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	68%	-	-	-	-	-	-	-
390	-	100%	57%	100%	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	76%	-	-	-	100%	-	100%	-	-	-	-
391	-	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
392	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
393	-	-	-	-	-	-	-	-	98%	100%	-	-	-	-	-	-	-	9%	-	-	100%	-	-	-	-	-	-	-
394	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	51%	-	-	90%	-	-	-	-	-	-	-
395	-	60%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	48%	-	-	87%	-	-	-	-	-	-	-
396	-	-	-	-	-	-	-	-	100%	79%	94%	-	-	-	-	-	-	100%	-	-	71%	-	-	-	-	-	-	-
397	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	%	-	-	97%	8%	-	-	-	-	-	-
398	-	-	-	-	50%	-	-	-	-	100%	-	-	-	-	-	-	-	%	-	-	98%	18%	-	-	-	-	-	-
399	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
400	-	-	-	-	-	-	-	-	-	22%	-	-	-	-	-	-	-	38%	-	-	73%	-	-	-	-	-	-	-
401	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-
402	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	93%	-	-	-	-	-	-	-
403	-	-	-	-	-	-	-	-	47%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
404	-	-	-	-	-	-	-	-	30%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
405	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
406	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	-
407	-	57%	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	98%	-	-	-	95%	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																										
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
408	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	89%	-	-	79%	-	-	-	-	-	-	-
409	-	36%	-	-	-	-	-	-	-	100%	-	-	-	-	68%	-	-	24%	-	-	70%	-	-	-	-	-	-	-
410	-	-	-	-	-	-	-	-	-	-	-	-	-	-	88%	-	-	-	-	-	-	-	-	-	-	-	-	-
411	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76%	-	-	-	-	-	87%	-	-	-	-	-	-	-
412	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
413	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
414	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
415	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
416	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-
417	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17%	-	-	1%	-	-	-	-	-	-	-	-	-	-
418	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	-	-	-	-	-	-	-	-	-	-	-
419	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	91%	-	-	53%	-	-	63%	-	-	-	-	-	-	-
420	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	37%	-	-	52%	-	-	87%	100%	-	-	-	-	-	-
421	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93%	-	-	20%	-	-	-	-	-	-	-	-	-	-
422	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	100%	-	-	63%	-	-	-	-	-	-	-	-	-	-
423	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	98%	-	-	-	-	-	-	-
424	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
425	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
426	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
427	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
428	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
429	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
430	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14%	-	-	94%	-	-	-	-	-	-	-
431	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
432	-	100%	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
433	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	45%	-	-	13%	78%	-	-	-	-	-	-
434	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	82%	94%	-	-	-	-	-	-
435	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	100%	-	-	-	-	-	-
436	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34%	-	-	-	-	-	-
437	-	-	81%	23%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
438	100%	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	99%	-	-	-	96%	87%	-	-	-	-	-	-
439	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-
440	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	99%	-	-	-	-	-	-
441	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	100%	-	-	-	-	-	-
442	-	-	-	-	-	-	-	-	-	65%	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-
443	100%	-	-	-	-	-	-	-	-	89%	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-
444	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	97%	99%	-	-	-	-	-	-
445	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	99%	97%	-	-	-	-	-	-
446	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-
447	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
448	-	-	-	-	35%	-	-	-	36%	-	-	-	-	-	-	-	100%	-	33%	-	100%	-	-	-	-	-	-	-
449	-	-	23%	-	1%	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	-	-	-	-	-	-	-	-
450	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	35%	28%	-	88%	-	-	-	-	-	-
451	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	98%	8%	86%	-	-	-	-	-	-
452	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	100%	100%	-	46%	-	29%	-	-	-	-	-	-
453	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	87%	-	-	-	-	-	-
454	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	94%	-	-	-	-	-	-
455	87%	-	-	-	-	-	-	-	-	93%	97%	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
456	-	-	-	-	-	-	-	-	-	79%	60%	-	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-
457	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
458	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
459	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
460	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
461	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
462	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
463	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-	-	-
464	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-
465	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
466	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	99%	-	100%	-	-	-	-	-	-	-	-	-	-	-
467	-	-	-	-	24%	-	-	-	-	-	-	-	-	-	-	-	-	11%	-	-	52%	100%	-	-	-	-	-	-
468	-	-	100%	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
469	-	-	100%	-	-	-	100%	-	-	100%	-	-	-	-	-	-	100%	-	-	100%	100%	100%	-	-	-	-	-	-
470	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
471	45%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
472	64%	-	-	-	5%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
473	-	-	-	-	1%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29%	-	-	-	-	-	-	-	-
474	-	-	-	-	4%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18%	-	-	-	-	-	-	-	-
475	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
476	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	%	10%	-	-	-	-	-	-	-	-
477	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41%	9%	-	-	-	-	-	-	-	-
478	-	-	-	-	2%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
479	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
480	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	99%	-	-	-	-	-	-	-
481	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
482	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
483	82%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
484	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	50%	-	-	-	-	-	-
485	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	100%	100%	-	-	18%	-	-	-	-	-	-
486	-	-	-	-	-	-	-	-	-	78%	-	-	-	-	-	-	-	5%	-	-	-	68%	-	-	-	-	-	-
487	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
488	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	98%	-	100%	-	-	-	-	-	-
489	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	95%	-	100%	-	-	-	-	-	-
490	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	99%	-	-	-	-	-	-
491	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
492	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	2%	-	-	-	-	-	-
493	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	60%	-	-	-	-	-	-
494	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	78%	-	-	-	-	-	-
495	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	99%	-	-	-	-	-	-
496	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	28%	-	-	-	-	-	-
497	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	23%	-	-	-	-	-	-
498	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	85%	-	-	-	-	-	-
499	100%	91%	98%	-	-	-	-	-	-	32%	-	-	-	-	-	-	1%	-	98%	-	-	91%	-	-	-	-	-	-
500	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	72%	-	-	11%	-	-	-	-	-	-
501	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27%	-	100%	20%	-	81%	-	-	-	-	-	-
502	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	74%	-	-	-	-	68%	-	-	-	-	-	-
503	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	96%	-	-	-	-	-	-
504	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	-	-	-	-
505	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
506	-	-	-	-	-	-	-	-	-	61%	-	-	-	-	-	-	-	17%	100%	-	-	98%	-	-	-	-	-	-
507	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
508	-	-	100%	-	-	-	-	-	-	77%	-	-	-	-	-	-	100%	100%	98%	-	-	-	-	-	-	-	-	-
509	-	-	-	-	100%	-	%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
510	-	-	-	-	1%	-	24%	-	-	-	-	-	-	-	-	-	-	%	98%	-	-	-	-	-	-	-	-	-
511	39%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	62%	-	-	100%	-	-	-	-	-	-
512	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
513	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
514	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
515	-	-	-	-	-	-	-	-	-	93%	-	-	-	-	100%	-	-	100%	-	-	100%	-	-	-	-	-	-	-
516	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	83%	-	-	99%	-	-	-	-	-	-	-
517	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
518	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	99%	-	-	-	-	-	-	-
519	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	78%	-	-	-	-	-	-	-
520	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	93%	-	-	-	-	-	-	-
521	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-	-	-	-	-
522	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	92%	-	-	-	-	-	-	-
523	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
524	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	65%	-	-	-	-	-	-	-
525	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
526	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	-
527	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
528	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	95%	-	-	-	-	-	-	-
529	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	64%	-	-	70%	-	-	-	-	-	-	-
530	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	5%	-	-	85%	-	-	-	-	-	-	-
531	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	13%	-	-	94%	-	-	-	-	-	-	-
532	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27%	-	-	95%	-	-	-	-	-	-	-
533	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	85%	-	-	84%	-	-	-	-	-	-	-
534	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
535	-	100%	-	-	-	-	-	-	92%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
536	-	-	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
537	-	94%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
538	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	-	-
539	-	-	-	-	-	-	-	-	98%	100%	-	-	-	-	-	-	-	3%	-	-	100%	-	-	-	-	-	-	-
540	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
541	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
542	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	96%	-	100%	-	-	-	100%	-	-	-	-	-	-	-
543	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
544	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
545	-	-	-	-	-	-	-	-	100%	40%	-	-	-	-	83%	-	-	-	-	-	-	-	-	-	-	-	-	-
546	-	-	-	-	-	-	-	-	72%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
547	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
548	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
549	-	-	-	-	-	-	-	-	42%	97%	-	-	-	-	-	-	100%	6%	-	-	-	-	-	-	-	-	-	-
550	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
551	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
552	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-
553	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
554	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	100%	-	-	-	-	-	-	-
555	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	99%	-	-	-	-	-	-	-
556	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	93%	-	-	-	-	-	-	-	-	-	-	-	-	-
557	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	99%	-	-	-	-	-	-	-
558	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-
559	-	-	-	-	-	-	-	-	-	64%	-	-	-	-	-	-	-	98%	-	-	100%	-	-	-	-	-	-	-
560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	90%	-	-	-	-	-	-	-
561	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
562	-	-	-	-	-	-	-	-	-	45%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
563	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
564	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	16%	-	-	90%	-	-	-	-	-	-	-
565	-	-	-	-	41%	-	-	-	-	100%	-	-	-	-	-	-	-	23%	-	-	95%	22%	-	-	-	-	-	-
566	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
567	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
568	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17%	-	-	62%	-	-	-	-	-	-	-
569	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
570	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
571	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	79%	-	-	21%	-	-	-	-	-	-
572	-	-	-	-	-	-	10%	-	-	48%	-	-	-	-	-	-	-	-	20%	-	-	14%	-	-	-	-	-	-
573	-	-	-	-	-	-	100%	-	-	88%	-	-	-	-	-	-	100%	-	%	-	-	-	-	-	-	-	-	-
574	100%	-	-	-	-	-	-	-	-	55%	-	-	-	-	-	-	-	-	100%	-	-	78%	-	-	-	-	-	-
575	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	14%	-	-	-	-	-	-
576	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-
577	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	50%	-	-	92%	-	-	-	-	-	-
578	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	-	-
579	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	57%	-	94%	-	-	-	-	-	-	-
580	-	-	100%	-	100%	-	100%	-	-	100%	-	-	-	-	-	-	-	-	100%	-	100%	100%	-	-	-	-	-	-
581	-	-	100%	-	100%	-	100%	-	-	100%	-	-	-	-	-	-	100%	-	100%	-	100%	100%	-	-	-	-	-	-
582	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	96%	-	100%	-	-	-	-	-	-
583	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
584	-	-	-	-	-	-	-	-	-	87%	100%	-	-	-	99%	-	-	-	-	-	100%	-	-	-	-	-	-	-
585	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	100%	-	-	79%	-	-	-	-	-	-	-
586	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-
587	-	100%	-	-	%	-	-	-	81%	-	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	-	-	-	-
588	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
589	-	-	100%	-	100%	-	100%	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
590	-	-	-	-	24%	-	-	-	-	-	-	-	-	-	-	-	-	23%	-	-	34%	-	-	-	-	-	-	-
591	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
592	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77%	-	-	-	-	-	-
593	-	-	-	-	7%	-	-	-	50%	-	-	-	-	-	-	-	-	50%	-	-	-	-	-	-	-	-	-	-
594	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
595	-	-	-	-	16%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
596	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
597	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	50%	-	-	-	-	-	-	-	-	-
598	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24%	-	-	-	-	-	-	-	-	-
599	-	-	-	-	2%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	50%	-	-	-	-	-	-
600	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
601	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
602	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
603	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	100%	-	-	-	-	-	-	-
604	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
605	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
606	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
607	-	-	-	-	6%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
608	-	-	-	-	7%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
609	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
610	-	-	-	-	30%	-	-	-	-	-	-	-	-	-	-	-	-	-	22%	-	-	-	-	-	-	-	-	-
611	-	-	-	-	50%	-	-	-	-	-	-	-	-	-	-	-	-	-	23%	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																										
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
612	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
613	-	-	-	-	1%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
614	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
615	-	-	-	-	2%	-	-	-	-	-	-	-	-	-	-	-	-	-	1%	-	-	50%	-	-	-	-	-	-
616	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
617	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
618	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-
619	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
620	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
621	99%	-	-	-	-	-	71%	-	-	98%	-	-	-	100%	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
622	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	85%	-	-	-	-	-	-
623	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
624	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	89%	-	-	-	-	-	-
625	-	-	-	-	-	-	21%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
626	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
627	-	-	-	-	13%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
628	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
629	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-
630	-	-	-	-	-	97%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
631	38%	65%	-	-	-	-	68%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
632	-	-	-	-	-	-	65%	-	-	13%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
633	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	-	40%	-	-	-	-	-	-
634	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	16%	-	-	-	-	100%	-	-	-	-	-	-
635	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-
636	-	-	-	-	100%	-	100%	-	-	86%	-	-	-	-	-	-	-	-	-	-	-	64%	-	-	-	-	-	-
637	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
638	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-
639	-	-	-	-	%	-	100%	-	-	88%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
640	78%	-	-	-	-	-	79%	-	-	89%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
641	34%	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
642	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
643	-	86%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
644	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
645	-	-	-	-	98%	100%	98%	-	-	-	-	-	-	-	-	-	100%	99%	100%	-	-	42%	-	-	-	-	-	-
646	-	96%	-	-	4%	-	58%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
647	-	42%	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	66%	100%	-	-	-	99%	-	-	-	-	-	-
648	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
649	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
650	-	-	-	-	-	-	100%	-	-	98%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
651	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
652	-	92%	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	96%	100%	-	-	-	95%	-	-	-	-	-	-
653	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
654	-	100%	-	-	-	-	-	-	-	69%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
655	-	85%	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
656	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	100%	-	100%	100%	-	-	-
657	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	100%	100%	-	-	-
658	-	61%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
659	-	-	100%	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-
660	-	95%	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	-	-	-	-
661	-	-	-	-	41%	-	50%	50%	-	-	-	-	-	-	-	-	50%	-	-	-	-	50%	-	-	-	-	-	-
662	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	88%	-	-	-	-	-	-
663	-	-	-	-	-	-	56%	-	-	-	-	-	-	-	-	-	-	1%	-	-	-	-	-	-	-	-	-	-
664	100%	96%	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
665	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-
666	-	-	-	-	-	-	97%	-	-	59%	-	-	-	-	-	-	48%	-	100%	-	-	-	-	-	-	-	-	-
667	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-
668	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
669	-	92%	-	-	-	-	3%	-	-	86%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
670	100%	100%	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	99%	100%	-	-	-	100%	-	-	-	-	-	-
671	-	81%	-	-	-	-	97%	-	-	93%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
672	-	-	-	-	-	-	-	-	-	1%	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-
673	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	89%	-	-	-	-	-	-
674	86%	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	89%	-	-	-	-	-	-
675	86%	-	-	-	-	-	-	-	-	100%	-	-	-	73%	-	-	100%	-	-	-	-	90%	-	-	-	-	-	-
676	-	-	-	-	25%	-	-	32%	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
677	-	-	-	-	-	-	63%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
678	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
679	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																										
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
680	-	60%	-	-	-	-	100%	13%	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
681	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2%	-	-
682	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54%	-	-	-	-	-	-	-
683	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-
684	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	89%	-	-	-	-	-	-	-	-	-
685	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	72%	-	-	-	-	-	-	-	-	-
686	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-	-	-
687	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	81%	-	-	-	-	-	-	-	-	-
688	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	-	-	-	48%	-	-	-	-	-	-	-	-	-
689	-	-	-	-	100%	34%	-	-	-	-	-	-	-	-	-	-	-	-	46%	-	28%	-	-	-	-	-	-	-
690	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	45%	-	40%	-	-	-	-	-	-	-
691	28%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10%	-	-	-	-	-	-	-	-	-
692	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3%	-	-	-	-	-	-	-	-	-
693	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1%	-	-	-	-	-	-	-	-	-
694	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6%	-	-	-	-	-	-	-	-	-
695	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
696	55%	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	97%	-	-	-	-	-	-	-	-	-	-
697	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
698	-	-	-	-	-	-	-	-	-	89%	100%	-	100%	100%	-	87%	-	-	-	-	-	100%	-	100%	-	-	-	-
699	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
700	-	-	-	-	9%	-	-	100%	-	-	-	-	-	-	-	-	-	-	42%	-	-	-	-	-	-	-	-	-
701	-	-	-	-	2%	-	100%	-	-	-	-	-	-	-	-	-	-	-	43%	-	-	-	-	-	-	-	-	-
702	-	-	-	-	19%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
703	-	-	-	-	11%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
704	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13%	-	-	-	-	-	-	-	-	-
705	-	-	-	-	84%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
706	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	%	100%	-	%	52%	-	-	35%	-	-	-
707	-	-	-	-	51%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
708	-	-	-	-	11%	-	-	-	-	-	-	-	-	-	-	-	-	-	23%	-	-	-	-	-	-	-	-	-
709	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4%	-	-	-	-	-	-	-	-	-
710	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
711	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-	-	-	-	-
712	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	91%	-	-	-	-	-	-	-
713	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	63%	-	-	-	-	-	-
714	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	94%	-	-	-	-	-	-
715	-	-	-	-	-	-	45%	12%	-	-	-	-	-	-	-	-	-	75%	-	-	-	-	-	28%	-	-	-	-
716	-	-	-	-	-	-	-	81%	-	-	-	-	-	-	-	-	-	13%	-	-	-	-	-	85%	-	-	-	-
717	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
718	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
719	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	91%	52%	-	-	-	-	-
720	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
721	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	100%	-	-	-	-	-
722	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
723	-	-	-	-	-	-	-	-	-	-	100%	-	100%	100%	93%	100%	-	-	-	-	-	-	-	-	-	-	-	-
724	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	30%	-	-	-	100%	100%	91%	-	-	-	-
725	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	94%	-	-	-	-	-	-	-	-	-	-	-	-	-
726	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	63%	-	-	-	-	-	-	-	-	-	-	-	-	-
727	-	100%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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729	-	100%	-	-	-	-	-	-	-	-	-	-	-	9%	93%	-	-	-	-	-	-	-	-	-	-	-	-	-
730	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-
731	-	-	-	-	-	-	-	-	-	-	100%	-	100%	100%	-	98%	-	-	-	-	-	-	-	-	-	-	-	-
732	-	-	100%	-	-	-	-	-	-	100%	73%	-	-	-	-	-	100%	-	-	-	-	89%	-	-	-	-	-	-
733	-	-	-	-	-	-	-	-	-	15%	-	-	-	-	-	-	100%	-	-	-	-	45%	100%	-	-	-	-	-
734	-	-	100%	-	-	-	-	-	-	61%	-	-	-	-	-	-	100%	-	-	-	-	67%	-	-	-	-	-	-
735	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
736	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	63%	77%	-	-	-	-	-	-
737	100%	-	-	-	-	-	-	47%	-	-	-	-	-	-	-	-	-	70%	-	-	100%	-	-	-	-	-	-	-
738	60%	100%	-	-	-	-	-	-	-	44%	-	-	-	-	-	-	-	-	-	-	38%	-	-	-	100%	100%	-	-
739	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-	87%	-	-	-
740	100%	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	95%	56%	-	-
741	-	-	-	-	-	-	100%	15%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
742	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	58%	99%	-	-	-	100%	-	-	-
743	-	-	-	-	-	-	-	99%	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
744	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	94%	-	-	-	-	-
745	-	100%	100%	-	-	-	-	-	-	97%	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
746	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
747	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	99%	99%	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
748	-	100%	-	-	-	100%	-	28%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	92%	-	-	-	-	-
749	-	100%	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-
750	-	-	100%	100%	-	-	-	100%	-	100%	78%	-	-	100%	67%	100%	-	-	-	-	100%	84%	-	-	-	-	-	-
751	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	95%	-	-	-	-	-	-
752	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	91%	99%	-	-	-	-	-
753	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-	-	-	-	-	-	-
754	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	97%	99%	-	-	-	-
755	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	89%	97%	98%	-	-	-	-
756	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	95%	99%	-	-	-	-
757	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	88%	-	-	-	-	-	-
758	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	81%	-	-	-	-	-	-
759	-	-	-	-	-	-	98%	87%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
760	-	-	-	-	-	-	-	70%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
761	-	70%	-	-	-	-	100%	71%	-	68%	-	-	-	-	-	-	-	59%	-	-	100%	6%	-	100%	-	100%	-	-
762	-	-	-	-	-	-	86%	66%	-	-	-	-	-	-	-	-	-	29%	-	-	-	-	-	-	-	-	-	-
763	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
764	82%	-	-	-	-	-	-	-	-	98%	-	-	91%	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-
765	-	-	-	100%	-	-	100%	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	100%	-	-
766	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
767	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	85%	75%	-	100%	-	100%	-	-
768	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	98%	-	-	-	-
769	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
770	100%	-	-	79%	-	-	81%	65%	-	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-	-	-	-	-
771	100%	100%	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	25%	100%	-	-	-	-	-	97%	-	100%	-	-
772	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
773	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
774	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	-
775	-	-	-	-	100%	-	-	9%	-	-	-	-	-	-	-	-	-	-	-	69%	100%	-	-	-	99%	100%	-	-
776	87%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	69%	-	98%	-	-	-	99%	95%	-	-
777	-	-	-	-	-	-	-	38%	-	-	-	-	-	-	-	-	-	-	-	-	96%	-	-	-	100%	94%	-	-
778	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-	100%	100%	-	-
779	-	-	-	-	2%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
780	-	-	100%	-	-	-	-	-	-	51%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-
781	99%	97%	-	58%	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	100%	100%	-	-
782	-	54%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	83%	10%	-	-	-	-	-	-
783	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	52%	-	-
784	-	-	-	-	-	-	85%	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-
785	-	-	-	-	-	-	71%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
786	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
787	-	-	-	-	-	-	86%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
788	-	-	-	-	-	-	57%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
789	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-
790	-	-	-	-	-	-	67%	-	-	-	-	-	-	-	-	-	-	4%	-	-	-	-	-	-	-	-	-	-
791	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	36%	-	-	-	-	-	-	-	-	-	-
792	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
793	-	-	-	-	-	75%	78%	-	79%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
794	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-	-	23%	-	-	-	-	-	-	-	-	-	-
795	-	-	-	-	-	-	79%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
796	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
797	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
798	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	98%	-	-	-	-
799	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
800	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
801	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
802	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-
803	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
804	-	-	-	-	-	-	-	86%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
805	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
806	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
807	100%	100%	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
808	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	93%	-	-	-	-	-	100%	-	97%	-	-
809	100%	100%	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
810	98%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17%	-	-	-	-	-	-	-	-	-	-
811	73%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-	-	-	-
812	-	-	-	77%	-	-	-	-	-	-	-	-	-	-	-	-	-	16%	-	-	-	-	-	100%	-	-	-	-
813	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	100%	-	-
814	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
815	-	96%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	97%	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																										
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
816	-	-	-	84%	-	-	-	100%	-	-	-	-	-	-	-	91%	-	35%	-	-	92%	80%	-	-	-	-	-	-
817	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61%	100%	-	-	-	-	21%	100%	-	-	-	-	-	-
818	-	-	100%	-	-	-	-	-	-	-	96%	-	-	-	72%	-	100%	-	-	-	91%	98%	-	-	-	-	-	-
819	100%	100%	-	100%	-	-	-	99%	-	100%	-	-	-	-	-	-	100%	76%	-	-	92%	91%	-	-	-	-	-	-
820	93%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	89%	-	-	-	-	-	-	-
821	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	83%	93%	-	-	-	-	-	-
822	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	91%	-	-	-	-
823	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
824	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	85%	-	-	-	-	-	-
825	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	100%	-	-	-	-	-	-
826	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	88%	61%	-	-	-	-	-	-
827	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	95%	95%	-	-	-	-	-	-
828	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	81%	97%	-	-	-	-	-	-
829	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	84%	100%	-	-	-	-	-	-
830	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	-	-	-	56%	63%	-	100%	-	-	-	-
831	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-
832	-	98%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	93%	100%	-	-	-	-	-	-
833	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	51%	92%	-	-	-	-	-	-
834	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85%	100%	-	95%	97%	-	26%	-	-	-	-
835	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
836	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	93%	-	-	-	-
837	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	76%	99%	-	-	-	-	-	-
838	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	59%	40%	-	-	-	-	-	-
839	-	100%	100%	-	-	-	-	-	-	88%	100%	-	-	-	-	-	100%	-	-	-	82%	1%	-	-	100%	-	-	-
840	100%	-	-	-	-	-	-	-	-	74%	-	-	-	-	-	-	56%	100%	100%	-	-	85%	-	-	100%	-	-	-
841	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-
842	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63%	-	100%	-	-
843	-	64%	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
844	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	100%	97%	-	-	99%	-	-	-
845	-	-	-	-	-	-	-	-	-	82%	-	-	-	-	-	-	-	-	-	-	-	76%	-	-	-	-	-	-
846	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-
847	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	93%	-	-	-	-	-	92%	-	-	-	-
848	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93%	-	-	-	-
849	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	53%	-	-	-	-
850	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	52%	-	-	-	-
851	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	54%	68%	-	-	-	-
852	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	100%	-	-	-	-
853	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	98%	-	-	-	-
854	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	94%	-	-	-	-
855	-	-	-	-	-	-	-	-	-	-	-	91%	83%	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
856	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	-	-	-	-	-	-	-	100%	-	97%	-	-	-	-
857	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35%	-	-	-	100%	-	100%	-	-	-	-
858	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	78%	-	-	-	-
859	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26%	-	-	100%	-	98%	-	-	-	-
860	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	100%	-	89%	-	-	-	-
861	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	12%	-	-	89%	-	97%	-	-	-	-
862	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	100%	-	-	100%	100%	-	-	-	-	-	-
863	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93%	100%	-	-	88%	94%	-	-	-	-	-	-
864	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
865	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	93%	-	-	77%	-	-	-	-	-	-	-
866	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-
867	-	-	-	-	-	-	-	-	-	90%	-	-	-	100%	-	-	-	100%	-	-	100%	100%	-	-	-	-	-	-
868	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	96%	100%	-	-	-	-	-	-
869	-	100%	100%	100%	-	-	-	-	-	72%	-	-	-	-	-	-	100%	93%	-	-	100%	100%	-	-	-	-	-	-
870	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	97%	-	-	99%	100%	-	-	-	-	-	-
871	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
872	-	100%	-	100%	-	-	-	-	-	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
873	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
874	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-
875	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	96%	74%	-	-	-	-
876	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	97%	-	-	-	-	-
877	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
878	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
879	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	99%	-	-	-	-
880	-	100%	-	-	-	-	-	-	-	82%	-	-	-	-	-	-	-	95%	-	-	-	100%	-	95%	-	-	-	-
881	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
882	-	-	-	-	-	-	-	-	-	95%	-	99%	100%	35%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
883	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
884	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	97%	-	100%	-	-	100%	100%	-	-	-	-	-	-
885	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	100%	-	-	80%	97%	-	-	-	-	-	-
886	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-
887	-	77%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
888	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	100%	-	-	-	-	-	-	-
889	-	-	-	4%	-	-	100%	75%	-	-	-	-	-	-	-	-	-	64%	-	-	100%	98%	-	-	-	-	-	-
890	-	-	-	97%	-	-	100%	100%	-	100%	-	-	-	-	37%	-	-	100%	-	-	100%	-	-	-	-	-	-	-
891	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-
892	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	71%	-	-	-
893	-	100%	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-
894	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-	-	-	-	-
895	-	97%	-	96%	-	-	-	-	73%	98%	-	-	-	-	-	-	-	95%	-	-	96%	-	100%	-	100%	-	-	-
896	-	100%	-	100%	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	42%	-	-	-	-	-	-	-
897	-	-	-	-	-	-	-	8%	-	-	-	-	-	-	-	-	-	30%	-	-	80%	80%	-	-	-	-	-	-
898	-	95%	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-
899	-	100%	-	69%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
900	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
901	-	99%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	99%	-	-	-
902	-	-	-	96%	-	-	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	92%	-	-	-	-	-	-	-
903	-	100%	-	45%	-	-	-	92%	-	100%	-	-	-	-	-	100%	100%	97%	-	-	56%	31%	-	-	-	-	-	-
904	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	89%	65%	-	-	-	-	-	-
905	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	55%	-	-	-	-	-	-
906	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	100%	87%	-	-	-	-	-	-
907	-	100%	-	94%	-	-	-	-	-	100%	94%	-	-	-	55%	-	-	-	-	-	100%	87%	-	-	-	-	-	-
908	-	66%	-	-	-	-	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-	-	-	100%	-	-	-	-
909	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	94%	-	100%	-	62%	-	-	-
910	85%	98%	-	71%	-	-	-	100%	-	-	-	-	-	-	-	-	-	86%	-	-	78%	-	-	-	-	-	-	-
911	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-
912	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	97%	-	-	-	65%	98%	-	-	-	-	-
913	-	100%	-	78%	-	-	-	-	-	99%	-	-	-	-	-	-	-	100%	-	-	80%	76%	66%	-	-	-	-	-
914	100%	-	100%	79%	-	-	-	-	-	97%	-	-	-	100%	-	-	-	-	-	-	-	86%	100%	78%	-	90%	-	-
915	-	-	-	100%	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	85%	-	73%	-	-	-	-
916	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
917	-	-	-	96%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	96%	-	100%	-	-	-	-
918	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-
919	-	84%	100%	18%	-	-	-	-	-	100%	-	-	-	-	72%	-	-	-	-	-	98%	99%	-	-	-	-	-	-
920	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	100%	88%	-	-	-	-	-	-
921	100%	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
922	85%	100%	-	100%	-	-	-	-	-	96%	-	-	-	-	-	-	100%	100%	-	-	-	94%	30%	-	-	-	-	-
923	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	97%	-	-	-	-	-
924	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
925	-	-	70%	-	-	-	-	-	-	82%	-	-	-	-	-	-	100%	-	-	-	-	95%	100%	100%	-	-	-	-
926	100%	92%	94%	88%	-	-	-	-	-	78%	-	-	-	-	-	-	-	-	-	-	-	93%	88%	-	-	-	-	-
927	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	88%	-	-	-	-	-	-
928	-	100%	-	-	-	100%	-	56%	100%	-	-	-	100%	-	-	-	-	100%	-	-	100%	100%	80%	-	-	-	-	-
929	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-
930	-	-	100%	-	-	-	-	-	100%	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-
931	-	-	100%	-	-	99%	-	100%	100%	-	100%	-	-	-	-	-	-	-	-	-	-	100%	86%	64%	-	-	-	-
932	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-
933	83%	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
934	-	92%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
935	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	%	-	-	-	98%	-	100%	-	-	-	-
936	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
937	-	68%	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
938	-	-	-	-	-	-	-	-	-	16%	-	-	-	100%	-	64%	-	-	-	-	-	100%	50%	-	-	-	-	-
939	-	-	-	-	-	-	-	-	-	-	100%	-	100%	100%	75%	-	-	-	-	-	-	-	-	-	-	-	-	-
940	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
941	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	73%	-	-	-	-	100%	-	-	-	-	-
942	-	94%	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
943	-	100%	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
944	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
945	-	-	-	-	-	-	-	28%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
946	-	-	-	-	-	-	-	100%	100%	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
947	-	-	-	-	-	-	-	93%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-
948	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	77%	-	-	-	-
949	-	100%	-	90%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	100%	99%	100%	-	-	-	-
950	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
951	-	97%	100%	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	100%	-	-	93%	94%	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
952	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	89%	-	-	-	-	-	-	-	-	-	-	-	-
953	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	54%	100%	-	-	-	-	-	-	-	-	-	-	-	-
954	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	98%	-	-	-	-	-	-	-	-	-	-	-	-
955	-	-	100%	-	-	-	-	100%	100%	99%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	98%	-	-	-	-
956	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
957	-	-	-	-	-	-	-	-	-	100%	100%	-	100%	-	-	-	-	100%	-	-	-	84%	100%	100%	-	-	-	-
958	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-
959	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-
960	-	-	100%	-	-	-	-	-	-	99%	100%	-	100%	100%	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-
961	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-
962	-	-	100%	-	-	-	-	-	-	78%	92%	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
963	-	100%	-	-	-	-	-	-	-	74%	-	-	-	-	-	-	-	100%	-	-	-	100%	98%	88%	-	-	-	-
964	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	100%	-	-	-	77%	100%	-	-	-	-	-
965	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-
966	100%	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
967	-	100%	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	96%	-	-	-	-	-
968	-	-	-	-	-	99%	-	94%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
969	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
970	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
971	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
972	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	72%	-	-	-	-	-	-
973	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	93%	100%	-	-	-	-	-
974	-	71%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
975	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
976	100%	84%	-	100%	-	-	-	-	-	96%	-	-	-	-	-	-	100%	100%	-	-	-	74%	-	-	-	-	-	-
977	-	100%	100%	100%	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	-	91%	96%	-	-	-	-	-
978	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	98%	91%	-	-	-	-	-
979	-	-	100%	100%	-	-	-	-	-	100%	100%	-	-	-	80%	-	-	-	-	-	-	100%	100%	-	-	-	-	-
980	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	95%	-	-	-	-	-	-
981	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
982	-	-	-	100%	-	-	-	-	-	89%	-	-	-	-	-	-	100%	-	-	-	-	94%	-	-	-	-	-	-
983	95%	100%	-	100%	-	-	-	-	-	100%	17%	-	-	-	-	-	100%	-	-	-	-	100%	75%	100%	-	-	-	-
984	-	92%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
985	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-
986	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
987	-	50%	-	50%	-	-	-	-	-	83%	-	-	-	-	-	-	100%	100%	-	-	-	100%	87%	-	-	-	-	-
988	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	66%	53%	-	-	-	-	-
989	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	100%	-	-	-	-	64%	66%	-	-	-	-	-
990	-	-	-	-	-	-	-	-	-	88%	-	48%	-	100%	-	-	-	58%	-	-	-	100%	-	96%	-	-	-	-
991	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	52%	-	97%	100%	-	-	-	-	-	-
992	-	100%	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	100%	-	%	95%	-	88%	-	-	-	-
993	-	-	-	-	-	-	-	-	-	-	-	28%	38%	45%	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-
994	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
995	-	-	-	-	-	-	81%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
996	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-
997	-	-	100%	64%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	48%	-	-
998	-	70%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	83%	57%	-	-
999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	-	-
1000	-	-	-	-	-	-	-	87%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1001	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1002	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1003	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
1004	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8%	-	-	-	-	-	-	-	-	-	-
1005	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
1006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	100%	-	-	-	-
1007	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-
1008	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	-	-	-	-	-	-	-
1009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-
1010	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-
1011	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40%	-	-	-	-	-	-	-
1012	-	-	-	-	-	-	-	-	-	71%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-
1013	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-
1014	-	100%	-	-	-	-	-	-	-	-	-	-	66%	100%	-	95%	-	100%	-	-	-	100%	-	-	-	-	-	-
1015	-	85%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	89%	69%	-	-	-	-	-
1016	100%	96%	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	100%	81%	-	-	-	-
1017	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1018	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
1019	-	-	-	-	-	-	-	17%	77%	-	-	-	-	-	81%	-	-	100%	-	-	-	-	-	-	-	-	-	-

Table D-1. Detailed Land Use and Development Condition Data - Existing Conditions (2006)

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
1020	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
1021	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1022	100%	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	64%	-	-	-	100%	-	-	-	-	-	-
1023	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	-	-	-	-	75%	-	-	-	-
1024	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11%	-	-	-	-	-	49%	-	-	-	-
1025	-	-	-	-	-	-	-	21%	-	-	-	-	-	-	-	-	-	-	71%	-	-	-	-	-	-	-	-	-
1026	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46%	-	-	-	-	-	15%	-	-	-	-
1027	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	%	-	-	-	-	-	73%	-	-	-	-
1028	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	60%	-	-	-	-	-	24%	-	-	-	-
1029	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10%	-	100%	-	-	2%	-	-	-	-
1030	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	73%	-	99%	-	-	6%	-	-	-	-
1031	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
1032	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
1033	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33%	-	-	-	-	-	56%	-	-	-	-
1034	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	100%	88%	-	-	-	100%	-	-
1035	-	100%	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-
1036	-	100%	-	-	-	-	100%	78%	89%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1037	-	-	23%	-	-	-	-	-	-	80%	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	100%	-	-	-
1038	-	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	-	-	8%	-	-	-	-	-	-	-	-	-	-
1039	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	68%	100%	-	-	-	-	-	-
1040	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1041	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	-	-	-
1042	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	22%	-	67%	-	-	-	-	-	-	-
1043	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
1044	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	97%	-	-	-	-	-	-
1045	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
1046	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21%	-	-	-	-	-	-	-	-	-
1047	-	-	-	-	47%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1048	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	81%	-	-	-	-	-	-	-
1049	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36%	-	-	-	-	-	-	-	-	-
1050	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	81%	-	-	-	-	-	-
1051	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32%	-	-	-	-	-	-	-	-	-
1052	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	89%	78%	18%	-	57%	-	-	-	-	-	-
1053	-	-	-	-	1%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3%	-	-	-	-	-	-	-	-
1054	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1055	-	100%	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1056	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	56%	-	-	100%	-	-	100%	-	-	-	-
9999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	98%	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
0																												
1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.04	-	-	-	-	-	25.9	-	-	-	-
2	-	19.6	-	-	-	-	-	-	-	8.68	-	-	-	-	-	-	-	6.14	-	-	-	2.61	-	0.998	-	32.2	-	-
3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.0	-	-	-	-	-	-	-	-	-
5	-	0.145	-	-	0.819	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
6	13.9	-	-	-	0.0243	-	-	32.7	-	25.5	-	-	-	-	-	-	-	-	2.79	-	-	-	-	-	-	-	-	-
7	22.1	12.9	-	-	0.202	-	-	-	-	12.3	-	-	-	-	-	-	4.82	-	0.907	-	22.3	-	-	-	24.7	13.9	-	-
8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.5	-	-	-	-	-	-	-
9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.94	-	9.66	-	-	-	-	0.0000	-	-	-	-
12	-	-	-	-	16.1	-	9.99	-	-	-	-	-	-	-	-	-	-	-	5.42	-	6.44	-	-	-	-	-	-	-
13	-	-	-	-	0.0015	-	-	-	-	-	-	-	-	-	-	-	-	-	84.6	-	2.25	-	-	-	-	-	-	-
14	2.31	-	-	-	-	-	2.57	-	-	0.338	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
15	-	-	-	-	18.9	-	44.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
16	-	-	-	-	-	-	-	-	-	17.8	-	-	-	-	-	-	13.2	-	0.0063	-	-	28.0	-	-	-	-	-	-
17	12.1	12.7	-	-	-	-	-	-	-	19.2	-	-	-	-	-	-	60.5	-	0.0001	-	-	22.6	-	-	-	-	-	-
18	-	-	-	-	0.0225	-	33.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
19	-	-	-	-	-	-	-	-	-	6.91	-	-	-	-	-	-	-	17.3	0.0135	-	-	-	-	-	-	-	-	-
20	-	-	-	-	0.0152	-	16.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
21	-	3.90	-	-	-	-	-	-	1.54	-	-	-	-	-	-	-	0.303	-	-	-	-	-	-	-	-	-	-	-
22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.1	-	-	-	-	-	-	-	-	-
23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	39.4	-	-	-	-	-	-	-	-	-
24	-	-	-	-	-	-	-	-	1.92	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
25	-	-	-	-	5.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
26	-	-	-	-	2.73	-	-	0.0251	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
28	-	-	-	-	1.71	-	-	-	-	-	-	-	-	-	-	-	-	-	0.159	-	-	-	-	-	-	-	-	-
29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.36	-	-	-	-	-	-	-	-	-
30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.76	-	-	-	-	-	-	-	-	-
31	-	-	-	-	1.66	-	-	-	-	-	-	-	-	-	-	-	-	-	7.79	-	-	-	-	-	-	-	-	-
32	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.66	-	-	-	-	-	-	-	-	-
33	-	-	-	-	0.0004	-	-	-	-	-	-	-	-	-	-	-	-	-	6.78	-	-	-	-	-	-	-	-	-
34	-	-	-	-	9.15	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-
35	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.19	0.858	-	-	-	-	-	-	-	-	-	-
36	-	-	-	-	-	-	-	-	1.51	-	-	-	-	-	-	-	-	7.63	-	-	-	-	-	-	-	-	-	-
37	-	-	-	-	-	-	-	-	3.27	-	-	-	-	-	-	-	417	9.15	-	-	-	-	-	-	-	-	-	-
38	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	-	-	9.81	-	-	-	-	-	-	-	-	-	-	-
39	-	-	-	-	-	-	-	-	34.4	-	-	-	-	-	-	-	0.197	-	-	-	-	-	-	-	-	-	-	-
40	-	23.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
41	-	-	-	-	-	-	-	-	30.7	-	-	-	-	-	-	-	-	5.74	-	-	-	-	-	-	-	-	-	-
42	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.297	-	-	-	64.3	-	-	-	-	-	-	-
43	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
44	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.2	-	0.0490	-	-	-	-	-	-	-	-	-
45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.8	-	0.0002	-	-	-	-	-	-	-	-	-
46	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.37	-	-	-	-	-	-	-	-	-
47	-	-	-	-	-	-	-	-	8.58	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
48	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0353	-	199	45.4	-	-	-	-	-	-
49	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.52	1.30	-	-	45.7	-	-	-	-	-	-	-
50	-	1.35	-	-	-	-	-	0.0168	120	5.87	-	-	-	-	-	-	-	-	-	-	-	4.21	-	-	-	-	-	-
51	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.61	34.3	-	-	2.82	-	-	-	-	-	-	-
52	-	-	-	-	-	-	-	-	45.1	-	-	-	-	-	-	-	-	4.08	-	-	-	-	-	-	-	-	-	-
53	-	-	-	-	-	-	-	-	25.2	-	-	-	-	-	-	-	-	0.0120	-	-	-	-	-	-	-	-	-	-
54	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.78	196	-	-	0.686	-	-	-	-	-	-	-
55	8.37	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.4	-	-	-	-	-	-	-	-	-
56	0.0397	-	-	-	-	7.16	-	-	-	-	-	-	-	-	-	-	-	-	4.18	-	-	-	-	-	-	-	-	-
57	-	-	-	-	43.4	-	-	-	-	17.1	-	-	-	1.20	-	-	16.3	4.05	36.4	-	5.19	-	-	-	-	-	-	-
58	-	-	-	-	-	-	-	-	0.0065	13.2	-	-	-	-	-	-	-	-	-	-	-	0.304	-	-	-	-	-	-
59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	9.02	-	-	-	-	-	-	-	-	-
60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.2	-	1.84	1.53	-	-	-	-	-	-
61	-	-	-	-	-	-	-	-	5.84	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
62	-	-	-	-	-	-	-	-	28.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
63	-	-	-	-	-	-	-	-	9.04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
64	-	-	-	-	-	-	-	-	5.13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
65	-	-	-	-	-	-	-	-	17.5	-	-	-	-	-	-	-	5.73	-	0.0067	-	-	-	-	-	-	-	-	-
66	-	-	0.921	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0836	-	-	-	83.6	55.5	-	-	-	-	-	-
67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.77	69.8	-	-	-	-	-	-
68	-	-	-	-	0.0050	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44.1	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
69	-	-	-	-	-	-	-	-	33.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
70	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.98	-	-	-	-	-	-	-	-	-	-	-	-	-
71	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-	-	-	3.59	-	-	30.7	-	-	-	-	-	-	-
72	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.03	-	-	-	2.36	-	-	-	-	-	-	-
73	-	0.0004	-	-	-	-	-	-	-	22.4	-	-	-	-	-	-	-	-	-	-	-	0.0016	27.9	-	-	-	-	-
74	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.80	-	-	-	-	-	-	-
75	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
76	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.9	-	-	-	-	-	-	-	-	-
77	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41.4	-	0.0553	-	-	-	-	-	-	-
78	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0342	-	23.8	-	0.0001	0.0395	-	-	-	-	-	-
79	6.80	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
80	-	-	-	-	-	-	-	-	-	1.15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
81	-	-	2.37	-	-	-	-	-	-	16.5	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-
82	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.03	-	-	7.36	-	-	-	-	-	-	-	-	-	-
83	-	-	-	-	-	-	-	-	8.92	-	-	-	-	-	-	-	-	3.70	-	-	-	-	-	-	-	-	-	-
84	-	-	-	-	-	-	-	-	-	8.15	-	-	-	-	17.8	-	-	3.84	-	-	14.5	-	-	-	-	-	-	-
85	-	-	-	-	-	-	-	-	41.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
86	-	-	-	-	-	-	-	-	2.89	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
87	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.2	-	-	-	-	-	-	-	-	-
88	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
89	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.66	-	-	-	-	-	-	-	-	-
90	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.0	-	-	-	-	-	-	-	-	-
91	-	-	-	-	0.0018	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0265	-	-	-	-	-	-	-	-	-
92	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.3	-	-	0.0000	-	-	-	-	-	-
93	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.625	-	-	30.9	-	-	-	-	-	-
94	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.36	-	-	-	-	-	-	-	-	-
95	-	-	-	-	232	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
96	-	-	-	-	12.9	-	-	-	-	-	-	-	-	-	-	-	-	-	1.63	-	-	-	-	-	-	-	-	-
97	-	-	-	-	4.32	-	-	-	-	-	-	-	-	-	-	-	-	-	33.9	-	-	-	-	-	-	-	-	-
98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.4	-	-	-	-	-	-	-	-	-
99	-	-	-	-	-	-	-	-	3.06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
100	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.203	-	10.6	-	-	-	-	-	-	-	-	-
101	-	-	-	-	32.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
102	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
103	-	-	-	-	46.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
104	-	-	-	-	135	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
105	-	-	-	-	246	-	-	-	-	-	-	-	-	-	-	-	-	-	31.2	-	-	-	-	-	-	-	-	-
106	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.8	-	-	0.0909	-	-	-	-	-	-	-	-	-	-
107	-	0.0001	-	-	-	-	-	-	54.4	0.0024	-	-	-	-	-	-	3.11	3.42	-	-	3.47	-	-	-	-	-	-	-
108	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.66	-	-	4.98	-	-	-	-	-	-	-
109	-	-	-	-	-	-	-	-	86.1	5.52	-	-	-	-	-	-	4.98	-	-	-	13.4	-	-	-	-	-	-	-
110	-	0.0834	-	-	-	-	-	-	-	3.97	-	-	-	-	-	-	-	39.6	-	-	2.96	-	-	-	-	-	-	-
111	-	10.2	-	-	-	-	-	-	-	14.4	-	-	-	-	-	-	-	5.58	-	-	3.85	-	-	-	-	-	-	-
112	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.618	-	-	-	-	-	-	-
113	-	-	-	-	-	-	-	-	-	5.40	-	-	-	-	-	-	-	13.1	-	-	53.7	-	-	-	-	-	-	-
114	-	-	-	-	-	-	-	-	-	0.0013	-	-	-	-	-	-	-	-	-	-	14.5	-	-	-	-	-	-	-
115	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.946	-	-	5.94	-	-	-	-	-	-	-
116	-	-	-	-	-	-	-	-	15.4	14.5	-	-	-	-	-	-	-	6.10	-	-	-	-	-	-	-	-	-	-
117	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.0	-	-	15.4	-	-	-	-	-	-	-
118	-	-	-	-	-	-	-	-	-	13.0	-	-	-	-	-	-	-	8.16	-	-	20.1	-	-	-	-	-	-	-
119	-	-	-	-	-	-	-	-	-	7.41	-	-	-	-	-	-	49.0	-	-	-	65.8	-	-	-	-	-	-	-
120	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.171	-	-	14.6	-	-	-	-	-	-	-
121	-	-	-	-	-	-	-	-	-	17.9	-	-	-	-	-	-	-	-	-	-	13.1	-	-	-	-	-	-	-
122	-	-	-	-	-	-	-	-	18.7	4.12	-	-	-	-	-	-	-	-	-	-	11.1	-	-	-	-	-	-	-
123	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.57	-	-	27.1	-	-	-	-	-	-	-
124	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.796	-	-	30.9	-	-	-	-	-	-	-
125	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.14	-	-	13.1	-	-	-	-	-	-	-
126	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0048	-	-	17.3	-	-	-	-	-	-	-
127	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.864	-	-	31.9	-	-	-	-	-	-	-
128	-	13.6	-	-	-	-	-	-	0.198	11.2	0.497	-	-	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-
129	-	10.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.7	-	-	-	-	-	-	-
130	-	-	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
131	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.2	-	5.38	4.33	-	-	-	-	-	-	-	-	-	-
132	-	-	-	-	-	-	-	-	-	3.97	-	-	-	-	9.49	-	-	1.92	-	-	31.7	-	-	-	-	-	-	-
133	-	-	-	-	-	-	-	-	-	4.48	-	-	-	-	39.0	-	-	1.62	-	-	9.65	-	-	-	-	-	-	-
134	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.997	-	-	11.9	-	-	-	-	-	-	-
135	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.12	-	-	16.2	-	-	-	-	-	-	-
136	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.2	-	-	-	-	-	-	-
137	-	-	-	-	-	-	-	-	-	3.10	-	-	-	-	-	-	-	-	-	-	24.6	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
138	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.51	-	-	18.2	-	-	-	-	-	-	-
139	-	-	-	-	-	-	-	-	0.965	21.6	-	-	-	-	25.2	-	0.0000	8.03	-	-	74.2	-	-	-	-	-	-	-
140	-	-	-	-	-	-	-	-	-	2.34	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-	-	-	-
141	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.63	-	-	-	3.52	-	-	-	-	-	-	-
142	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.7	-	-	-	-	-	-	-
143	-	-	-	-	-	-	-	-	-	7.71	-	-	-	5.21	0.421	-	-	-	-	-	59.6	-	-	-	-	-	-	-
144	-	7.10	-	-	-	-	-	-	-	6.70	-	-	-	-	87.5	-	11.2	1.37	-	-	8.90	-	-	-	-	-	-	-
145	-	-	-	-	-	-	-	-	-	1.97	-	-	-	1.85	-	-	-	1.08	-	-	25.7	-	-	-	-	-	-	-
146	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.193	-	-	1.50	-	-	10.9	-	-	-	-	-	-	-
147	-	-	-	-	-	-	-	-	-	12.7	-	-	-	5.45	-	-	5.61	4.51	-	-	8.55	-	-	-	-	-	-	-
148	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.32	-	-	1.84	-	-	1.20	-	-	-	-	-	-	-
149	-	-	-	-	-	-	-	-	-	3.93	-	-	-	-	8.60	-	-	1.45	-	-	3.71	-	-	-	-	-	-	-
150	-	-	-	-	-	-	-	-	-	6.12	-	-	-	-	-	-	18.1	-	-	-	7.23	-	-	-	-	-	-	-
151	-	20.5	-	-	-	-	-	-	0.0019	16.9	-	-	-	-	-	-	-	-	-	-	11.1	-	-	-	-	-	-	-
152	-	4.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0014	-	-	-	21.1	-	-	-	-	-	-	-
153	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.13	-	-	-	-	-	-	-
154	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.14	-	-	-	-	-	-	-
155	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.5	-	-	-	-	-	-	-
156	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.6	-	-	-	-	-	-	-
157	-	-	-	-	-	-	-	-	-	1.41	-	-	-	-	7.11	-	-	-	-	-	6.66	-	-	-	-	-	-	-
158	-	-	3.05	-	-	-	-	-	-	-	18.1	-	8.46	0.503	-	-	0.547	-	-	-	19.2	7.27	0.734	0.604	-	-	-	-
159	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.09	-	-	-	117	8.85	-	-	-	-	-	-
160	-	-	0.592	-	-	-	-	-	-	-	-	-	-	-	-	-	10.7	-	-	-	124	75.1	3.05	0.692	-	-	-	-
161	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.3	0.0007	-	-	-	-	-	-
162	-	-	-	-	-	-	-	-	-	7.97	-	-	-	-	-	-	-	-	11.5	-	40.4	38.4	-	-	-	-	-	-
163	-	-	-	-	-	-	-	-	-	31.5	-	-	-	2.29	-	-	-	3.12	0.0028	-	-	150	-	-	-	-	-	-
164	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	86.3	-	-	-	-	-	-
165	-	-	-	-	-	-	-	-	-	0.107	-	-	-	-	-	-	-	-	-	-	0.0001	63.7	-	-	-	-	-	-
166	-	-	-	-	-	-	-	-	0.0000	5.25	-	-	-	-	-	-	33.7	-	-	-	1.72	83.1	-	-	-	-	-	-
167	-	-	-	-	-	-	-	0.0004	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
168	-	-	-	-	-	-	-	-	31.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
169	-	-	7.40	2.34	-	-	-	-	-	95.6	-	-	-	-	-	-	-	-	-	-	1.26	15.5	-	-	-	-	-	-
170	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	153	-	-	-	-	-	-	-	-	-	-	-
171	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.8	3.88	-	-	-	-	-	-
172	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.8	19.5	-	-	-	-	-	-
173	-	-	-	-	-	-	-	-	-	6.05	-	-	-	-	-	-	-	-	-	-	45.6	24.3	-	-	-	-	-	-
174	-	-	-	-	-	-	-	-	-	2.04	-	-	-	-	-	-	-	-	-	-	-	73.9	-	-	-	-	-	-
175	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.95	-	-	-	4.47	95.6	-	-	-	-	-	-
176	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.7	-	-	-	-	-	-
177	-	-	-	2.41	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.6	-	-	-	-	-	-
178	-	10.8	-	9.13	-	-	-	-	3.31	33.5	-	-	-	-	-	-	1.40	-	-	-	-	44.2	-	2.45	-	-	-	-
179	-	-	-	-	-	-	-	-	-	0.0027	-	-	-	-	-	-	-	-	-	-	54.8	5.35	-	-	-	-	-	-
180	-	-	-	-	-	-	-	-	-	5.54	-	-	-	-	-	-	3.88	-	-	-	2.12	35.0	-	-	-	-	-	-
181	-	-	-	9.14	-	-	-	30.3	36.9	47.3	-	-	-	-	-	-	10.2	-	-	-	-	2.52	3.58	-	-	-	-	-
182	-	-	1.86	-	-	-	-	18.3	4.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
183	-	9.39	3.96	5.10	-	-	-	4.20	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-
184	-	-	0.315	-	-	-	-	-	-	13.5	-	-	-	-	-	-	-	-	-	-	-	9.29	0.115	-	-	-	-	-
185	-	1.50	1.97	-	-	-	-	-	11.1	1.17	-	-	-	-	-	-	-	-	-	-	-	43.3	10.0	-	-	-	-	-
186	-	-	-	3.74	-	-	-	111	2.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
187	-	-	-	-	-	-	-	1.50	19.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
188	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.18	-	-	-	0.0235	40.5	-	-	-	-	-
189	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.94	-	-	-	0.0007	-	34.2	-	-	-	-
190	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.22	-	-	-	0.208	26.0	12.6	-	-	-	-
191	-	3.40	-	21.1	-	-	-	-	-	32.3	-	-	-	-	-	-	-	5.29	-	-	-	-	-	-	-	-	-	-
192	-	1.93	-	6.49	-	-	-	22.9	18.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
193	-	-	-	-	-	-	-	-	-	6.08	-	-	-	-	-	-	-	5.72	-	-	-	0.363	-	29.7	-	-	-	-
194	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.11	-	-	-	0.0027	34.8	0.180	-	-	-	-
195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.91	-	-	-	0.0009	19.1	-	-	-	-	-
196	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.43	-	-	-	0.0428	47.9	0.762	-	-	-	-
197	-	-	-	-	-	-	-	-	-	1.16	-	-	8.55	-	-	-	-	8.37	-	-	-	0.0001	-	21.7	-	-	-	-
198	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.13	0.185	-	2.61	-	-	-	-
199	-	13.7	-	2.64	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
200	-	-	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	-	-	3.09	13.6	-	-	-	-	-	-
201	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	50.6	-	-	-	-	-	-	-
202	-	-	-	-	-	-	-	-	83.7	-	-	-	-	-	-	-	0.0024	0.0062	-	-	-	-	-	-	-	-	-	-
203	-	-	-	-	-	-	-	-	84.9	-	-	-	-	-	-	-	-	2.06	-	-	-	-	-	-	-	-	-	-
204	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.39	-	-	-	-	-	-	-	-	-	-	-	-	-
205	-	-	-	-	-	-	-	-	0.0303	-	-	-	-	-	57.3	-	-	2.81	-	-	-	-	-	-	-	-	-	-
206	-	-	-	-	-	-	-	-	-	-	-	-	-	-	68.2	-	-	11.2	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
207	-	-	-	-	-	-	49.6	-	-	0.146	-	-	-	-	0.146	-	-	5.18	-	-	-	-	-	-	-	-	-	-
208	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.2	-	-	3.79	-	-	-	-	-	-	-	-	-	-
209	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.0	-	-	4.69	-	-	-	-	-	-	-	-	-	-
210	-	0.0009	-	-	-	-	-	-	-	7.41	88.3	-	-	-	4.18	-	-	32.3	-	-	-	-	-	-	-	-	-	-
211	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
212	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98.6	-	-	-	-	-	-	-	-	-	-	-	-	-
213	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.0	-	-	-	-	-	-	-	-	-	-	-	-	-
214	-	4.64	-	-	-	-	-	-	-	10.5	-	-	-	-	17.6	-	-	15.8	-	-	36.1	-	-	-	-	-	-	-
215	-	-	-	-	-	-	-	-	-	-	-	-	-	-	60.3	-	-	2.86	-	-	-	-	-	-	-	-	-	-
216	-	0.0004	-	-	-	-	-	-	-	23.4	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	-	-	-	-	-
217	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93.9	-	-	-	-	23.7	-	-	-	-	-	-
218	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	0.0061	-	-	-	-	-	-	-	0.0058	-	-	-	-	-
219	-	-	-	-	-	-	8.50	-	-	0.0085	-	-	-	-	33.0	-	-	14.2	-	-	5.81	2.77	-	-	-	-	-	-
220	-	-	-	-	-	-	-	-	-	4.34	0.0146	-	-	3.56	46.1	-	-	5.34	-	-	-	-	-	-	-	-	-	-
221	-	7.52	-	-	-	-	-	-	12.2	7.68	20.0	-	-	-	-	-	-	0.0023	-	-	-	-	-	-	-	-	-	-
222	-	51.8	-	-	-	-	-	-	-	18.4	44.9	-	-	24.3	18.7	-	-	0.774	-	-	-	-	-	-	-	-	-	-
223	-	10.6	-	-	-	-	-	-	-	0.0017	0.276	-	-	0.920	-	-	-	3.94	-	-	-	-	-	-	-	-	-	-
224	-	-	-	-	-	-	-	-	22.5	-	-	-	-	-	-	-	-	10.3	-	-	-	-	-	-	-	-	-	-
225	-	-	-	-	-	-	-	-	-	7.55	-	-	-	-	-	-	0.0003	-	-	-	-	48.9	-	-	-	-	-	-
226	-	-	-	-	-	-	-	-	1.99	0.141	-	-	-	-	-	-	30.2	31.8	-	-	7.18	-	-	-	-	-	-	-
227	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0041	-	-	-	-	-	-	0.0015	18.7	-	-	-	-	-
228	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	10.4	-	2.81	-	-	-	-
229	-	-	-	-	-	-	-	-	-	0.780	-	-	-	-	-	-	-	-	-	-	-	0.0015	-	16.7	-	-	-	-
230	-	-	-	-	-	-	-	-	-	37.6	-	-	-	-	-	-	-	-	-	-	-	0.967	-	22.7	-	-	-	-
231	-	61.6	-	0.0852	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
232	-	0.0073	-	-	-	-	-	-	0.0003	-	-	-	-	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-
233	-	0.0019	3.46	-	-	-	-	-	-	36.1	-	-	-	-	-	-	7.16	-	-	-	-	29.4	-	-	-	-	-	-
234	-	-	-	-	-	-	-	-	0.0445	-	-	-	-	-	-	-	6.56	0.0063	-	-	-	45.0	-	-	-	-	-	-
235	-	-	-	-	-	-	-	-	14.1	-	-	-	-	-	-	-	59.3	-	-	-	-	-	-	-	-	-	-	-
236	-	17.7	-	-	-	-	-	-	37.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
237	-	-	1.56	-	-	-	-	-	-	-	-	-	-	-	-	-	42.7	-	-	-	-	57.8	-	-	-	-	-	-
238	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.262	-	-	-	16.5	35.0	-	-	-	-	-	-
239	-	-	-	-	-	-	-	-	-	8.02	-	-	-	-	-	-	73.0	-	-	-	-	61.8	-	-	-	-	-	-
240	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	60.9	-	-	-	-	-	-
241	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	113	45.4	-	-	-	-	-	-
242	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	139	22.7	-	-	-	-	-	-
243	-	-	2.04	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55.8	63.5	-	-	-	-	-	-
244	-	-	-	-	-	-	-	-	-	7.63	-	-	-	-	-	-	-	-	-	-	48.8	131	-	-	-	-	-	-
245	-	-	0.386	-	-	-	-	-	-	3.02	-	-	-	-	-	-	7.93	-	-	-	94.3	96.0	-	-	-	-	-	-
246	-	-	10.2	3.42	-	-	-	-	-	-	0.720	-	-	0.464	-	-	0.110	-	-	-	-	158	-	-	-	-	-	-
247	-	-	2.30	0.794	-	-	-	-	-	-	-	-	-	-	-	-	7.80	-	-	-	102	105	-	-	-	-	-	-
248	-	-	35.4	2.27	-	-	-	-	-	0.0001	23.0	-	-	-	-	-	23.9	-	-	-	2.38	17.0	-	-	-	-	-	-
249	-	-	0.0011	-	-	-	-	-	-	-	31.4	-	-	0.701	-	-	-	-	-	-	-	-	-	-	-	-	-	-
250	-	-	1.37	-	-	-	-	-	-	0.483	15.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
251	-	-	-	-	-	-	-	-	-	-	0.492	-	-	-	-	-	38.6	-	-	-	-	9.51	-	-	-	-	-	-
252	-	-	-	-	-	-	-	0.734	-	8.42	-	-	-	-	-	-	7.56	-	-	-	-	74.9	-	-	-	-	-	-
253	-	-	1.15	1.88	-	-	-	89.7	-	29.1	-	-	-	-	-	-	-	-	-	-	-	11.7	0.901	-	-	-	-	-
254	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.8	-	-	-	-	33.1	-	-	-	-	-	-
255	-	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	-	19.0	-	-	-	-	23.1	2.84	-	-	-	-	-
256	6.02	-	-	0.444	-	-	-	-	-	11.2	2.79	-	-	-	-	-	-	0.0010	-	-	-	6.94	-	-	-	-	-	-
257	-	-	-	-	-	-	-	-	-	2.09	15.2	-	-	-	-	-	13.3	-	-	-	11.9	29.8	-	-	-	-	-	-
258	-	-	-	-	-	-	-	49.0	-	-	-	-	-	3.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-
259	-	-	-	-	-	-	-	4.09	-	0.0013	-	-	-	-	6.52	-	-	-	-	-	-	-	-	-	-	-	-	-
260	-	-	-	-	-	-	-	-	-	0.0724	-	-	0.0104	-	-	-	-	218	-	-	-	-	-	-	-	-	-	-
261	-	-	-	-	-	-	-	-	-	-	-	-	61.5	-	-	-	-	3.23	-	-	-	-	-	-	-	-	-	-
262	-	3.44	-	-	-	-	-	-	5.93	12.0	4.03	-	-	-	-	-	0.222	-	-	-	-	97.0	-	-	-	-	-	-
263	-	-	-	-	-	-	-	0.518	0.0000	12.8	12.2	-	-	-	-	-	-	-	-	-	0.0001	114	-	-	-	-	-	-
264	-	0.0014	-	-	-	-	-	7.25	-	52.1	17.0	-	-	-	-	-	20.1	-	-	-	-	-	-	-	-	-	-	-
265	-	-	4.23	0.102	-	-	-	-	-	18.9	-	-	-	-	-	-	-	3.28	-	-	-	14.9	-	-	-	-	-	-
266	-	-	-	-	-	-	-	-	-	7.41	-	-	-	-	-	-	-	-	-	-	-	25.5	-	-	-	-	-	-
267	-	0.0205	0.449	-	-	-	-	-	-	34.1	-	-	-	-	-	-	-	0.502	-	-	-	24.2	-	10.4	-	-	-	-
268	-	21.2	-	-	-	-	-	-	-	0.0004	-	-	23.3	-	10.5	-	-	-	-	-	-	-	-	-	-	-	-	-
269	-	30.4	-	-	-	-	-	-	-	35.8	-	-	5.07	-	-	-	3.21	-	-	-	0.0002	5.08	-	-	-	-	-	-
270	-	-	-	-	-	-	-	-	-	-	0.0003	-	14.1	-	-	-	-	2.82	-	-	0.0000	6.83	-	-	-	-	-	-
271	-	0.0711	-	-	-	-	-	-	-	46.3	-	-	-	-	-	-	-	-	-	-	0.0001	5.82	17.4	1.15	-	-	-	-
272	-	17.2	-	-	-	-	-	36.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
273	-	-	-	-	-	-	-	8.37	-	-	-	-	-	-	-	-	-	14.7	-	-	-	-	-	-	-	-	-	-
274	-	-	-	-	-	-	-	49.9	0.0004	0.0008	0.0006	-	39.9	-	-	-	-	4.41	-	-	-	-	-	-	-	-	-	-
275	-	-	-	-	-	-	-	3.42	0.0000	0.0053	-	13.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
276	-	-	12.3	-	-	-	-	0.548	0.0079	0.0842	24.0	-	-	14.1	65.0	-	24.5	-	-	-	-	7.62	-	-	-	-	-	-
277	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.2	-	-	-	-	-	-	-	-	-	-	-	-	-
278	-	-	-	-	-	-	-	26.3	0.0022	-	-	0.0010	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-
279	-	0.0003	-	0.370	-	-	-	-	-	-	-	-	6.43	-	-	-	0.0000	-	-	-	0.0006	45.3	3.26	1.62	-	-	-	-
280	-	-	5.05	-	-	-	-	-	5.86	0.430	-	-	-	-	-	-	3.54	-	-	-	-	88.3	-	-	-	-	-	-
281	-	-	-	-	-	-	-	-	26.4	-	-	-	-	-	-	-	8.69	-	-	-	-	12.2	-	-	-	-	-	-
282	-	-	-	-	-	-	-	-	-	14.4	-	-	-	-	-	-	-	-	-	-	-	14.6	-	-	-	-	-	-
283	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	18.0	-	-	-	0.308	49.7	-	-	-	-	-	-
284	-	21.2	-	-	4.03	-	-	0.0037	5.37	13.5	-	-	-	-	-	-	18.7	-	-	-	5.98	31.4	-	-	-	-	-	-
285	-	-	-	-	-	-	-	-	-	1.08	-	-	-	-	-	-	16.4	-	-	-	13.4	90.2	-	-	-	-	-	-
286	16.2	7.97	-	-	-	-	-	-	3.60	22.4	-	-	-	-	-	-	1.54	-	-	-	-	27.4	-	-	-	-	-	-
287	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.40	-	-	-	-	-	-
288	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.1	-	-	-	3.70	20.9	-	-	-	-	-	-
289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.50	-	-	-	24.6	21.5	-	-	-	-	-	-
290	-	-	-	-	-	-	-	-	-	16.3	-	-	-	-	-	-	0.0003	-	-	-	-	74.9	-	-	-	-	-	-
291	7.16	-	-	-	-	-	-	-	-	33.1	-	-	-	-	-	-	2.62	-	-	-	-	-	-	-	-	-	-	-
292	4.88	-	-	-	-	-	-	-	-	16.8	-	-	-	-	-	-	3.32	-	-	-	-	67.1	-	-	-	-	-	-
293	-	-	-	-	-	-	-	-	38.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
294	21.4	-	-	-	-	-	-	-	-	8.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
295	3.68	-	-	-	-	-	-	-	-	16.6	-	-	-	-	-	-	-	-	-	-	-	14.2	-	-	-	-	-	-
296	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.1	-	-	-	-	12.8	-	-	-	-	-	-
297	0.973	-	0.0637	19.7	-	-	-	-	10.7	11.3	7.14	-	-	-	-	-	13.9	-	-	-	-	87.6	-	-	-	-	-	-
298	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.0	-	-	-	-	-	-
299	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.0	-	-	-	-	41.4	-	-	-	-	-	-
300	17.7	-	-	-	-	-	-	-	-	0.368	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
301	-	-	-	-	-	-	-	-	-	9.62	-	-	-	-	-	-	6.17	-	-	-	5.78	64.0	-	-	-	-	-	-
302	3.45	-	-	-	-	-	-	-	-	31.6	-	-	-	-	-	-	5.67	-	-	-	-	17.6	-	-	-	-	-	-
303	-	-	-	-	-	-	-	-	-	15.7	1.71	-	-	-	-	-	14.3	-	-	-	-	43.7	-	-	-	-	-	-
304	5.70	-	-	-	-	-	-	-	-	19.1	-	-	-	-	-	-	2.71	-	-	-	-	34.8	-	-	-	-	-	-
305	-	-	7.54	-	-	-	-	-	0.731	14.4	19.3	-	-	-	2.40	-	1.43	-	-	-	18.8	44.2	-	-	-	-	-	-
306	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.0	-	-	50.5	7.56	0.378	38.0	-	-	-	-
307	-	10.4	0.996	-	-	-	-	-	-	7.28	-	-	-	-	-	-	-	4.42	-	-	-	0.0163	-	60.6	-	-	-	-
308	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-	-	-	-	-	0.0010	12.5	-	-	-	-	-
309	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.26	24.4	-	-	-	-	-	-
310	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.66	-	-	16.3	0.0008	-	19.7	-	-	-	-
311	-	-	2.43	-	-	-	-	-	-	-	-	-	-	-	-	-	9.05	-	-	-	-	96.7	28.2	7.98	-	-	-	-
312	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0035	54.1	-	-	-	-	-
313	-	-	-	-	-	-	-	-	-	6.81	9.79	-	-	-	-	-	-	-	-	-	-	0.0060	69.8	-	-	-	-	-
314	-	-	0.0000	-	-	-	-	-	-	0.0001	1.58	-	-	-	-	-	-	15.3	-	-	-	0.334	65.6	-	-	-	-	-
315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.2	-	-	0.0017	1.03	61.1	8.63	-	-	-	-
316	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.54	-	-	-	1.02	83.1	16.7	-	-	-	-
317	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	0.726	35.2	55.1	-	-	-	-
318	-	0.0003	-	-	-	-	-	-	-	4.61	-	-	-	-	-	-	-	29.5	-	-	-	0.0073	106	6.28	-	-	-	-
319	-	-	-	-	-	-	-	-	-	6.07	-	-	-	-	-	-	-	-	-	-	-	0.0959	107	5.11	-	-	-	-
320	-	-	-	-	-	-	-	-	-	1.89	-	-	-	-	-	-	-	-	-	-	-	30.1	-	-	-	-	-	-
321	-	-	1.07	-	-	-	-	-	-	26.9	-	-	-	-	-	-	3.02	-	-	-	2.54	78.6	-	-	-	-	-	-
322	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	57.3	1.93	-	-	-	-	-	-
323	-	-	-	-	-	-	-	-	-	23.3	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-
324	-	-	-	-	-	-	-	-	-	1.55	-	-	-	-	-	-	13.9	-	-	-	-	54.9	-	-	-	-	-	-
325	-	-	0.573	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	8.10	-	-	-	99.8	73.1	-	-	-	-	-	-
326	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.05	-	-	-	62.5	55.4	-	-	-	-	-	-
327	-	-	-	-	-	-	-	-	-	8.75	-	-	-	-	-	-	24.6	8.22	-	-	51.8	102	33.8	18.7	-	-	-	-
328	-	-	-	-	-	-	-	-	-	21.9	-	-	-	-	-	-	-	-	-	-	-	92.7	-	-	-	-	-	-
329	-	-	0.618	2.65	-	-	-	-	-	8.27	-	-	-	-	-	-	1.04	-	-	-	0.573	92.8	-	-	-	-	-	-
330	20.1	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	1.01	-	-	-	0.0000	14.7	-	-	-	-	-	-
331	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	4.09	68.2	-	-	-	-	-	-
332	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.49	-	-	-	-	53.9	-	-	-	-	-	-
333	-	-	8.27	-	-	-	-	-	-	24.1	-	-	-	-	-	-	0.0001	-	-	-	5.37	107	-	-	-	-	-	-
334	-	-	2.01	-	-	-	-	-	-	28.1	-	-	-	-	-	-	3.33	-	-	-	-	29.4	-	-	-	-	-	-
335	-	-	0.937	-	-	-	-	-	-	11.6	-	-	-	-	-	-	0.0001	-	-	-	15.2	6.88	-	-	-	-	-	-
336	0.0047	-	-	-	-	-	-	-	-	7.88	-	-	-	-	-	-	6.84	-	-	-	16.9	26.6	-	-	-	-	-	-
337	-	6.11	0.0004	0.762	-	-	-	-	-	4.13	-	-	-	-	-	-	-	0.307	-	-	-	8.36	85.8	26.0	-	-	-	-
338	-	0.0001	-	-	-	-	-	-	-	28.7	-	-	0.284	-	-	-	-	7.23	-	-	0.0003	2.01	34.2	4.36	-	-	-	-
339	-	11.3	0.0349	4.10	-	-	-	-	-	12.5	-	-	-	-	-	-	-	-	-	-	-	0.0010	20.8	-	-	-	-	-
340	-	-	-	-	-	-	-	-	-	1.91	-	-	-	-	-	-	20.9	-	-	-	-	19.8	-	-	-	-	-	-
341	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77.7	-	-	-	-	-	-
342	-	-	-	1.04	-	-	-	-	-	0.234	2.83	-	-	-	-	-	22.7	-	-	-	-	87.6	0.415	-	-	-	-	-
343	-	0.0003	0.572	-	-	-	-	-	-	13.5	0.0000	-	0.927	-	-	1.22	-	-	-	-	-	0.793	5.65	39.5	-	-	-	-
344	-	0.385	4.73	-	-	-	-	-	-	15.1	1.11	-	9.75	-	-	-	-	0.0308	-	-	-	0.0061	58.6	1.16	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
345	-	-	-	-	-	-	-	-	-	20.9	-	-	-	-	44.7	-	0.0059	7.61	-	-	91.4	21.3	-	-	-	-	-	-
346	-	9.48	-	-	-	-	-	-	-	15.9	-	-	-	-	-	-	4.44	4.37	-	-	9.18	-	-	-	-	-	-	-
347	-	0.0075	-	-	-	-	-	-	-	8.10	-	-	-	-	-	-	-	16.1	-	-	96.8	-	-	-	-	-	-	-
348	-	-	12.5	3.94	-	-	-	-	-	-	0.802	-	17.0	0.0001	-	-	7.49	-	-	-	-	15.4	-	-	-	-	-	-
349	-	-	0.332	3.79	-	-	-	-	-	-	5.00	-	-	-	-	-	17.5	-	-	-	-	7.54	6.83	-	-	-	-	-
350	-	-	-	3.94	-	-	-	-	-	-	4.48	-	-	-	-	-	0.0004	-	-	-	-	27.1	2.07	-	-	-	-	-
351	-	-	15.6	36.5	-	-	-	-	-	0.151	10.2	-	-	-	5.34	-	-	0.564	-	-	-	19.8	-	-	-	-	-	-
352	-	-	-	-	-	-	-	-	-	15.1	10.9	-	-	-	-	-	-	-	-	-	-	48.2	5.19	-	-	-	-	-
353	-	-	-	-	-	-	-	-	-	-	0.0952	-	-	-	-	-	-	-	-	-	-	58.5	-	-	-	-	-	-
354	-	-	-	-	-	-	-	-	-	-	1.60	-	-	-	-	-	-	-	-	-	-	64.7	-	-	-	-	-	-
355	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.79	-	-	-	-	169	-	-	-	-	-	-
356	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	29.0	-	-	-	-	-	-
357	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.5	-	-	-	-	-	-
358	-	-	-	-	-	-	-	-	-	5.85	-	-	-	-	-	-	-	-	-	-	-	22.3	-	-	-	-	-	-
359	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	6.32	-	-	-	-	-	-
360	-	-	-	-	-	-	-	-	-	6.57	-	-	-	-	-	-	0.0000	-	-	-	-	54.0	-	-	-	-	-	-
361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.9	0.309	-	-	-	-	-
362	-	0.839	1.53	-	-	-	-	-	0.0001	15.7	-	-	-	-	-	-	-	-	-	-	-	73.8	-	-	-	-	-	-
363	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.140	64.6	-	-	-	-	-
364	-	24.1	0.0026	6.71	-	-	-	4.93	-	8.28	25.9	-	5.57	-	-	-	-	-	-	-	-	0.0000	-	0.692	-	-	-	-
365	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.26	-	-	64.1	0.0030	-	10.3	-	-	-	-
366	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	9.08	-	-	-	0.0002	24.0	-	-	-	-	-	-
367	-	0.0008	-	17.7	-	-	-	108	0.0225	0.0009	5.48	-	-	20.0	29.3	-	-	-	-	-	-	-	-	-	-	-	-	-
368	-	0.0556	-	-	-	-	-	1.06	-	0.0009	17.7	-	15.5	4.65	0.0995	-	-	2.84	-	-	12.3	0.0510	59.9	22.1	-	-	-	-
369	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.28	-	-	1.44	-	-	4.94	5.04	-	-	-	-	-	-
370	-	-	0.888	3.30	-	-	-	-	7.21	4.40	14.1	-	-	-	11.6	-	2.69	1.74	-	-	0.0649	60.5	-	-	-	-	-	-
371	-	-	-	-	14.5	-	-	-	4.11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
372	-	-	-	-	-	-	-	-	24.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
373	-	-	-	-	-	-	-	-	75.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
374	-	4.19	-	-	-	-	-	-	-	23.3	-	-	-	-	-	-	-	-	-	-	13.6	-	-	-	-	-	-	-
375	-	0.453	-	-	-	-	-	-	-	6.74	-	-	-	-	-	-	0.0022	9.12	-	-	35.0	-	-	-	-	-	-	-
376	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.79	0.0000	-	-	12.3	-	-	-	-	-	-	-
377	-	-	-	-	-	-	-	-	-	23.9	-	-	-	-	-	-	-	5.14	-	-	4.34	-	-	-	-	-	-	-
378	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.5	-	-	-	-	-	-	-
379	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	96.7	-	-	2.28	-	-	-	-	-	-	-	-	-	-
380	-	30.2	-	-	-	-	-	-	12.4	21.3	-	-	-	-	13.2	-	-	3.31	-	-	40.3	-	-	-	-	-	-	-
381	-	-	-	-	-	-	-	-	-	32.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
382	-	-	-	-	-	-	-	-	88.7	0.269	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
383	-	-	-	-	-	-	-	-	-	10.2	-	-	-	-	-	-	4.39	-	-	-	27.7	14.2	-	-	-	-	-	-
384	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.5	56.7	-	-	-	-	-	-
385	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	-	-	9.02	-	-	-	-	-	-	-
386	-	-	-	-	-	-	-	-	-	3.48	-	-	-	-	-	-	19.5	-	-	-	19.1	-	-	-	-	-	-	-
387	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.4	-	-	-	0.367	47.4	-	-	-	-	-	-
388	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.0	-	-	-	-	-	-	-
389	-	55.2	-	-	-	-	-	-	0.0151	-	-	-	-	-	-	-	-	-	-	-	2.62	-	-	-	-	-	-	-
390	-	12.9	0.943	3.35	-	-	-	-	-	1.98	5.61	-	-	-	0.0063	-	-	5.87	-	-	-	0.0008	-	23.5	-	-	-	-
391	-	-	-	-	-	-	-	-	18.1	18.9	-	-	-	-	-	-	15.1	-	-	-	-	-	-	-	-	-	-	-
392	-	0.0017	-	-	-	-	-	-	-	38.4	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-
393	-	-	-	-	-	-	-	-	42.0	11.1	-	-	-	-	-	-	-	1.27	-	-	13.6	-	-	-	-	-	-	-
394	-	6.32	-	-	-	-	-	-	6.76	11.2	-	-	-	-	-	-	0.0002	2.66	-	-	68.0	-	-	-	-	-	-	-
395	-	15.0	-	-	-	-	-	-	-	8.03	-	-	-	-	-	-	8.45	4.62	-	-	82.6	-	-	-	-	-	-	-
396	-	-	-	-	-	-	-	-	2.19	22.2	11.1	-	-	-	-	-	-	0.429	-	-	4.43	-	-	-	-	-	-	-
397	-	-	-	-	0.0138	-	-	-	-	-	-	-	-	-	-	-	-	0.0049	-	-	32.9	0.0197	-	-	-	-	-	-
398	-	-	-	-	0.0029	-	-	-	-	2.51	-	-	-	-	-	-	-	0.0322	-	-	65.9	0.0018	-	-	-	-	-	-
399	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
400	-	-	-	-	-	-	-	-	-	0.684	-	-	-	-	-	-	-	12.0	-	-	35.5	-	-	-	-	-	-	-
401	-	-	-	-	-	-	-	-	-	18.0	-	-	-	-	6.69	-	-	-	-	-	4.76	-	-	-	-	-	-	-
402	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.3	-	-	41.8	-	-	-	-	-	-	-
403	-	-	-	-	-	-	-	-	25.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
404	-	-	-	-	-	-	-	-	32.2	-	-	-	-	-	-	-	-	5.08	-	-	-	-	-	-	-	-	-	-
405	-	-	-	-	-	-	-	-	23.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
406	-	17.1	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-	53.3	-	-	-	-	-	-	-
407	-	22.0	-	-	-	-	-	-	-	50.0	-	-	-	-	-	-	0.0134	-	-	-	207	-	-	-	-	-	-	-
408	-	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	-	-	17.2	-	-	96.3	-	-	-	-	-	-	-
409	-	3.76	-	-	-	-	-	-	-	18.5	-	-	-	-	25.3	-	-	4.87	-	-	59.1	-	-	-	-	-	-	-
410	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.2	-	-	-	-	-	-	-	-	-	-	-	-	-
411	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76.9	-	-	-	-	-	28.8	-	-	-	-	-	-	-
412	-	-	-	-	-	-	-	-	255	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
413	-	-	-	-	-	-	-	-	111	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
414	-	15.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
415	-	21.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.63	-	-	-	-	-	-	-	-	-	-
416	-	-	-	-	-	-	137	-	-	-	-	-	-	-	12.4	-	-	1.70	-	-	-	-	-	-	-	-	-	-
417	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	-	-	19.1	-	-	-	-	-	-	-	-	-	-
418	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.31	-	-	1.72	-	-	-	-	-	-	-	-	-	-
419	-	-	-	-	-	-	-	-	-	2.29	-	-	-	-	47.1	-	-	24.4	-	-	5.19	-	-	-	-	-	-	-
420	-	-	-	-	-	-	-	-	-	16.2	-	-	-	-	10.7	-	-	2.14	-	-	3.95	5.79	-	-	-	-	-	-
421	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.0	-	-	0.349	-	-	-	-	-	-	-	-	-	-
422	-	-	-	-	-	-	-	-	112	-	-	-	-	-	1.63	-	-	22.3	-	-	-	-	-	-	-	-	-	-
423	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.905	-	-	23.6	-	-	-	-	-	-	-
424	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.3	-	-	-	-	-	-	-
425	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-	-	-	-
426	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.9	-	-	-	-	-	-	-
427	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.86	-	-	19.3	-	-	-	-	-	-	-
428	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.0	-	-	-	14.4	-	-	-	-	-	-	-
429	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	-	-	-	-	-	-	-
430	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.309	-	-	6.32	-	-	-	-	-	-	-
431	-	-	-	-	-	-	-	-	0.396	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
432	-	4.21	-	-	-	-	-	-	93.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
433	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	38.5	-	-	14.9	-	-	4.14	9.80	-	-	-	-	-	-
434	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	38.4	82.8	-	-	-	-	-	-
435	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.116	-	-	-	19.4	74.4	-	-	-	-	-	-
436	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.18	-	-	-	-	-	-
437	-	-	0.297	5.49	-	-	-	-	-	10.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
438	4.25	-	-	-	-	-	-	-	-	22.4	-	-	-	-	-	-	5.74	-	-	-	46.3	66.2	-	-	-	-	-	-
439	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90.1	-	-	-	-	-	-	-
440	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52.8	28.4	-	-	-	-	-	-
441	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	101	13.3	-	-	-	-	-	-
442	-	-	-	-	-	-	-	-	-	12.9	-	-	-	-	-	-	-	-	-	-	20.9	40.3	-	-	-	-	-	-
443	5.64	-	-	-	-	-	-	-	-	96.2	-	-	-	-	-	-	-	-	-	-	5.44	32.8	-	-	-	-	-	-
444	-	-	-	-	-	-	-	-	-	9.01	-	-	-	-	-	-	-	-	-	-	11.8	27.6	-	-	-	-	-	-
445	-	-	-	-	-	-	-	-	-	24.0	-	-	-	-	-	-	-	-	-	-	29.0	24.6	-	-	-	-	-	-
446	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44.4	-	-	-	-	-	-	-	-	-
447	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
448	-	-	-	-	87.9	-	-	-	3.60	-	-	-	-	-	-	-	0.0026	-	54.1	-	0.0000	-	-	-	-	-	-	-
449	-	-	0.932	-	1.58	-	-	-	-	-	-	-	-	-	-	-	-	-	17.4	-	-	-	-	-	-	-	-	-
450	-	-	-	-	-	-	-	-	-	0.854	-	-	-	-	-	-	-	-	4.77	4.00	-	270	-	-	-	-	-	-
451	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	2.50	0.0017	119	-	-	-	-	-	-
452	-	-	-	-	-	-	-	-	-	-	-	-	-	1.71	-	-	0.0254	1.41	-	13.3	-	67.1	-	-	-	-	-	-
453	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.9	14.6	-	-	-	-	-	-
454	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	28.2	-	-	-	-	-	-
455	18.4	-	-	-	-	-	-	-	-	12.2	10.6	-	-	-	-	-	5.69	-	-	-	-	1.60	-	-	-	-	-	-
456	-	-	-	-	-	-	-	-	-	16.6	0.0000	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-	-	-	-
457	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
458	-	-	-	-	-	-	-	-	55.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
459	-	-	-	-	21.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
460	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	-	-	-	-
461	-	-	-	-	3.59	-	-	-	-	-	-	-	-	-	-	-	-	-	69.0	-	-	-	-	-	-	-	-	-
462	-	-	-	-	1.40	-	85.7	-	-	-	-	-	-	-	-	-	-	-	7.80	-	-	-	-	-	-	-	-	-
463	-	-	0.216	-	0.612	-	-	-	-	-	-	-	-	-	-	-	-	-	0.433	0.0000	6.68	-	-	-	-	-	-	-
464	-	-	-	-	0.0338	-	-	-	-	-	-	-	-	-	-	-	-	-	1.19	-	10.8	-	-	-	-	-	-	-
465	-	-	-	-	0.620	-	-	-	-	-	-	-	-	-	-	-	-	-	73.4	-	-	-	-	-	-	-	-	-
466	-	0.0105	-	-	-	-	-	-	1.27	-	-	-	-	-	12.1	-	2.99	-	-	-	-	-	-	-	-	-	-	-
467	-	-	-	-	1.00	-	-	-	-	-	-	-	-	-	-	-	-	4.53	-	-	20.5	0.0017	-	-	-	-	-	-
468	-	-	9.83	-	-	-	32.6	-	-	0.778	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-
469	-	-	0.0001	-	-	-	21.9	-	-	16.8	-	-	-	-	-	-	13.1	-	-	0.0000	21.7	9.32	-	-	-	-	-	-
470	-	-	-	-	-	-	-	-	-	1.81	-	-	-	-	-	-	-	2.16	-	-	2.04	-	-	-	-	-	-	-
471	6.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
472	9.85	-	-	-	14.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
473	-	-	-	-	40.3	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0086	2.14	-	-	-	-	-	-	-	-
474	-	-	-	-	13.2	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0054	0.548	-	-	-	-	-	-	-	-
475	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0072	13.1	-	-	-	-	-	-	-	-
476	-	-	-	-	0.0028	-	-	-	-	-	-	-	-	-	-	-	-	-	0.228	41.7	-	-	-	-	-	-	-	-
477	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0486	-	0.0048	26.7	-	2.72	-	-	-	-	-	-
478	-	-	-	-	27.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
479	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
480	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.31	-	-	-	36.5	-	-	-	-	-	-	-
481	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.25	-	-	-	-	38.6	-	-	-	-	-	-
482	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	12.3	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
483	29.1	-	-	-	-	-	-	-	-	9.46	-	-	-	-	-	-	0.960	-	-	-	-	19.7	-	-	-	-	-	-
484	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0018	-	-	7.23	-	-	-	-	-	-
485	-	-	-	-	-	-	-	-	-	8.81	-	-	-	-	-	-	-	2.02	0.0000	-	-	0.344	-	-	-	-	-	-
486	-	-	-	-	-	-	-	-	-	0.0008	-	-	-	-	-	-	-	0.448	-	-	-	9.85	-	-	-	-	-	-
487	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-
488	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.89	-	-	18.6	-	0.0000	-	-	-	-	-	-
489	-	-	-	-	-	-	-	-	-	0.0004	-	-	-	-	-	-	0.0021	-	-	23.1	-	7.01	-	-	-	-	-	-
490	-	-	-	-	0.183	-	-	-	-	-	-	-	-	-	-	-	0.0001	5.96	-	-	-	46.2	-	-	-	-	-	-
491	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.3	-	-	-	-	2.27	-	-	-	-	-	-
492	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.1	0.0001	-	-	0.720	-	-	-	-	-	-
493	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.4	-	-	-	-	-	-
494	-	-	-	-	0.0147	-	-	-	-	-	-	-	-	-	-	-	-	10.7	-	-	-	61.4	-	-	-	-	-	-
495	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.49	-	-	-	23.4	-	-	-	-	-	-
496	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0020	-	-	-	-	13.4	-	-	-	-	-	-
497	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.414	-	-	-	13.1	-	-	-	-	-	-
498	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	0.0038	-	-	-	16.5	-	-	-	-	-	-
499	0.0008	5.58	0.591	-	-	-	-	-	-	2.33	-	-	-	-	-	-	0.0270	-	0.0430	-	-	11.0	-	-	-	-	-	-
500	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.6	0.132	-	-	3.71	-	-	-	-	-	-
501	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0398	-	0.154	6.49	-	23.6	-	-	-	-	-	-
502	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0063	-	-	-	-	31.4	-	-	-	-	-	-
503	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	0.549	-	-	-	23.6	-	-	-	-	-	-
504	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	6.48	-	-	-	17.9	-	-	-	-	-	-
505	-	-	-	-	-	-	-	-	-	5.70	-	-	-	-	-	-	-	-	-	-	-	9.40	-	-	-	-	-	-
506	-	-	-	-	-	-	-	-	-	6.71	-	-	-	-	-	-	-	0.0002	0.0284	-	-	7.64	-	-	-	-	-	-
507	-	-	-	-	-	-	-	-	-	16.7	-	-	-	-	-	-	-	-	-	-	-	1.59	-	-	-	-	-	-
508	-	-	0.197	-	-	-	-	-	-	35.9	-	-	-	-	-	-	1.28	4.11	0.0317	-	-	-	-	-	-	-	-	-
509	-	-	-	-	0.0057	-	42.0	-	-	-	-	-	-	-	-	-	7.27	-	-	-	-	-	-	-	-	-	-	-
510	-	-	-	-	1.42	-	31.6	-	-	-	-	-	-	-	-	-	-	0.0046	0.256	-	-	-	-	-	-	-	-	-
511	1.71	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.8	-	-	0.0001	-	-	-	-	-	-
512	-	-	-	-	-	-	-	-	115	-	-	-	-	-	-	-	18.7	-	-	-	-	-	-	-	-	-	-	-
513	-	0.442	-	-	-	-	-	-	3.89	1.69	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
514	-	-	-	-	-	-	-	-	-	5.02	-	-	-	-	-	-	-	92.6	-	-	-	-	-	-	-	-	-	-
515	-	-	-	-	-	-	-	-	-	5.46	-	-	-	-	4.82	-	-	14.0	-	-	10.00	-	-	-	-	-	-	-
516	-	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	-	8.04	-	-	20.3	-	-	-	-	-	-	-
517	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0029	9.31	-	-	14.9	-	-	-	-	-	-	-
518	-	-	-	-	-	-	-	-	-	4.92	-	-	-	-	-	-	0.0003	1.92	-	-	12.2	-	-	-	-	-	-	-
519	-	-	-	-	-	-	-	-	-	5.96	-	-	-	-	-	-	9.71	-	-	-	30.9	-	-	-	-	-	-	-
520	-	-	-	-	-	-	-	-	-	3.84	-	-	-	-	-	-	-	-	-	-	20.9	-	-	-	-	-	-	-
521	-	-	-	-	-	-	-	-	-	9.74	-	-	-	-	-	-	0.0065	-	-	-	28.5	-	-	-	-	-	-	-
522	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.1	-	-	-	36.2	-	-	-	-	-	-	-
523	-	-	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	-	-
524	-	-	-	-	-	-	-	-	-	0.339	-	-	-	-	-	-	-	-	-	-	27.7	-	-	-	-	-	-	-
525	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.6	-	-	-	-	-	-	-
526	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.7	-	-	-	-	-	-	-
527	-	-	-	-	-	-	-	-	-	0.0034	-	-	-	-	-	-	-	-	-	-	36.2	-	-	-	-	-	-	-
528	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-	-	0.833	-	-	4.83	-	-	-	-	-	-	-
529	-	-	-	-	-	-	-	-	-	1.76	-	-	-	-	-	-	-	3.67	-	-	36.5	-	-	-	-	-	-	-
530	-	-	-	-	-	-	-	-	-	1.30	-	-	-	-	-	-	-	0.333	-	-	12.0	-	-	-	-	-	-	-
531	-	-	-	-	0.225	-	-	-	-	3.64	-	-	-	-	-	-	9.51	2.99	-	-	36.2	-	-	-	-	-	-	-
532	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.63	-	-	14.0	-	-	-	-	-	-	-
533	-	-	-	-	-	-	-	-	-	1.32	-	-	-	-	-	-	-	2.62	-	-	10.7	-	-	-	-	-	-	-
534	-	-	-	-	0.110	-	-	-	-	5.34	-	-	-	-	-	-	-	24.7	-	-	-	-	-	-	-	-	-	-
535	-	2.36	-	-	-	-	-	-	22.6	-	-	-	-	-	4.71	-	-	-	-	-	-	-	-	-	-	-	-	-
536	-	-	-	-	-	-	-	-	28.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
537	-	24.8	-	-	-	-	-	-	7.67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
538	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.41	-	-	-	-	-	-	-	-	-	-	-	-	-
539	-	-	-	-	-	-	-	-	14.1	6.61	-	-	-	-	-	-	-	0.370	-	-	0.0811	-	-	-	-	-	-	-
540	-	-	-	-	-	-	-	-	-	6.03	-	-	-	-	-	-	-	-	-	-	0.0689	-	-	-	-	-	-	-
541	-	-	-	-	-	-	-	-	-	17.4	-	-	-	-	-	-	-	1.86	-	-	21.3	-	-	-	-	-	-	-
542	-	1.61	-	-	-	-	-	-	-	8.75	-	-	-	-	15.3	-	0.515	-	-	-	1.48	-	-	-	-	-	-	-
543	-	-	-	-	-	-	-	-	5.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
544	-	-	-	-	-	-	-	-	3.89	-	-	-	-	-	10.5	-	-	-	-	-	-	-	-	-	-	-	-	-
545	-	-	-	-	-	-	-	-	3.42	2.62	-	-	-	-	3.70	-	-	-	-	-	-	-	-	-	-	-	-	-
546	-	-	-	-	-	-	-	-	0.555	-	-	-	-	-	22.8	-	-	-	-	-	-	-	-	-	-	-	-	-
547	-	-	-	-	-	-	-	-	1.70	-	-	-	-	-	19.6	-	-	-	-	-	-	-	-	-	-	-	-	-
548	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.6	-	-	-	-	-	-	-	-	-	-	-	-	-
549	-	-	-	-	-	-	-	-	0.708	11.6	-	-	-	-	-	-	5.04	0.362	-	-	-	-	-	-	-	-	-	-
550	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.98	-	-	-	-	-	-	-	-	-	-	-	-	-
551	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
552	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.6	-	-	-	-	-	-	-	-	-	-	-	-	-
553	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.3	-	-	-	-	-	-	-	-	-	-	-	-	-
554	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.27	-	0.0001	-	-	-	6.40	-	-	-	-	-	-	-
555	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.41	-	-	-	-	-	16.1	-	-	-	-	-	-	-
556	-	-	-	-	-	-	-	-	-	0.142	-	-	-	-	9.01	-	-	-	-	-	-	-	-	-	-	-	-	-
557	-	-	-	-	-	-	-	-	-	1.93	-	-	-	-	-	-	0.0038	1.72	-	-	33.3	-	-	-	-	-	-	-
558	-	-	-	-	-	-	-	-	-	6.16	-	-	-	-	-	-	35.8	5.46	-	-	-	-	-	-	-	-	-	-
559	-	-	-	-	-	-	-	-	-	3.56	-	-	-	-	-	-	-	13.8	-	-	59.9	-	-	-	-	-	-	-
560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.98	-	-	-	43.2	-	-	-	-	-	-	-
561	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
562	-	-	-	-	-	-	-	-	-	5.07	-	-	-	-	-	-	-	-	-	-	18.9	-	-	-	-	-	-	-
563	-	-	-	-	-	-	-	-	-	24.9	-	-	-	-	-	-	-	-	-	-	59.0	-	-	-	-	-	-	-
564	-	-	-	-	0.0738	-	-	-	-	3.44	-	-	-	-	-	-	-	4.50	-	-	36.1	-	-	-	-	-	-	-
565	-	-	-	-	0.521	-	-	-	-	0.971	-	-	-	-	-	-	-	3.07	-	-	21.1	0.0803	-	-	-	-	-	-
566	-	-	-	-	-	-	-	-	26.3	8.76	-	-	-	-	-	-	0.0203	-	-	-	44.0	-	-	-	-	-	-	-
567	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
568	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.13	-	-	6.11	-	-	-	-	-	-	-
569	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.5	-	-	-	-	-	-	-	-	-	-	-	-	-
570	-	-	-	-	25.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
571	-	-	-	-	0.160	-	-	-	-	-	-	-	-	-	-	-	-	-	0.152	-	-	5.41	-	-	-	-	-	-
572	-	-	-	-	1.97	-	15.8	-	-	32.5	-	-	-	-	-	-	-	-	0.0102	-	-	0.493	-	-	-	-	-	-
573	-	-	-	-	-	-	8.56	-	-	43.4	-	-	-	-	-	-	1.05	-	0.0047	-	-	-	-	-	-	-	-	-
574	2.12	-	-	-	-	-	-	-	-	5.28	-	-	-	-	-	-	-	-	10.4	-	-	50.8	-	-	-	-	-	-
575	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.93	-	3.24	-	-	-	-	-	-
576	-	-	-	-	-	-	-	-	-	0.0006	-	-	-	-	-	-	-	0.0004	-	-	-	13.9	-	-	-	-	-	-
577	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0015	-	-	-	-	9.06	-	-	-	-	-	-
578	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.52	-	-	-	-	-	-	-	-	-	-	-	-	-
579	-	-	-	-	0.0014	-	-	-	-	-	-	-	-	-	-	-	-	-	27.2	-	14.3	-	-	-	-	-	-	-
580	-	-	6.58	-	2.01	-	3.80	-	-	20.8	-	-	-	-	-	-	-	-	5.20	-	6.56	24.1	-	-	-	-	-	-
581	-	-	32.5	-	0.699	-	14.9	-	-	35.9	-	-	-	-	-	-	4.23	-	3.45	-	16.0	13.4	-	-	-	-	-	-
582	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0054	0.0000	11.2	-	13.0	-	-	-	-	-	-
583	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.1	-	-	-	-	-	-	-	-	-	-	-	-	-
584	-	-	-	-	-	-	-	-	-	14.7	2.57	-	-	-	17.5	-	-	-	-	-	1.27	-	-	-	-	-	-	-
585	-	-	-	-	-	-	-	-	-	5.89	-	-	-	-	-	-	-	0.0306	-	-	19.2	-	-	-	-	-	-	-
586	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.7	-	-	-	-	-	-	-	-	-	-	-	-	-
587	-	30.8	-	-	3.37	-	-	-	22.9	-	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-
588	-	-	16.9	-	-	-	7.11	-	-	-	-	-	-	-	-	-	36.9	-	-	-	47.8	-	-	-	-	-	-	-
589	-	-	6.86	-	52.3	-	23.3	-	-	1.74	-	-	-	-	-	-	0.0048	6.23	-	-	37.2	-	-	-	-	-	-	-
590	-	-	-	-	0.610	-	-	-	-	-	-	-	-	-	-	-	-	1.09	-	-	2.24	-	-	-	-	-	-	-
591	-	5.95	-	-	-	-	-	-	-	7.06	-	-	-	-	15.2	-	-	-	-	-	-	-	-	-	-	-	-	-
592	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.2	-	-	-	-	-	-
593	-	-	-	-	11.9	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
594	-	-	-	-	6.68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
595	-	-	-	-	4.21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
596	-	-	-	-	0.985	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
597	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
598	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.13	-	-	-	-	-	-	-	-	-
599	-	-	-	-	9.71	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0172	-	-	-	-	-	-	-	-	-
600	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
601	-	-	-	-	38.4	0.0009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
602	-	-	-	-	27.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
603	-	-	-	-	86.0	-	-	-	-	-	-	-	-	-	-	-	-	3.18	1.24	-	0.350	-	-	-	-	-	-	-
604	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.29	-	-	-	-	-	-	-	-	-
605	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
606	-	-	-	-	1.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0055	-	-	-	-	-	-	-
607	-	-	-	-	10.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
608	-	-	-	-	7.91	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
609	-	-	-	-	2.07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
610	-	-	-	-	5.60	-	-	-	-	-	-	-	-	-	-	-	-	-	2.65	-	-	-	-	-	-	-	-	-
611	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	2.91	-	-	-	-	-	-	-	-	-
612	-	-	-	-	9.48	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
613	-	-	-	-	35.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
614	-	-	-	-	30.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
615	-	-	-	-	28.6	-	-	-	-	-	-	-	-	-	-	-	-	-	24.0	-	-	0.0730	-	-	-	-	-	-
616	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
617	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
618	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.1	-	-	-	-	-	-	-	-
619	-	11.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0019	-	-	-	-	1.05	-	-	-	-	-	-
620	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.40	-	-	-	-	10.2	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
621	6.68	-	-	-	-	-	2.79	-	-	21.1	-	-	-	3.68	-	-	9.98	-	-	-	-	15.0	-	-	-	-	-	-
622	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.8	-	-	-	-	17.7	-	-	-	-	-	-
623	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.41	-	-	-	-	-	-
624	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.797	-	-	-	-	22.6	-	-	-	-	-	-
625	-	-	-	-	-	-	35.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
626	-	-	-	-	4.62	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
627	-	-	-	-	27.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
628	-	-	-	-	-	-	0.483	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
629	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.17	-	-	-	-	-	-
630	-	-	-	-	-	4.61	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
631	1.21	8.58	-	-	-	-	9.78	-	-	3.65	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
632	-	-	-	-	-	-	11.3	-	-	0.924	-	-	-	-	-	-	0.0382	-	-	-	-	1.30	-	-	-	-	-	-
633	-	-	-	-	-	-	-	-	-	2.07	-	-	-	-	-	-	-	-	-	-	-	0.446	-	-	-	-	-	-
634	-	-	-	-	-	-	-	-	-	17.7	-	-	-	-	-	-	0.0001	-	-	-	-	33.0	-	-	-	-	-	-
635	-	-	-	-	7.84	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.8	-	-	-	-	-	-
636	-	-	-	-	6.16	-	10.3	-	-	12.9	-	-	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-
637	5.20	-	-	-	-	-	-	-	-	7.47	-	-	-	-	-	-	0.590	-	-	-	-	22.0	-	-	-	-	-	-
638	-	-	-	-	-	-	6.78	-	-	4.49	-	-	-	-	-	-	-	-	-	-	-	20.8	-	-	-	-	-	-
639	-	-	-	-	0.490	-	9.32	-	-	7.41	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
640	16.4	-	-	-	-	-	10.8	-	-	30.9	-	-	-	2.39	-	-	-	-	-	-	-	-	-	-	-	-	-	-
641	0.565	-	-	-	-	-	-	-	-	3.57	-	-	-	-	-	-	-	-	-	-	-	15.2	-	-	-	-	-	-
642	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-
643	-	4.86	-	-	-	-	-	-	-	0.664	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
644	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.3	-	-	-	-	-	-
645	-	-	-	-	36.6	1.50	1.89	-	-	-	-	-	-	-	-	-	0.572	5.50	1.33	-	-	2.31	-	-	-	-	-	-
646	-	4.36	-	-	25.4	-	40.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
647	-	3.85	-	-	-	-	-	-	-	6.98	-	-	-	-	-	-	4.45	2.01	-	-	-	57.4	-	-	-	-	-	-
648	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.04	-	-	-	-	-	-
649	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.04	-	-	-	-	-	-
650	-	-	-	-	-	-	8.82	-	-	16.4	-	-	-	-	-	-	4.10	-	-	-	-	-	-	-	-	-	-	-
651	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.294	-	-	-	-	10.9	-	-	-	-	-	-
652	-	3.53	-	-	-	-	-	-	-	17.5	-	-	-	-	-	-	5.18	3.62	-	-	-	2.19	-	-	-	-	-	-
653	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.44	-	-	-	-	25.6	-	-	-	-	-	-
654	-	5.73	-	-	-	-	-	-	-	2.36	-	-	-	-	-	-	-	-	-	-	-	8.99	-	-	-	-	-	-
655	-	11.9	-	-	-	-	44.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
656	-	-	2.12	-	-	-	2.59	-	-	-	-	-	-	-	-	-	-	3.25	-	0.0001	-	3.29	-	26.0	6.90	-	-	-
657	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-	-	-	4.29	0.0035	-	-	16.8	-	12.7	2.89	-	-	-
658	-	10.4	-	-	-	-	-	0.0044	-	-	-	-	-	-	-	-	6.84	-	-	-	-	15.4	-	-	-	-	-	-
659	-	-	5.09	-	1.66	-	9.32	-	-	-	-	-	-	-	-	-	-	12.0	-	-	-	-	-	-	3.79	-	-	-
660	-	43.8	-	-	-	-	-	-	-	50.7	-	-	-	-	-	-	5.36	2.75	-	-	-	1.27	-	-	-	-	-	-
661	-	-	-	-	0.0035	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
662	-	-	-	-	-	-	-	-	-	4.09	-	-	-	-	-	-	9.28	3.58	-	-	-	34.0	-	-	-	-	-	-
663	-	-	-	-	0.0000	-	15.8	-	-	-	-	-	-	-	-	-	-	0.0421	-	-	-	-	-	-	-	-	-	-
664	8.49	23.9	-	-	-	-	2.04	-	-	8.27	-	-	-	-	-	-	4.35	-	-	-	-	-	-	-	-	-	-	-
665	-	-	-	-	-	-	0.0431	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.9	-	-	-	-	-	-
666	-	-	-	-	-	-	9.12	-	-	23.8	-	-	-	-	-	-	6.31	-	0.0033	-	-	-	-	-	-	-	-	-
667	-	-	-	-	-	-	-	-	-	4.10	-	-	-	-	-	-	9.42	1.82	-	-	-	-	-	-	-	-	-	-
668	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.5	-	-	-	-	-	-
669	-	36.1	-	-	-	-	4.21	-	-	24.6	-	-	-	-	-	-	-	-	-	-	-	6.22	-	-	-	-	-	-
670	6.29	1.71	-	-	-	-	-	-	-	49.4	-	-	-	-	-	-	5.35	0.0005	-	-	-	5.11	-	-	-	-	-	-
671	-	6.35	-	-	-	-	12.1	-	-	7.52	-	-	-	-	-	-	31.4	-	-	-	-	-	-	-	-	-	-	-
672	-	-	-	-	0.181	-	0.0346	-	-	0.679	-	-	-	-	-	-	-	-	0.0000	-	-	0.551	-	-	-	-	-	-
673	-	-	-	-	0.117	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	3.90	-	-	-	-	-	-
674	19.1	-	-	-	0.656	-	-	-	-	9.93	-	-	-	-	-	-	-	-	-	-	-	87.0	-	-	-	-	-	-
675	24.1	-	-	-	-	-	-	-	-	0.740	-	-	-	6.72	-	-	2.46	-	-	-	-	5.07	-	-	-	-	-	-
676	-	-	-	-	0.411	-	-	25.8	-	-	-	-	-	-	-	-	42.8	-	-	-	-	34.4	-	-	-	-	-	-
677	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
678	-	33.3	-	-	-	-	-	-	-	3.59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
679	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	0.0024	-	-	-	-	4.48	-	-	-	-	-	-
680	-	20.5	-	-	-	-	0.0037	1.29	-	8.35	-	-	-	-	-	-	0.0008	-	-	-	-	18.0	-	-	-	-	-	-
681	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.216	-	-
682	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.28	-	-	-	-	-	-	-
683	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	87.9	-	-	-	-	-	-	-	-	-
684	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.7	-	-	-	-	-	-	-	-	-
685	-	-	-	-	0.0506	-	-	-	-	-	-	-	-	-	-	-	-	-	29.3	-	-	-	-	-	-	-	-	-
686	-	-	-	-	0.0991	-	-	-	-	-	-	-	-	-	-	-	-	-	18.5	-	-	-	-	-	-	-	-	-
687	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.4	-	-	-	-	-	-	-	-	-
688	-	-	-	-	0.0522	-	-	-	-	-	-	-	-	-	-	-	-	-	26.7	-	-	-	-	-	-	-	-	-
689	-	-	-	-	-	2.59	-	-	-	-	-	-	-	-	-	-	-	-	9.06	-	0.552	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
690	-	-	-	-	0.880	-	-	-	-	-	-	-	-	-	-	-	-	-	10.8	-	2.86	-	-	-	-	-	-	-
691	0.0034	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.15	-	-	-	-	-	-	-	-	-
692	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.6	-	-	-	-	-	-	-	-	-
693	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.8	-	-	-	-	-	-	-	-	-
694	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.12	-	-	-	-	-	-	-	-	-
695	35.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.91	-	-	-	-	-	-	-	-	-	-
696	10.6	-	-	9.55	-	-	-	-	-	3.94	-	-	0.229	-	-	-	-	10.3	-	-	-	-	-	-	-	-	-	-
697	-	-	-	-	-	-	-	-	-	9.98	-	-	-	-	-	-	-	-	-	-	-	0.0162	12.9	13.9	-	-	-	-
698	-	-	-	-	-	-	-	-	-	4.06	0.0165	-	4.94	0.0250	-	7.06	-	-	-	-	-	0.0016	-	13.8	-	-	-	-
699	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
700	-	-	-	-	0.557	-	-	3.75	-	-	-	-	-	-	-	-	-	-	62.9	-	-	-	-	-	-	-	-	-
701	-	-	-	-	41.1	-	2.27	-	-	-	-	-	-	-	-	-	-	-	38.2	-	-	-	-	-	-	-	-	-
702	-	-	-	-	147	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
703	-	-	-	-	78.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
704	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.08	-	-	-	-	-	-	-	-	-
705	-	-	-	-	46.9	-	-	-	-	-	-	-	-	-	-	-	-	-	1.78	-	1.39	-	-	-	-	-	-	-
706	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0570	1.46	-	0.0000	12.7	-	-	47.0	-	-	-
707	-	-	-	-	0.132	-	-	-	-	-	-	-	-	-	-	-	-	-	53.6	-	-	-	-	-	-	-	-	-
708	-	-	-	-	0.0236	-	-	-	-	-	-	-	-	-	-	-	-	-	12.8	-	-	-	-	-	-	-	-	-
709	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.03	-	-	-	-	-	-	-	-	-
710	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-
711	81.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.0	-	-	-	-	-	-	-	-	-	-
712	13.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.120	-	-	48.0	-	-	-	-	-	-	-
713	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.9	5.21	-	-	-	-	-	-
714	-	8.71	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	67.4	12.2	-	-	-	-	-	-
715	-	-	-	-	-	-	100	1.61	-	-	-	-	-	-	-	-	-	5.31	-	-	-	-	-	1.22	-	-	-	-
716	-	-	-	-	-	-	-	32.5	-	-	-	-	-	-	-	-	-	0.184	-	-	-	-	-	30.4	-	-	-	-
717	-	-	-	5.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
718	-	-	-	4.83	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.7	-	-	-	-	-	-
719	-	-	-	7.80	-	-	-	-	-	-	-	-	-	-	-	-	-	5.73	-	-	-	75.1	1.99	-	-	-	-	-
720	-	-	-	-	-	-	-	-	-	0.260	-	-	-	-	-	-	-	-	-	-	-	30.9	0.311	-	-	-	-	-
721	1.67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.9	19.4	-	-	-	-	-
722	-	1.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.6	-	-	-	-	-	-
723	-	-	-	-	-	-	-	-	-	-	7.44	-	0.415	0.0129	7.17	5.44	-	-	-	-	-	-	-	-	-	-	-	-
724	-	-	0.427	-	-	-	-	-	-	7.81	-	-	-	-	-	-	-	0.554	-	-	-	0.0001	4.37	2.68	-	-	-	-
725	-	-	-	-	-	-	-	-	-	-	-	-	-	0.367	14.9	-	-	-	-	-	-	-	-	-	-	-	-	-
726	-	-	-	-	-	-	-	-	-	-	-	-	-	0.895	10.2	-	-	-	-	-	-	-	-	-	-	-	-	-
727	-	11.6	-	-	-	-	-	-	-	0.0000	-	-	0.361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
728	-	-	-	-	-	-	-	-	-	-	-	-	12.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
729	-	3.19	-	-	-	-	-	-	-	-	-	-	-	0.0001	21.4	-	-	-	-	-	-	-	-	-	-	-	-	-
730	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	10.6	-	-	-	-	-	-
731	-	-	-	-	-	-	-	-	-	-	0.0000	-	0.501	0.0182	-	14.4	-	-	-	-	-	-	-	-	-	-	-	-
732	-	-	0.187	-	-	-	-	-	-	5.01	4.87	-	-	-	-	-	33.4	-	-	-	-	30.1	-	-	-	-	-	-
733	-	-	-	-	-	-	-	-	-	3.40	-	-	-	-	-	-	33.2	-	-	-	-	25.7	0.120	-	-	-	-	-
734	-	-	7.84	-	-	-	-	-	-	28.4	-	-	-	-	-	-	0.238	-	-	-	-	40.4	-	-	-	-	-	-
735	-	-	0.704	0.646	-	-	-	-	-	3.35	-	-	-	-	-	-	-	-	-	-	-	9.70	-	-	-	-	-	-
736	-	-	-	-	-	-	-	-	-	1.26	-	-	-	-	-	-	-	-	-	-	8.66	99.0	-	-	-	-	-	-
737	0.266	-	-	-	-	-	-	63.1	-	-	-	-	-	-	-	-	-	16.6	-	-	8.49	-	-	-	-	-	-	-
738	9.93	3.14	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-	-	-	-	-	3.25	-	-	-	5.69	0.0302	-	-
739	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.1	-	-	-	54.7	-	-	-	9.86	-	-	-
740	9.94	-	-	-	-	-	-	4.15	-	2.52	-	-	-	-	-	-	45.2	-	-	-	-	-	-	-	24.2	12.0	-	-
741	-	-	-	-	-	-	8.18	8.52	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
742	-	-	-	-	1.06	-	-	-	-	-	-	-	-	-	-	-	0.685	-	0.0023	54.1	62.0	-	-	-	3.71	-	-	-
743	-	-	-	-	-	-	-	81.9	-	-	-	-	-	0.0027	-	-	-	85.7	-	-	-	-	-	-	-	-	-	-
744	-	-	-	-	-	-	-	-	-	10.7	-	-	-	-	-	-	-	9.45	-	-	-	0.0872	76.4	-	-	-	-	-
745	-	0.0003	4.00	-	-	-	-	-	-	25.0	-	-	9.86	-	-	-	-	-	-	-	-	0.0008	21.4	-	-	-	-	-
746	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0418	117	12.0	-	-	-	-
747	-	-	-	-	-	-	-	-	-	-	9.74	-	-	-	-	-	-	3.36	-	-	-	0.0054	70.7	6.61	-	-	-	-
748	-	8.85	-	-	-	6.84	-	0.877	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	8.47	-	-	-	-	-
749	-	11.9	-	0.937	-	-	-	-	-	4.17	6.95	-	-	-	-	0.0980	-	-	-	-	-	0.0005	45.7	-	-	-	-	-
750	-	-	6.70	2.00	-	-	-	2.09	-	13.4	16.1	-	-	2.80	7.32	62.4	-	-	-	-	21.6	63.2	-	-	-	-	-	-
751	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	52.7	-	-	-	-	-	-
752	-	-	-	1.37	-	-	-	-	-	2.18	2.53	-	-	-	-	-	-	-	-	-	-	107	15.0	-	-	-	-	-
753	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.3	148	-	-	-	-	-	-	-	-	-	-	-
754	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63.7	28.7	8.39	-	-	-	-
755	-	-	-	-	-	-	-	-	-	-	-	-	-	0.257	-	-	-	-	-	-	-	39.5	31.4	5.03	-	-	-	-
756	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.26	14.0	8.42	-	-	-	-
757	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.77	-	-	-	-	54.7	-	-	-	-	-	-
758	-	-	-	1.93	-	-	-	-	-	0.171	0.921	-	-	-	-	-	-	-	-	-	-	60.7	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
759	-	-	-	-	-	-	13.0	57.4	-	-	-	-	-	-	-	-	-	0.434	-	-	-	-	-	-	-	-	-	-
760	-	6.57	-	-	-	-	-	113	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
761	-	8.27	-	-	-	-	7.94	12.8	-	9.42	-	-	-	-	-	-	-	1.89	0.0219	-	0.447	6.40	-	36.8	-	3.48	-	-
762	-	-	-	-	-	-	135	27.6	-	-	-	-	-	-	-	-	-	4.62	-	-	-	-	-	-	-	-	-	-
763	-	-	-	-	-	-	-	3.69	-	9.54	-	-	-	-	-	-	-	7.32	-	-	-	-	-	-	-	-	-	-
764	2.34	-	-	-	-	-	-	-	-	40.9	-	-	10.6	-	-	-	-	25.9	-	-	-	-	-	-	-	-	-	-
765	-	-	-	0.0000	-	-	40.1	3.85	-	0.754	-	-	-	-	-	-	-	2.90	-	-	-	-	-	4.41	-	2.27	-	-
766	-	-	-	-	-	-	24.6	13.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
767	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.9	0.340	-	43.3	85.0	-	0.271	-	0.0092	-	-
768	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.91	-	-	-	-	-	117	-	-	-	-
769	-	-	-	-	-	-	2.25	19.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.991	-	-	-	-
770	23.2	-	-	5.33	-	-	2.08	14.4	-	-	-	-	-	-	-	-	-	9.30	-	-	-	-	-	-	-	-	-	-
771	1.49	0.115	-	-	-	-	-	-	-	9.89	-	-	-	-	-	-	0.936	0.0625	-	-	-	-	-	92.3	-	0.404	-	-
772	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.2	-	-	-	-
773	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.554	-	-	-	-	-	20.2	-	-	-	-
774	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	0.964	-	-	-	-	-	91.8	-	-	-	-
775	-	-	-	-	0.211	-	-	3.28	-	-	-	-	-	-	-	-	-	-	-	8.57	23.7	-	-	-	14.7	33.8	-	-
776	10.8	-	-	-	-	-	-	-	-	1.53	-	-	-	-	-	-	8.21	-	0.0466	-	103	-	-	-	42.9	5.29	-	-
777	-	-	-	-	-	-	-	1.87	-	-	-	-	-	-	-	-	-	-	-	-	89.8	-	-	-	3.04	22.9	-	-
778	-	-	-	-	0.0423	-	-	-	-	-	-	-	-	-	-	-	16.4	-	0.0000	-	59.2	-	-	-	14.6	5.33	-	-
779	-	-	-	-	0.0001	-	81.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
780	-	-	1.03	-	-	-	-	-	-	5.19	-	-	-	-	-	-	21.5	-	-	-	-	-	-	-	3.78	-	-	-
781	32.9	25.2	-	0.775	-	-	-	-	-	51.3	-	-	-	-	-	-	7.25	-	-	-	10.2	-	-	-	17.1	4.26	-	-
782	-	27.7	-	-	0.434	-	-	-	-	-	-	-	-	-	-	-	-	-	14.3	-	114	0.559	-	-	-	-	-	-
783	-	-	-	1.91	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85.5	-	-	-	-	14.0	-	-
784	-	-	-	-	-	-	14.7	-	-	-	-	-	-	-	-	-	-	7.45	-	-	-	-	-	-	-	-	-	-
785	-	-	-	-	-	-	33.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
786	-	-	-	-	-	-	-	35.1	-	-	-	-	-	-	-	-	-	6.29	-	-	-	-	-	22.6	-	-	-	-
787	-	-	-	-	-	-	86.7	-	-	-	-	-	-	-	-	-	-	5.76	-	-	-	-	-	-	-	-	-	-
788	-	-	-	-	-	-	31.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
789	-	-	-	-	-	-	13.3	-	-	-	-	-	-	-	-	-	-	0.191	-	-	-	-	-	-	-	-	-	-
790	-	-	-	-	-	-	58.1	-	-	-	-	-	-	-	-	-	-	3.26	-	-	-	-	-	-	-	-	-	-
791	-	-	-	-	-	-	20.2	-	-	-	-	-	-	-	-	-	-	1.59	-	-	-	-	-	-	-	-	-	-
792	-	-	-	-	-	-	59.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
793	-	-	-	-	-	2.23	87.7	-	12.2	-	-	-	-	-	-	-	-	-	0.789	-	-	-	-	-	-	-	-	-
794	-	-	-	-	-	-	35.5	-	-	-	-	-	-	-	-	-	-	2.06	-	-	-	-	-	-	-	-	-	-
795	-	-	-	-	-	-	47.9	2.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
796	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.37	-	-	-	-
797	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.860	-	-	-	-	-	16.3	-	-	-	-
798	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.0	-	-	-	-	-	43.3	-	-	-	-
799	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.00	-	-	-	-	-	25.4	-	-	-	-
800	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.59	-	-	-	-	-	17.7	-	-	-	-
801	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-
802	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.8	-	-	-	-
803	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	43.7	-	-	-	-
804	-	-	-	-	-	-	-	65.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
805	-	-	-	-	-	-	28.1	-	-	-	-	-	-	-	-	-	-	5.05	-	-	-	-	-	-	-	-	-	-
806	-	-	-	-	-	-	19.3	-	-	-	-	-	-	-	-	-	-	13.5	-	-	-	-	-	-	-	-	-	-
807	1.92	0.346	-	-	-	-	-	19.1	-	0.560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
808	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.89	3.58	-	-	-	-	-	65.5	-	25.8	-	-
809	11.6	1.07	-	4.94	-	-	-	-	-	15.2	-	-	-	-	-	-	-	1.32	-	-	-	-	-	-	-	-	-	-
810	29.4	5.96	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.65	-	-	-	-	-	-	-	-	-	-
811	3.04	-	-	29.4	-	-	-	-	-	-	-	-	-	-	-	-	-	0.151	-	-	-	-	-	-	-	-	-	-
812	-	-	-	13.0	-	-	-	-	-	-	-	-	-	-	-	-	-	0.789	-	-	-	-	-	0.741	-	-	-	-
813	-	-	-	7.13	-	-	-	-	-	19.9	-	-	-	-	-	-	-	0.229	-	-	-	-	-	21.7	-	19.0	-	-
814	-	39.4	-	4.98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.09	-	-	-	-
815	-	32.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	51.1	37.0	-	-	-	-	-	-
816	-	-	-	4.79	-	-	-	0.0134	-	-	-	-	-	-	-	4.92	-	2.61	-	-	26.7	29.8	-	-	-	-	-	-
817	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.8	0.159	-	-	-	-	0.0510	2.48	-	-	-	-	-	-
818	-	-	3.13	-	-	-	-	-	-	-	3.87	-	-	-	19.2	-	1.65	-	-	-	11.4	39.6	-	-	-	-	-	-
819	1.58	17.3	-	9.49	-	-	-	22.4	-	5.94	-	-	-	-	-	-	0.199	25.0	-	-	73.5	33.1	-	-	-	-	-	-
820	20.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0269	-	-	40.3	-	-	-	-	-	-	-
821	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.9	21.6	-	-	211	80.3	-	-	-	-	-	-
822	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	0.0377	-	126	-	-	-	-
823	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	82.6	-	-	-	-	-	0.189	-	-	-	-
824	-	-	0.761	-	-	-	-	8.21	-	-	-	-	-	-	-	-	43.7	0.0023	-	-	64.2	57.2	-	-	-	-	-	-
825	-	-	-	-	-	-	-	4.68	-	-	-	-	-	-	-	-	0.907	32.9	-	-	9.31	9.26	-	-	-	-	-	-
826	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	110	28.9	-	-	-	-	-	-
827	-	8.01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0056	-	-	-	122	7.16	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
828	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55.0	109	-	-	-	-	-	-
829	-	0.0000	-	-	-	-	-	-	-	19.1	-	-	-	-	-	-	-	-	5.03	-	33.5	24.6	-	-	-	-	-	-
830	-	-	-	-	-	-	-	-	-	49.4	-	-	-	-	-	-	-	-	-	-	53.0	40.0	-	0.118	-	-	-	-
831	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69.4	-	-	-	-	-	-	-
832	-	16.7	0.177	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0072	-	-	46.9	23.1	-	-	-	-	-	-
833	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.62	47.3	-	-	-	-	-	-
834	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.1	0.835	-	40.8	21.0	-	8.64	-	-	-	-
835	-	-	-	6.68	-	-	-	-	-	0.786	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
836	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.7	0.0035	-	-	-	-	-	33.5	-	-	-	-
837	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.655	-	-	-	115	18.4	-	-	-	-	-	-
838	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40.6	45.2	-	-	-	-	-	-
839	-	1.46	12.0	-	-	-	-	-	-	26.3	4.18	-	-	-	-	-	20.5	-	-	-	37.6	0.0184	-	-	17.2	-	-	-
840	4.51	-	-	-	-	-	-	-	-	31.4	-	-	-	-	-	-	1.21	2.44	0.301	-	-	41.0	-	-	0.0000	-	-	-
841	-	-	7.76	-	-	-	-	-	-	7.09	-	-	-	-	-	-	17.9	-	-	-	-	-	-	-	27.3	-	-	-
842	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.22	-	30.1	-	-
843	-	4.82	-	-	-	-	-	-	-	11.2	-	-	-	-	-	-	16.3	-	-	-	-	-	-	-	-	-	-	-
844	-	-	-	-	-	-	-	-	-	32.9	-	-	-	-	-	-	0.0001	-	-	-	0.752	30.4	-	-	8.76	-	-	-
845	-	-	-	-	-	-	-	-	-	6.50	-	-	-	-	-	-	-	-	-	-	-	15.3	-	-	-	-	-	-
846	-	-	-	-	-	-	-	-	-	33.8	-	-	-	-	-	-	-	-	0.232	-	-	35.0	-	-	-	-	-	-
847	-	-	-	-	-	-	-	5.87	-	-	-	-	-	-	-	-	-	10.7	-	-	-	-	-	76.2	-	-	-	-
848	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.5	-	-	-	-
849	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.15	-	-	-	-	-	25.4	-	-	-	-
850	-	0.0068	-	-	-	-	-	-	-	17.6	-	-	-	-	-	-	-	3.21	-	-	-	0.0043	7.76	31.2	-	-	-	-
851	-	0.0004	-	-	-	-	-	-	-	4.56	-	-	-	-	-	-	-	-	-	-	-	0.0014	1.67	26.0	-	-	-	-
852	-	19.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.39	-	-	-	0.0020	-	39.3	-	-	-	-
853	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0048	-	57.6	-	-	-	-
854	-	26.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0030	-	38.7	-	-	-	-
855	-	-	-	-	-	-	-	-	-	-	-	3.42	40.9	0.0009	-	-	-	0.0084	-	-	-	-	-	-	-	-	-	-
856	-	-	-	-	-	-	-	-	-	20.7	-	-	-	-	-	-	-	-	-	-	-	0.0045	-	43.9	-	-	-	-
857	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.19	-	-	-	0.0040	-	27.5	-	-	-	-
858	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0008	-	-	-	0.0833	-	26.1	-	-	-	-
859	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.297	-	-	0.0051	-	58.2	-	-	-	-
860	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.38	-	-	0.830	0.0700	-	85.1	-	-	-	-
861	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.6	0.0703	-	-	0.0000	-	22.3	-	-	-	-
862	-	10.9	-	-	-	-	-	-	-	0.0434	-	-	-	-	2.26	-	-	24.8	-	-	61.4	18.9	-	-	-	-	-	-
863	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.181	8.32	-	-	89.0	14.0	-	-	-	-	-	-
864	-	-	-	-	-	-	-	62.7	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-
865	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.3	25.9	-	-	7.04	-	-	-	-	-	-	-
866	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.9	-	-	-	-	-	-	-
867	-	-	-	-	-	-	-	-	-	64.0	-	-	-	7.14	-	-	-	18.5	-	-	6.68	57.9	-	-	-	-	-	-
868	-	-	-	-	-	-	-	-	-	21.4	-	-	-	-	-	-	-	2.23	-	-	61.5	2.40	-	-	-	-	-	-
869	-	2.18	2.04	2.25	-	-	-	-	-	29.8	-	-	-	-	-	-	0.0056	15.5	-	-	27.5	55.9	-	-	-	-	-	-
870	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.5	14.8	-	-	107	3.80	-	-	-	-	-	-
871	-	2.42	-	-	-	-	-	-	-	-	15.5	-	-	-	-	-	-	0.0173	-	-	-	-	-	-	-	-	-	-
872	-	0.0004	-	2.68	-	-	-	-	-	7.87	26.1	-	1.34	-	-	-	-	-	-	-	-	0.0001	26.3	-	-	-	-	-
873	-	-	-	-	-	-	-	-	-	9.27	-	-	3.95	-	-	-	-	-	-	-	-	0.0014	15.8	-	-	-	-	-
874	-	-	2.32	-	-	-	-	-	-	13.2	-	-	-	-	-	-	-	0.0017	-	-	-	0.0063	30.2	-	-	-	-	-
875	-	-	0.508	-	-	-	-	-	-	3.76	-	-	-	-	-	-	-	-	-	-	-	0.864	77.8	1.46	-	-	-	-
876	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0282	35.5	-	-	-	-	-
877	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0054	51.8	11.6	-	-	-	-
878	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0115	55.8	1.43	-	-	-	-
879	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0030	13.7	20.8	-	-	-	-
880	-	0.116	-	-	-	-	-	-	-	20.1	-	-	-	-	-	-	-	5.74	-	-	-	0.0005	-	17.7	-	-	-	-
881	-	0.0010	-	-	-	-	-	-	-	20.6	-	-	-	-	-	-	-	-	-	-	-	-	-	8.15	-	-	-	-
882	-	1.79	-	-	-	-	-	-	-	25.8	-	11.5	12.1	0.249	-	-	-	-	-	-	-	-	-	-	-	-	-	-
883	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0266	5.31	-	-	44.7	-	-	-	-	-	-	-
884	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.08	34.4	-	28.9	-	-	7.59	3.46	-	-	-	-	-	-
885	-	-	-	-	-	-	-	12.1	-	-	-	-	-	-	-	1.79	-	8.44	-	-	1.55	9.39	-	-	-	-	-	-
886	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.148	-	-	-	-	-	-	-	-	-	-	-	-
887	-	25.2	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	-	-	-	-	-	-	-	-
888	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.9	65.7	-	-	-	-	0.0447	-	-	-	-	-	-	-
889	-	-	-	0.268	-	-	6.80	34.4	-	-	-	-	-	-	-	-	-	33.1	-	-	4.53	23.9	-	-	-	-	-	-
890	-	-	-	27.5	-	-	45.1	41.9	-	4.72	-	-	-	-	5.17	-	-	0.0172	-	-	9.81	-	-	-	-	-	-	-
891	-	3.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-
892	-	15.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34.1	-	-	-
893	-	3.20	-	-	-	-	-	67.2	-	-	-	-	-	-	-	-	-	-	-	-	0.0031	-	0.120	-	-	-	-	-
894	-	-	-	-	-	-	-	57.2	-	-	-	-	-	-	-	-	-	7.76	-	-	-	-	-	-	-	-	-	-
895	-	57.1	-	21.5	-	-	-	-	20.4	16.3	-	-	-	-	-	-	-	24.2	-	-	72.0	-	8.70	-	0.478	-	-	-
896	-	0.0351	-	1.99	-	-	-	78.0	-	-	-	-	-	-	-	-	-	-	-	-	3.64	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
897	-	-	-	-	-	-	-	0.0212	-	-	-	-	-	-	-	-	-	2.45	-	-	49.2	81.6	-	-	-	-	-	-
898	-	60.0	-	2.75	-	-	-	5.94	-	-	-	-	-	-	-	-	1.94	0.163	-	-	-	-	-	-	-	-	-	-
899	-	0.178	-	10.0	-	-	-	-	-	-	-	-	-	-	-	-	-	3.55	-	-	41.3	-	-	-	-	-	-	-
900	-	-	-	-	-	-	33.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
901	-	16.4	-	4.76	-	-	-	-	-	-	-	-	-	-	-	-	-	16.2	-	-	-	-	-	-	55.7	-	-	-
902	0.0000	-	-	17.0	-	-	-	4.51	-	-	-	-	-	-	-	-	-	7.45	-	-	43.6	-	-	-	-	-	-	-
903	-	7.42	-	5.53	-	-	-	23.3	-	1.90	-	-	-	-	-	7.42	48.4	38.5	-	-	10.2	0.526	-	-	-	-	-	-
904	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	119	6.44	-	-	-	-	-	-
905	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.30	-	-	-	8.89	8.51	-	-	-	-	-	-
906	-	-	-	-	-	-	-	-	-	-	0.0590	-	-	-	-	-	6.61	-	-	-	2.20	43.1	-	-	-	-	-	-
907	-	30.6	-	13.5	-	-	-	-	-	5.95	5.54	-	-	-	12.9	-	-	-	-	-	46.4	43.2	-	-	-	-	-	-
908	-	99.2	-	-	-	-	-	-	-	-	-	-	-	-	68.1	-	-	-	-	-	-	-	-	3.49	-	-	-	-
909	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75.9	-	2.79	-	0.342	-	-	-
910	0.0654	22.6	-	9.42	-	-	-	43.8	-	-	-	-	-	-	-	-	-	10.1	-	-	13.3	-	-	-	-	-	-	-
911	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	49.4	-	-	-	-	-	-
912	-	-	-	-	-	-	-	-	-	0.656	-	-	-	-	-	-	-	21.5	-	-	-	36.5	37.1	-	-	-	-	-
913	-	0.0110	-	1.25	-	-	-	-	-	13.8	-	-	-	-	-	-	-	0.358	-	-	9.99	5.47	110	-	-	-	-	-
914	4.03	-	1.44	11.1	-	-	-	-	-	26.5	-	-	-	2.86	-	-	-	-	-	-	-	0.930	2.10	62.4	-	13.4	-	-
915	-	-	-	44.1	-	-	-	-	-	2.55	-	-	-	2.75	-	-	-	-	-	-	-	32.6	-	5.69	-	-	-	-
916	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.7	-	-	-	-	-	-
917	-	-	-	32.4	-	-	-	-	-	-	0.0172	-	-	-	-	-	-	9.16	-	-	-	106	-	0.0033	-	-	-	-
918	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.428	-	-	-	53.7	-	-	-
919	-	6.39	1.41	2.22	-	-	-	-	-	0.768	-	-	-	-	1.83	-	-	-	-	-	28.4	91.2	-	-	-	-	-	-
920	-	-	0.970	-	-	-	-	-	-	2.60	4.09	-	-	-	-	-	2.69	-	-	-	1.19	101	-	-	-	-	-	-
921	0.779	4.09	-	-	-	-	-	-	-	1.12	-	-	-	-	-	-	2.25	-	-	-	-	61.2	-	-	-	-	-	-
922	2.92	17.4	-	1.27	-	-	-	-	-	10.6	-	-	-	-	-	-	12.0	5.05	-	-	-	69.8	0.684	-	-	-	-	-
923	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	123	12.1	-	-	-	-	-
924	-	-	-	-	-	-	-	-	-	4.85	-	-	-	-	-	-	-	-	-	-	-	0.132	34.3	6.16	-	-	-	-
925	-	-	0.0001	-	-	-	-	-	-	23.6	-	-	-	-	-	-	16.3	-	-	-	-	79.9	4.07	0.621	-	-	-	-
926	2.08	9.76	2.60	13.6	-	-	-	-	-	4.94	-	-	-	-	-	-	-	-	-	-	-	56.9	2.21	-	-	-	-	-
927	-	0.0002	-	-	-	-	-	-	-	1.29	-	-	-	-	-	-	0.446	-	-	-	-	62.8	-	-	-	-	-	-
928	-	15.3	-	-	-	10.6	-	9.80	0.0000	-	-	-	6.75	-	-	-	-	1.82	-	-	0.0001	15.7	0.788	-	-	-	-	-
929	-	-	-	-	-	-	-	0.0000	0.236	-	-	-	-	-	-	-	-	-	-	-	0.0001	6.81	50.2	-	-	-	-	-
930	-	-	5.45	-	-	-	-	-	0.0041	3.67	0.0002	-	2.82	-	-	-	-	-	-	-	-	0.475	29.2	-	-	-	-	-
931	-	-	0.0003	-	-	27.8	-	2.70	0.0944	-	2.43	-	-	-	-	-	-	-	-	-	-	0.0935	2.15	4.96	-	-	-	-
932	-	-	-	-	-	-	-	-	-	8.13	-	-	-	-	-	-	-	-	-	-	-	5.29	0.979	-	-	-	-	-
933	3.18	4.98	-	-	-	-	-	-	-	8.01	-	-	-	-	-	-	8.11	-	-	-	-	43.0	-	-	-	-	-	-
934	-	23.2	-	-	-	-	-	-	-	2.58	-	-	-	-	2.93	-	-	-	-	-	-	-	-	-	-	-	-	-
935	-	-	-	-	-	-	-	-	-	14.2	-	-	-	-	-	-	-	0.0001	-	-	-	16.4	-	2.95	-	-	-	-
936	-	36.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
937	-	9.81	-	1.88	-	-	-	-	20.5	-	-	-	-	-	-	-	-	1.78	-	-	-	-	-	-	-	-	-	-
938	-	-	-	-	-	-	-	-	-	0.810	-	-	-	0.136	-	30.6	-	-	-	-	-	1.12	1.32	-	-	-	-	-
939	-	-	-	-	-	-	-	-	-	-	0.0006	-	11.9	0.0003	17.7	-	-	-	-	-	-	-	-	-	-	-	-	-
940	-	-	-	-	-	-	-	-	-	1.19	-	-	-	-	-	-	-	-	-	-	-	14.1	-	-	-	-	-	-
941	-	-	-	-	-	-	-	56.2	-	-	-	-	-	0.0002	-	-	-	4.93	-	-	-	-	0.0023	-	-	-	-	-
942	-	13.0	-	-	-	16.8	-	0.0839	4.10	-	-	-	-	-	-	-	-	2.73	-	-	-	-	-	-	-	-	-	-
943	-	0.264	-	1.05	-	1.68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0006	9.36	-	-	-	-	-
944	-	-	-	-	-	53.1	-	4.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
945	-	-	-	-	-	-	-	4.81	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
946	-	-	-	-	-	-	-	6.57	0.0022	2.01	0.0001	-	2.54	-	-	-	-	-	-	-	-	0.0006	8.26	-	-	-	-	-
947	-	-	-	-	-	-	-	30.7	-	-	-	-	-	-	-	-	-	6.05	-	-	-	-	0.0021	-	-	-	-	-
948	-	-	-	-	-	-	-	0.0326	-	-	-	-	-	-	-	-	-	-	-	-	-	0.865	34.0	3.82	-	-	-	-
949	-	0.0000	-	4.02	-	-	-	-	-	5.93	4.48	-	-	-	-	-	-	2.57	-	-	-	0.0122	68.1	5.66	-	-	-	-
950	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-	-	-	-	-	-	-	-
951	-	44.3	1.43	-	-	-	-	-	-	59.4	-	-	-	-	-	-	-	29.7	-	-	58.3	63.9	-	-	-	-	-	-
952	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0031	4.62	10.8	-	-	-	-	-	-	-	-	-	-	-	-
953	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	20.7	1.71	-	-	-	-	-	-	-	-	-	-	-	-
954	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	35.9	-	-	-	-	-	-	-	-	-	-	-	-
955	-	-	0.548	-	-	-	-	2.99	0.0004	13.1	-	-	-	-	-	-	-	-	-	-	-	0.0027	17.9	7.35	-	-	-	-
956	-	-	-	-	-	-	-	2.69	-	-	-	-	6.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
957	-	-	-	-	-	-	-	-	-	0.348	14.0	-	4.57	-	-	-	-	2.44	-	-	-	0.0017	69.2	0.873	-	-	-	-
958	-	-	-	-	-	-	-	5.77	-	-	-	-	-	0.443	-	26.2	-	-	-	-	-	-	-	-	-	-	-	-
959	-	-	-	-	-	-	-	0.161	-	-	-	-	-	0.0523	-	14.2	-	-	-	-	-	-	-	-	-	-	-	-
960	-	-	0.0160	-	-	-	-	-	-	8.95	0.0001	-	3.09	0.0005	-	9.98	-	-	-	-	-	-	-	0.791	-	-	-	-
961	-	0.164	-	-	-	-	-	-	-	-	-	-	-	0.0801	0.606	6.20	-	-	-	-	-	-	-	-	-	-	-	-
962	-	-	6.53	-	-	-	-	-	-	2.79	0.171	-	20.6	-	-	-	-	-	-	-	-	0.0440	6.86	-	-	-	-	-
963	-	0.0006	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-	0.0145	-	-	-	0.0545	46.6	33.0	-	-	-	-
964	-	-	-	-	-	-	-	19.9	0.0000	-	-	-	-	-	-	-	-	7.16	-	-	-	0.0000	0.0056	-	-	-	-	-
965	-	-	-	-	-	0.168	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.157	31.8	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
966	5.56	7.27	-	0.289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
967	-	20.7	-	0.939	-	11.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	2.99	-	-	-	-	-
968	-	-	-	-	-	35.8	-	61.1	0.0006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
969	-	17.6	-	-	-	46.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
970	-	2.62	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
971	-	0.266	-	-	-	-	-	-	-	18.2	-	-	-	-	-	-	-	-	-	-	-	0.0101	11.1	-	-	-	-	-
972	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.21	-	-	0.721	15.3	-	-	-	-	-	-
973	-	-	-	3.43	-	-	-	-	-	-	8.78	-	-	-	-	-	-	-	-	-	-	69.7	18.8	-	-	-	-	-
974	-	1.27	-	-	-	-	-	-	-	2.66	-	-	-	-	-	-	-	-	-	-	-	115	5.02	-	-	-	-	-
975	-	23.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
976	4.73	23.0	-	0.140	-	-	-	-	-	3.80	-	-	-	-	-	-	0.813	0.0306	-	-	-	7.16	-	-	-	-	-	-
977	-	0.0446	0.170	0.390	-	-	-	-	-	16.0	-	-	-	-	-	-	9.56	-	-	-	-	72.2	41.5	-	-	-	-	-
978	-	0.0000	-	-	-	-	-	-	-	3.22	-	-	-	-	-	-	7.51	-	-	-	-	76.8	9.08	-	-	-	-	-
979	-	-	0.781	30.5	-	-	-	-	-	0.0005	5.45	-	-	-	5.64	-	-	-	-	-	-	10.4	1.27	-	-	-	-	-
980	-	0.0000	-	-	-	-	-	-	-	1.16	-	-	-	-	-	-	2.18	-	-	-	0.0002	97.0	-	-	-	-	-	-
981	-	0.0002	-	-	-	-	-	-	-	2.69	-	-	-	-	-	-	0.0006	-	-	-	-	33.4	-	-	-	-	-	-
982	-	-	-	2.34	-	-	-	-	-	3.07	-	-	-	-	-	-	10.9	-	-	-	-	88.1	-	-	-	-	-	-
983	15.4	0.0001	-	0.230	-	-	-	-	-	12.8	1.59	-	-	-	-	-	10.4	-	-	-	-	28.6	2.68	0.589	-	-	-	-
984	-	35.1	-	32.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
985	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.7	-	-	-	-	-	-
986	-	-	-	-	-	-	-	-	-	3.70	-	-	-	-	-	-	-	-	-	-	-	51.8	-	-	-	-	-	-
987	-	2.19	-	0.236	-	-	-	-	-	8.01	-	-	-	-	-	-	0.0002	5.17	-	-	-	0.0879	117	-	-	-	-	-
988	0.318	-	-	-	-	-	-	-	-	9.71	-	-	-	-	-	-	6.12	-	-	-	-	35.2	6.67	-	-	-	-	-
989	-	-	-	-	-	-	-	-	-	85.5	-	-	-	-	-	-	22.5	-	-	-	-	26.3	6.62	-	-	-	-	-
990	-	-	-	-	-	-	-	-	-	4.95	-	7.19	-	14.1	-	-	-	0.788	-	-	-	0.636	-	72.7	-	-	-	-
991	-	-	-	-	-	-	-	-	-	2.78	-	-	-	-	-	-	-	-	11.2	-	14.7	9.61	-	-	-	-	-	-
992	-	1.22	3.47	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-	-	0.284	-	0.0010	0.0023	-	29.0	-	-	-	-
993	-	-	-	-	-	-	-	-	-	-	-	3.99	11.1	10.9	-	-	-	0.499	-	-	-	1.25	-	-	-	-	-	-
994	-	-	-	-	-	-	-	4.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
995	-	-	-	-	-	-	71.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
996	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.41	-	-	-
997	-	-	0.0002	13.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58.9	-	-	-	-	2.90	-	-
998	-	1.02	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.7	12.6	-	-
999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.3	-	-	-	-
1000	-	-	-	-	-	-	-	28.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1001	-	-	-	-	-	-	-	57.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1002	-	-	-	-	-	-	45.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1003	-	-	-	-	-	-	23.0	-	-	-	-	-	-	-	-	-	-	0.795	-	-	-	-	-	-	-	-	-	-
1004	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.841	-	-	-	-	-	-	-	-	-	-
1005	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.06	-	-	-	-
1006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.37	0.592	-	-	-	-	5.56	-	-	-	-
1007	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0239	16.7	-	-	-	-	-	-
1008	-	11.6	-	-	-	-	-	-	-	-	-	-	-	-	75.6	-	-	-	-	-	-	-	-	-	-	-	-	-
1009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91.7	-	-	-	-	-	-	-
1010	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.6	-	-	-	-	-	-	-
1011	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.6	-	-	-	-	-	-	-
1012	-	-	-	-	-	-	-	-	-	7.49	-	-	-	-	-	-	-	7.82	-	-	-	1.07	-	-	-	-	-	-
1013	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.73	-	-	-	-	-
1014	-	2.39	-	-	-	-	-	-	-	-	-	-	2.27	0.0064	-	12.0	-	0.0312	-	-	-	0.694	-	-	-	-	-	-
1015	-	4.38	-	-	-	-	-	-	-	9.94	-	-	-	-	-	-	7.24	-	-	-	-	87.1	17.5	-	-	-	-	-
1016	14.6	24.4	-	0.248	-	-	-	-	-	18.1	-	-	-	-	-	-	1.91	-	-	-	-	13.3	0.512	2.40	-	-	-	-
1017	-	11.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1018	-	-	-	-	-	-	-	-	-	-	-	-	5.22	-	4.73	-	-	-	-	-	-	-	-	-	-	-	-	-
1019	-	-	-	-	-	-	-	11.6	42.4	-	-	-	-	-	10.7	-	-	0.190	-	-	-	-	-	-	-	-	-	-
1020	-	2.79	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	2.05	-	-	-	-	-
1021	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1022	1.25	3.38	-	-	-	-	-	-	-	4.74	-	-	-	-	-	-	-	3.06	-	-	-	3.77	-	-	-	-	-	-
1023	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.01	-	-	-	-	-	90.0	-	-	-	-
1024	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.932	-	-	-	-	-	0.332	-	-	-	-
1025	-	-	-	-	-	-	-	1.71	-	-	-	-	-	-	-	-	-	-	0.136	-	-	-	-	-	-	-	-	-
1026	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.235	-	-	-	-	-	2.73	-	-	-	-
1027	-	6.56	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	0.0288	-	-	-	-	-	61.3	-	-	-	-
1028	-	1.04	-	2.43	-	-	-	-	-	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	0.106	-	-	-	-
1029	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.7	-	0.115	-	-	0.248	-	-	-	-
1030	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.9	-	0.213	-	-	0.386	-	-	-	-
1031	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.7	-	-	-	-	-	45.8	-	-	-	-
1032	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.6	-	-	-	-	-	16.6	-	-	-	-
1033	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.54	-	-	-	-	-	25.3	-	-	-	-
1034	-	-	-	-	-	-	-	-	0.0002	0.0058	-	-	-	-	-	-	-	-	-	-	5.41	25.1	-	-	-	12.5	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
1035	-	20.8	-	-	-	-	-	26.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-
1036	-	19.7	-	-	-	-	21.9	10.9	0.0664	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1037	-	-	7.72	-	-	-	-	-	-	4.60	-	-	-	-	-	-	1.71	-	-	-	2.02	1.89	-	-	24.7	-	-	-
1038	-	-	-	-	-	-	-	24.3	-	-	-	-	-	-	-	-	-	0.721	-	-	-	-	-	-	-	-	-	-
1039	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.6	-	-	-	70.2	0.801	-	-	-	-	-	-
1040	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1041	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.28	-	-	-	-	-	-	-
1042	-	-	-	-	-	-	-	-	-	17.1	-	-	-	-	-	-	-	-	0.0171	-	27.3	-	-	-	-	-	-	-
1043	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.1	-	-	-	-	-	-	-
1044	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.4	13.5	-	-	-	-	-	-
1045	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91.4	-	-	-	-	-	-	-
1046	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	49.2	-	-	-	-	-	-	-	-	-
1047	-	-	-	-	0.0215	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1048	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	50.3	-	-	-	-	-	-	-
1049	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.69	-	-	-	-	-	-	-	-	-
1050	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41.9	11.0	-	-	-	-	-	-
1051	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.0	-	-	-	-	-	-	-	-	-
1052	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61.7	0.367	34.2	-	20.5	-	-	-	-	-	-
1053	-	-	-	-	0.0093	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.8	-	-	-	-	-	-	-	-
1054	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1055	-	0.0002	-	-	-	-	-	-	158	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1056	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.27	-	-	0.0031	-	-	22.2	-	-	-	-
9999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.43	-	-	-	-	-	88.4	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
0																												
1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
2	-	85%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	32%	-	-	-	100%	-	100%	-	100%	-	-
3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
5	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
6	100%	-	-	-	100%	-	-	36%	-	74%	-	-	-	-	-	-	-	-	27%	-	-	-	-	-	-	-	-	-
7	100%	100%	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	38%	-	100%	-	87%	-	-	-	95%	70%	-	-
8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25%	-	19%	-	-	-	-	100%	-	-	-	-
12	-	-	-	-	99%	-	72%	-	-	-	-	-	-	-	-	-	-	-	100%	-	53%	-	-	-	-	-	-	-
13	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	45%	-	22%	-	-	-	-	-	-	-
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15	-	-	-	-	99%	-	59%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
16	-	-	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	100%	-	100%	-	-	100%	-	-	-	-	-	-
17	100%	99%	-	-	-	-	-	-	-	68%	-	-	-	-	-	-	100%	-	100%	-	-	100%	-	-	-	-	-	-
18	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
19	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-	-	-	-	-
20	-	-	-	-	100%	-	70%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
21	-	61%	-	-	-	-	-	-	12%	-	-	-	-	-	-	-	5%	-	-	-	-	-	-	-	-	-	-	-
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31	-	-	-	-	7%	-	-	-	-	-	-	-	-	-	-	-	-	-	16%	-	-	-	-	-	-	-	-	-
32	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12%	-	-	-	-	-	-	-	-	-
33	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	-	-	-	-	-	-	-	-
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35	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	34%	-	-	-	-	-	-	-	-	-	-
36	-	-	-	-	-	-	-	-	9%	-	-	-	-	-	-	-	-	34%	-	-	-	-	-	-	-	-	-	-
37	-	-	-	-	-	-	-	-	31%	-	-	-	-	-	-	-	98%	100%	-	-	-	-	-	-	-	-	-	-
38	-	-	-	-	-	-	-	-	16%	-	-	-	-	-	-	-	55%	-	-	-	-	-	-	-	-	-	-	-
39	-	-	-	-	-	-	-	-	76%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
40	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
41	-	-	-	-	-	-	-	-	61%	-	-	-	-	-	-	-	-	51%	-	-	-	-	-	-	-	-	-	-
42	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	82%	-	-	-	-	-	-	-
43	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
44	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-
45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-
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47	-	-	-	-	-	-	-	-	62%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
48	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	77%	91%	-	-	-	-	-	-
49	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	21%	-	-	87%	-	-	-	-	-	-	-
50	-	100%	-	-	-	-	-	61%	65%	91%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
51	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	90%	-	-	28%	-	-	-	-	-	-	-
52	-	-	-	-	-	-	-	-	73%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
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57	-	-	-	-	94%	-	-	-	-	29%	-	-	-	25%	-	-	99%	56%	61%	-	100%	-	-	-	-	-	-	-
58	-	-	-	-	-	-	-	-	100%	96%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	75%	-	-	-	-	-	-	-	-	-
60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	86%	-	100%	100%	-	-	-	-	-	-
61	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
62	-	-	-	-	-	-	-	-	41%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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66	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	69%	99%	-	-	-	-	-	-
67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69%	73%	-	-	-	-	-	-
68	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69%	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
69	-	-	-	-	-	-	-	-	63%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
70	-	-	-	-	-	-	-	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	-	-	-	-	-	-	-
71	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
72	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
73	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
74	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-
75	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
76	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61%	-	-	-	-	-	-	-	-	-
77	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63%	-	100%	-	-	-	-	-	-	-
78	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	60%	-	100%	18%	-	-	-	-	-	-
79	100%	-	-	-	-	-	-	-	-	51%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
80	-	-	-	-	-	-	-	-	-	23%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
81	-	-	100%	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	-
82	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-
83	-	-	-	-	-	-	-	-	48%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
84	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	48%	-	-	100%	-	-	100%	-	-	-	-	-	-	-
85	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
86	-	-	-	-	-	-	-	-	30%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
87	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	-	-
88	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
89	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19%	-	-	-	-	-	-	-	-	-
90	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15%	-	-	-	-	-	-	-	-	-
91	-	-	-	-	20%	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-
92	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22%	-	-	14%	-	-	-	-	-	-
93	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	30%	-	-	-	-	-	-
94	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17%	-	-	-	-	-	-	-	-	-
95	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
96	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	13%	-	-	-	-	-	-	-	-	-
97	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	50%	-	-	-	-	-	-	-	-	-
98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	-	-	-	-	-	-	-
99	-	-	-	-	-	-	-	-	2%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
100	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2%	-	43%	-	-	-	-	-	-	-	-	-
101	-	-	-	-	48%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
102	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
103	-	-	-	-	29%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
104	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
105	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	55%	-	-	-	-	-	-	-	-	-
106	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	100%	-	-	-	-	-	-	-	-	-	-
107	-	100%	-	-	-	-	-	-	90%	100%	-	-	-	-	-	-	54%	35%	-	-	100%	-	-	-	-	-	-	-
108	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	65%	-	-	100%	-	-	-	-	-	-	-
109	-	-	-	-	-	-	-	-	85%	85%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
110	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	99%	-	-	100%	-	-	-	-	-	-	-
111	-	100%	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	-	80%	-	-	100%	-	-	-	-	-	-	-
112	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-
113	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	79%	-	-	87%	-	-	-	-	-	-	-
114	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
115	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63%	-	-	81%	-	-	-	-	-	-	-
116	-	-	-	-	-	-	-	-	91%	97%	-	-	-	-	-	-	-	30%	-	-	-	-	-	-	-	-	-	-
117	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
118	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
119	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
120	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	98%	-	-	-	-	-	-	-
121	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
122	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
123	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	92%	-	-	-	-	-	-	-
124	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33%	-	-	100%	-	-	-	-	-	-	-
125	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	66%	-	-	100%	-	-	-	-	-	-	-
126	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1%	-	-	98%	-	-	-	-	-	-	-
127	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33%	-	-	97%	-	-	-	-	-	-	-
128	-	100%	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-
129	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
130	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
131	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	100%	39%	-	-	-	-	-	-	-	-	-	-
132	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	47%	-	-	100%	-	-	-	-	-	-	-
133	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	69%	-	-	95%	-	-	-	-	-	-	-
134	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52%	-	-	93%	-	-	-	-	-	-	-
135	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
136	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
137	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
138	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69%	-	-	86%	-	-	-	-	-	-	-
139	-	-	-	-	-	-	-	-	11%	78%	-	-	-	-	100%	-	%	47%	-	-	75%	-	-	-	-	-	-	-
140	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
141	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
142	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
143	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	96%	-	-	-	-	-	-	-
144	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	100%	34%	-	-	100%	-	-	-	-	-	-	-
145	-	-	-	-	-	-	-	-	-	80%	-	-	-	86%	-	-	-	38%	-	-	93%	-	-	-	-	-	-	-
146	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	46%	-	-	84%	-	-	-	-	-	-	-
147	-	-	-	-	-	-	-	-	-	89%	-	-	-	100%	-	-	100%	100%	-	-	69%	-	-	-	-	-	-	-
148	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	60%	-	-	71%	-	-	-	-	-	-	-
149	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	97%	-	-	60%	-	-	97%	-	-	-	-	-	-	-
150	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
151	-	100%	-	-	-	-	-	-	100%	98%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
152	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
153	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
154	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
155	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
156	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-
157	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	97%	-	-	-	-	-	100%	-	-	-	-	-	-	-
158	-	-	100%	-	-	-	-	-	-	-	89%	-	16%	53%	-	-	100%	-	-	-	78%	92%	100%	14%	-	-	-	-
159	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	86%	92%	-	-	-	-	-	-
160	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	80%	81%	100%	100%	-	-	-	-
161	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	%	-	-	-	-	-	-
162	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	56%	-	84%	79%	-	-	-	-	-	-
163	-	-	-	-	-	-	-	-	-	92%	-	-	-	100%	-	-	-	98%	49%	-	-	97%	-	-	-	-	-	-
164	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-
165	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	9%	99%	-	-	-	-	-	-
166	-	-	-	-	-	-	-	-	40%	100%	-	-	-	-	-	-	79%	-	-	-	87%	100%	-	-	-	-	-	-
167	-	-	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
168	-	-	-	-	-	-	-	-	60%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
169	-	-	86%	100%	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	35%	83%	-	-	-	-	-	-
170	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
171	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	96%	-	-	-	-	-	-
172	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-	-
173	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	100%	97%	-	-	-	-	-	-
174	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
175	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	91%	100%	-	-	-	-	-	-
176	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-
177	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
178	-	100%	-	100%	-	-	-	-	100%	88%	-	-	-	-	-	-	100%	-	-	-	-	90%	-	100%	-	-	-	-
179	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	71%	94%	-	-	-	-	-	-
180	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	100%	-	-	-	100%	99%	-	-	-	-	-	-
181	-	-	-	100%	-	-	-	100%	100%	98%	-	-	-	-	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-
182	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
183	-	100%	100%	100%	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
184	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	99%	91%	-	-	-	-	-
185	-	100%	100%	-	-	-	-	-	79%	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
186	-	-	-	100%	-	-	-	98%	7%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
187	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
188	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-
189	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	99%	-	-	-	-
190	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	98%	-	-	-	-
191	-	100%	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
192	-	100%	-	100%	-	-	-	75%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
193	-	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	100%	-	-	-	-
194	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	100%	-	-	-	-
195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-
196	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	74%	-	-	-	55%	96%	100%	-	-	-	-
197	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	100%	-	-	-	100%	-	100%	-	-	-	-
198	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	73%	100%	-	96%	-	-	-	-
199	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
200	-	-	-	-	-	-	-	-	-	22%	-	-	-	-	-	-	-	-	-	-	54%	100%	-	-	-	-	-	-
201	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
202	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-
203	-	-	-	-	-	-	-	-	74%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
204	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
205	-	-	-	-	-	-	-	-	4%	-	-	-	-	-	69%	-	-	100%	-	-	-	-	-	-	-	-	-	-
206	-	-	-	-	-	-	-	-	-	-	-	-	-	-	89%	-	-	100%	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
207	-	-	-	-	-	-	85%	-	-	100%	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-
208	-	-	-	-	-	-	-	-	-	-	-	-	-	-	67%	-	-	100%	-	-	-	-	-	-	-	-	-	-
209	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75%	-	-	100%	-	-	-	-	-	-	-	-	-	-
210	-	%	-	-	-	-	-	-	-	100%	100%	-	-	-	89%	-	-	100%	-	-	-	-	-	-	-	-	-	-
211	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
212	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-	-	-	-	-	-	-
213	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58%	-	-	-	-	-	-	-	-	-	-	-	-	-
214	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	62%	-	-	57%	-	-	100%	-	-	-	-	-	-	-
215	-	-	-	-	-	-	-	-	-	-	-	-	-	-	80%	-	-	55%	-	-	-	-	-	-	-	-	-	-
216	-	100%	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
217	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
218	-	-	-	-	-	-	68%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-
219	-	-	-	-	-	-	30%	-	-	22%	-	-	-	-	97%	-	-	100%	-	-	100%	100%	-	-	-	-	-	-
220	-	-	-	-	-	-	-	-	-	91%	18%	-	-	57%	98%	-	-	100%	-	-	-	-	-	-	-	-	-	-
221	-	43%	-	-	-	-	-	-	61%	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
222	-	96%	-	-	-	-	-	-	-	100%	91%	-	-	95%	93%	-	-	100%	-	-	-	-	-	-	-	-	-	-
223	-	100%	-	-	-	-	-	-	-	7%	4%	-	-	27%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
224	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
225	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	96%	-	-	-	-	-	-
226	-	-	-	-	-	-	-	-	72%	100%	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
227	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-
228	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	100%	-	-	-	-
229	-	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-	-	-	-	-	100%	-	81%	-	-	-	-
230	-	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-	-	-	-	-	-	100%	-	92%	-	-	-	-
231	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
232	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
233	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
234	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	-	-	-	-
235	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
236	-	100%	-	-	-	-	-	-	83%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
237	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
238	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	77%	100%	-	-	-	-	-	-
239	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
240	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
241	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	88%	100%	-	-	-	-	-	-
242	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	72%	62%	-	-	-	-	-	-
243	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41%	78%	-	-	-	-	-	-
244	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	92%	-	-	-	-	-	-
245	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	74%	97%	-	-	-	-	-	-
246	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	100%	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
247	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	81%	-	-	-	79%	77%	-	-	-	-	-	-
248	-	-	98%	100%	-	-	-	-	-	100%	98%	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
249	-	-	100%	-	-	-	-	-	-	-	89%	-	-	4%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
250	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
251	-	-	-	-	-	-	-	-	-	-	7%	-	-	-	-	-	100%	-	-	-	-	92%	-	-	-	-	-	-
252	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
253	-	-	100%	100%	-	-	-	100%	-	98%	-	-	-	-	-	-	-	-	-	-	-	97%	53%	-	-	-	-	-
254	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
255	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	89%	100%	-	-	-	-	-
256	100%	-	-	100%	-	-	-	-	-	88%	100%	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-	-	-	-
257	-	-	-	-	-	-	-	-	-	31%	53%	-	-	-	-	-	100%	-	-	-	89%	88%	-	-	-	-	-	-
258	-	-	-	-	-	-	-	100%	-	-	-	-	-	35%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
259	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	8%	-	-	-	-	-	-	-	-	-	-	-	-	-
260	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
261	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	27%	-	-	-	-	-	-	-	-	-	-
262	-	100%	-	-	-	-	-	-	100%	94%	91%	-	-	-	-	-	3%	-	-	-	-	94%	-	-	-	-	-	-
263	-	-	-	-	-	-	-	100%	100%	88%	100%	-	-	-	-	-	-	-	-	-	100%	87%	-	-	-	-	-	-
264	-	100%	-	-	-	-	-	100%	-	78%	96%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
265	-	-	100%	5%	-	-	-	-	-	92%	-	-	-	-	-	-	-	100%	-	-	-	58%	-	-	-	-	-	-
266	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
267	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	79%	-	100%	-	-	-	-
268	-	100%	-	-	-	-	-	-	-	100%	-	-	87%	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-
269	-	94%	-	-	-	-	-	-	-	98%	-	-	100%	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
270	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	100%	-	-	100%	100%	-	-	-	-	-	-
271	-	100%	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	100%	-	-	-	-
272	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
273	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
274	-	-	-	-	-	-	-	100%	100%	100%	100%	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
275	-	-	-	-	-	-	-	100%	100%	100%	-	77%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
276	-	-	100%	-	-	-	-	100%	100%	51%	86%	-	-	75%	99%	-	99%	-	-	-	-	65%	-	-	-	-	-	-
277	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
278	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-
279	-	100%	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	100%	100%	100%	100%	-	-	-	-
280	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	-	97%	-	-	-	-	-	-
281	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
282	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
283	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	91%	-	-	-	-	-	-
284	-	100%	-	-	100%	-	-	100%	100%	91%	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
285	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	97%	-	-	-	-	-	-
286	84%	100%	-	-	-	-	-	-	100%	94%	-	-	-	-	-	-	64%	-	-	-	-	100%	-	-	-	-	-	-
287	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-
288	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	94%	-	-	-	-	-	-
290	-	-	-	-	-	-	-	-	-	73%	-	-	-	-	-	-	100%	-	-	-	-	82%	-	-	-	-	-	-
291	100%	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
292	100%	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
293	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
294	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
295	100%	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-	-	-	67%	-	-	-	-	-	-
296	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
297	100%	-	10%	100%	-	-	-	-	100%	64%	100%	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
298	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
299	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	96%	-	-	-	-	-	-
300	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
301	-	-	-	-	-	-	-	-	-	69%	-	-	-	-	-	-	93%	-	-	-	98%	80%	-	-	-	-	-	-
302	81%	-	-	-	-	-	-	-	-	83%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
303	-	-	-	-	-	-	-	-	-	97%	100%	-	-	-	-	-	85%	-	-	-	-	84%	-	-	-	-	-	-
304	100%	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	100%	-	-	-	-	93%	-	-	-	-	-	-
305	-	-	90%	-	-	-	-	-	100%	98%	57%	-	-	-	71%	-	100%	-	-	-	100%	81%	-	-	-	-	-	-
306	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	94%	-	-	72%	100%	100%	65%	-	-	-	-
307	-	100%	100%	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	89%	-	-	-	-
308	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	1%	44%	-	-	-	-	-
309	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	97%	-	-	-	-	-	-
310	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	72%	100%	-	99%	-	-	-	-
311	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	96%	100%	-	-	-	-
312	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	87%	-	-	-	-	-
313	-	-	-	-	-	-	-	-	-	100%	95%	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
314	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	100%	96%	-	-	-	-	-
315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	91%	100%	97%	68%	-	-	-	-
316	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	99%	92%	-	-	-	-
317	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	100%	100%	99%	-	-	-	-
318	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	92%	97%	-	-	-	-
319	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
320	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
321	-	-	100%	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	74%	99%	-	-	-	-	-	-
322	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	53%	100%	-	-	-	-	-	-
323	-	-	-	-	-	-	-	-	-	93%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
324	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
325	-	-	57%	-	-	-	-	-	-	%	-	-	-	-	-	-	100%	-	-	-	73%	94%	-	-	-	-	-	-
326	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	84%	100%	-	-	-	-	-	-
327	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	85%	97%	99%	98%	-	-	-	-
328	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
329	-	-	100%	100%	-	-	-	-	-	88%	-	-	-	-	-	-	100%	-	-	-	100%	91%	-	-	-	-	-	-
330	100%	-	-	-	-	-	-	-	-	83%	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
331	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
332	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
333	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	94%	-	-	-	-	-	-
334	-	-	100%	-	-	-	-	-	-	96%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
335	-	-	100%	-	-	-	-	-	-	75%	-	-	-	-	-	-	100%	-	-	-	100%	61%	-	-	-	-	-	-
336	100%	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-	100%	-	-	-	87%	83%	-	-	-	-	-	-
337	-	100%	100%	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	95%	98%	96%	-	-	-	-
338	-	100%	-	-	-	-	-	-	-	98%	-	-	100%	-	-	-	-	100%	-	-	100%	100%	100%	100%	-	-	-	-
339	-	100%	100%	100%	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
340	-	-	-	-	-	-	-	-	-	10%	-	-	-	-	-	-	100%	-	-	-	-	96%	-	-	-	-	-	-
341	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
342	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-
343	-	100%	100%	-	-	-	-	-	-	94%	100%	-	100%	-	-	86%	-	-	-	-	-	100%	100%	100%	-	-	-	-
344	-	100%	100%	-	-	-	-	-	-	98%	100%	-	95%	-	-	-	-	100%	-	-	-	100%	82%	100%	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
345	-	-	-	-	-	-	-	-	-	81%	-	-	-	-	82%	-	100%	100%	-	-	100%	87%	-	-	-	-	-	-
346	-	100%	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	97%	57%	-	-	100%	-	-	-	-	-	-	-
347	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	58%	-	-	100%	-	-	-	-	-	-	-
348	-	-	100%	100%	-	-	-	-	-	-	4%	-	84%	%	-	-	100%	-	-	-	-	92%	-	-	-	-	-	-
349	-	-	100%	100%	-	-	-	-	-	-	55%	-	-	-	-	-	100%	-	-	-	-	100%	100%	-	-	-	-	-
350	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	86%	-	-	-	-	93%	100%	-	-	-	-	-
351	-	-	100%	100%	-	-	-	-	-	100%	14%	-	-	-	100%	-	-	58%	-	-	-	89%	-	-	-	-	-	-
352	-	-	-	-	-	-	-	-	-	99%	38%	-	-	-	-	-	-	-	-	-	-	89%	61%	-	-	-	-	-
353	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-
354	-	-	-	-	-	-	-	-	-	-	49%	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-
355	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	95%	-	-	-	-	-	-
356	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
357	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
358	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
359	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
360	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	18%	-	-	-	-	97%	-	-	-	-	-	-
361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	21%	-	-	-	-	-
362	-	100%	100%	-	-	-	-	-	77%	73%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
363	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	55%	-	-	-	-	-
364	-	100%	100%	100%	-	-	-	100%	-	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-
365	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52%	-	-	93%	96%	-	100%	-	-	-	-
366	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
367	-	100%	-	100%	-	-	-	100%	100%	100%	86%	-	-	79%	98%	-	-	-	-	-	-	-	-	-	-	-	-	-
368	-	100%	-	-	-	-	-	100%	-	100%	100%	-	99%	100%	100%	-	-	61%	-	-	82%	99%	99%	93%	-	-	-	-
369	-	-	-	-	-	-	-	-	-	-	-	-	-	-	68%	-	-	100%	-	-	100%	68%	-	-	-	-	-	-
370	-	-	100%	90%	-	-	-	-	100%	100%	100%	-	-	-	84%	-	100%	99%	-	-	100%	98%	-	-	-	-	-	-
371	-	-	-	-	100%	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
372	-	-	-	-	-	-	-	-	50%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
373	-	-	-	-	-	-	-	-	68%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
374	-	100%	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-
375	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
376	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76%	34%	-	-	100%	-	-	-	-	-	-	-
377	-	-	-	-	-	-	-	-	-	67%	-	-	-	-	-	-	-	40%	-	-	83%	-	-	-	-	-	-	-
378	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
379	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	84%	-	-	34%	-	-	-	-	-	-	-	-	-	-
380	-	100%	-	-	-	-	-	-	86%	72%	-	-	-	-	100%	-	-	39%	-	-	100%	-	-	-	-	-	-	-
381	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
382	-	-	-	-	-	-	-	-	100%	21%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
383	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	56%	91%	-	-	-	-	-	-
384	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-	-
385	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
386	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
387	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
388	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
389	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-
390	-	100%	57%	100%	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	100%	-	-	-	100%	-	100%	-	-	-	-
391	-	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
392	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
393	-	-	-	-	-	-	-	-	98%	100%	-	-	-	-	-	-	-	9%	-	-	100%	-	-	-	-	-	-	-
394	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	51%	-	-	90%	-	-	-	-	-	-	-
395	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	48%	-	-	87%	-	-	-	-	-	-	-
396	-	-	-	-	-	-	-	-	100%	79%	94%	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
397	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	%	-	-	100%	8%	-	-	-	-	-	-
398	-	-	-	-	50%	-	-	-	-	100%	-	-	-	-	-	-	-	%	-	-	100%	18%	-	-	-	-	-	-
399	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
400	-	-	-	-	-	-	-	-	-	22%	-	-	-	-	-	-	-	49%	-	-	73%	-	-	-	-	-	-	-
401	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-
402	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	93%	-	-	-	-	-	-	-
403	-	-	-	-	-	-	-	-	47%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
404	-	-	-	-	-	-	-	-	30%	-	-	-	-	-	-	-	-	34%	-	-	-	-	-	-	-	-	-	-
405	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
406	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	-
407	-	100%	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	98%	-	-	-	95%	-	-	-	-	-	-	-
408	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	89%	-	-	79%	-	-	-	-	-	-	-
409	-	36%	-	-	-	-	-	-	-	100%	-	-	-	-	68%	-	-	24%	-	-	70%	-	-	-	-	-	-	-
410	-	-	-	-	-	-	-	-	-	-	-	-	-	-	88%	-	-	-	-	-	-	-	-	-	-	-	-	-
411	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76%	-	-	-	-	-	87%	-	-	-	-	-	-	-
412	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
413	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
414	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
415	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
416	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	99%	-	-	100%	-	-	-	-	-	-	-	-	-	-
417	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17%	-	-	100%	-	-	-	-	-	-	-	-	-	-
418	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	100%	-	-	-	-	-	-	-	-	-	-
419	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	91%	-	-	88%	-	-	100%	-	-	-	-	-	-	-
420	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	37%	-	-	54%	-	-	87%	100%	-	-	-	-	-	-
421	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93%	-	-	24%	-	-	-	-	-	-	-	-	-	-
422	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-
423	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	98%	-	-	-	-	-	-	-
424	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
425	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
426	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
427	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
428	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
429	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
430	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	43%	-	-	94%	-	-	-	-	-	-	-
431	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
432	-	100%	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
433	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	100%	-	-	100%	95%	-	-	-	-	-	-
434	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95%	97%	-	-	-	-	-	-
435	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	100%	-	-	-	-	-	-
436	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34%	-	-	-	-	-	-
437	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
438	100%	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	99%	-	-	-	96%	87%	-	-	-	-	-	-
439	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-
440	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	99%	-	-	-	-	-	-
441	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	100%	-	-	-	-	-	-
442	-	-	-	-	-	-	-	-	-	65%	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-
443	100%	-	-	-	-	-	-	-	-	89%	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-
444	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	97%	99%	-	-	-	-	-	-
445	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	99%	97%	-	-	-	-	-	-
446	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-
447	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
448	-	-	-	-	72%	-	-	-	36%	-	-	-	-	-	-	-	100%	-	33%	-	100%	-	-	-	-	-	-	-
449	-	-	23%	-	1%	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	-	-	-	-	-	-	-	-
450	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	67%	54%	-	88%	-	-	-	-	-	-
451	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	-	-	-	-	99%	8%	86%	-	-	-	-	-	-
452	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	100%	100%	-	46%	-	29%	-	-	-	-	-	-
453	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	87%	-	-	-	-	-	-
454	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	94%	-	-	-	-	-	-
455	87%	-	-	-	-	-	-	-	-	93%	97%	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
456	-	-	-	-	-	-	-	-	-	79%	60%	-	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-
457	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
458	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
459	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
460	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
461	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
462	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
463	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-	-	-
464	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-
465	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
466	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	99%	-	100%	-	-	-	-	-	-	-	-	-	-	-
467	-	-	-	-	24%	-	-	-	-	-	-	-	-	-	-	-	-	11%	-	-	52%	100%	-	-	-	-	-	-
468	-	-	100%	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
469	-	-	100%	-	-	-	100%	-	-	100%	-	-	-	-	-	-	100%	-	-	100%	100%	100%	-	-	-	-	-	-
470	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
471	45%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
472	64%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
473	-	-	-	-	24%	-	-	-	-	-	-	-	-	-	-	-	-	-	25%	10%	-	-	-	-	-	-	-	-
474	-	-	-	-	23%	-	-	-	-	-	-	-	-	-	-	-	-	-	25%	16%	-	-	-	-	-	-	-	-
475	-	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	25%	25%	-	-	-	-	-	-	-	-
476	-	-	-	-	50%	-	-	-	-	-	-	-	-	-	-	-	-	-	50%	40%	-	-	-	-	-	-	-	-
477	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	50%	-	9%	41%	-	50%	-	-	-	-	-	-
478	-	-	-	-	24%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
479	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
480	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	99%	-	-	-	-	-	-	-
481	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
482	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
483	82%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
484	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	50%	-	-	-	-	-	-
485	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	100%	100%	-	-	18%	-	-	-	-	-	-
486	-	-	-	-	-	-	-	-	-	78%	-	-	-	-	-	-	-	5%	-	-	-	68%	-	-	-	-	-	-
487	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
488	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	98%	-	100%	-	-	-	-	-	-
489	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	95%	-	100%	-	-	-	-	-	-
490	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	99%	-	-	-	-	-	-
491	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
492	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	2%	-	-	-	-	-	-
493	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	60%	-	-	-	-	-	-
494	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	78%	-	-	-	-	-	-
495	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	99%	-	-	-	-	-	-
496	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	28%	-	-	-	-	-	-
497	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	23%	-	-	-	-	-	-
498	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	85%	-	-	-	-	-	-
499	100%	91%	98%	-	-	-	-	-	-	32%	-	-	-	-	-	-	1%	-	98%	-	-	91%	-	-	-	-	-	-
500	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	72%	-	-	11%	-	-	-	-	-	-
501	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27%	-	100%	20%	-	81%	-	-	-	-	-	-
502	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	48%	-	-	-	-	40%	-	-	-	-	-	-
503	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	96%	-	-	-	-	-	-
504	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	-	-	-	-
505	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
506	-	-	-	-	-	-	-	-	-	61%	-	-	-	-	-	-	-	17%	100%	-	-	98%	-	-	-	-	-	-
507	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
508	-	-	100%	-	-	-	-	-	-	77%	-	-	-	-	-	-	100%	100%	98%	-	-	-	-	-	-	-	-	-
509	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
510	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	%	98%	-	-	-	-	-	-	-	-	-
511	39%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	62%	-	-	100%	-	-	-	-	-	-
512	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
513	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
514	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
515	-	-	-	-	-	-	-	-	-	93%	-	-	-	-	100%	-	-	100%	-	-	100%	-	-	-	-	-	-	-
516	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	83%	-	-	99%	-	-	-	-	-	-	-
517	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
518	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	99%	-	-	-	-	-	-	-
519	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	78%	-	-	-	-	-	-	-
520	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	93%	-	-	-	-	-	-	-
521	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-	-	-	-	-
522	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	92%	-	-	-	-	-	-	-
523	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
524	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	65%	-	-	-	-	-	-	-
525	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
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527	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
528	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	95%	-	-	-	-	-	-	-
529	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	64%	-	-	70%	-	-	-	-	-	-	-
530	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	5%	-	-	85%	-	-	-	-	-	-	-
531	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	100%	13%	-	-	94%	-	-	-	-	-	-	-
532	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27%	-	-	95%	-	-	-	-	-	-	-
533	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	85%	-	-	84%	-	-	-	-	-	-	-
534	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
535	-	100%	-	-	-	-	-	-	92%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
536	-	-	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
537	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
538	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
539	-	-	-	-	-	-	-	-	98%	100%	-	-	-	-	-	-	-	3%	-	-	100%	-	-	-	-	-	-	-
540	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
541	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
542	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	96%	-	100%	-	-	-	100%	-	-	-	-	-	-	-
543	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
544	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
545	-	-	-	-	-	-	-	-	100%	40%	-	-	-	-	83%	-	-	-	-	-	-	-	-	-	-	-	-	-
546	-	-	-	-	-	-	-	-	72%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
547	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
548	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
549	-	-	-	-	-	-	-	-	42%	97%	-	-	-	-	-	-	100%	6%	-	-	-	-	-	-	-	-	-	-
550	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
551	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
552	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-
553	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
554	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	100%	-	-	-	-	-	-	-
555	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	99%	-	-	-	-	-	-	-
556	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	93%	-	-	-	-	-	-	-	-	-	-	-	-	-
557	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	99%	-	-	-	-	-	-	-
558	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-
559	-	-	-	-	-	-	-	-	-	64%	-	-	-	-	-	-	-	98%	-	-	100%	-	-	-	-	-	-	-
560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	90%	-	-	-	-	-	-	-
561	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
562	-	-	-	-	-	-	-	-	-	45%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
563	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
564	-	-	-	-	10%	-	-	-	-	96%	-	-	-	-	-	-	-	16%	-	-	90%	-	-	-	-	-	-	-
565	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	23%	-	-	95%	22%	-	-	-	-	-	-
566	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
567	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
568	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17%	-	-	100%	-	-	-	-	-	-	-
569	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
570	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
571	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	79%	-	-	21%	-	-	-	-	-	-
572	-	-	-	-	100%	-	100%	-	-	48%	-	-	-	-	-	-	-	-	20%	-	-	14%	-	-	-	-	-	-
573	-	-	-	-	-	-	100%	-	-	88%	-	-	-	-	-	-	100%	-	%	-	-	-	-	-	-	-	-	-
574	100%	-	-	-	-	-	-	-	-	55%	-	-	-	-	-	-	-	-	100%	-	-	78%	-	-	-	-	-	-
575	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	14%	-	-	-	-	-	-
576	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-
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578	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	-	-
579	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	57%	-	94%	-	-	-	-	-	-	-
580	-	-	100%	-	100%	-	100%	-	-	100%	-	-	-	-	-	-	-	-	100%	-	100%	100%	-	-	-	-	-	-
581	-	-	100%	-	100%	-	100%	-	-	100%	-	-	-	-	-	-	100%	-	100%	-	100%	100%	-	-	-	-	-	-
582	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	96%	-	100%	-	-	-	-	-	-
583	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
584	-	-	-	-	-	-	-	-	-	87%	100%	-	-	-	99%	-	-	-	-	-	100%	-	-	-	-	-	-	-
585	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	100%	-	-	79%	-	-	-	-	-	-	-
586	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-
587	-	100%	-	-	100%	-	-	-	81%	-	-	-	-	-	-	-	-	80%	-	-	-	-	-	-	-	-	-	-
588	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-
589	-	-	100%	-	100%	-	100%	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
590	-	-	-	-	24%	-	-	-	-	-	-	-	-	-	-	-	-	23%	-	-	34%	-	-	-	-	-	-	-
591	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
592	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77%	-	-	-	-	-	-
593	-	-	-	-	22%	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
594	-	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
595	-	-	-	-	17%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
596	-	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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598	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13%	-	-	-	-	-	-	-	-	-
599	-	-	-	-	24%	-	-	-	-	-	-	-	-	-	-	-	-	-	25%	-	-	-	-	-	-	-	-	-
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603	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	100%	-	-	-	-	-	-	-
604	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
605	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
606	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
607	-	-	-	-	22%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
608	-	-	-	-	21%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
609	-	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
610	-	-	-	-	10%	-	-	-	-	-	-	-	-	-	-	-	-	-	14%	-	-	-	-	-	-	-	-	-
611	-	-	-	-	%	-	-	-	-	-	-	-	-	-	-	-	-	-	13%	-	-	-	-	-	-	-	-	-
612	-	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
613	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
614	-	-	-	-	50%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
615	-	-	-	-	48%	-	-	-	-	-	-	-	-	-	-	-	-	-	49%	-	-	%	-	-	-	-	-	-
616	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
617	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
618	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-
619	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
620	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
621	99%	-	-	-	-	-	71%	-	-	98%	-	-	-	100%	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
622	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	85%	-	-	-	-	-	-
623	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
624	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	89%	-	-	-	-	-	-
625	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
626	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
627	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
628	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
629	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	79%	-	-	-	-	-	-
630	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
631	38%	100%	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
632	-	-	-	-	-	-	100%	-	-	13%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
633	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-	-	-	40%	-	-	-	-	-	-
634	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	16%	-	-	-	-	100%	-	-	-	-	-	-
635	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	-	-	-	-	-	-
636	-	-	-	-	100%	-	100%	-	-	86%	-	-	-	-	-	-	-	-	-	-	-	64%	-	-	-	-	-	-
637	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
638	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-
639	-	-	-	-	100%	-	100%	-	-	88%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
640	78%	-	-	-	-	-	81%	-	-	89%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
641	34%	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
642	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
643	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
644	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
645	-	-	-	-	100%	100%	100%	-	-	-	-	-	-	-	-	-	100%	99%	100%	-	-	42%	-	-	-	-	-	-
646	-	100%	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
647	-	100%	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	66%	100%	-	-	-	99%	-	-	-	-	-	-
648	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
649	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
650	-	-	-	-	-	-	100%	-	-	98%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
651	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
652	-	100%	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	96%	100%	-	-	-	100%	-	-	-	-	-	-
653	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-
654	-	100%	-	-	-	-	-	-	-	69%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
655	-	85%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
656	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	100%	-	100%	100%	-	-	-
657	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	100%	100%	-	-	-
658	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
659	-	-	100%	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-
660	-	98%	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	-	-	-	-
661	-	-	-	-	9%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
662	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	100%	-	-	-	-	-	-
663	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	1%	-	-	-	-	-	-	-	-	-	-
664	100%	100%	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
665	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
666	-	-	-	-	-	-	100%	-	-	59%	-	-	-	-	-	-	48%	-	100%	-	-	-	-	-	-	-	-	-
667	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-
668	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
669	-	95%	-	-	-	-	100%	-	-	86%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
670	100%	100%	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	99%	100%	-	-	-	100%	-	-	-	-	-	-
671	-	81%	-	-	-	-	100%	-	-	93%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
672	-	-	-	-	100%	-	100%	-	-	1%	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-
673	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	89%	-	-	-	-	-	-
674	86%	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	89%	-	-	-	-	-	-
675	86%	-	-	-	-	-	-	-	-	100%	-	-	-	73%	-	-	100%	-	-	-	-	90%	-	-	-	-	-	-
676	-	-	-	-	100%	-	-	32%	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
677	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
678	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
679	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
680	-	94%	-	-	-	-	100%	13%	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
681	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2%	-	-
682	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54%	-	-	-	-	-	-	-
683	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	-	-	-	-	-
684	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	89%	-	-	-	-	-	-	-	-	-
685	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	72%	-	-	-	-	-	-	-	-	-
686	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	70%	-	-	-	-	-	-	-	-	-
687	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	81%	-	-	-	-	-	-	-	-	-
688	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	48%	-	-	-	-	-	-	-	-	-
689	-	-	-	-	-	17%	-	-	-	-	-	-	-	-	-	-	-	-	14%	-	18%	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
690	-	-	-	-	25%	-	-	-	-	-	-	-	-	-	-	-	-	-	14%	-	15%	-	-	-	-	-	-	-
691	28%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10%	-	-	-	-	-	-	-	-	-
692	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24%	-	-	-	-	-	-	-	-	-
693	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25%	-	-	-	-	-	-	-	-	-
694	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23%	-	-	-	-	-	-	-	-	-
695	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
696	100%	-	-	100%	-	-	-	-	-	100%	-	-	100%	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-
697	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
698	-	-	-	-	-	-	-	-	-	89%	100%	-	100%	100%	-	87%	-	-	-	-	-	100%	-	100%	-	-	-	-
699	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
700	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	42%	-	-	-	-	-	-	-	-	-
701	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	43%	-	-	-	-	-	-	-	-	-
702	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
703	-	-	-	-	70%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
704	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13%	-	-	-	-	-	-	-	-	-
705	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	25%	-	-	-	-	-	-	-
706	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	%	100%	-	%	68%	-	-	73%	-	-	-
707	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	63%	-	-	-	-	-	-	-	-	-
708	-	-	-	-	13%	-	-	-	-	-	-	-	-	-	-	-	-	-	23%	-	-	-	-	-	-	-	-	-
709	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4%	-	-	-	-	-	-	-	-	-
710	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-
711	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-	-	-	-	-
712	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	91%	-	-	-	-	-	-	-
713	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	63%	-	-	-	-	-	-
714	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	94%	-	-	-	-	-	-
715	-	-	-	-	-	-	56%	12%	-	-	-	-	-	-	-	-	-	75%	-	-	-	-	-	28%	-	-	-	-
716	-	-	-	-	-	-	-	81%	-	-	-	-	-	-	-	-	-	13%	-	-	-	-	-	85%	-	-	-	-
717	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
718	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
719	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	91%	52%	-	-	-	-	-
720	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
721	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	100%	-	-	-	-	-
722	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
723	-	-	-	-	-	-	-	-	-	-	100%	-	100%	100%	93%	100%	-	-	-	-	-	-	-	-	-	-	-	-
724	-	-	100%	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	30%	-	-	-	100%	100%	91%	-	-	-	-
725	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	94%	-	-	-	-	-	-	-	-	-	-	-	-	-
726	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	63%	-	-	-	-	-	-	-	-	-	-	-	-	-
727	-	100%	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
728	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
729	-	100%	-	-	-	-	-	-	-	-	-	-	-	9%	93%	-	-	-	-	-	-	-	-	-	-	-	-	-
730	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-
731	-	-	-	-	-	-	-	-	-	-	100%	-	100%	100%	-	98%	-	-	-	-	-	-	-	-	-	-	-	-
732	-	-	100%	-	-	-	-	-	-	100%	74%	-	-	-	-	-	100%	-	-	-	-	89%	-	-	-	-	-	-
733	-	-	-	-	-	-	-	-	-	15%	-	-	-	-	-	-	100%	-	-	-	-	45%	100%	-	-	-	-	-
734	-	-	100%	-	-	-	-	-	-	61%	-	-	-	-	-	-	100%	-	-	-	-	67%	-	-	-	-	-	-
735	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
736	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	63%	77%	-	-	-	-	-	-
737	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	70%	-	-	100%	-	-	-	-	-	-	-
738	100%	100%	-	-	-	-	-	-	-	44%	-	-	-	-	-	-	-	-	-	-	38%	-	-	-	100%	100%	-	-
739	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-	87%	-	-	-
740	100%	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	95%	56%	-	-
741	-	-	-	-	-	-	100%	15%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
742	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	13%	58%	99%	-	-	-	100%	-	-	-
743	-	-	-	-	-	-	-	99%	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
744	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	94%	-	-	-	-	-
745	-	100%	100%	-	-	-	-	-	-	97%	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
746	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
747	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	99%	99%	-	-	-	-
748	-	100%	-	-	-	100%	-	28%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	92%	-	-	-	-	-
749	-	100%	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-
750	-	-	100%	100%	-	-	-	100%	-	100%	100%	-	-	100%	67%	100%	-	-	-	-	100%	100%	-	-	-	-	-	-
751	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
752	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	91%	99%	-	-	-	-	-
753	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-	-	-	-	-	-	-
754	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	97%	99%	-	-	-	-
755	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	89%	97%	98%	-	-	-	-
756	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	95%	99%	-	-	-	-
757	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	88%	-	-	-	-	-	-
758	-	-	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
759	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	3%	-	-	-	-	-	-	-	-	-	-
760	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
761	-	100%	-	-	-	-	100%	100%	-	68%	-	-	-	-	-	-	-	61%	63%	-	100%	37%	-	100%	-	100%	-	-
762	-	-	-	-	-	-	87%	100%	-	-	-	-	-	-	-	-	-	31%	-	-	-	-	-	-	-	-	-	-
763	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
764	100%	-	-	-	-	-	-	-	-	98%	-	-	91%	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-
765	-	-	-	100%	-	-	100%	100%	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	100%	-	-
766	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
767	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	85%	75%	-	100%	-	100%	-	-
768	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	98%	-	-	-	-
769	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
770	100%	-	-	100%	-	-	100%	100%	-	-	-	-	-	-	-	-	-	83%	-	-	-	-	-	-	-	-	-	-
771	100%	100%	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	25%	100%	-	-	-	-	-	97%	-	100%	-	-
772	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
773	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
774	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	-
775	-	-	-	-	100%	-	-	9%	-	-	-	-	-	-	-	-	-	-	-	69%	100%	-	-	-	99%	100%	-	-
776	87%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	73%	-	98%	-	-	-	99%	95%	-	-
777	-	-	-	-	-	-	-	38%	-	-	-	-	-	-	-	-	-	-	-	-	96%	-	-	-	100%	94%	-	-
778	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	13%	-	98%	-	-	-	100%	100%	-	-
779	-	-	-	-	2%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
780	-	-	100%	-	-	-	-	-	-	51%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-
781	99%	97%	-	100%	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	100%	100%	-	-
782	-	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	83%	46%	-	-	-	-	-	-
783	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92%	-	-	-	-	52%	-	-
784	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-
785	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
786	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
787	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	20%	-	-	-	-	-	-	-	-	-	-
788	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
789	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	-	-	-	3%	-	-	-	-	-	-	-	-	-	-
790	-	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	-	-	23%	-	-	-	-	-	-	-	-	-	-
791	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	38%	-	-	-	-	-	-	-	-	-	-
792	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
793	-	-	-	-	-	100%	99%	-	100%	-	-	-	-	-	-	-	-	-	27%	-	-	-	-	-	-	-	-	-
794	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	39%	-	-	-	-	-	-	-	-	-	-
795	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
796	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
797	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
798	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	98%	-	-	-	-
799	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
800	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
801	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
802	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95%	-	-	-	-
803	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
804	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
805	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
806	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
807	100%	100%	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
808	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	93%	-	-	-	-	-	100%	-	97%	-	-
809	100%	100%	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
810	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34%	-	-	-	-	-	-	-	-	-	-
811	100%	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	73%	-	-	-	-	-	-	-	-	-	-
812	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	33%	-	-	-	-	-	100%	-	-	-	-
813	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	100%	-	-
814	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
815	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90%	97%	-	-	-	-	-	-
816	-	-	-	85%	-	-	-	100%	-	-	-	-	-	-	-	91%	-	35%	-	-	92%	80%	-	-	-	-	-	-
817	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61%	100%	-	-	-	-	21%	100%	-	-	-	-	-	-
818	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	72%	-	100%	-	-	-	91%	98%	-	-	-	-	-	-
819	100%	100%	-	100%	-	-	-	100%	-	100%	-	-	-	-	-	-	100%	93%	-	-	92%	91%	-	-	-	-	-	-
820	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	89%	-	-	-	-	-	-	-
821	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	83%	93%	-	-	-	-	-	-
822	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	91%	-	-	-	-
823	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
824	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	85%	-	-	-	-	-	-
825	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	100%	-	-	-	-	-	-
826	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	88%	61%	-	-	-	-	-	-
827	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	95%	95%	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
828	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	81%	97%	-	-	-	-	-	-
829	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	84%	100%	-	-	-	-	-	-
830	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	-	-	-	56%	63%	-	100%	-	-	-	-
831	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-
832	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	93%	100%	-	-	-	-	-	-
833	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	51%	92%	-	-	-	-	-	-
834	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	86%	100%	-	95%	97%	-	26%	-	-	-	-
835	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
836	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	3%	-	-	-	-	-	93%	-	-	-	-
837	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	76%	99%	-	-	-	-	-	-
838	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	59%	60%	-	-	-	-	-	-
839	-	100%	100%	-	-	-	-	-	-	88%	100%	-	-	-	-	-	100%	-	-	-	82%	1%	-	-	100%	-	-	-
840	100%	-	-	-	-	-	-	-	-	74%	-	-	-	-	-	-	56%	100%	100%	-	-	85%	-	-	100%	-	-	-
841	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-
842	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63%	-	100%	-	-
843	-	100%	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-
844	-	-	-	-	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	100%	97%	-	-	99%	-	-	-
845	-	-	-	-	-	-	-	-	-	82%	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-
846	-	-	-	-	-	-	-	-	-	95%	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-
847	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	92%	-	-	-	-
848	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93%	-	-	-	-
849	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	53%	-	-	-	-
850	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	52%	-	-	-	-
851	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	54%	68%	-	-	-	-
852	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	100%	-	-	-	-
853	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	98%	-	-	-	-
854	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	94%	-	-	-	-
855	-	-	-	-	-	-	-	-	-	-	-	91%	83%	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
856	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	-	-	-	-	-	-	-	100%	-	97%	-	-	-	-
857	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35%	-	-	-	100%	-	100%	-	-	-	-
858	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	100%	-	78%	-	-	-	-
859	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26%	-	-	100%	-	98%	-	-	-	-
860	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	100%	-	89%	-	-	-	-
861	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	12%	-	-	89%	-	97%	-	-	-	-
862	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	100%	-	-	100%	100%	-	-	-	-	-	-
863	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93%	100%	-	-	90%	95%	-	-	-	-	-	-
864	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
865	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	93%	-	-	77%	-	-	-	-	-	-	-
866	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-
867	-	-	-	-	-	-	-	-	-	90%	-	-	-	100%	-	-	-	100%	-	-	100%	100%	-	-	-	-	-	-
868	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	96%	100%	-	-	-	-	-	-
869	-	100%	100%	100%	-	-	-	-	-	72%	-	-	-	-	-	-	100%	94%	-	-	100%	100%	-	-	-	-	-	-
870	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	97%	-	-	99%	100%	-	-	-	-	-	-
871	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
872	-	100%	-	100%	-	-	-	-	-	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
873	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
874	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-
875	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	96%	74%	-	-	-	-
876	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	97%	-	-	-	-	-
877	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
878	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
879	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	99%	-	-	-	-
880	-	100%	-	-	-	-	-	-	-	82%	-	-	-	-	-	-	-	95%	-	-	-	100%	-	95%	-	-	-	-
881	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
882	-	100%	-	-	-	-	-	-	-	95%	-	99%	100%	35%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
883	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	100%	-	-	-	-	-	-	-
884	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	97%	-	100%	-	-	100%	100%	-	-	-	-	-	-
885	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	100%	-	100%	-	-	80%	97%	-	-	-	-	-	-
886	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-
887	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-
888	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	100%	-	-	-	-	-	-	-
889	-	-	-	100%	-	-	100%	75%	-	-	-	-	-	-	-	-	-	64%	-	-	100%	98%	-	-	-	-	-	-
890	-	-	-	100%	-	-	100%	100%	-	100%	-	-	-	-	37%	-	-	100%	-	-	100%	-	-	-	-	-	-	-
891	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-
892	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	71%	-	-	-
893	-	100%	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-
894	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-	-	-	85%	-	-	-	-	-	-	-	-	-	-
895	-	100%	-	96%	-	-	-	-	73%	98%	-	-	-	-	-	-	-	95%	-	-	96%	-	100%	-	100%	-	-	-
896	-	100%	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	42%	-	-	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
897	-	-	-	-	-	-	-	8%	-	-	-	-	-	-	-	-	-	30%	-	-	80%	80%	-	-	-	-	-	-
898	-	95%	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-
899	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	-	-	-	-	-	-	-
900	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
901	-	99%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	99%	-	-	-
902	100%	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	100%	-	-	92%	-	-	-	-	-	-	-
903	-	100%	-	100%	-	-	-	92%	-	100%	-	-	-	-	-	100%	100%	97%	-	-	56%	31%	-	-	-	-	-	-
904	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	100%	-	-	-	-	-	-
905	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	55%	-	-	-	-	-	-
906	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	100%	98%	-	-	-	-	-	-
907	-	100%	-	100%	-	-	-	-	-	100%	94%	-	-	-	55%	-	-	-	-	-	100%	87%	-	-	-	-	-	-
908	-	66%	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-
909	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	94%	-	100%	-	62%	-	-	-
910	100%	98%	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	86%	-	-	82%	-	-	-	-	-	-	-
911	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91%	-	-	-	-	-	-
912	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	97%	-	-	-	65%	98%	-	-	-	-	-
913	-	100%	-	78%	-	-	-	-	-	99%	-	-	-	-	-	-	-	100%	-	-	80%	76%	66%	-	-	-	-	-
914	100%	-	100%	100%	-	-	-	-	-	97%	-	-	-	100%	-	-	-	-	-	-	-	86%	100%	78%	-	90%	-	-
915	-	-	-	100%	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-	-	85%	-	73%	-	-	-	-
916	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-
917	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	96%	-	100%	-	-	-	-
918	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	98%	-	-	-
919	-	100%	100%	100%	-	-	-	-	-	100%	-	-	-	-	72%	-	-	-	-	-	98%	100%	-	-	-	-	-	-
920	-	-	100%	-	-	-	-	-	-	100%	100%	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	-	-	-	-
921	100%	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
922	100%	100%	-	100%	-	-	-	-	-	96%	-	-	-	-	-	-	100%	100%	-	-	-	94%	69%	-	-	-	-	-
923	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	99%	97%	-	-	-	-	-
924	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-
925	-	-	100%	-	-	-	-	-	-	82%	-	-	-	-	-	-	100%	-	-	-	-	95%	100%	100%	-	-	-	-
926	100%	95%	100%	100%	-	-	-	-	-	78%	-	-	-	-	-	-	-	-	-	-	-	95%	88%	-	-	-	-	-
927	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	93%	-	-	-	-	-	-
928	-	100%	-	-	-	100%	-	100%	100%	-	-	-	100%	-	-	-	-	100%	-	-	100%	100%	80%	-	-	-	-	-
929	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-
930	-	-	100%	-	-	-	-	-	100%	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-
931	-	-	100%	-	-	99%	-	100%	100%	-	100%	-	-	-	-	-	-	-	-	-	-	100%	86%	67%	-	-	-	-
932	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	96%	100%	-	-	-	-	-
933	83%	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
934	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
935	-	-	-	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	%	-	-	-	98%	-	100%	-	-	-	-
936	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
937	-	100%	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	40%	-	-	-	-	-	-	-	-	-	-
938	-	-	-	-	-	-	-	-	-	16%	-	-	-	100%	-	64%	-	-	-	-	-	100%	50%	-	-	-	-	-
939	-	-	-	-	-	-	-	-	-	-	100%	-	100%	100%	75%	-	-	-	-	-	-	-	-	-	-	-	-	-
940	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
941	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	73%	-	-	-	-	100%	-	-	-	-	-
942	-	94%	-	-	-	100%	-	100%	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
943	-	100%	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
944	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
945	-	-	-	-	-	-	-	28%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
946	-	-	-	-	-	-	-	100%	100%	100%	100%	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
947	-	-	-	-	-	-	-	93%	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-
948	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	77%	-	-	-	-
949	-	100%	-	100%	-	-	-	-	-	100%	100%	-	-	-	-	-	-	100%	-	-	-	100%	99%	100%	-	-	-	-
950	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
951	-	100%	100%	-	-	-	-	-	-	90%	-	-	-	-	-	-	-	100%	-	-	93%	94%	-	-	-	-	-	-
952	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	89%	-	-	-	-	-	-	-	-	-	-	-	-
953	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	54%	100%	-	-	-	-	-	-	-	-	-	-	-	-
954	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	98%	-	-	-	-	-	-	-	-	-	-	-	-
955	-	-	100%	-	-	-	-	100%	100%	99%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	98%	-	-	-	-
956	-	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
957	-	-	-	-	-	-	-	-	-	100%	100%	-	100%	-	-	-	-	100%	-	-	-	84%	100%	100%	-	-	-	-
958	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-
959	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-
960	-	-	100%	-	-	-	-	-	-	99%	100%	-	100%	100%	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-
961	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-
962	-	-	100%	-	-	-	-	-	-	100%	92%	-	100%	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
963	-	100%	-	-	-	-	-	-	-	74%	-	-	-	-	-	-	-	100%	-	-	-	100%	98%	89%	-	-	-	-
964	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	100%	-	-	-	77%	100%	-	-	-	-	-
965	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	99%	-	-	-	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
966	100%	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
967	-	100%	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	96%	-	-	-	-	-
968	-	-	-	-	-	99%	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
969	-	100%	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
970	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
971	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
972	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	100%	72%	-	-	-	-	-	-
973	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	93%	100%	-	-	-	-	-
974	-	71%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
975	-	98%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
976	100%	84%	-	100%	-	-	-	-	-	96%	-	-	-	-	-	-	100%	100%	-	-	-	74%	-	-	-	-	-	-
977	-	100%	100%	100%	-	-	-	-	-	98%	-	-	-	-	-	-	100%	-	-	-	-	91%	96%	-	-	-	-	-
978	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	98%	91%	-	-	-	-	-
979	-	-	100%	100%	-	-	-	-	-	100%	100%	-	-	-	80%	-	-	-	-	-	-	100%	100%	-	-	-	-	-
980	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	100%	95%	-	-	-	-	-	-
981	-	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	-	-	-	-	-	-
982	-	-	-	100%	-	-	-	-	-	89%	-	-	-	-	-	-	100%	-	-	-	-	100%	-	-	-	-	-	-
983	95%	100%	-	100%	-	-	-	-	-	100%	37%	-	-	-	-	-	100%	-	-	-	-	100%	75%	100%	-	-	-	-
984	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
985	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-
986	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-
987	-	50%	-	50%	-	-	-	-	-	83%	-	-	-	-	-	-	100%	100%	-	-	-	100%	87%	-	-	-	-	-
988	100%	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	66%	53%	-	-	-	-	-
989	-	-	-	-	-	-	-	-	-	94%	-	-	-	-	-	-	100%	-	-	-	-	64%	66%	-	-	-	-	-
990	-	-	-	-	-	-	-	-	-	88%	-	48%	-	100%	-	-	-	58%	-	-	-	100%	-	96%	-	-	-	-
991	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	52%	-	97%	100%	-	-	-	-	-	-
992	-	100%	100%	-	-	-	-	-	-	98%	-	-	-	-	-	-	-	-	100%	-	%	95%	-	88%	-	-	-	-
993	-	-	-	-	-	-	-	-	-	-	-	28%	38%	45%	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-
994	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
995	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
996	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-
997	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	48%	-	-
998	-	70%	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	83%	57%	-	-
999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	-	-	-
1000	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1001	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1002	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1003	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-
1004	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11%	-	-	-	-	-	-	-	-	-	-
1005	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-
1006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	100%	-	-	-	-
1007	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-
1008	-	99%	-	-	-	-	-	-	-	-	-	-	-	-	97%	-	-	-	-	-	-	-	-	-	-	-	-	-
1009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	84%	-	-	-	-	-	-	-
1010	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	66%	-	-	-	-	-	-	-
1011	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40%	-	-	-	-	-	-	-
1012	-	-	-	-	-	-	-	-	-	71%	-	-	-	-	-	-	-	100%	-	-	-	100%	-	-	-	-	-	-
1013	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-
1014	-	100%	-	-	-	-	-	-	-	-	-	-	66%	100%	-	95%	-	100%	-	-	-	100%	-	-	-	-	-	-
1015	-	85%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	99%	76%	-	-	-	-	-
1016	100%	100%	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	100%	-	-	-	-	100%	100%	81%	-	-	-	-
1017	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1018	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-
1019	-	-	-	-	-	-	-	100%	77%	-	-	-	-	-	81%	-	-	100%	-	-	-	-	-	-	-	-	-	-
1020	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-
1021	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1022	100%	100%	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	64%	-	-	-	100%	-	-	-	-	-	-
1023	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28%	-	-	-	-	-	75%	-	-	-	-
1024	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20%	-	-	-	-	-	1%	-	-	-	-
1025	-	-	-	-	-	-	-	15%	-	-	-	-	-	-	-	-	-	-	71%	-	-	-	-	-	-	-	-	-
1026	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2%	-	-	-	-	-	18%	-	-	-	-
1027	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	%	-	-	-	-	-	73%	-	-	-	-
1028	-	100%	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	68%	-	-	-	-	-	24%	-	-	-	-
1029	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26%	-	100%	-	-	2%	-	-	-	-
1030	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78%	-	99%	-	-	6%	-	-	-	-
1031	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
1032	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	100%	-	-	-	-
1033	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33%	-	-	-	-	-	56%	-	-	-	-
1034	-	-	-	-	-	-	-	-	100%	100%	-	-	-	-	-	-	-	-	-	-	100%	88%	-	-	-	100%	-	-

Table D-2. Detailed Land Use and Development Condition Data - 2015

Land Use Polygon ID	Percent of Buildout Net Acreage by Land Use Category																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
1035	-	100%	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-
1036	-	100%	-	-	-	-	100%	100%	89%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1037	-	-	100%	-	-	-	-	-	-	80%	-	-	-	-	-	-	100%	-	-	-	100%	100%	-	-	100%	-	-	-
1038	-	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	-	-	8%	-	-	-	-	-	-	-	-	-	-
1039	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	68%	100%	-	-	-	-	-	-
1040	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1041	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	87%	-	-	-	-	-	-	-
1042	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-	-	71%	-	67%	-	-	-	-	-	-	-
1043	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	-	-
1044	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	97%	98%	-	-	-	-	-	-
1045	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99%	-	-	-	-	-	-	-
1046	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	71%	-	-	-	-	-	-	-	-	-
1047	-	-	-	-	47%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1048	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	%	-	81%	-	-	-	-	-	-	-
1049	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36%	-	-	-	-	-	-	-	-	-
1050	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96%	87%	-	-	-	-	-	-
1051	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75%	-	-	-	-	-	-	-	-	-
1052	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	89%	89%	49%	-	57%	-	-	-	-	-	-
1053	-	-	-	-	100%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	39%	-	-	-	-	-	-	-	-
1054	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1055	-	100%	-	-	-	-	-	-	96%	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1056	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	56%	-	-	100%	-	-	100%	-	-	-	-
9999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100%	-	-	-	-	-	98%	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.04	-	-	-	-	-	25.9	-	-	-	-
2	-	23.1	-	-	-	-	-	-	-	8.68	-	-	-	-	-	-	-	19.0	-	-	-	2.61	-	0.998	-	32.3	-	-
3	-	-	-	-	-	-	-	6.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
4	-	-	-	-	0.246	-	-	14.4	-	-	-	-	-	-	-	-	-	-	21.0	-	-	-	-	-	-	-	-	-
5	-	0.145	-	-	0.819	-	-	-	-	-	-	-	-	-	-	-	-	-	6.48	-	-	-	-	-	-	-	-	-
6	13.9	-	-	-	0.0243	-	-	91.9	-	34.7	-	-	-	-	-	-	-	-	10.5	-	-	-	-	-	-	-	-	-
7	22.1	12.9	-	-	0.202	-	-	-	-	12.3	-	-	-	-	-	-	12.5	-	0.907	-	25.6	-	-	-	26.0	19.7	-	-
8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.5	-	-	-	-	-	-	-
9	-	-	-	-	28.6	-	-	-	-	-	-	-	-	-	-	-	-	-	3.11	-	-	-	-	-	-	-	-	-
10	-	-	-	-	7.70	-	-	-	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-	-	-	-	-	-	-
11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.8	-	50.3	-	-	-	-	0.0000	-	-	-	-
12	-	-	-	-	16.2	0.0647	13.9	-	-	-	-	-	-	-	-	-	-	-	5.42	-	12.1	-	-	-	-	-	-	-
13	-	-	-	-	0.0015	-	-	-	-	-	-	-	-	-	-	-	-	-	188	-	10.1	-	-	-	-	-	-	-
14	13.9	-	-	-	-	-	7.04	-	-	2.68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
15	-	-	-	-	19.1	-	74.3	-	-	-	-	-	-	-	-	-	-	2.99	0.0574	-	-	-	-	-	-	-	-	-
16	-	-	-	-	-	-	-	-	-	22.2	-	-	-	-	-	-	13.2	-	0.0063	-	-	28.0	-	-	-	-	-	-
17	12.1	12.8	-	-	-	-	-	-	-	28.2	-	-	-	-	-	-	60.5	-	0.0001	-	-	22.6	-	-	-	-	-	-
18	-	-	-	-	0.0225	-	33.9	-	-	-	-	-	-	-	-	-	-	5.72	0.0431	-	-	-	-	-	-	-	-	-
19	-	-	-	-	-	-	-	-	-	6.91	-	-	-	-	-	-	-	17.9	0.0135	-	-	-	-	-	-	-	-	-
20	-	-	-	-	0.0152	-	23.8	-	-	-	-	-	-	-	-	-	-	-	0.0067	-	-	-	-	-	-	-	-	-
21	-	6.41	-	-	-	-	-	-	13.3	-	-	-	-	-	-	-	6.19	0.0013	-	-	-	-	-	-	-	-	-	-
22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	59.6	-	-	-	-	-	-	-	-	-
23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63.9	-	-	-	-	-	-	-	-	-
24	-	-	-	-	0.0195	-	-	0.0004	34.1	-	-	-	-	-	-	-	-	5.52	-	-	-	-	-	-	-	-	-	-
25	-	-	-	-	34.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
26	-	-	-	-	70.2	-	-	0.0251	0.0155	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
27	-	-	-	-	74.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
28	-	-	-	-	25.7	-	-	-	-	-	-	-	-	-	-	-	-	-	0.159	-	-	-	-	-	-	-	-	-
29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.5	-	-	-	-	-	-	-	-	-
30	-	-	-	-	33.9	-	-	-	-	-	-	-	-	-	-	-	-	-	22.2	-	-	-	-	-	-	-	-	-
31	-	-	-	-	24.0	-	-	-	-	-	-	-	-	-	-	-	-	-	49.4	-	-	-	-	-	-	-	-	-
32	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.3	-	-	-	-	-	-	-	-	-
33	-	-	-	-	13.4	-	-	-	-	-	-	-	-	-	-	-	-	-	24.6	-	-	-	-	-	-	-	-	-
34	-	-	-	-	20.5	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	0.966	-	-	-	-	-	-	-	-	-
35	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.19	2.54	-	-	-	-	-	-	-	-	-	-
36	-	-	-	-	-	-	-	-	17.1	-	-	-	-	-	-	-	18.8	22.6	-	-	-	-	-	-	-	-	-	-
37	-	-	-	-	-	-	-	-	10.6	-	-	-	-	-	-	-	427	9.15	-	-	-	-	-	-	-	-	-	-
38	-	-	-	-	-	-	-	-	93.9	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-	-
39	-	-	-	-	-	-	-	-	45.2	-	-	-	-	-	-	-	0.197	-	-	-	-	-	-	-	-	-	-	-
40	-	23.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
41	-	-	-	-	-	-	-	-	50.2	-	-	-	-	-	-	-	-	11.3	-	-	-	-	-	-	-	-	-	-
42	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.297	-	-	-	78.5	-	-	-	-	-	-	-
43	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.09	-	-	0.286	-	-	14.5	-	-	-	-
44	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.2	-	0.0490	-	-	-	-	-	-	-	-	-
45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.8	-	0.0002	-	-	-	-	-	-	-	-	-
46	-	-	-	-	0.0029	-	-	-	-	-	-	-	-	-	-	-	-	-	42.1	-	-	-	-	-	-	-	-	-
47	-	-	-	-	-	-	-	-	13.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
48	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.9	-	258	49.9	-	-	-	-	-	-
49	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.52	6.19	-	-	52.8	-	-	-	-	-	-	-
50	-	1.35	-	-	-	-	-	0.0277	184	6.48	-	-	-	-	-	-	0.0088	-	-	-	-	4.21	-	-	-	-	-	-
51	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.61	38.2	-	-	10.2	-	-	-	-	-	-	-
52	-	-	-	-	-	-	-	-	62.0	-	-	-	-	-	-	-	-	4.08	-	-	-	-	-	-	-	-	-	-
53	-	-	-	-	-	-	-	-	37.9	-	-	-	-	-	-	-	-	4.43	-	-	-	-	-	-	-	-	-	-
54	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.78	196	-	-	0.686	-	-	-	-	-	-	-
55	34.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	145	-	-	-	-	-	-	-	-	-
56	65.8	-	-	-	-	76.7	-	-	-	-	-	-	-	-	-	-	-	-	18.4	-	-	-	-	-	-	-	-	-
57	-	-	-	-	45.9	-	-	-	-	58.6	-	-	-	4.81	-	-	16.5	7.20	59.4	-	5.19	-	-	-	-	-	-	-
58	-	-	-	-	-	-	-	-	0.0065	13.7	-	-	-	-	-	-	-	-	-	-	-	0.304	-	-	-	-	-	-
59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	12.0	-	-	-	-	-	-	-	-	-
60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.9	-	1.84	1.53	-	-	-	-	-	-
61	-	-	-	-	-	-	-	-	5.84	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
62	-	-	-	-	-	-	-	-	69.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
63	-	-	-	-	-	-	-	-	9.04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
64	-	-	-	-	-	-	-	-	9.58	-	-	-	-	-	-	-	-	0.448	-	-	-	-	-	-	-	-	-	-
65	-	-	-	-	-	-	-	-	112	-	-	-	-	-	-	-	6.02	-	0.0075	-	-	-	-	-	-	-	-	-
66	-	-	0.921	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0996	-	-	-	121	56.0	-	-	-	-	-	-
67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.50	96.3	-	-	-	-	-	-
68	-	-	-	-	0.0050	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	64.1	-	-	-	-	-	-	-
69	-	-	-	-	-	-	-	-	53.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
70	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	-	-	-	-	-	-	-	-	-	-	-	-	-
71	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-	-	-	3.59	-	-	30.7	-	-	-	-	-	-	-
72	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.03	-	-	-	2.36	-	-	-	-	-	-	-
73	-	0.0004	-	-	-	-	-	-	-	22.4	-	-	-	-	-	-	-	-	-	-	-	0.0016	27.9	-	-	-	-	-
74	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.09	-	-	-	-	-	-	-
75	-	-	-	-	11.0	-	-	-	-	-	-	-	-	-	-	-	-	-	1.81	-	-	-	-	-	-	-	-	-
76	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.0	-	-	-	-	-	-	-	-	-
77	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	65.6	-	0.0553	-	-	-	-	-	-	-
78	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0342	-	39.9	-	0.0001	0.219	-	-	-	-	-	-
79	6.80	-	-	-	-	-	-	-	-	21.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
80	-	-	-	-	-	-	-	-	-	4.91	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
81	-	-	2.37	-	-	-	-	-	-	17.1	-	-	-	-	-	-	-	-	-	-	-	0.196	-	-	-	-	-	-
82	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.03	-	-	7.36	-	-	-	-	-	-	-	-	-	-
83	-	-	-	-	-	-	-	-	18.7	-	-	-	-	-	-	-	-	3.70	-	-	-	-	-	-	-	-	-	-
84	-	-	-	-	-	-	-	-	-	8.15	-	-	-	-	36.8	-	-	3.84	-	-	14.5	-	-	-	-	-	-	-
85	-	-	-	-	-	-	-	-	41.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
86	-	-	-	-	-	-	-	-	9.66	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
87	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.2	-	-	-	-	-	-	-	-	-
88	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.72	-	-	-	-	-	-	-	-	-
89	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52.1	-	-	-	-	-	-	-	-	-
90	-	-	-	-	0.751	-	-	-	-	-	-	-	-	-	-	-	-	-	211	-	-	-	-	-	-	-	-	-
91	-	-	-	-	0.0091	-	-	-	-	-	-	-	-	-	-	-	-	-	95.1	-	-	-	-	-	-	-	-	-
92	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	59.7	-	-	0.0002	-	-	-	-	-	-
93	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.631	-	-	101	-	-	-	-	-	-
94	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	-	-	-	-	-
95	-	0.0035	-	-	232	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
96	-	-	-	-	12.9	-	-	-	-	-	-	-	-	-	-	-	-	-	12.6	-	-	-	-	-	-	-	-	-
97	-	-	-	-	4.32	-	-	-	-	-	-	-	-	-	-	-	-	-	67.4	-	-	-	-	-	-	-	-	-
98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.6	-	0.141	-	-	-	-	-	-	-
99	-	-	-	-	-	-	-	-	135	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
100	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.5	-	25.0	-	-	-	-	-	-	-	-	-
101	-	-	-	-	66.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
102	-	-	-	-	573	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
103	-	-	-	-	158	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
104	-	-	-	-	135	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0003	-	-	-	-	-	-	-	-	-
105	-	-	-	-	250	-	-	-	-	-	-	-	-	-	-	-	-	-	57.1	-	-	-	-	-	-	-	-	-
106	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.4	-	-	0.0909	-	-	-	-	-	-	-	-	-	-
107	-	0.0001	-	-	-	-	-	-	60.1	0.0024	-	-	-	-	-	-	5.76	9.86	-	-	3.47	-	-	-	-	-	-	-
108	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.56	-	-	4.98	-	-	-	-	-	-	-
109	-	-	-	-	-	-	-	-	101	6.51	-	-	-	-	-	-	4.98	-	-	-	13.4	-	-	-	-	-	-	-
110	-	0.0834	-	-	-	-	-	-	-	3.97	-	-	-	-	-	-	-	39.8	-	-	2.96	-	-	-	-	-	-	-
111	-	10.2	-	-	-	-	-	-	-	15.3	-	-	-	-	-	-	-	7.01	-	-	3.85	-	-	-	-	-	-	-
112	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44.5	-	-	0.929	-	-	-	-	-	-	-
113	-	-	-	-	-	-	-	-	-	5.40	-	-	-	-	-	-	-	16.5	-	-	61.8	-	-	-	-	-	-	-
114	-	-	-	-	-	-	-	-	-	0.0013	-	-	-	-	-	-	-	-	-	-	14.5	-	-	-	-	-	-	-
115	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.50	-	-	7.37	-	-	-	-	-	-	-
116	-	-	-	-	-	-	-	-	16.9	14.9	-	-	-	-	-	-	-	20.5	-	-	-	-	-	-	-	-	-	-
117	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.0	-	-	15.4	-	-	-	-	-	-	-
118	-	-	-	-	-	-	-	-	-	13.0	-	-	-	-	-	-	-	8.16	-	-	20.1	-	-	-	-	-	-	-
119	-	-	-	-	-	-	-	-	-	7.41	-	-	-	-	-	-	49.0	-	-	-	65.8	-	-	-	-	-	-	-
120	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.171	-	-	14.8	-	-	-	-	-	-	-
121	-	-	-	-	-	-	-	-	-	17.9	-	-	-	-	-	-	-	-	-	-	13.1	-	-	-	-	-	-	-
122	-	-	-	-	-	-	-	-	18.7	4.12	-	-	-	-	-	-	-	-	-	-	11.1	-	-	-	-	-	-	-
123	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.57	-	-	29.4	-	-	-	-	-	-	-
124	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.41	-	-	30.9	-	-	-	-	-	-	-
125	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.79	-	-	13.1	-	-	-	-	-	-	-
126	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.574	-	-	17.5	-	-	-	-	-	-	-
127	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.64	-	-	32.8	-	-	-	-	-	-	-
128	-	13.6	-	-	-	-	-	-	0.198	11.2	0.497	-	-	-	-	-	-	-	-	-	12.5	-	-	-	-	-	-	-
129	-	10.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.7	-	-	-	-	-	-	-
130	-	-	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
131	-	-	-	-	-	-	-	-	-	-	-	-	-	-	62.3	-	5.38	11.0	-	-	-	-	-	-	-	-	-	-
132	-	-	-	-	-	-	-	-	-	3.97	-	-	-	-	9.49	-	-	4.09	-	-	31.9	-	-	-	-	-	-	-
133	-	-	-	-	-	-	-	-	-	4.48	-	-	-	-	39.3	-	-	2.35	-	-	10.1	-	-	-	-	-	-	-
134	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.92	-	-	12.8	-	-	-	-	-	-	-
135	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.12	-	-	16.2	-	-	-	-	-	-	-
136	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.2	-	-	-	-	-	-	-
137	-	-	-	-	-	-	-	-	-	3.38	-	-	-	-	-	-	-	-	-	-	25.8	-	-	-	-	-	-	-
138	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.66	-	-	21.1	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
139	-	-	-	-	-	-	-	-	8.89	27.7	-	-	-	-	25.2	-	1.42	16.9	-	-	99.6	-	-	-	-	-	-	-
140	-	-	-	-	-	-	-	-	-	2.34	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-	-	-	-
141	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.63	-	-	-	3.52	-	-	-	-	-	-	-
142	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.7	-	-	-	-	-	-	-
143	-	-	-	-	-	-	-	-	-	7.72	-	-	-	5.21	0.421	-	-	-	-	-	61.8	-	-	-	-	-	-	-
144	-	7.10	-	-	-	-	-	-	-	6.70	-	-	-	-	87.5	-	11.2	4.07	-	-	8.90	-	-	-	-	-	-	-
145	-	-	-	-	-	-	-	-	-	2.48	-	-	-	2.15	-	-	-	2.83	-	-	27.7	-	-	-	-	-	-	-
146	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.193	-	-	3.24	-	-	13.0	-	-	-	-	-	-	-
147	-	-	-	-	-	-	-	-	-	14.3	-	-	-	5.45	-	-	5.62	4.51	-	-	12.4	-	-	-	-	-	-	-
148	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.32	-	-	3.06	-	-	1.69	-	-	-	-	-	-	-
149	-	-	-	-	-	-	-	-	-	3.93	-	-	-	-	8.83	-	-	2.43	-	-	3.81	-	-	-	-	-	-	-
150	-	-	-	-	-	-	-	-	-	6.43	-	-	-	-	-	-	18.1	-	-	-	7.23	-	-	-	-	-	-	-
151	-	20.5	-	-	-	-	-	-	0.0019	17.2	-	-	-	-	-	-	-	-	-	-	11.1	-	-	-	-	-	-	-
152	-	4.95	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0014	-	-	-	21.1	-	-	-	-	-	-	-
153	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.13	-	-	-	-	-	-	-
154	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.14	-	-	-	-	-	-	-
155	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.0	-	-	-	-	-	-	-
156	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.0	-	-	-	-	-	-	-
157	-	-	-	-	-	-	-	-	-	1.41	-	-	-	-	7.32	-	-	-	-	-	6.66	-	-	-	-	-	-	-
158	-	0.356	3.05	-	-	-	-	-	-	-	20.4	-	51.9	0.949	-	-	0.547	-	-	-	24.8	7.92	0.734	4.34	-	-	-	-
159	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.09	-	-	-	136	9.58	-	-	-	-	-	-
160	-	-	0.592	-	-	-	-	-	-	-	-	-	-	-	-	-	10.7	-	-	-	156	93.1	3.05	0.692	-	-	-	-
161	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	38.5	1.42	-	-	-	-	-	-
162	-	-	-	-	-	-	-	-	-	8.27	-	-	-	-	-	-	-	1.72	20.6	-	47.8	48.7	-	-	-	-	-	-
163	-	-	-	-	-	-	-	-	-	34.3	-	-	-	2.29	-	-	-	3.19	0.0058	-	-	154	-	-	-	-	-	-
164	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91.1	-	-	-	-	-	-
165	-	-	-	-	-	-	-	-	-	0.107	-	-	-	-	-	-	-	-	-	-	0.0013	64.5	-	-	-	-	-	-
166	-	-	-	-	-	-	-	-	0.0000	5.25	-	-	-	-	-	-	42.5	-	-	-	1.98	83.4	-	-	-	-	-	-
167	-	-	-	-	-	-	-	0.407	51.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
168	-	-	-	-	-	-	-	-	53.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
169	-	-	8.55	2.34	0.0103	-	-	-	-	104	-	-	-	-	-	-	-	-	-	-	3.57	18.6	-	-	-	-	-	-
170	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	153	-	-	-	-	-	-	-	-	-	-	-
171	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.8	4.05	-	-	-	-	-	-
172	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.5	19.5	-	-	-	-	-	-
173	-	-	-	-	-	-	-	-	-	6.17	-	-	-	-	-	-	-	-	-	-	45.6	25.1	-	-	-	-	-	-
174	-	-	-	-	-	-	-	-	-	2.04	-	-	-	-	-	-	-	-	-	-	-	73.9	-	-	-	-	-	-
175	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.95	-	-	-	4.92	95.6	-	-	-	-	-	-
176	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.2	-	-	-	-	-	-
177	-	-	-	2.41	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.6	-	-	-	-	-	-
178	-	10.8	-	9.13	-	-	-	0.221	3.31	37.9	-	-	-	-	-	-	1.40	-	-	-	-	49.3	-	2.45	-	-	-	-
179	-	-	-	-	-	-	-	-	-	0.0027	-	-	-	-	-	-	-	-	-	-	77.4	5.72	-	-	-	-	-	-
180	-	-	-	-	-	-	-	-	-	5.58	-	-	-	-	-	-	3.88	-	-	-	2.12	35.3	-	-	-	-	-	-
181	-	-	-	9.14	-	-	-	30.3	36.9	48.1	-	-	-	-	-	-	10.2	-	-	-	-	2.52	3.58	-	-	-	-	-
182	-	-	1.86	-	-	-	-	18.3	4.75	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
183	-	9.39	3.96	5.10	-	-	-	4.20	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-
184	-	-	0.315	-	-	-	-	-	-	13.5	-	-	-	-	-	-	-	-	-	-	-	9.35	0.126	-	-	-	-	-
185	-	1.50	1.97	-	-	-	-	-	14.1	1.17	-	-	-	-	-	-	-	-	-	-	-	43.4	10.0	-	-	-	-	-
186	-	-	-	3.74	-	-	-	114	33.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
187	-	-	-	-	-	-	-	1.50	19.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
188	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.18	-	-	-	0.0235	40.5	-	-	-	-	-
189	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.94	-	-	-	0.0007	-	34.4	-	-	-	-
190	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.22	-	-	-	0.208	26.0	12.9	-	-	-	-
191	-	3.40	-	21.1	-	-	-	-	-	32.3	-	-	-	-	-	-	-	5.29	-	-	-	-	-	-	-	-	-	-
192	-	1.93	-	6.49	-	-	-	30.7	18.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
193	-	-	-	-	-	-	-	-	-	7.65	-	-	-	-	-	-	-	5.72	-	-	-	0.363	-	29.7	-	-	-	-
194	-	-	-	-	-	-	-	0.612	-	-	-	-	-	-	-	-	-	9.11	-	-	-	0.0027	34.8	0.180	-	-	-	-
195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.91	-	-	-	0.0009	19.1	-	-	-	-	-
196	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.61	-	-	-	0.0780	49.8	0.762	-	-	-	-
197	-	-	-	-	-	-	-	-	-	1.16	-	-	8.55	-	-	-	-	8.37	-	-	-	0.0001	-	21.7	-	-	-	-
198	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.2	0.185	-	2.73	-	-	-	-
199	-	13.7	-	2.64	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
200	-	-	-	-	-	-	-	-	-	10.0	-	-	-	-	-	-	-	-	-	-	5.73	13.6	-	-	-	-	-	-
201	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	51.0	-	-	-	-	-	-	-
202	-	-	-	-	-	-	-	0.0000	83.7	-	-	-	-	-	-	-	0.0024	0.0062	-	-	-	-	-	-	-	-	-	-
203	-	-	-	-	-	-	-	-	115	-	-	-	-	-	-	-	-	2.06	-	-	-	-	-	-	-	-	-	-
204	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.39	-	-	-	-	-	-	-	-	-	-	-	-	-
205	-	-	-	-	-	-	-	-	0.702	-	-	-	-	-	83.5	-	-	2.81	-	-	-	-	-	-	-	-	-	-
206	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77.0	-	-	11.2	-	-	-	-	-	-	-	-	-	-
207	-	-	-	-	-	-	58.0	-	-	0.147	-	-	-	-	0.147	-	-	5.18	-	-	-	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
208	-	-	-	-	-	-	-	-	-	-	-	-	-	-	42.3	-	-	3.79	-	-	-	-	-	-	-	-	-	-
209	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.4	-	-	4.69	-	-	-	-	-	-	-	-	-	-
210	-	4.60	-	-	-	-	-	-	-	7.41	88.3	-	-	-	4.68	-	-	32.3	-	-	-	-	-	-	-	-	-	-
211	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
212	-	-	-	-	-	-	-	-	23.9	-	-	-	-	-	117	-	-	-	-	-	-	-	-	-	-	-	-	-
213	-	-	-	-	-	-	-	-	-	-	-	-	-	-	45.1	-	-	-	-	-	-	-	-	-	-	-	-	-
214	-	4.64	-	-	-	-	-	-	-	10.5	-	-	-	-	28.5	-	-	27.9	-	-	36.1	-	-	-	-	-	-	-
215	-	-	-	-	-	-	-	-	-	-	-	-	-	-	75.6	-	-	5.17	-	-	-	-	-	-	-	-	-	-
216	-	0.0004	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	-	-	-	-	-
217	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93.9	-	-	-	-	23.7	-	-	-	-	-	-
218	-	-	-	-	-	-	38.6	-	-	-	-	-	-	-	0.0061	-	-	-	-	-	-	-	0.0058	-	-	-	-	-
219	-	-	-	-	-	-	28.1	-	-	0.0385	0.0000	-	-	-	33.8	-	-	14.2	-	-	5.81	2.77	-	-	-	-	-	-
220	-	-	-	-	-	-	-	-	-	4.78	0.0815	-	-	6.30	47.0	-	-	5.34	-	-	-	-	-	-	-	-	-	-
221	-	17.5	-	-	-	-	-	-	20.0	7.68	20.0	-	-	-	-	-	-	0.0023	-	-	-	-	-	-	-	-	-	-
222	-	53.9	-	-	-	-	-	-	-	18.4	49.3	-	-	25.5	20.1	-	-	0.774	-	-	-	-	-	-	-	-	-	-
223	-	10.6	-	-	-	-	-	-	-	0.0225	7.59	-	-	3.38	-	-	-	3.94	-	-	-	-	-	-	-	-	-	-
224	-	-	-	-	-	-	-	-	26.7	-	-	-	-	-	-	-	-	10.3	-	-	-	-	-	-	-	-	-	-
225	-	-	-	-	-	-	-	-	-	7.55	-	-	-	-	-	-	0.0003	-	-	-	-	50.9	-	-	-	-	-	-
226	-	-	-	-	-	-	-	-	2.74	0.141	-	-	-	-	-	-	30.2	31.9	-	-	7.18	-	-	-	-	-	-	-
227	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0041	-	-	-	-	-	-	0.0015	18.7	-	-	-	-	-
228	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	10.4	-	2.81	-	-	-	-
229	-	-	-	-	-	-	-	-	-	1.18	-	-	-	-	-	-	-	-	-	-	-	0.0015	-	20.6	-	-	-	-
230	-	-	-	-	-	-	-	-	-	41.4	-	-	-	-	-	-	-	-	-	-	-	0.967	-	24.7	-	-	-	-
231	-	61.6	-	0.0852	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
232	-	0.0073	-	-	-	-	-	-	0.0003	-	-	-	-	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-
233	-	0.0019	3.46	-	-	-	-	-	-	36.1	-	-	-	-	-	-	7.16	-	-	-	-	29.4	-	-	-	-	-	-
234	-	-	-	-	-	-	-	-	0.0445	-	-	-	-	-	-	-	6.56	0.0063	-	-	-	45.0	-	-	-	-	-	-
235	-	-	-	-	-	-	-	-	17.7	-	-	-	-	-	-	-	59.3	-	-	-	-	-	-	-	-	-	-	-
236	-	17.7	-	-	-	-	-	-	45.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
237	-	-	1.56	-	-	-	-	-	-	-	-	-	-	-	-	-	42.7	-	-	-	-	58.0	-	-	-	-	-	-
238	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.262	-	-	-	21.5	35.0	-	-	-	-	-	-
239	-	-	-	-	-	-	-	-	-	8.02	-	-	-	-	-	-	73.0	-	-	-	-	62.1	-	-	-	-	-	-
240	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	60.9	-	-	-	-	-	-
241	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	127	45.4	-	-	-	-	-	-
242	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	194	36.6	-	-	-	-	-	-
243	-	-	2.04	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	2.57	-	-	-	137	81.0	-	-	-	-	-	-
244	-	-	-	-	-	-	-	-	-	7.63	-	-	-	-	-	-	-	-	-	-	49.0	142	-	-	-	-	-	-
245	-	-	0.386	-	-	-	-	-	-	3.02	-	-	-	-	-	-	7.93	-	-	-	127	98.9	-	-	-	-	-	-
246	-	-	10.2	3.42	-	-	-	-	-	-	0.720	-	-	0.464	-	-	0.110	-	-	-	-	160	-	-	-	-	-	-
247	-	-	2.30	0.794	-	-	-	-	-	-	-	-	-	-	-	-	9.62	-	-	-	129	135	-	-	-	-	-	-
248	-	-	36.3	2.27	-	-	-	-	-	0.0001	23.5	-	-	-	-	-	23.9	-	-	-	2.38	17.0	-	-	-	-	-	-
249	-	-	0.0011	-	-	-	-	-	-	-	35.1	-	-	18.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-
250	-	-	1.37	-	-	-	-	-	-	0.483	15.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
251	-	-	-	-	-	-	-	-	-	-	6.91	-	-	-	-	-	38.6	-	-	-	-	10.4	-	-	-	-	-	-
252	-	-	-	-	-	-	-	0.734	-	8.42	-	-	-	-	-	-	7.56	-	-	-	-	74.9	-	-	-	-	-	-
253	-	-	1.15	1.88	-	-	-	89.7	-	29.5	-	-	-	-	-	-	-	-	-	-	-	12.1	1.70	-	-	-	-	-
254	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.8	-	-	-	-	33.2	-	-	-	-	-	-
255	-	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	-	19.0	-	-	-	-	26.0	2.84	-	-	-	-	-
256	6.02	-	-	0.444	-	-	-	-	-	12.7	2.79	-	-	-	-	-	-	0.0010	-	-	-	7.11	-	-	-	-	-	-
257	-	-	-	-	-	-	-	-	-	6.81	28.4	-	-	-	-	-	13.3	-	-	-	13.4	33.7	-	-	-	-	-	-
258	-	-	-	-	-	-	-	49.0	-	-	-	-	-	8.85	-	-	-	-	-	-	-	-	-	-	-	-	-	-
259	-	-	-	-	-	-	-	4.09	0.0000	0.0013	-	-	-	-	78.7	-	-	-	-	-	-	-	-	-	-	-	-	-
260	-	-	-	-	-	-	-	-	-	0.0724	-	-	0.0104	-	-	-	-	218	-	-	-	-	-	-	-	-	-	-
261	-	-	-	-	-	-	-	-	-	-	-	-	61.5	-	-	-	-	11.9	-	-	-	-	-	-	-	-	-	-
262	-	3.44	-	-	-	-	-	-	5.93	12.8	4.42	-	-	-	-	-	8.86	-	-	-	-	104	-	-	-	-	-	-
263	-	-	-	-	-	-	-	0.518	0.0000	14.5	12.2	-	-	-	-	-	-	-	-	-	0.0001	132	-	-	-	-	-	-
264	-	0.0014	-	-	-	-	-	7.25	-	66.5	17.8	-	-	-	-	-	20.1	-	-	-	-	1.23	-	-	-	-	-	-
265	-	-	4.23	2.10	-	-	-	-	-	20.6	-	-	-	-	-	-	1.66	3.28	-	-	-	25.8	-	-	-	-	-	-
266	-	-	-	-	-	-	-	-	-	7.41	-	-	-	-	-	-	-	-	-	-	-	25.7	-	-	-	-	-	-
267	-	0.0205	0.449	-	-	-	-	-	-	34.1	-	-	-	-	-	-	-	0.502	-	-	-	30.5	-	10.4	-	-	-	-
268	-	21.2	-	-	-	-	-	-	-	0.0004	-	-	26.7	-	10.6	-	-	-	-	-	-	-	-	-	-	-	-	-
269	-	32.3	-	-	-	-	-	-	-	36.4	-	-	5.07	-	-	-	3.21	-	-	-	0.0002	5.08	-	-	-	-	-	-
270	-	0.555	-	-	-	-	-	-	-	-	0.0003	-	14.1	-	-	-	-	2.82	-	-	0.0000	6.83	-	-	-	-	-	-
271	-	0.0711	-	-	-	-	-	-	-	46.9	-	-	-	-	-	-	-	-	-	-	0.0001	5.82	17.4	1.15	-	-	-	-
272	-	17.2	-	-	-	-	-	36.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
273	-	-	-	-	-	-	-	8.37	-	-	-	-	-	-	-	-	-	14.7	-	-	-	-	-	-	-	-	-	-
274	-	-	-	-	-	-	-	49.9	0.0004	0.0008	0.0006	-	39.9	-	5.00	-	-	4.41	-	-	-	-	-	-	-	-	-	-
275	-	-	-	-	-	-	-	3.42	0.0000	0.0053	-	17.1	-	-	-	-	-	0.0025	-	-	-	-	-	-	-	-	-	-
276	-	-	12.3	-	-	-	-	0.548	0.0079	0.164	27.9	-	-	18.8	66.0	-	24.7	-	-	-	-	11.7	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
277	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.2	-	-	-	-	-	-	-	-	-	-	-	-	-
278	-	-	-	-	-	-	-	26.3	0.0022	-	-	0.0010	-	-	-	-	-	0.0003	-	-	-	-	-	-	-	-	-	-
279	-	0.0003	-	0.370	-	-	-	-	-	-	-	-	6.43	-	-	-	0.0000	-	-	-	0.0006	45.3	3.26	1.62	-	-	-	-
280	-	-	5.05	-	-	-	-	-	5.86	0.430	-	-	-	-	-	-	3.54	-	-	-	-	91.4	-	-	-	-	-	-
281	-	-	-	-	-	-	-	-	26.4	-	-	-	-	-	-	-	8.69	-	-	-	-	12.2	-	-	-	-	-	-
282	-	-	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-	-	-	-	-	-	14.6	-	-	-	-	-	-
283	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	18.0	-	-	-	0.308	54.4	-	-	-	-	-	-
284	-	21.2	-	-	4.03	-	-	0.0037	5.37	14.9	-	-	-	-	-	-	18.7	-	-	-	5.98	31.4	-	-	-	-	-	-
285	-	-	-	-	-	-	-	-	-	1.08	-	-	-	-	-	-	16.4	-	-	-	13.4	92.7	-	-	-	-	-	-
286	19.4	7.97	-	-	-	-	-	-	3.60	23.9	-	-	-	-	-	-	2.41	-	-	-	-	27.4	-	-	-	-	-	-
287	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.0	-	-	-	-	-	-
288	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.1	-	-	-	3.70	20.9	-	-	-	-	-	-
289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.50	-	-	-	24.6	22.9	-	-	-	-	-	-
290	-	-	-	-	-	-	-	-	-	22.5	-	-	-	-	-	-	0.0003	-	-	-	-	91.6	-	-	-	-	-	-
291	7.16	-	-	-	-	-	-	-	-	36.9	-	-	-	-	-	-	2.62	-	-	-	-	-	-	-	-	-	-	-
292	4.88	-	-	-	-	-	-	-	-	17.7	-	-	-	-	-	-	3.32	-	-	-	-	67.1	-	-	-	-	-	-
293	-	-	-	-	-	-	-	-	38.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
294	21.4	-	-	-	-	-	-	-	-	8.55	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
295	3.68	-	-	-	-	-	-	-	-	18.5	-	-	-	-	-	-	-	-	-	-	-	21.0	-	-	-	-	-	-
296	-	-	-	-	-	-	-	-	-	0.936	-	-	-	-	-	-	17.1	-	-	-	-	13.1	-	-	-	-	-	-
297	0.973	-	0.664	19.7	-	-	-	-	10.7	17.6	7.14	-	-	-	-	-	13.9	-	-	-	-	89.5	-	-	-	-	-	-
298	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.0	-	-	-	-	-	-
299	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.0	-	-	-	-	43.0	-	-	-	-	-	-
300	17.7	-	-	-	-	-	-	-	-	0.368	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
301	-	-	-	-	-	-	-	-	-	14.0	-	-	-	-	-	-	6.60	-	-	-	5.91	80.0	-	-	-	-	-	-
302	4.26	-	-	-	-	-	-	-	-	38.1	-	-	-	-	-	-	5.67	-	-	-	-	17.6	-	-	-	-	-	-
303	-	-	-	-	-	-	-	-	-	16.3	1.71	-	-	-	-	-	16.8	-	-	-	-	51.9	-	-	-	-	-	-
304	5.70	-	-	-	-	-	-	-	-	21.3	-	-	-	-	-	-	2.71	-	-	-	-	37.2	-	-	-	-	-	-
305	-	-	8.39	-	-	-	-	-	0.731	14.7	33.7	-	-	-	3.37	-	1.43	-	-	-	18.8	54.5	-	-	-	-	-	-
306	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.04	18.1	0.268	-	70.5	7.56	0.378	58.8	-	-	-	-
307	-	10.4	0.996	-	-	-	-	-	-	9.74	-	-	-	-	-	-	-	4.42	-	-	-	0.0163	-	68.4	-	-	-	-
308	-	-	-	-	-	-	-	-	-	18.4	-	-	-	-	-	-	-	-	-	-	-	0.0671	28.0	1.25	-	-	-	-
309	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.70	25.3	-	-	-	-	-	-
310	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.66	-	-	22.5	0.0008	-	20.0	-	-	-	-
311	-	-	2.43	-	-	-	-	-	-	-	-	-	-	-	-	-	9.05	-	-	-	-	98.1	29.3	7.98	-	-	-	-
312	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.0	-	-	-	0.0035	62.1	-	-	-	-	-
313	-	-	-	-	-	-	-	-	-	6.81	10.3	-	-	-	-	-	-	-	-	-	-	0.0060	69.8	-	-	-	-	-
314	-	-	0.0000	-	-	-	-	-	-	0.0001	1.58	-	-	-	-	-	-	15.3	-	-	-	0.334	68.2	-	-	-	-	-
315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.2	-	-	0.0019	1.03	62.8	12.7	-	-	-	-
316	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.54	-	-	-	1.02	84.3	18.2	-	-	-	-
317	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.6	-	-	-	0.726	35.2	55.7	-	-	-	-
318	-	0.0003	-	-	-	-	-	-	-	4.61	-	-	-	-	-	-	-	29.5	-	-	-	0.0073	115	6.47	-	-	-	-
319	-	-	-	-	-	-	-	-	-	6.34	-	-	-	-	-	-	-	-	-	-	-	0.0959	107	5.11	-	-	-	-
320	-	-	-	-	-	-	-	-	-	1.89	-	-	-	-	-	-	-	-	-	-	-	30.1	-	-	-	-	-	-
321	-	-	1.07	-	-	-	-	-	-	27.6	-	-	-	-	-	-	3.02	-	-	-	3.44	79.4	-	-	-	-	-	-
322	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	109	1.93	-	-	-	-	-	-
323	-	-	-	-	-	-	-	-	-	25.0	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-
324	-	-	-	-	-	-	-	-	-	1.55	-	-	-	-	-	-	13.9	-	-	-	-	55.6	-	-	-	-	-	-
325	-	-	0.997	-	-	-	-	-	-	7.70	-	-	-	-	-	-	8.10	-	-	-	136	77.7	-	-	-	-	-	-
326	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.05	-	-	-	74.7	55.5	-	-	-	-	-	-
327	-	-	-	-	-	-	-	-	-	8.75	-	-	-	-	-	-	24.6	8.22	-	-	60.8	106	34.3	19.1	-	-	-	-
328	-	-	-	-	-	-	-	-	-	22.0	-	-	-	-	-	-	-	-	-	-	-	93.1	-	-	-	-	-	-
329	-	-	0.618	2.65	-	-	-	-	-	9.44	-	-	-	-	-	-	1.04	-	-	-	0.573	102	-	-	-	-	-	-
330	20.1	-	-	-	-	-	-	-	-	13.1	-	-	-	-	-	-	1.01	-	-	-	0.0000	14.7	-	-	-	-	-	-
331	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	4.09	68.2	-	-	-	-	-	-
332	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.49	-	-	-	-	53.9	-	-	-	-	-	-
333	-	-	8.27	-	-	-	-	-	-	24.1	-	-	-	-	-	-	0.0001	-	-	-	5.37	115	-	-	-	-	-	-
334	-	-	2.01	-	-	-	-	-	-	29.2	-	-	-	-	-	-	3.33	-	-	-	-	29.4	-	-	-	-	-	-
335	-	-	0.937	-	-	-	-	-	-	15.3	-	-	-	-	-	-	0.0001	-	-	-	15.2	11.2	-	-	-	-	-	-
336	0.0047	-	-	-	-	-	-	-	-	9.24	-	-	-	-	-	-	6.84	-	-	-	19.3	32.1	-	-	-	-	-	-
337	-	6.11	0.0004	0.762	-	-	-	-	-	4.13	-	-	-	-	-	-	-	0.307	-	-	-	8.80	87.6	27.1	-	-	-	-
338	-	0.0001	-	-	-	-	-	-	-	29.3	-	-	0.284	-	-	-	-	7.23	-	-	0.0003	2.01	34.2	4.36	-	-	-	-
339	-	11.3	0.0349	4.10	-	-	-	-	-	12.7	-	-	-	-	-	-	-	-	-	-	-	0.0010	20.8	-	-	-	-	-
340	-	-	-	-	-	-	-	-	-	18.9	-	-	-	-	-	-	20.9	-	-	-	-	20.6	-	-	-	-	-	-
341	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77.7	-	-	-	-	-	-
342	-	-	-	1.04	-	-	-	-	-	0.234	2.83	-	-	-	-	-	22.7	-	-	-	-	87.6	0.415	-	-	-	-	-
343	-	0.0003	0.572	-	-	-	-	-	-	14.4	0.0000	-	0.927	-	-	1.42	-	-	-	-	-	0.793	5.65	39.5	-	-	-	-
344	-	0.385	4.73	-	-	-	-	-	-	15.4	1.11	-	10.3	-	-	-	-	0.0308	-	-	-	0.0061	71.6	1.16	-	-	-	-
345	-	-	-	-	-	-	-	-	-	25.8	-	-	-	-	54.7	-	0.0059	7.61	-	-	91.6	24.6	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
346	-	9.48	-	-	-	-	-	-	-	19.9	-	-	-	-	-	-	4.60	7.63	-	-	9.18	-	-	-	-	-	-	-
347	-	0.0075	-	-	-	-	-	-	-	8.10	-	-	-	-	-	-	-	27.9	-	-	96.8	-	-	-	-	-	-	-
348	-	-	12.5	3.94	-	-	-	-	-	-	19.1	-	20.2	0.761	-	-	7.50	-	-	-	-	16.8	-	-	-	-	-	-
349	-	-	0.332	3.79	-	-	-	-	-	-	9.12	-	-	1.01	-	-	17.5	-	-	-	-	7.54	6.83	-	-	-	-	-
350	-	-	-	3.94	-	-	-	-	-	-	4.48	-	-	-	-	-	0.0005	-	-	-	-	29.2	2.07	-	-	-	-	-
351	-	-	15.6	36.5	-	-	-	-	-	0.151	73.2	-	-	-	5.34	-	0.0000	0.965	-	-	-	22.2	-	-	-	-	-	-
352	-	-	-	-	-	-	-	-	-	15.2	28.3	-	-	-	-	-	-	-	-	-	-	54.2	8.58	-	-	-	-	-
353	-	-	-	-	-	-	-	-	-	-	0.0952	-	-	-	-	-	-	-	-	-	-	64.3	-	-	-	-	-	-
354	-	-	-	-	-	-	-	-	-	-	3.28	-	-	-	-	-	-	-	-	-	-	67.8	-	-	-	-	-	-
355	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.79	-	-	-	-	178	-	-	-	-	-	-
356	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	29.4	-	-	-	-	-	-
357	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.5	-	-	-	-	-	-
358	-	-	-	-	-	-	-	-	-	5.85	-	-	-	-	-	-	-	-	-	-	-	22.3	-	-	-	-	-	-
359	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	6.32	-	-	-	-	-	-
360	-	-	-	-	-	-	-	-	-	6.57	-	-	-	-	-	-	0.0002	-	-	-	-	55.4	-	-	-	-	-	-
361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.9	1.46	-	-	-	-	-
362	-	0.839	1.53	-	-	-	-	-	0.0001	21.6	-	-	-	-	-	-	-	-	-	-	-	73.8	-	-	-	-	-	-
363	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.140	118	-	-	-	-	-
364	-	24.1	0.0026	6.71	-	-	-	4.93	-	8.28	25.9	-	5.57	-	-	-	-	-	-	-	-	0.0000	-	0.692	-	-	-	-
365	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.43	-	-	68.9	0.0031	-	10.3	-	-	-	-
366	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	9.08	-	-	-	0.0002	24.0	-	-	-	-	-	-
367	-	0.0008	-	17.7	-	-	-	108	0.0225	0.0009	6.34	-	-	25.3	30.0	-	-	-	-	-	-	-	-	-	-	-	-	-
368	-	0.0556	-	-	-	-	-	1.06	-	0.0009	17.7	-	15.6	4.65	0.0995	-	-	4.68	-	-	15.0	0.0515	60.6	23.7	-	-	-	-
369	-	-	-	-	-	-	-	-	-	-	0.0374	-	-	-	1.90	-	-	1.44	-	-	4.94	7.38	-	-	-	-	-	-
370	-	-	0.888	3.66	-	-	-	-	7.21	4.40	14.1	-	-	-	13.7	-	2.69	1.76	-	-	0.0649	61.9	-	-	-	-	-	-
371	-	-	-	-	14.5	-	-	-	16.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
372	-	-	-	-	-	-	-	-	48.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
373	-	-	-	-	-	-	-	-	111	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
374	-	4.19	-	-	-	-	-	-	-	23.5	-	-	-	-	-	-	-	-	-	-	15.1	-	-	-	-	-	-	-
375	-	0.453	-	-	-	-	-	-	-	6.74	-	-	-	-	-	-	0.0022	9.12	-	-	35.2	-	-	-	-	-	-	-
376	-	-	-	-	-	-	-	-	-	0.152	-	-	-	-	-	-	10.3	0.0001	-	-	12.3	-	-	-	-	-	-	-
377	-	-	-	-	-	-	-	-	-	35.8	-	-	-	-	-	-	-	12.8	-	-	5.20	-	-	-	-	-	-	-
378	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.7	-	-	-	-	-	-	-
379	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	115	-	-	6.75	-	-	-	-	-	-	-	-	-	-
380	-	30.2	-	-	-	-	-	-	14.5	29.5	-	-	-	-	13.2	-	-	8.57	-	-	40.3	-	-	-	-	-	-	-
381	-	-	-	-	-	-	-	-	-	32.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
382	-	-	-	-	-	-	-	-	88.7	1.29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
383	-	-	-	-	-	-	-	-	-	10.2	-	-	-	-	-	-	4.39	-	-	-	49.1	15.6	-	-	-	-	-	-
384	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.5	57.2	-	-	-	-	-	-
385	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	-	-	9.02	-	-	-	-	-	-	-
386	-	-	-	-	-	-	-	-	-	3.48	-	-	-	-	-	-	19.5	-	-	-	19.1	-	-	-	-	-	-	-
387	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.4	-	-	-	0.367	47.4	-	-	-	-	-	-
388	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.0	-	-	-	-	-	-	-
389	-	55.2	-	-	-	-	-	-	0.0151	-	-	-	-	-	-	-	-	-	-	-	3.13	-	-	-	-	-	-	-
390	-	12.9	1.65	3.35	-	-	-	-	-	1.98	5.61	-	-	-	0.0063	-	-	5.87	-	-	-	0.0008	-	23.5	-	-	-	-
391	-	-	-	-	-	-	-	-	18.7	18.9	-	-	-	-	-	-	15.1	-	-	-	-	-	-	-	-	-	-	-
392	-	0.0017	-	-	-	-	-	-	-	38.4	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-
393	-	-	-	-	-	-	-	-	43.0	11.1	-	-	-	-	-	-	-	13.8	-	-	13.6	-	-	-	-	-	-	-
394	-	6.32	-	-	-	-	-	-	6.76	11.2	-	-	-	-	-	-	0.0002	5.23	-	-	75.9	-	-	-	-	-	-	-
395	-	15.0	-	-	-	-	-	-	-	8.03	-	-	-	-	-	-	8.45	9.55	-	-	95.0	-	-	-	-	-	-	-
396	-	-	-	-	-	-	-	-	2.19	28.3	11.8	-	-	-	-	-	-	0.429	-	-	4.43	-	-	-	-	-	-	-
397	-	-	-	-	0.0138	-	-	-	-	-	-	-	-	-	-	-	-	21.9	-	-	32.9	0.262	-	-	-	-	-	-
398	-	-	-	-	0.0059	-	-	-	-	2.51	-	-	-	-	-	-	-	17.8	-	-	65.9	0.0098	-	-	-	-	-	-
399	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
400	-	-	-	-	-	-	-	-	-	3.15	-	-	-	-	-	-	-	24.4	-	-	48.4	-	-	-	-	-	-	-
401	-	-	-	-	-	-	-	-	-	18.5	-	-	-	-	6.69	-	-	-	-	-	4.76	-	-	-	-	-	-	-
402	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.7	-	-	44.8	-	-	-	-	-	-	-
403	-	-	-	-	-	-	-	-	53.3	-	-	-	-	-	-	-	-	6.19	-	-	-	-	-	-	-	-	-	-
404	-	-	-	-	-	-	-	-	107	-	-	-	-	-	-	-	-	15.0	-	-	-	-	-	-	-	-	-	-
405	-	-	-	-	-	-	-	-	23.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
406	-	17.1	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-	56.4	-	-	-	-	-	-	-
407	-	22.0	-	-	-	-	-	-	-	52.7	-	-	-	-	-	-	0.0137	-	-	-	219	-	-	-	-	-	-	-
408	-	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	-	-	19.3	-	-	122	-	-	-	-	-	-	-
409	-	10.5	-	-	-	-	-	-	-	18.5	-	-	-	-	37.2	-	-	20.7	-	-	84.0	-	-	-	-	-	-	-
410	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61.9	-	-	-	-	-	-	-	-	-	-	-	-	-
411	-	-	-	-	-	-	-	-	-	-	-	-	-	-	102	-	-	-	-	-	33.2	-	-	-	-	-	-	-
412	-	-	-	-	-	-	-	-	255	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
413	-	-	-	-	-	-	-	-	111	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
414	-	15.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
415	-	21.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.63	-	-	-	-	-	-	-	-	-	-
416	-	-	-	-	-	-	137	-	-	-	-	-	-	-	12.5	-	-	1.70	-	-	-	-	-	-	-	-	-	-
417	-	-	-	-	-	-	-	-	-	-	-	-	-	-	67.8	-	-	19.1	-	-	-	-	-	-	-	-	-	-
418	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.0	-	-	1.72	-	-	-	-	-	-	-	-	-	-
419	-	-	-	-	-	-	-	-	-	2.72	-	-	-	-	51.8	-	-	27.6	-	-	5.19	-	-	-	-	-	-	-
420	-	-	-	-	-	-	-	-	-	18.6	-	-	-	-	29.2	-	-	3.95	-	-	4.54	5.79	-	-	-	-	-	-
421	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.2	-	-	1.48	-	-	-	-	-	-	-	-	-	-
422	-	-	-	-	-	-	-	-	124	-	-	-	-	-	1.63	-	-	22.3	-	-	-	-	-	-	-	-	-	-
423	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.905	-	-	24.1	-	-	-	-	-	-	-
424	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.3	-	-	-	-	-	-	-
425	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-	-	-	-
426	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.9	-	-	-	-	-	-	-
427	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.86	-	-	19.3	-	-	-	-	-	-	-
428	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.0	-	-	-	14.4	-	-	-	-	-	-	-
429	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	-	-	-	-	-	-	-
430	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.717	-	-	6.72	-	-	-	-	-	-	-
431	-	-	-	-	-	-	-	-	0.396	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
432	-	4.21	-	-	-	-	-	-	103	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
433	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	38.5	-	-	14.9	-	-	4.14	10.3	-	-	-	-	-	-
434	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40.6	85.6	-	-	-	-	-	-
435	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.116	-	-	-	19.8	74.6	-	-	-	-	-	-
436	-	-	-	-	-	-	-	-	-	13.7	-	-	-	-	-	-	-	-	-	-	-	21.3	-	-	-	-	-	-
437	-	-	0.297	5.49	-	-	-	-	-	10.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
438	4.25	-	-	-	-	-	-	-	-	23.0	-	-	-	-	-	-	5.81	-	-	-	48.0	75.8	-	-	-	-	-	-
439	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	91.7	-	-	-	-	-	-	-
440	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	53.1	28.8	-	-	-	-	-	-
441	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	112	13.3	-	-	-	-	-	-
442	-	-	-	-	-	-	-	-	-	19.9	-	-	-	-	-	-	-	-	-	-	20.9	40.3	-	-	-	-	-	-
443	5.64	-	-	-	-	-	-	-	-	108	-	-	-	-	-	-	-	-	-	-	5.44	32.9	-	-	-	-	-	-
444	-	-	-	-	-	-	-	-	-	9.01	-	-	-	-	-	-	-	-	-	-	12.2	28.0	-	-	-	-	-	-
445	-	-	-	-	-	-	-	-	-	24.3	-	-	-	-	-	-	-	-	-	-	29.2	25.3	-	-	-	-	-	-
446	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	49.2	-	-	-	-	-	-	-	-	-
447	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44.0	-	-	-	-	-	-	-	-	-
448	-	-	-	-	122	-	-	-	9.98	-	-	-	-	-	-	-	0.0026	-	166	-	0.0000	-	-	-	-	-	-	-
449	-	-	3.98	-	128	-	-	-	-	-	-	-	-	-	-	-	-	-	61.8	-	-	-	-	-	-	-	-	-
450	-	-	-	-	-	-	-	-	-	0.854	-	-	-	-	-	-	-	-	7.15	7.34	-	305	-	-	-	-	-	-
451	-	-	-	-	-	-	-	-	-	-	-	-	-	0.337	-	-	-	-	-	2.53	0.0211	139	-	-	-	-	-	-
452	-	-	-	-	-	-	-	-	-	-	-	-	-	1.89	-	-	0.0254	1.41	-	29.0	-	230	-	-	-	-	-	-
453	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.9	16.8	-	-	-	-	-	-
454	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	29.9	-	-	-	-	-	-
455	21.0	-	-	-	-	-	-	-	-	13.2	10.9	-	-	-	-	-	5.69	-	-	-	-	1.60	-	-	-	-	-	-
456	-	-	-	-	-	-	-	-	-	20.9	0.0000	-	-	-	-	-	-	-	-	-	-	16.7	-	-	-	-	-	-
457	-	-	-	-	-	-	-	-	30.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
458	-	-	-	-	-	-	-	-	56.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
459	-	-	-	-	21.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
460	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	-	-	-	-
461	-	-	-	-	3.59	-	-	-	-	-	-	-	-	-	-	-	-	-	69.0	-	-	-	-	-	-	-	-	-
462	-	-	-	-	1.40	-	85.7	-	-	-	-	-	-	-	-	-	-	-	7.80	-	-	-	-	-	-	-	-	-
463	-	-	0.216	-	0.612	-	-	-	-	-	-	-	-	-	-	-	-	-	0.433	0.0000	6.68	-	-	-	-	-	-	-
464	-	-	-	-	0.0338	-	-	-	-	-	-	-	-	-	-	-	-	-	1.19	-	10.8	-	-	-	-	-	-	-
465	-	-	-	-	0.620	-	-	-	-	-	-	-	-	-	-	-	-	-	73.4	-	-	-	-	-	-	-	-	-
466	-	0.0105	-	-	-	-	-	-	1.27	-	-	-	-	-	12.2	-	2.99	-	-	-	-	-	-	-	-	-	-	-
467	-	-	-	-	4.13	-	-	-	-	-	-	-	-	-	-	-	-	39.6	1.56	-	39.0	0.0017	0.0858	-	-	-	-	-
468	-	-	9.83	-	-	-	32.6	-	-	0.778	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-
469	-	-	0.0001	-	-	-	21.9	-	-	16.8	-	-	-	-	-	-	13.1	-	-	0.0000	21.7	9.32	-	-	-	-	-	-
470	-	-	-	-	-	-	-	-	-	2.01	-	-	-	-	-	-	-	2.16	-	-	2.04	-	-	-	-	-	-	-
471	14.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
472	15.3	-	-	-	14.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
473	-	-	-	-	166	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0344	20.5	-	-	-	-	-	-	-	-
474	-	-	-	-	57.5	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0215	3.37	-	-	-	-	-	-	-	-
475	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0289	52.4	-	-	-	-	-	-	-	-
476	-	-	-	-	0.0055	-	-	-	-	-	-	-	-	-	-	-	-	-	0.456	105	-	-	-	-	-	-	-	-
477	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0972	-	0.0554	64.6	-	5.44	-	-	-	-	-	-
478	-	-	-	-	114	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
479	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
480	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.31	-	-	-	36.7	-	-	-	-	-	-	-
481	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.25	-	-	-	-	39.5	-	-	-	-	-	-
482	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	12.3	-	-	-	-	-	-
483	35.6	-	-	-	-	-	-	-	-	9.46	-	-	-	-	-	-	0.960	-	0.0006	-	-	19.8	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
484	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0018	-	-	14.6	-	-	-	-	-	-
485	-	-	-	-	-	-	-	-	-	9.09	-	-	-	-	-	-	-	2.02	0.0000	-	-	1.94	-	-	-	-	-	-
486	-	-	-	-	-	-	-	-	-	0.0010	-	-	-	-	-	-	-	8.57	-	-	-	14.6	-	-	-	-	-	-
487	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-
488	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.89	-	-	18.9	-	0.0000	-	-	-	-	-	-
489	-	-	-	-	-	-	-	-	-	0.0004	-	-	-	-	-	-	0.0021	-	-	24.2	-	7.01	-	-	-	-	-	-
490	-	-	-	-	0.183	-	-	-	-	-	-	-	-	-	-	-	0.0001	5.96	-	-	-	46.7	-	-	-	-	-	-
491	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.3	-	-	-	-	2.27	-	-	-	-	-	-
492	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0006	11.1	0.0001	-	-	28.9	-	-	-	-	-	-
493	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.8	-	-	-	-	-	-
494	-	-	-	-	0.0147	-	-	-	-	-	-	-	-	-	-	-	-	10.7	-	-	-	78.4	-	-	-	-	-	-
495	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.49	-	-	-	23.6	-	-	-	-	-	-
496	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0020	-	-	-	-	47.6	-	-	-	-	-	-
497	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.460	-	-	-	56.5	-	-	-	-	-	-
498	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	0.0038	-	-	-	19.4	-	-	-	-	-	-
499	0.0008	6.15	0.604	-	-	-	-	-	-	7.18	-	-	-	-	-	-	2.40	-	0.0440	-	-	12.1	-	-	-	-	-	-
500	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.827	14.6	0.185	-	-	32.8	-	-	-	-	-	-
501	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.148	-	0.154	32.7	-	29.0	-	-	-	-	-	-
502	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0132	-	-	-	-	79.5	-	-	-	-	-	-
503	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	0.549	-	-	-	24.6	-	-	-	-	-	-
504	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	6.48	-	-	-	17.9	-	-	-	-	-	-
505	-	-	-	-	-	-	-	-	-	5.70	-	-	-	-	-	-	-	-	-	-	-	9.40	-	-	-	-	-	-
506	-	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	-	0.0015	0.0284	-	-	7.79	-	-	-	-	-	-
507	-	-	-	-	-	-	-	-	-	18.2	-	-	-	-	-	-	-	-	-	-	-	1.59	-	-	-	-	-	-
508	-	-	0.197	-	-	-	-	-	-	46.6	-	-	-	-	-	-	1.28	4.11	0.0322	-	-	-	-	-	-	-	-	-
509	-	-	-	-	0.0057	-	42.0	-	-	-	-	-	-	-	-	-	7.27	-	0.0023	-	-	-	-	-	-	-	-	-
510	-	-	-	-	1.42	-	31.6	-	-	-	-	-	-	-	-	-	-	2.08	0.261	-	-	-	-	-	-	-	-	-
511	4.41	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.7	-	-	0.0001	-	-	-	-	-	-
512	-	-	-	-	-	-	-	-	115	-	-	-	-	-	-	-	18.7	-	-	-	-	-	-	-	-	-	-	-
513	-	0.442	-	-	-	-	-	-	3.89	1.69	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
514	-	-	-	-	-	-	-	-	-	5.26	-	-	-	-	-	-	-	92.6	-	-	-	-	-	-	-	-	-	-
515	-	-	-	-	-	-	-	-	-	5.85	-	-	-	-	4.82	-	-	14.0	-	-	10.00	-	-	-	-	-	-	-
516	-	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	-	9.74	-	-	20.5	-	-	-	-	-	-	-
517	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0029	9.31	-	-	14.9	-	-	-	-	-	-	-
518	-	-	-	-	-	-	-	-	-	4.92	-	-	-	-	-	-	0.0003	1.92	-	-	12.3	-	-	-	-	-	-	-
519	-	-	-	-	-	-	-	-	-	5.96	-	-	-	-	-	-	9.71	-	-	-	39.4	-	-	-	-	-	-	-
520	-	-	-	-	-	-	-	-	-	3.84	-	-	-	-	-	-	-	-	-	-	22.5	-	-	-	-	-	-	-
521	-	-	-	-	-	-	-	-	-	9.95	-	-	-	-	-	-	0.0065	-	-	-	28.9	-	-	-	-	-	-	-
522	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.1	-	-	-	39.4	-	-	-	-	-	-	-
523	-	-	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-	-	-	-	-	2.59	-	-	-	-	-	-	-
524	-	-	-	-	-	-	-	-	-	0.339	-	-	-	-	-	-	-	-	-	-	42.7	-	-	-	-	-	-	-
525	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	48.0	-	-	-	-	-	-	-
526	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33.8	-	-	-	-	-	-	-
527	-	-	-	-	-	-	-	-	-	0.0034	-	-	-	-	-	-	-	-	-	-	36.2	-	-	-	-	-	-	-
528	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-	-	0.833	-	-	5.09	-	-	-	-	-	-	-
529	-	-	-	-	-	-	-	-	-	1.83	-	-	-	-	-	-	-	5.71	-	-	52.4	-	-	-	-	-	-	-
530	-	-	-	-	-	-	-	-	-	1.30	-	-	-	-	-	-	-	6.14	-	-	14.2	-	-	-	-	-	-	-
531	-	-	-	-	0.225	-	-	-	-	3.64	-	-	-	-	-	-	9.51	23.3	-	-	38.4	0.0001	-	-	-	-	-	-
532	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.15	-	-	14.7	-	-	-	-	-	-	-
533	-	-	-	-	-	-	-	-	-	1.32	-	-	-	-	-	-	-	3.09	-	-	12.7	-	-	-	-	-	-	-
534	-	-	-	-	0.110	-	-	-	-	5.34	-	-	-	-	-	-	-	24.7	-	-	-	-	-	-	-	-	-	-
535	-	2.36	-	-	-	-	-	-	24.6	-	-	-	-	-	4.71	-	-	-	-	-	-	-	-	-	-	-	-	-
536	-	-	-	-	-	-	-	-	37.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
537	-	24.8	-	-	-	-	-	-	7.67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
538	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.41	-	-	-	-	-	-	-	-	-	-	-	-	-
539	-	-	-	-	-	-	-	-	14.3	6.61	-	-	-	-	-	-	-	12.9	-	-	0.0811	-	-	-	-	-	-	-
540	-	-	-	-	-	-	-	-	-	6.03	-	-	-	-	-	-	-	-	-	-	0.0689	-	-	-	-	-	-	-
541	-	-	-	-	-	-	-	-	-	17.7	-	-	-	-	-	-	-	1.86	-	-	21.3	-	-	-	-	-	-	-
542	-	1.61	-	-	-	-	-	-	-	8.75	-	-	-	-	16.0	-	0.515	-	-	-	1.48	-	-	-	-	-	-	-
543	-	-	-	-	-	-	-	-	5.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
544	-	-	-	-	-	-	-	-	3.89	-	-	-	-	-	10.5	-	-	-	-	-	-	-	-	-	-	-	-	-
545	-	-	-	-	-	-	-	-	3.42	6.61	-	-	-	-	4.45	-	-	0.613	-	-	-	-	-	-	-	-	-	-
546	-	-	-	-	-	-	-	-	0.774	-	-	-	-	-	22.8	-	-	-	-	-	-	-	-	-	-	-	-	-
547	-	-	-	-	-	-	-	-	1.70	-	-	-	-	-	19.6	-	-	-	-	-	-	-	-	-	-	-	-	-
548	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.7	-	-	-	-	-	-	-	-	-	-	-	-	-
549	-	-	-	-	-	-	-	-	1.68	12.0	-	-	-	-	-	-	5.04	6.14	-	-	-	-	-	-	-	-	-	-
550	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.98	-	-	-	-	-	-	-	-	-	-	-	-	-
551	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.1	-	-	-	-	-	-	-	-	-	-	-	-	-
552	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.1	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
553	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.3	-	-	-	-	-	-	-	-	-	-	-	-	-
554	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.27	-	0.0001	-	-	-	6.40	-	-	-	-	-	-	-
555	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.41	-	-	-	-	-	16.3	-	-	-	-	-	-	-
556	-	-	-	-	-	-	-	-	-	0.142	-	-	-	-	9.67	-	-	-	-	-	-	-	-	-	-	-	-	-
557	-	-	-	-	-	-	-	-	-	1.93	-	-	-	-	-	-	0.0038	1.72	-	-	33.6	-	-	-	-	-	-	-
558	-	-	-	-	-	-	-	-	-	6.16	-	-	-	-	-	-	35.8	5.46	-	-	-	-	-	-	-	-	-	-
559	-	-	-	-	-	-	-	-	-	5.57	-	-	-	-	-	-	-	14.1	-	-	59.9	-	-	-	-	-	-	-
560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.98	-	-	-	48.1	-	-	-	-	-	-	-
561	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	-	-	-	-
562	-	-	-	-	-	-	-	-	-	11.2	-	-	-	-	-	-	-	-	-	-	19.0	-	-	-	-	-	-	-
563	-	-	-	-	-	-	-	-	-	24.9	-	-	-	-	-	-	-	-	-	-	59.0	-	-	-	-	-	-	-
564	-	-	-	-	0.718	-	-	-	-	3.59	-	-	-	-	-	-	-	27.5	-	-	40.1	0.0223	-	-	-	-	-	-
565	-	-	-	-	0.521	-	-	-	-	0.971	-	-	-	-	-	-	-	13.6	-	-	22.2	0.370	-	-	-	-	-	-
566	-	-	-	-	-	-	-	-	26.3	8.85	-	-	-	-	-	-	0.0203	-	-	-	44.0	-	-	-	-	-	-	-
567	-	-	-	-	0.0002	-	-	-	0.684	-	-	-	-	-	-	-	-	9.34	-	-	-	-	-	-	-	-	-	-
568	-	-	-	-	-	-	-	-	-	2.41	-	-	-	-	-	-	-	18.6	-	-	6.11	-	-	-	-	-	-	-
569	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.5	-	-	-	-	-	-	-	-	-	-	-	-	-
570	-	-	-	-	25.5	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
571	-	-	-	-	0.160	-	-	21.0	-	0.0000	-	-	-	-	-	-	-	0.685	0.193	-	-	25.9	-	-	-	-	-	-
572	-	-	-	-	1.97	-	15.8	-	-	68.2	-	-	-	-	-	-	-	5.86	0.0516	-	-	3.53	-	-	-	-	-	-
573	-	-	-	-	-	-	8.56	-	-	49.3	-	-	-	-	-	-	1.05	-	3.55	-	-	-	-	-	-	-	-	-
574	2.12	-	-	-	-	-	-	-	-	9.54	-	-	-	-	-	-	-	-	10.4	-	-	65.2	-	-	-	-	-	-
575	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	3.76	-	23.0	-	-	-	-	-	-
576	-	-	-	-	-	-	-	-	-	0.0006	-	-	-	-	-	-	-	0.0004	-	-	-	13.9	-	-	-	-	-	-
577	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.1	-	0.0027	-	-	9.91	-	-	-	-	-	-
578	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.72	-	-	-	-	-	-	-	-	-	-	-	-	-
579	-	-	-	-	17.3	-	-	-	-	-	-	-	-	-	-	-	-	0.140	47.3	-	15.3	-	-	-	-	-	-	-
580	-	-	6.58	-	2.01	-	3.80	-	-	20.8	-	-	-	-	-	-	-	-	5.20	-	6.56	24.1	-	-	-	-	-	-
581	-	-	32.5	-	0.699	-	14.9	-	-	35.9	-	-	-	-	-	-	4.23	-	3.45	-	16.0	13.4	-	-	-	-	-	-
582	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0054	0.0000	11.6	-	13.0	-	-	-	-	-	-
583	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.1	-	-	-	-	-	-	-	-	-	-	-	-	-
584	-	-	-	-	-	-	-	-	-	16.9	2.57	-	-	-	17.6	-	-	-	-	-	1.27	-	-	-	-	-	-	-
585	-	-	-	-	-	-	-	-	-	6.06	-	-	-	-	-	-	-	0.0306	-	-	24.1	-	-	-	-	-	-	-
586	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.1	-	-	-	-	-	-	-	-	-	-	-	-	-
587	-	30.8	-	-	3.37	-	-	-	28.2	-	-	-	-	-	-	-	-	22.4	-	-	-	-	-	-	-	-	-	-
588	-	-	16.9	-	-	-	7.11	-	-	-	-	-	-	-	-	-	36.9	-	-	-	47.8	-	-	-	-	-	-	-
589	-	-	6.86	-	52.3	-	23.3	-	-	1.74	-	-	-	-	-	-	0.0048	6.23	-	-	37.2	-	-	-	-	-	-	-
590	-	-	-	-	2.52	-	-	-	-	-	-	-	-	-	-	-	-	4.65	-	-	6.62	-	-	-	-	-	-	-
591	-	5.95	-	-	-	-	-	-	-	7.06	-	-	-	-	15.2	-	-	-	-	-	-	-	-	-	-	-	-	-
592	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0372	-	-	15.9	-	-	-	-	-	-
593	-	-	-	-	55.2	-	-	-	4.41	-	-	-	-	-	-	-	-	0.0091	-	-	-	-	-	-	-	-	-	-
594	-	-	-	-	26.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
595	-	-	-	-	24.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
596	-	-	-	-	3.94	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
597	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.2	-	-	-	-	-	-	-	-	-
598	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.63	-	-	-	-	-	-	-	-	-
599	-	-	-	-	40.8	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0689	-	-	3.88	-	-	-	-	-	-
600	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
601	-	-	-	-	38.4	0.0009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
602	-	-	-	-	27.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
603	-	-	-	-	86.0	-	-	-	-	-	-	-	-	-	-	-	-	3.18	1.24	-	0.350	-	-	-	-	-	-	-
604	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.29	-	-	-	-	-	-	-	-	-
605	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
606	-	-	-	-	1.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0055	-	-	-	-	-	-	-
607	-	-	-	-	49.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
608	-	-	-	-	36.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
609	-	-	-	-	8.28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
610	-	-	-	-	57.3	-	-	-	-	-	-	-	-	-	-	-	-	-	19.0	-	-	-	-	-	-	-	-	-
611	-	-	-	-	61.8	-	-	-	-	-	-	-	-	-	-	-	-	-	21.6	-	-	-	-	-	-	-	-	-
612	-	-	-	-	37.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
613	-	-	-	-	35.6	-	-	-	-	-	-	-	-	-	-	-	-	0.0097	-	-	-	-	-	-	-	-	-	-
614	-	-	-	-	60.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
615	-	-	-	-	59.4	-	-	-	-	-	-	-	-	-	-	-	-	-	49.0	-	-	18.4	-	-	-	-	-	-
616	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
617	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
618	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.1	-	-	-	-	-	-	-	-
619	-	11.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0019	-	-	-	-	1.05	-	-	-	-	-	-
620	-	-	-	-	0.0069	-	-	-	-	-	-	-	-	-	-	-	2.40	-	1.83	-	-	10.2	-	-	-	-	-	-
621	6.78	-	-	-	-	-	3.94	-	-	21.6	-	-	-	3.68	-	-	9.98	-	-	-	-	15.0	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
622	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.8	-	-	-	-	20.8	-	-	-	-	-	-
623	-	-	-	-	0.0355	-	-	-	-	-	-	-	-	-	-	-	-	-	2.45	-	-	8.44	-	-	-	-	-	-
624	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.797	-	-	-	-	25.3	-	-	-	-	-	-
625	-	-	-	-	-	-	35.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
626	-	-	-	-	4.62	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
627	-	-	-	-	27.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
628	-	-	-	-	-	-	0.483	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
629	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.49	-	-	-	-	-	-
630	-	-	-	-	-	4.61	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
631	3.18	8.58	-	-	-	-	9.78	-	-	3.65	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
632	-	-	-	-	0.287	-	11.3	-	-	7.01	-	-	-	-	-	-	0.0382	2.11	-	-	-	1.30	-	-	-	-	-	-
633	-	-	-	-	-	-	-	-	-	2.26	-	-	-	-	-	-	-	-	0.487	-	-	1.12	-	-	-	-	-	-
634	-	-	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	0.0007	-	-	-	-	33.0	-	-	-	-	-	-
635	-	-	-	-	7.84	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	15.3	-	-	-	-	-	-
636	-	-	-	-	6.16	-	10.3	-	-	14.9	-	-	-	-	-	-	-	-	-	-	-	19.5	-	-	-	-	-	-
637	5.20	-	-	-	-	-	-	-	-	7.47	-	-	-	-	-	-	0.590	-	-	-	-	22.3	-	-	-	-	-	-
638	-	-	-	-	-	-	6.78	-	-	4.49	-	-	-	-	-	-	-	-	-	-	-	21.5	-	-	-	-	-	-
639	-	-	-	-	0.490	-	9.32	-	-	8.43	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
640	21.0	-	-	-	-	-	13.4	-	-	34.7	-	-	-	2.39	-	-	-	-	-	-	-	-	-	-	-	-	-	-
641	1.66	-	-	-	-	-	-	-	-	3.93	-	-	-	-	-	-	-	-	-	-	-	15.2	-	-	-	-	-	-
642	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.1	-	-	-	-	-	-
643	-	4.86	-	-	-	-	-	-	-	0.664	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
644	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.5	-	-	-	-	-	-
645	-	-	-	-	36.6	1.50	1.89	-	-	0.0396	-	-	-	-	-	-	0.572	5.57	1.33	-	-	5.55	-	-	-	-	-	-
646	-	4.36	-	-	25.4	-	40.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
647	-	3.85	-	-	-	-	-	-	-	7.41	-	-	-	-	-	-	6.76	2.01	0.367	-	-	58.1	-	-	-	-	-	-
648	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.04	-	-	-	-	-	-
649	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.04	-	-	-	-	-	-
650	-	-	-	-	-	-	8.82	-	-	16.8	-	-	-	-	-	-	4.10	-	-	-	-	-	-	-	-	-	-	-
651	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.294	-	-	-	-	11.0	-	-	-	-	-	-
652	-	3.53	-	-	-	-	-	-	-	18.0	-	-	-	-	-	-	5.40	3.62	-	-	-	2.19	-	-	-	-	-	-
653	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.44	-	-	-	-	26.0	-	-	-	-	-	-
654	-	5.73	-	-	-	-	-	-	-	3.41	-	-	-	-	-	-	-	-	-	-	-	8.99	-	-	-	-	-	-
655	-	14.0	-	-	-	-	44.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
656	-	-	2.12	-	-	-	2.59	-	-	-	-	-	-	-	-	-	-	3.25	-	0.0001	-	3.29	-	26.0	6.90	-	-	-
657	-	-	-	-	0.0007	-	-	-	-	-	-	-	-	-	-	-	-	4.29	0.0035	-	-	16.8	-	12.7	2.89	-	-	-
658	-	10.4	-	-	-	-	-	0.0044	-	-	-	-	-	-	-	-	6.84	-	-	-	-	15.4	-	-	-	-	-	-
659	-	-	5.09	-	1.66	-	9.32	-	-	-	-	-	-	-	-	-	-	12.0	-	-	-	-	-	-	3.79	-	-	-
660	-	44.6	-	-	-	-	-	-	-	51.9	-	-	-	-	-	-	5.36	2.75	-	-	-	1.27	-	-	-	-	-	-
661	-	-	-	-	0.0382	-	0.0053	1.77	-	-	-	-	-	-	-	-	357	-	-	-	-	0.0000	-	-	-	-	-	-
662	-	-	-	-	-	-	-	-	-	4.09	-	-	-	-	-	-	9.28	3.58	-	-	-	34.0	-	-	-	-	-	-
663	-	-	-	-	0.0000	-	15.8	-	-	-	-	-	-	-	-	-	-	5.83	-	-	-	-	-	-	-	-	-	-
664	8.49	23.9	-	-	-	-	2.04	-	-	8.27	-	-	-	-	-	-	4.35	-	-	-	-	-	-	-	-	-	-	-
665	-	-	-	-	-	-	0.0431	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.9	-	-	-	-	-	-
666	-	-	-	-	-	-	9.12	-	-	40.1	-	-	-	-	-	-	13.1	-	0.0033	-	-	-	-	-	-	-	-	-
667	-	-	-	-	-	-	-	-	-	4.10	-	-	-	-	-	-	9.42	1.82	-	-	-	-	-	-	-	-	-	-
668	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.8	-	-	-	-	-	-
669	-	37.8	-	-	-	-	4.21	-	-	28.5	-	-	-	-	-	-	-	-	-	-	-	6.22	-	-	-	-	-	-
670	6.29	1.71	-	-	-	-	-	-	-	51.5	-	-	-	-	-	-	5.42	0.0005	-	-	-	5.11	-	-	-	-	-	-
671	-	7.83	-	-	-	-	12.1	-	-	8.08	-	-	-	-	-	-	31.5	-	-	-	-	-	-	-	-	-	-	-
672	-	-	-	-	0.181	-	0.0346	-	-	65.8	-	-	-	-	-	-	-	0.0010	0.0000	-	-	0.551	-	-	-	-	-	-
673	-	-	-	-	0.117	-	-	-	-	-	-	-	-	-	-	-	0.0020	-	0.0001	-	-	4.37	-	-	-	-	-	-
674	22.2	-	-	-	0.656	-	-	-	-	10.1	-	-	-	-	-	-	-	-	-	-	-	97.4	-	-	-	-	-	-
675	28.1	-	-	-	-	-	-	-	-	0.740	-	-	-	9.16	-	-	2.46	-	-	-	-	5.60	-	-	-	-	-	-
676	-	-	-	-	0.411	-	-	81.8	-	-	-	-	-	-	-	-	42.8	-	-	-	-	34.7	-	-	-	-	-	-
677	-	-	-	-	-	-	18.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
678	-	33.3	-	-	-	-	-	-	-	3.59	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
679	-	-	-	-	-	-	-	2.19	-	-	-	-	-	-	-	-	0.0024	-	-	-	-	4.48	-	-	-	-	-	-
680	-	21.9	-	-	-	-	0.0037	9.81	-	8.35	-	-	-	-	-	-	0.0008	-	-	-	-	18.0	-	-	-	-	-	-
681	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.90	-	-
682	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.481	-	6.08	-	-	-	-	-	-	-
683	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	96.0	-	-	-	-	-	-	-	-	-
684	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.8	-	-	-	-	-	-	-	-	-
685	-	-	-	-	0.0506	-	-	-	-	-	-	-	-	-	-	-	-	-	40.5	-	-	-	-	-	-	-	-	-
686	-	-	-	-	0.0991	-	-	-	-	-	-	-	-	-	-	-	-	-	26.4	-	-	-	-	-	-	-	-	-
687	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	43.5	-	-	-	-	-	-	-	-	-
688	-	-	-	-	0.0522	-	-	-	-	-	-	-	-	-	-	-	-	-	55.7	-	-	-	-	-	-	-	-	-
689	-	-	-	-	0.0078	15.6	-	-	-	-	-	-	-	-	-	-	-	-	67.0	-	3.09	-	-	-	-	-	-	-
690	-	-	-	-	3.52	-	-	-	-	-	-	-	-	-	-	-	-	-	78.1	-	19.0	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
691	0.0118	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52.1	-	-	-	-	-	-	-	-	-
692	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	64.4	-	-	-	-	-	-	-	-	-
693	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	51.9	-	-	-	-	-	-	-	-	-
694	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.4	-	-	-	-	-	-	-	-	-
695	35.1	-	-	-	-	-	-	-	-	0.647	-	-	-	-	-	-	-	2.91	-	-	-	-	-	-	-	-	-	-
696	10.6	-	-	9.55	-	-	-	-	-	3.94	-	-	0.229	-	-	-	-	10.6	-	-	-	-	-	-	-	-	-	-
697	-	-	-	-	-	-	-	-	-	9.98	-	-	-	-	-	-	-	-	-	-	-	0.0162	12.9	13.9	-	-	-	-
698	-	-	-	-	-	-	-	-	-	4.56	0.0165	-	4.94	0.0250	-	8.08	-	-	-	-	-	0.0016	-	13.8	-	-	-	-
699	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0023	-	-	-	-	6.98	-	-	-	-
700	-	-	-	-	0.557	-	-	3.75	-	-	-	-	-	-	-	-	-	-	150	-	-	-	-	-	-	-	-	-
701	-	-	-	-	41.1	-	2.27	-	-	-	-	-	-	-	-	-	-	-	88.1	-	-	-	-	-	-	-	-	-
702	-	-	-	-	149	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
703	-	-	-	-	112	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
704	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61.2	-	-	-	-	-	-	-	-	-
705	-	-	-	-	46.9	-	-	-	-	-	-	-	-	-	-	-	-	-	1.78	-	5.57	-	-	-	-	-	-	-
706	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.0	1.46	-	16.2	18.7	-	-	64.5	-	-	-
707	-	-	-	-	0.132	-	-	-	-	-	-	-	-	-	-	-	-	-	85.6	-	-	-	-	-	-	-	-	-
708	-	-	-	-	0.175	-	-	-	-	-	-	-	-	-	-	-	-	-	55.6	-	-	-	-	-	-	-	-	-
709	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.1	-	-	-	-	-	-	-	-	-
710	-	-	-	-	-	-	-	-	-	12.4	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-
711	81.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26.0	-	-	-	-	-	-	-	-	-	-
712	13.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.120	-	-	52.6	-	-	-	-	-	-	-
713	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34.1	8.30	-	-	-	-	-	-
714	-	8.71	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	74.4	13.0	-	-	-	-	-	-
715	-	-	-	-	-	-	179	13.1	-	-	-	-	-	-	-	-	-	7.11	-	-	-	-	-	4.38	-	-	-	-
716	-	-	-	-	-	-	-	40.0	-	-	-	-	-	-	-	-	-	1.40	-	-	-	-	-	35.7	-	-	-	-
717	-	-	-	5.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
718	-	-	-	4.83	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.7	-	-	-	-	-	-
719	-	-	-	7.80	-	-	-	-	-	-	-	-	-	-	-	-	-	5.73	-	-	-	82.2	3.78	-	-	-	-	-
720	-	-	-	-	-	-	-	-	-	0.260	-	-	-	-	-	-	-	-	-	-	-	30.9	0.311	-	-	-	-	-
721	1.67	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.5	19.4	-	-	-	-	-
722	-	1.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.8	-	-	-	-	-	-
723	-	-	-	-	-	-	-	-	-	-	7.44	-	0.415	0.0129	7.74	5.44	-	-	-	-	-	-	-	-	-	-	-	-
724	-	-	0.427	-	-	-	-	-	-	7.86	-	-	-	-	-	-	-	1.82	-	-	-	0.0001	4.37	2.93	-	-	-	-
725	-	-	-	-	-	-	-	-	-	-	-	-	-	0.367	15.8	-	-	-	-	-	-	-	-	-	-	-	-	-
726	-	-	-	-	-	-	-	-	-	-	-	-	-	0.895	16.2	-	-	-	-	-	-	-	-	-	-	-	-	-
727	-	11.6	-	-	-	-	-	-	-	0.0000	-	-	0.361	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
728	-	-	-	-	-	-	-	-	-	-	-	-	12.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
729	-	3.19	-	-	-	-	-	-	-	-	-	-	-	0.0008	23.0	-	-	-	-	-	-	-	-	-	-	-	-	-
730	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	-	-	-	-	-	-	-	11.6	-	-	-	-	-	-
731	-	-	-	-	-	-	-	-	-	-	0.0000	-	0.501	0.0182	-	14.7	-	-	-	-	-	-	-	-	-	-	-	-
732	-	-	0.187	-	-	-	-	-	-	5.01	6.59	-	-	-	-	-	33.4	-	-	-	-	33.9	-	-	-	-	-	-
733	-	-	-	-	-	-	-	-	-	22.1	-	-	-	-	-	-	33.2	-	-	-	-	57.6	0.120	-	-	-	-	-
734	-	-	7.84	-	-	-	-	-	-	46.9	-	-	-	-	-	-	0.238	-	-	-	-	60.7	-	-	-	-	-	-
735	-	-	0.704	0.646	-	-	-	-	-	3.35	-	-	-	-	-	-	-	-	-	-	-	9.70	-	-	-	-	-	-
736	-	-	-	-	-	-	-	-	-	1.26	-	-	-	-	-	-	-	-	-	-	13.8	128	-	-	-	-	-	-
737	0.266	-	-	-	-	-	-	63.1	-	-	-	-	-	-	-	-	-	23.9	-	-	8.49	-	-	-	-	-	-	-
738	9.93	3.14	-	-	-	-	-	-	-	33.6	-	-	-	-	-	-	-	-	-	-	8.51	-	-	-	5.69	0.0302	-	-
739	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.1	-	-	-	55.7	-	-	-	11.4	-	-	-
740	9.94	-	-	-	-	-	-	4.15	-	2.52	-	-	-	-	-	-	45.6	-	-	-	-	-	-	-	25.3	21.4	-	-
741	-	-	-	-	-	-	8.18	57.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
742	-	-	-	-	1.06	-	-	-	-	-	-	-	-	-	-	-	0.685	-	0.0174	92.5	62.9	-	-	-	3.71	-	-	-
743	-	-	-	-	-	-	-	82.6	-	-	-	-	-	0.0027	-	-	-	85.7	-	-	-	-	-	-	-	-	-	-
744	-	-	-	-	-	-	-	-	-	10.7	-	-	-	-	-	-	-	9.45	-	-	-	0.0872	81.2	-	-	-	-	-
745	-	0.0003	4.00	-	-	-	-	-	-	25.8	-	-	9.86	-	-	-	-	-	-	-	-	0.0008	21.4	-	-	-	-	-
746	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0418	118	12.0	-	-	-	-
747	-	-	-	-	-	-	-	-	-	-	9.74	-	-	-	-	-	-	3.36	-	-	-	0.0054	71.2	6.67	-	-	-	-
748	-	8.85	-	-	-	6.84	-	3.09	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	9.18	-	-	-	-	-
749	-	11.9	-	0.937	-	-	-	-	-	4.17	6.95	-	-	-	-	0.0980	-	-	-	-	-	0.0005	45.7	-	-	-	-	-
750	-	-	6.70	2.00	-	-	-	2.09	-	13.4	16.1	-	-	2.80	10.9	62.4	-	-	-	-	21.6	63.5	-	-	-	-	-	-
751	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	-	-	-	-	53.0	-	-	-	-	-	-
752	-	-	-	1.37	-	-	-	-	-	2.18	2.53	-	-	-	-	-	-	-	-	-	-	117	15.2	-	-	-	-	-
753	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.3	148	-	-	-	-	-	-	-	-	-	-	-
754	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69.9	29.5	8.51	-	-	-	-
755	-	-	-	-	-	-	-	-	-	-	-	-	-	0.257	-	-	-	-	-	-	-	44.5	32.2	5.13	-	-	-	-
756	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.26	14.7	8.53	-	-	-	-
757	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.77	-	-	-	-	62.5	-	-	-	-	-	-
758	-	-	-	1.93	-	-	-	-	-	0.171	0.921	-	-	-	-	-	-	-	-	-	-	64.7	-	-	-	-	-	-
759	-	-	-	-	-	-	13.0	57.4	-	-	-	-	-	-	-	-	-	14.0	-	-	-	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
760	-	6.57	-	-	-	-	-	113	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
761	-	8.27	-	-	-	-	7.94	12.8	-	13.8	-	-	-	-	-	-	-	3.11	0.0350	-	0.447	17.2	-	36.8	-	3.48	-	-
762	-	-	-	-	-	-	155	27.6	-	-	-	-	-	-	-	-	-	15.0	-	-	-	-	-	-	-	-	-	-
763	-	-	-	-	-	-	-	3.69	-	9.54	-	-	-	-	-	-	-	7.32	-	-	-	-	-	-	-	-	-	-
764	2.34	-	-	-	-	-	-	-	-	41.7	-	-	11.7	-	-	-	-	26.1	-	-	-	-	-	-	-	-	-	-
765	-	-	-	0.0000	-	-	40.1	3.85	-	0.754	-	-	-	-	-	-	-	2.90	-	-	-	-	-	4.41	-	2.27	-	-
766	-	-	-	-	-	-	24.6	13.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
767	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.0	0.340	-	51.2	114	-	0.271	-	0.0092	-	-
768	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.91	-	-	-	-	-	120	-	-	-	-
769	-	-	-	-	-	-	2.25	19.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.991	-	-	-	-
770	23.2	-	-	5.33	-	-	2.08	14.4	-	-	-	-	-	-	-	-	-	11.2	-	-	-	-	-	-	-	-	-	-
771	1.49	0.115	-	-	-	-	-	-	-	10.2	-	-	-	-	-	-	3.75	0.0625	-	-	-	-	-	95.3	-	0.404	-	-
772	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.2	-	-	-	-
773	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.554	-	-	-	-	-	20.2	-	-	-	-
774	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	0.964	-	-	-	-	-	91.8	-	-	-	-
775	-	-	-	-	0.211	-	-	35.2	-	-	-	-	-	-	-	-	-	-	-	12.5	23.7	5.33	-	-	14.8	33.8	-	-
776	12.4	-	-	-	-	-	-	-	-	1.53	-	-	-	-	-	-	8.22	-	0.0637	-	105	-	-	-	43.4	5.59	-	-
777	-	-	-	-	-	-	-	4.93	-	-	-	-	-	-	-	-	-	-	-	-	93.2	-	-	-	3.04	24.3	-	-
778	-	-	-	-	0.0423	-	-	-	-	-	-	-	-	-	-	-	16.4	-	0.0000	-	60.6	-	-	-	14.6	5.33	-	-
779	-	-	-	-	0.0054	-	81.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
780	-	-	1.03	-	-	-	-	-	-	10.3	-	-	-	-	-	-	21.5	-	-	-	-	-	-	-	3.78	-	-	-
781	33.3	26.0	-	0.775	-	-	-	-	-	52.4	-	-	-	-	-	-	7.25	-	-	-	10.2	-	-	-	17.1	4.26	-	-
782	-	27.7	-	-	0.434	-	-	-	-	-	-	-	-	-	-	-	-	-	14.3	-	136	1.21	-	-	-	-	-	-
783	-	-	-	1.91	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92.9	-	-	-	-	27.1	-	-
784	-	-	-	-	-	-	14.7	-	-	-	-	-	-	-	-	-	-	7.50	-	-	-	-	-	-	-	-	-	-
785	-	-	-	-	-	-	33.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
786	-	-	-	-	-	-	-	35.1	-	-	-	-	-	-	-	-	-	6.29	-	-	-	-	-	22.6	-	-	-	-
787	-	-	-	-	-	-	86.7	-	-	-	-	-	-	-	-	-	-	28.3	-	-	-	-	-	-	-	-	-	-
788	-	-	-	-	-	-	31.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
789	-	-	-	-	-	-	14.8	-	-	-	-	-	-	-	-	-	-	6.12	-	-	-	-	-	-	-	-	-	-
790	-	-	-	-	-	-	59.3	-	-	-	-	-	-	-	-	-	-	14.2	-	-	-	-	-	-	-	-	-	-
791	-	-	-	-	-	-	20.2	-	-	-	-	-	-	-	-	-	-	4.19	-	-	-	-	-	-	-	-	-	-
792	-	-	-	-	-	-	59.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
793	-	-	-	-	0.0417	2.23	88.8	-	12.2	-	-	-	-	-	-	-	-	-	2.94	-	-	-	-	-	-	-	-	-
794	-	-	-	-	-	-	35.5	-	-	-	-	-	-	-	-	-	-	5.31	-	-	-	-	-	-	-	-	-	-
795	-	-	-	-	-	-	47.9	2.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
796	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.37	-	-	-	-
797	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.860	-	-	-	-	-	16.3	-	-	-	-
798	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.0	-	-	-	-	-	44.2	-	-	-	-
799	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.00	-	-	-	-	-	25.4	-	-	-	-
800	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.59	-	-	-	-	-	17.7	-	-	-	-
801	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.3	-	-	-	-
802	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.7	-	-	-	-
803	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.179	-	-	-	-	-	43.7	-	-	-	-
804	-	-	-	-	-	-	-	65.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
805	-	-	-	-	-	-	28.1	-	-	-	-	-	-	-	-	-	-	5.06	-	-	-	-	-	-	-	-	-	-
806	-	-	-	-	-	-	19.3	-	-	-	-	-	-	-	-	-	-	13.5	-	-	-	-	-	-	-	-	-	-
807	1.92	0.346	-	-	-	-	-	19.1	-	0.560	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
808	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.89	3.85	-	-	-	-	-	65.5	-	26.7	-	-
809	11.6	1.07	-	4.94	-	-	-	-	-	15.2	-	-	-	-	-	-	-	1.32	-	-	-	-	-	-	-	-	-	-
810	29.4	5.96	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.9	-	-	-	-	-	-	-	-	-	-
811	3.04	-	-	29.4	-	-	-	-	-	-	-	-	-	-	-	-	-	0.206	-	-	-	-	-	-	-	-	-	-
812	-	-	-	13.0	-	-	-	-	-	-	-	-	-	-	-	-	-	2.37	-	-	-	-	-	0.741	-	-	-	-
813	-	-	-	7.13	-	-	-	-	-	19.9	-	-	-	-	-	-	-	0.229	-	-	-	-	-	21.7	-	19.0	-	-
814	-	39.4	-	4.98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.09	-	-	-	-
815	-	32.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	57.0	38.1	-	-	-	-	-	-
816	-	-	-	5.64	-	-	-	0.0134	-	-	-	-	-	-	-	5.41	-	7.54	-	-	29.1	37.1	-	-	-	-	-	-
817	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52.5	0.159	-	-	-	-	0.238	2.48	-	-	-	-	-	-
818	-	-	3.13	-	-	-	-	-	-	-	3.87	-	-	-	26.5	-	1.65	-	-	-	12.5	40.4	-	-	-	-	-	-
819	1.58	17.3	-	9.49	-	-	-	22.4	-	5.94	-	-	-	-	-	-	0.199	27.0	-	-	80.1	36.3	-	-	-	-	-	-
820	20.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0269	-	-	45.2	-	-	-	-	-	-	-
821	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.9	21.6	-	-	254	86.7	-	-	-	-	-	-
822	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.3	-	-	-	0.0377	-	139	-	-	-	-
823	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	82.6	-	-	-	-	-	0.189	-	-	-	-
824	-	-	0.761	-	-	-	-	8.21	-	-	-	-	-	-	-	-	43.7	0.0023	-	-	64.4	67.0	-	-	-	-	-	-
825	-	-	-	-	-	-	-	4.68	-	-	-	-	-	-	-	-	0.908	32.9	-	-	9.31	9.26	-	-	-	-	-	-
826	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	125	47.4	-	-	-	-	-	-
827	-	8.01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0056	-	-	-	128	7.52	-	-	-	-	-	-
828	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	68.1	112	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
829	-	0.0000	-	-	-	-	-	-	-	19.1	-	-	-	-	-	-	-	-	5.03	-	39.8	24.6	-	-	-	-	-	-
830	-	-	-	-	-	-	-	-	-	50.7	-	2.99	-	-	-	-	-	-	-	-	94.8	63.8	-	0.118	-	-	-	-
831	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	72.4	-	-	-	-	-	-	-
832	-	16.7	0.177	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0072	-	-	50.6	23.1	-	-	-	-	-	-
833	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.00	51.6	-	-	-	-	-	-
834	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40.7	0.835	-	43.1	21.6	-	32.9	-	-	-	-
835	-	-	-	6.68	-	-	-	-	-	0.786	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
836	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.7	0.112	-	-	-	-	-	36.0	-	-	-	-
837	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.655	-	-	-	151	18.5	-	-	-	-	-	-
838	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.444	-	-	-	69.4	75.7	-	-	-	-	-	-
839	-	1.46	12.0	-	-	-	-	-	-	30.0	4.20	-	-	-	-	-	20.5	-	-	-	46.1	2.05	-	-	17.2	-	-	-
840	4.51	-	-	-	-	-	-	-	-	42.5	-	-	-	-	-	-	2.14	2.44	0.301	-	-	48.3	-	21.1	0.0000	-	-	-
841	-	-	7.76	-	-	-	-	-	-	7.09	-	-	-	-	-	-	17.9	-	-	-	-	0.0498	-	-	27.3	-	-	-
842	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.7	-	30.1	-	-
843	-	4.82	-	-	-	-	-	-	-	13.4	-	-	-	-	-	-	16.3	-	-	-	-	-	-	-	-	-	-	-
844	-	-	-	-	-	-	-	-	-	33.7	-	-	-	-	-	-	0.0001	-	-	-	0.752	31.3	-	-	8.81	-	-	-
845	-	-	-	-	-	-	-	-	-	7.97	-	-	-	-	-	-	-	-	-	-	-	18.1	-	-	-	-	-	-
846	-	-	-	-	-	-	-	-	-	35.5	-	-	-	-	-	-	-	-	0.232	-	-	35.0	-	-	-	-	-	-
847	-	-	-	-	-	-	-	5.87	-	-	-	-	-	-	-	-	-	11.3	-	-	-	-	-	82.4	-	-	-	-
848	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.4	-	-	-	-
849	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.15	-	-	-	-	-	48.0	-	-	-	-
850	-	0.0068	-	-	-	-	-	-	-	17.6	-	-	-	-	-	-	-	3.21	-	-	-	0.0043	7.76	59.7	-	-	-	-
851	-	0.0004	-	-	-	-	-	-	-	4.56	-	-	-	-	-	-	-	0.941	-	-	-	0.0014	3.09	38.3	-	-	-	-
852	-	19.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.39	-	-	-	0.0020	-	39.3	-	-	-	-
853	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0048	-	58.8	-	-	-	-
854	-	26.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0030	-	41.1	-	-	-	-
855	-	-	-	-	-	-	-	-	-	-	-	3.74	49.2	0.0009	-	-	-	0.0084	-	-	-	-	-	-	-	-	-	-
856	-	-	-	-	-	-	-	-	-	23.9	-	-	-	-	-	-	-	-	-	-	-	0.0045	-	45.1	-	-	-	-
857	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.6	-	-	-	0.0040	-	27.5	-	-	-	-
858	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0008	-	-	-	0.0833	-	33.4	-	-	-	-
859	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.14	-	-	0.0051	-	59.2	-	-	-	-
860	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.38	-	-	0.830	0.0700	-	95.3	-	-	-	-
861	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.6	0.572	-	0.135	0.0001	-	23.0	-	-	-	-
862	-	10.9	-	-	-	-	-	-	-	0.0434	-	-	-	-	2.26	-	-	24.8	-	-	61.4	18.9	-	-	-	-	-	-
863	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.195	8.32	-	-	99.2	14.7	-	-	-	-	-	-
864	-	-	-	-	-	-	-	62.7	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-
865	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.3	27.8	-	-	9.10	-	-	-	-	-	-	-
866	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.5	-	-	-	-	-	-	-
867	-	-	-	-	-	-	-	-	-	71.1	-	-	-	7.14	-	-	-	18.5	-	-	6.68	58.2	-	-	-	-	-	-
868	-	-	-	-	-	-	-	-	-	21.4	-	-	-	-	-	-	-	2.23	-	-	63.9	2.40	-	-	-	-	-	-
869	-	2.18	2.04	2.25	-	-	-	-	-	41.2	-	-	-	-	-	-	0.0056	16.6	-	-	27.5	56.1	-	-	-	-	-	-
870	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10.5	15.3	-	-	108	3.80	-	-	-	-	-	-
871	-	2.42	-	-	-	-	-	-	-	-	15.5	-	-	-	-	-	-	0.0173	-	-	-	-	-	-	-	-	-	-
872	-	0.0004	-	2.68	-	-	-	-	-	7.87	26.1	-	1.34	-	-	-	-	-	-	-	-	0.0001	26.3	-	-	-	-	-
873	-	-	-	-	-	-	-	-	-	9.27	-	-	3.95	-	-	-	-	-	-	-	-	0.0014	15.8	-	-	-	-	-
874	-	-	2.32	-	-	-	-	-	-	13.2	-	-	-	-	-	-	-	0.0017	-	-	-	0.0063	30.2	-	-	-	-	-
875	-	-	0.508	-	-	-	-	-	-	3.76	-	-	-	-	-	-	-	-	-	-	-	0.864	80.8	1.95	-	-	-	-
876	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0282	36.7	-	-	-	-	-
877	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0054	51.8	11.6	-	-	-	-
878	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0115	55.9	1.43	-	-	-	-
879	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0030	13.7	21.0	-	-	-	-
880	-	0.116	-	-	-	-	-	-	-	24.4	-	-	-	-	-	-	-	6.05	-	-	-	0.0005	-	18.5	-	-	-	-
881	-	0.0010	-	-	-	-	-	-	-	20.6	-	-	-	-	-	-	-	-	-	-	-	-	-	8.15	-	-	-	-
882	-	1.79	-	-	-	-	-	-	-	27.2	-	11.6	12.1	0.705	-	-	-	-	-	-	-	-	-	-	-	-	-	-
883	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0266	5.31	-	-	44.7	-	-	-	-	-	-	-
884	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.08	35.5	-	28.9	-	-	7.59	3.46	-	-	-	-	-	-
885	-	-	-	-	-	-	-	12.1	-	-	-	-	-	-	-	1.79	-	8.44	-	-	1.94	9.73	-	-	-	-	-	-
886	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.148	-	-	-	-	-	-	-	-	-	-	-	-
887	-	25.2	-	-	-	-	-	-	-	-	-	-	-	0.0002	-	-	-	-	-	-	-	-	-	-	-	-	-	-
888	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.9	65.7	-	-	-	-	0.0447	-	-	-	-	-	-	-
889	-	-	-	0.268	-	-	6.80	45.7	-	-	-	-	-	-	-	-	-	52.1	-	-	4.53	24.4	-	-	-	-	-	-
890	-	-	-	27.5	-	-	45.1	41.9	-	4.72	-	-	-	-	14.0	-	-	0.0172	-	-	9.81	-	-	-	-	-	-	-
891	-	3.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.4	-	-	-
892	-	15.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	48.0	-	-	-
893	-	3.20	-	-	-	-	-	67.8	-	-	-	-	-	-	-	-	-	-	-	-	0.0031	-	0.120	-	-	-	-	-
894	-	-	-	-	-	-	-	57.6	-	-	-	-	-	-	-	-	-	9.08	-	-	-	-	-	-	-	-	-	-
895	-	57.1	-	22.3	-	-	-	-	27.9	16.5	-	-	-	-	-	-	-	25.5	-	-	75.2	-	8.70	-	0.478	-	-	-
896	-	0.0351	-	1.99	-	-	-	78.0	-	-	-	-	-	-	-	-	-	8.04	-	-	8.58	-	-	-	-	-	-	-
897	-	-	-	-	-	-	-	0.279	-	-	-	-	-	-	-	-	-	8.29	-	-	61.5	103	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
898	-	63.4	-	2.75	-	-	-	5.94	-	-	-	-	-	-	-	-	1.94	0.163	-	-	-	-	-	-	-	-	-	-
899	-	0.178	-	10.0	-	-	-	-	-	-	-	-	-	-	-	-	-	3.55	-	-	41.3	-	-	-	-	-	-	-
900	-	-	-	-	-	-	33.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
901	-	16.5	-	4.76	-	-	-	-	-	-	-	-	-	-	-	-	-	16.2	-	-	-	-	-	-	56.5	-	-	-
902	0.0000	-	-	17.0	-	-	-	4.51	-	-	-	-	-	-	-	-	-	7.45	-	-	47.4	-	-	-	-	-	-	-
903	-	7.42	-	5.53	-	-	-	25.3	-	1.90	-	-	-	-	-	7.42	48.4	39.9	-	-	18.2	1.70	-	-	-	-	-	-
904	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	131	6.44	-	-	-	-	-	-
905	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.30	-	-	-	9.08	15.6	-	-	-	-	-	-
906	-	-	-	-	-	-	-	-	-	-	0.0590	-	-	-	-	-	6.61	-	-	-	2.20	44.0	-	-	-	-	-	-
907	-	30.6	-	13.5	-	-	-	-	-	5.96	5.88	-	-	-	23.6	-	-	-	-	-	46.5	49.6	-	-	-	-	-	-
908	-	151	-	-	-	-	-	-	-	-	-	-	-	-	68.1	-	-	-	-	-	-	-	-	3.49	-	-	-	-
909	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	80.5	-	2.79	-	0.551	-	-	-
910	0.0654	22.9	-	9.42	-	-	-	43.8	-	-	-	-	-	-	-	-	-	11.8	-	-	16.2	-	-	-	-	-	-	-
911	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.6	-	-	-	-	-	-
912	-	-	-	-	-	-	-	-	-	0.656	-	-	-	-	-	-	-	22.1	-	-	-	56.0	38.0	-	-	-	-	-
913	-	0.0110	-	1.60	-	-	-	-	-	14.0	-	-	-	-	-	-	-	0.358	-	-	12.5	7.16	167	-	-	-	-	-
914	4.03	-	1.44	11.1	-	-	-	-	-	27.5	-	-	-	2.86	-	-	-	-	-	-	-	1.08	2.10	80.2	-	14.9	-	-
915	-	-	-	44.1	-	-	-	-	-	2.55	-	-	-	2.75	-	-	-	-	-	-	-	38.2	-	7.79	-	-	-	-
916	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.9	-	-	-	-	-	-
917	-	-	-	32.4	-	-	-	-	-	-	0.0172	-	-	-	-	-	-	9.16	-	-	-	109	-	0.0033	-	-	-	-
918	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.428	-	-	-	54.5	-	-	-
919	-	6.39	1.41	2.22	-	-	-	-	-	0.768	-	-	-	-	2.54	-	-	-	-	-	28.9	91.4	-	-	-	-	-	-
920	-	-	0.970	-	-	-	-	-	-	2.60	4.09	-	-	-	-	-	2.69	-	-	-	1.19	101	-	-	-	-	-	-
921	0.779	4.09	-	-	-	-	-	-	-	1.12	-	-	-	-	-	-	2.25	-	-	-	-	61.9	-	-	-	-	-	-
922	2.92	17.4	-	1.27	-	-	-	-	-	11.0	-	-	-	-	-	-	12.0	5.05	-	-	-	74.3	0.993	-	-	-	-	-
923	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-	-	-	124	12.5	-	-	-	-	-
924	-	-	-	-	-	-	-	-	-	4.85	-	-	-	-	-	-	-	-	-	-	-	0.132	34.3	6.16	-	-	-	-
925	-	-	0.0001	-	-	-	-	-	-	28.7	-	-	-	-	-	-	16.3	-	-	-	-	84.3	4.07	0.621	-	-	-	-
926	2.08	10.3	2.60	13.6	-	-	-	-	-	6.37	-	-	-	-	-	-	-	-	-	-	-	59.9	2.50	-	-	-	-	-
927	-	0.0002	-	-	-	-	-	-	-	1.29	-	-	-	-	-	-	0.446	-	-	-	-	67.9	-	-	-	-	-	-
928	-	15.3	-	-	-	10.6	-	9.80	0.0000	-	-	-	6.75	-	-	-	-	1.82	-	-	0.0001	15.7	0.990	-	-	-	-	-
929	-	-	-	-	-	-	-	0.0000	0.236	-	-	-	-	-	-	-	-	-	-	-	0.0001	6.81	50.3	-	-	-	-	-
930	-	-	5.45	-	-	-	-	-	0.0041	3.67	0.0002	-	2.82	-	-	-	-	-	-	-	-	0.475	29.5	-	-	-	-	-
931	-	-	0.0003	-	-	28.2	-	2.70	0.0944	-	2.43	-	-	-	-	-	-	-	-	-	-	0.0935	2.49	7.38	-	-	-	-
932	-	-	-	-	-	-	-	-	-	8.13	-	-	-	-	-	-	-	-	-	-	-	5.50	0.979	-	-	-	-	-
933	3.84	4.98	-	-	-	-	-	-	-	8.01	-	-	-	-	-	-	8.11	-	-	-	-	43.4	-	-	-	-	-	-
934	-	23.2	-	-	-	-	-	-	-	2.58	-	-	-	-	2.93	-	-	-	-	-	-	-	-	-	-	-	-	-
935	-	-	-	-	-	-	-	-	-	14.9	-	-	-	-	-	-	-	2.16	-	-	-	16.7	-	2.95	-	-	-	-
936	-	36.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
937	-	9.81	-	1.88	-	-	-	-	20.5	-	-	-	-	-	-	-	-	4.48	-	-	-	-	-	-	-	-	-	-
938	-	-	-	-	-	-	-	-	-	5.00	-	-	-	0.136	-	47.7	-	-	-	-	-	1.12	2.65	-	-	-	-	-
939	-	-	-	-	-	-	-	-	-	-	0.0006	-	11.9	0.0003	23.7	-	-	-	-	-	-	-	-	-	-	-	-	-
940	-	-	-	-	-	-	-	-	-	1.19	-	-	-	-	-	-	-	-	-	-	-	14.1	-	-	-	-	-	-
941	-	-	-	-	-	-	-	56.2	-	-	-	-	-	0.0002	-	-	-	6.71	-	-	-	-	0.0023	-	-	-	-	-
942	-	13.7	-	-	-	16.8	-	0.0839	4.10	-	-	-	-	-	-	-	-	2.73	-	-	-	-	-	-	-	-	-	-
943	-	0.264	-	1.05	-	1.68	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0006	9.36	-	-	-	-	-
944	-	-	-	-	-	53.1	-	4.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
945	-	-	-	-	-	-	-	17.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
946	-	-	-	-	-	-	-	6.57	0.0022	2.01	0.0001	-	2.54	-	-	-	-	-	-	-	-	0.0006	8.26	-	-	-	-	-
947	-	-	-	-	-	-	-	33.0	-	-	-	-	-	-	-	-	-	6.05	-	-	-	-	0.0021	-	-	-	-	-
948	-	-	-	-	-	-	-	0.0326	-	-	-	-	-	-	-	-	-	-	-	-	-	0.865	34.0	4.99	-	-	-	-
949	-	0.0000	-	4.02	-	-	-	-	-	5.93	4.48	-	-	-	-	-	-	2.57	-	-	-	0.0122	68.9	5.66	-	-	-	-
950	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.8	-	-	-	-	-	-	-	-	-	-	-	-	-
951	-	44.3	1.43	-	-	-	-	-	-	66.2	-	-	-	-	-	-	-	29.8	-	-	62.7	68.3	-	-	-	-	-	-
952	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0031	4.62	12.2	-	-	-	-	-	-	-	-	-	-	-	-
953	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	38.1	1.71	-	-	-	-	-	-	-	-	-	-	-	-
954	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0004	-	36.7	-	-	-	-	-	-	-	-	-	-	-	-
955	-	-	0.548	-	-	-	-	2.99	0.0004	13.2	-	-	-	-	-	-	-	-	-	-	-	0.0027	17.9	7.47	-	-	-	-
956	-	-	-	-	-	-	-	2.69	-	-	-	-	6.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
957	-	-	-	-	-	-	-	-	-	0.348	14.0	-	4.57	-	-	-	-	2.44	-	-	-	0.0020	69.3	0.873	-	-	-	-
958	-	-	-	-	-	-	-	5.77	-	-	-	-	-	0.443	-	26.2	-	-	-	-	-	-	-	-	-	-	-	-
959	-	-	-	-	-	-	-	0.161	-	-	-	-	-	0.0523	-	14.2	-	-	-	-	-	-	-	-	-	-	-	-
960	-	-	0.0160	-	-	-	-	-	-	9.04	0.0001	-	3.09	0.0005	-	9.98	-	-	-	-	-	-	-	0.791	-	-	-	-
961	-	0.164	-	-	-	-	-	-	-	-	-	-	-	0.0801	0.606	6.20	-	-	-	-	-	-	-	-	-	-	-	-
962	-	-	6.53	-	-	-	-	-	-	2.79	0.187	-	20.6	-	-	-	-	-	-	-	-	0.0440	6.86	-	-	-	-	-
963	-	0.0006	-	-	-	-	-	-	-	15.6	-	-	-	-	-	-	-	0.0145	-	-	-	0.0545	47.4	36.9	-	-	-	-
964	-	-	-	-	-	-	-	19.9	0.0000	-	-	-	-	-	-	-	-	7.16	-	-	-	0.0000	0.0056	-	-	-	-	-
965	-	-	-	-	-	0.168	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.157	32.0	-	-	-	-	-
966	5.56	7.27	-	0.289	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
967	-	20.7	-	0.939	-	11.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0002	3.11	-	-	-	-	-
968	-	-	-	-	-	36.1	-	61.1	0.0006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
969	-	17.6	-	-	-	46.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
970	-	2.62	-	-	-	-	-	-	0.0000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
971	-	0.266	-	-	-	-	-	-	-	18.2	-	-	-	-	-	-	-	-	-	-	-	0.0101	11.1	-	-	-	-	-
972	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.21	-	-	0.721	21.2	-	-	-	-	-	-
973	-	-	-	3.43	-	-	-	-	-	-	8.78	-	-	-	-	-	-	-	-	-	-	74.6	18.8	-	-	-	-	-
974	-	1.78	-	-	-	-	-	-	-	2.66	-	-	-	-	-	-	-	-	-	-	-	115	5.02	-	-	-	-	-
975	-	24.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
976	4.73	27.3	-	0.140	-	-	-	-	-	3.94	-	-	-	-	-	-	0.813	0.0306	-	-	-	9.65	-	-	-	-	-	-
977	-	0.0446	0.170	0.390	-	-	-	-	-	16.4	-	-	-	-	-	-	9.56	-	-	-	-	79.6	43.3	-	-	-	-	-
978	-	0.0000	-	-	-	-	-	-	-	3.22	-	-	-	-	-	-	7.51	-	-	-	-	78.1	9.97	-	-	-	-	-
979	-	-	0.781	30.5	-	-	-	-	-	0.0005	5.45	-	-	-	7.04	-	-	-	-	-	-	10.4	1.27	-	-	-	-	-
980	-	0.0000	-	-	-	-	-	-	-	1.16	-	-	-	-	-	-	2.18	-	-	-	0.0002	102	-	-	-	-	-	-
981	-	0.0002	-	-	-	-	-	-	-	2.69	-	-	-	-	-	-	0.0006	-	-	-	-	33.7	-	-	-	-	-	-
982	-	-	-	2.34	-	-	-	-	-	3.47	-	-	-	-	-	-	10.9	-	-	-	-	88.1	-	-	-	-	-	-
983	16.2	0.0001	-	0.230	-	-	-	-	-	12.8	4.35	-	-	-	-	-	10.4	-	-	-	-	28.6	3.57	0.589	-	-	-	-
984	-	35.1	-	32.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
985	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.8	-	-	-	-	-	-
986	-	-	-	-	-	-	-	-	-	3.70	-	-	-	-	-	-	-	-	-	-	-	51.8	-	-	-	-	-	-
987	-	4.37	-	0.473	-	-	-	-	-	9.61	-	-	-	-	-	-	0.0002	5.17	-	-	-	0.0880	135	-	-	-	-	-
988	0.318	-	-	-	-	-	-	-	-	9.71	-	-	-	-	-	-	6.12	-	-	-	-	53.5	12.6	-	-	-	-	-
989	-	-	-	-	-	-	-	-	-	90.8	-	-	-	-	-	-	22.5	-	-	-	-	41.0	10.0	-	-	-	-	-
990	-	-	-	-	-	-	-	-	-	5.62	-	15.0	2.18	14.1	-	-	-	1.35	-	-	-	0.636	-	76.1	-	-	-	-
991	-	-	-	-	-	-	-	-	-	2.78	-	-	-	-	-	-	-	-	21.3	-	15.1	9.61	-	-	-	-	-	-
992	-	1.22	3.47	-	0.814	-	-	-	-	11.9	-	-	-	-	-	-	-	-	0.284	-	0.269	0.0024	-	32.9	-	-	-	-
993	-	-	-	-	-	-	-	-	-	0.985	-	14.5	29.1	24.0	-	-	-	0.499	-	-	-	1.25	-	-	-	-	-	-
994	-	-	-	-	-	-	-	4.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
995	-	-	-	-	-	-	71.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
996	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.41	-	-	-
997	-	-	0.0002	13.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58.9	-	-	-	-	5.99	-	-
998	-	1.47	0.0001	-	-	-	-	-	-	-	-	-	-	-	-	-	0.653	-	-	-	-	-	-	-	15.3	22.1	-	-
999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.04	-	-	-	-	-	19.6	-	-	-	-
1000	-	-	-	-	-	-	-	28.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1001	-	-	-	-	-	-	-	57.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1002	-	-	-	-	-	-	45.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1003	-	-	-	-	-	-	23.0	-	-	-	-	-	-	-	-	-	-	0.795	-	-	-	-	-	-	-	-	-	-
1004	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.57	-	-	-	-	-	-	-	-	-	-
1005	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.06	-	-	-	-
1006	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.37	0.592	-	-	-	-	5.56	-	-	-	-
1007	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0239	16.7	-	-	-	-	-	-
1008	-	11.7	-	-	-	-	-	-	-	-	-	-	-	-	77.8	-	-	-	-	-	-	-	-	-	-	-	-	-
1009	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	109	-	-	-	-	-	-	-
1010	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34.1	-	-	-	-	-	-	-
1011	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.7	-	-	-	-	-	-	-
1012	-	-	-	-	-	-	-	-	-	10.6	-	-	-	-	-	-	-	7.82	-	-	-	1.07	-	-	-	-	-	-
1013	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.73	-	-	-	-	-
1014	-	2.39	-	-	-	-	-	-	-	-	-	-	3.44	0.0064	-	12.6	-	0.0312	-	-	-	0.694	-	-	-	-	-	-
1015	-	5.14	-	-	-	-	-	-	-	9.94	-	-	-	-	-	-	7.24	-	-	-	-	88.2	23.1	-	-	-	-	-
1016	14.6	24.4	-	0.248	-	-	-	-	-	18.1	-	-	-	-	-	-	1.91	-	-	-	-	13.3	0.512	2.96	-	-	-	-
1017	-	11.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1018	-	-	-	-	-	-	-	-	-	-	-	-	5.22	-	4.73	-	-	-	-	-	-	-	-	-	-	-	-	-
1019	-	-	-	-	-	-	-	11.6	55.4	-	-	-	-	-	13.2	-	-	0.190	-	-	-	-	-	-	-	-	-	-
1020	-	2.79	-	-	-	-	-	1.50	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0000	2.05	-	-	-	-	-
1021	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1022	1.25	3.38	-	-	-	-	-	-	-	4.74	-	-	-	-	-	-	-	4.79	-	-	-	3.77	-	-	-	-	-	-
1023	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.68	-	-	-	-	-	119	-	-	-	-
1024	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.77	-	-	-	-	-	57.4	-	-	-	-
1025	-	-	-	-	-	-	-	11.7	-	-	-	-	-	-	-	-	-	-	0.191	-	-	-	-	-	-	-	-	-
1026	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.1	-	-	-	-	-	15.5	-	-	-	-
1027	-	6.56	-	-	-	-	-	-	-	-	-	-	-	-	-	-	11.3	7.55	-	-	-	-	-	84.2	-	-	-	-
1028	-	1.04	-	2.43	-	-	-	-	-	-	-	-	-	-	-	-	-	21.8	-	-	-	-	-	0.444	-	-	-	-
1029	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	48.5	-	0.116	-	-	10.8	-	-	-	-
1030	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.889	20.4	-	0.214	-	-	7.01	-	-	-	-
1031	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	36.7	-	-	-	-	-	45.8	-	-	-	-
1032	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.6	-	-	-	-	-	16.6	-	-	-	-
1033	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.7	-	-	-	-	-	45.5	-	-	-	-
1034	-	-	-	-	-	-	-	-	0.0002	0.0058	-	-	-	-	-	-	-	-	-	-	5.41	28.6	-	-	-	12.5	-	-
1035	-	20.8	-	-	-	-	-	26.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0001	-	-

Table D-3. Detailed Land Use and Development Condition Data - Buildout

Land Use Polygon ID	Net Acreage by Land Use Category, acres																											
	CC	CG	CN	CO	FF	IA	IH	IL	IMU	MFR1	MFR2	MFR3	MFR4	MUC1	MUC2	MUC3	PF	POS	RRFU	SFR1	SFR2	SFR3	SFR4	SFR5	SFR6	SFR7	SFR8	SFR9
1036	-	19.7	-	-	-	-	21.9	10.9	0.0744	-	-	-	-	-	-	-	-	-	-	-	-	-	0.150	-	-	-	-	-
1037	-	-	7.72	-	-	-	-	-	-	5.72	-	-	-	-	-	-	1.71	-	-	-	2.02	1.89	-	-	24.7	-	-	-
1038	-	-	-	-	-	-	-	32.5	-	-	-	-	-	-	-	-	-	8.89	-	-	-	-	-	-	-	-	-	-
1039	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.6	-	-	-	103	0.801	-	-	-	-	-	-
1040	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1041	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.38	-	-	-	-	-	-	-
1042	-	-	-	-	0.0043	-	-	-	-	17.2	-	-	-	-	-	-	-	-	0.0241	-	40.8	-	-	-	-	-	-	-
1043	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	18.1	-	-	-	-	-	-	-
1044	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.2	13.8	-	-	-	-	-	-
1045	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92.0	-	-	-	-	-	-	-
1046	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69.7	-	-	-	-	-	-	-	-	-
1047	-	-	-	-	0.0457	-	-	-	-	-	-	-	-	-	-	-	-	-	68.4	-	-	-	-	-	-	-	-	-
1048	-	-	-	-	0.0019	-	-	-	-	-	-	-	-	-	-	-	-	-	0.141	-	62.1	-	-	-	-	-	-	-
1049	-	-	-	-	0.0354	-	-	-	-	-	-	-	-	-	-	-	-	-	24.0	-	-	-	-	-	-	-	-	-
1050	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	43.9	12.6	-	-	-	-	-	-
1051	-	-	-	-	0.0047	-	-	-	-	-	-	-	-	-	-	-	-	-	36.1	-	-	-	-	-	-	-	-	-
1052	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69.1	0.414	70.4	-	36.1	-	-	-	-	-	-
1053	-	-	-	-	0.0093	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76.9	-	-	-	-	-	-	-	-
1054	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1055	-	0.0002	-	-	-	-	-	-	165	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1056	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.9	-	-	0.0031	-	-	22.2	-	-	-	-
9999	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.4	-	-	-	-	-	90.0	-	-	-	-

APPENDIX E

Aggregate Unit Wastewater Flow Rate by Service Area (electronic file only)

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
1	2.49	48.8	25.9	0.0389	-	-	7.04	-	33.0	0.0389	1,181
2	2.49	89.8	44.5	0.154	-	-	22.6	0.0536	67.1	0.207	3,090
3	1.00	9.9	-	-	-	-	-	-	-	-	-
4	2.49	35.6	-	0.0008	-	-	21.0	-	21.0	0.0008	37.7
5	1.00	121.7	-	-	-	-	-	-	-	-	-
6	0.52	218.9	25.5	0.0265	-	-	46.6	0.0263	72.1	0.0528	732
7	0.52	132.3	73.1	0.0359	-	-	33.4	0.0184	106	0.0543	510
8	0.52	114.9	15.5	0.0022	-	-	-	-	15.5	0.0022	143
9	1.00	149.4	-	0.0000	-	-	31.7	-	31.7	0.0000	1.49
10	1.00	264.3	-	0.0002	-	-	24.1	-	24.1	0.0002	10.3
11	2.49	82.1	0.0000	0.0004	-	-	9.66	-	9.66	0.0004	37.7
12	2.49	127.1	4.56	0.0033	-	-	16.0	0.0546	20.5	0.0579	2,824
13	2.49	198.3	2.25	0.0034	-	-	48.7	-	51.0	0.0034	66.5
14	0.52	91.1	0.338	0.0004	-	-	4.87	0.0043	5.21	0.0046	891
15	1.03	98.3	-	-	-	-	57.8	0.0977	57.8	0.0977	1,690
16	0.89	133.1	45.7	0.0415	-	-	13.2	0.0129	58.9	0.0544	924
17	0.53	136.2	41.8	0.0251	-	-	85.2	0.0495	127	0.0747	588
18	1.03	53.1	-	-	-	-	12.2	0.0276	12.2	0.0276	2,267
19	0.89	137.1	6.91	0.0124	-	-	17.3	-	24.2	0.0124	511
20	1.00	153.4	-	-	-	-	-	-	-	-	-
21	1.55	36.2	-	-	-	-	5.75	0.0102	5.75	0.0102	1,769
22	2.49	59.6	-	0.0018	-	-	47.1	-	47.1	0.0018	37.7
23	2.49	76.8	-	0.0015	-	-	39.4	-	39.4	0.0015	37.7
24	0.49	91.0	-	-	-	-	1.92	0.0010	1.92	0.0010	537
25	1.00	109.5	-	-	-	-	5.25	-	5.25	-	-
26	0.49	70.2	-	-	-	-	2.75	0.0000	2.75	0.0000	4.89
27	1.00	74.2	-	-	-	-	-	-	-	-	-
28	0.49	114.6	-	0.0000	-	-	1.87	-	1.87	0.0000	0.634
29	0.49	83.2	-	0.0000	-	-	6.36	-	6.36	0.0000	7.42
30	0.49	218.9	-	0.0000	-	-	1.76	-	1.76	0.0000	7.42
31	0.49	140.7	-	0.0001	-	-	9.45	-	9.45	0.0001	6.12
32	0.49	66.4	-	0.0000	-	-	3.66	-	3.66	0.0000	7.42
33	0.49	117.4	-	0.0001	-	-	6.78	-	6.78	0.0001	7.42
34	0.49	65.3	-	0.0000	-	-	9.15	-	9.15	0.0000	0.0000
35	1.00	349.0	-	-	-	-	6.19	0.0068	6.19	0.0068	1,098
36	1.00	150.5	-	-	-	-	1.51	0.0017	1.51	0.0017	1,098
37	1.61	447.0	-	-	-	-	429	0.743	429	0.743	1,731
38	1.46	111.9	-	-	-	-	24.7	0.0436	24.7	0.0436	1,769
39	1.00	158.6	-	-	-	-	34.6	0.0379	34.6	0.0379	1,098
40	1.00	42.2	-	-	-	-	0.901	0.0010	0.901	0.0010	1,098
41	0.54	76.2	-	-	-	-	36.4	0.0183	36.4	0.0183	503
42	2.05	286.5	64.3	0.0365	-	-	0.297	0.0007	64.6	0.0372	575
43	1.00	164.1	-	-	-	-	-	-	-	-	-
44	1.00	58.5	-	0.0000	-	-	19.2	0.0211	19.2	0.0211	1,097
45	1.00	274.8	-	0.0000	-	-	46.8	0.0514	46.8	0.0514	1,100
46	1.00	55.2	-	0.0000	-	-	2.20	-	2.20	0.0000	15.2
47	0.54	88.3	-	-	-	-	4.77	0.0029	4.77	0.0029	597
48	1.00	324.3	244	0.0729	-	-	0.0353	-	244	0.0729	298
49	1.00	143.4	45.7	0.0127	-	-	9.82	0.0094	55.5	0.0220	397
50	0.54	195.8	10.1	0.0073	-	-	114	0.0682	124	0.0756	608
51	1.00	56.0	2.82	0.0008	-	-	41.9	0.0084	44.7	0.0091	204
52	0.49	83.7	-	-	-	-	49.2	0.0242	49.2	0.0242	493
53	0.49	117.4	-	-	-	-	25.2	0.0135	25.2	0.0135	537
54	0.49	199.3	0.686	0.0001	-	-	199	0.0015	199	0.0016	7.97
55	2.49	180.0	-	0.0010	-	-	29.0	0.0033	29.0	0.0043	149
56	0.00	160.9	-	0.0001	-	-	115	0.311	115	0.311	2,692
57	1.00	197.7	17.2	0.0350	1.20	0.0017	55.5	0.0179	73.9	0.0546	739
58	0.54	46.1	13.5	0.0145	-	-	0.0065	0.0000	13.5	0.0145	1,073
59	1.00	145.6	-	0.0001	-	-	9.02	0.0000	9.02	0.0001	15.2
60	1.00	137.4	3.38	0.0015	-	-	24.8	-	28.2	0.0015	52.8
61	1.00	38.1	-	-	-	-	5.84	0.0064	5.84	0.0064	1,098
62	1.00	141.0	-	-	-	-	28.4	0.0311	28.4	0.0311	1,098
63	1.00	45.1	-	-	-	-	9.04	0.0099	9.04	0.0099	1,098
64	0.54	107.6	-	-	-	-	5.13	0.0031	5.13	0.0031	597
65	0.54	118.3	-	0.0000	-	-	23.3	0.0139	23.3	0.0139	597
66	1.00	178.2	139	0.0449	-	-	1.00	0.0011	140	0.0460	328
67	1.00	117.6	73.6	0.0284	-	-	-	-	73.6	0.0284	385
68	1.06	64.1	44.1	0.0130	-	-	-	-	44.1	0.0130	294
69	0.84	84.7	-	-	-	-	33.3	0.0366	33.3	0.0366	1,098
70	1.00	63.6	-	-	8.98	0.0230	-	-	8.98	0.0230	2,563
71	1.00	107.3	30.7	0.0085	-	-	3.59	-	34.3	0.0085	248
72	1.00	168.0	2.36	0.0007	-	-	8.03	0.0088	10.4	0.0095	913
73	1.24	65.4	50.3	0.0734	-	-	0.0004	0.0000	50.3	0.0734	1,458
74	1.00	37.0	6.80	0.0019	-	-	-	-	6.80	0.0019	277
75	1.00	58.4	-	0.0000	-	-	12.8	-	12.8	0.0000	2.15
76	1.00	72.2	-	0.0001	-	-	8.49	-	8.49	0.0001	15.2
77	1.00	65.7	0.0553	0.0003	-	-	18.3	-	18.3	0.0003	16.0
78	1.00	40.2	0.0396	0.0001	-	-	8.46	-	8.50	0.0001	16.9
79	0.54	220.3	10.9	0.0119	-	-	6.80	0.0041	17.7	0.0160	903
80	1.00	67.0	0.0847	0.0002	-	-	-	-	0.0847	0.0002	2,013
81	1.00	61.7	16.5	0.0331	-	-	2.37	0.0026	18.8	0.0358	1,898
82	1.00	40.0	-	-	7.03	0.0181	0.330	-	7.36	0.0181	2,453
83	1.00	96.3	-	-	-	-	9.18	0.0098	9.18	0.0098	1,068
84	1.00	145.7	22.7	0.0204	17.8	0.0457	3.84	-	44.3	0.0661	1,493
85	1.00	77.0	-	-	-	-	41.4	0.0454	41.4	0.0454	1,098
86	0.54	63.1	-	-	-	-	2.89	0.0017	2.89	0.0017	597
87	1.00	102.2	-	0.0003	-	-	21.2	-	21.2	0.0003	15.2
88	1.00	56.7	-	-	-	-	-	-	-	-	-
89	1.00	143.0	-	0.0001	-	-	9.66	-	9.66	0.0001	15.2
90	1.00	212.0	-	0.0005	-	-	31.0	-	31.0	0.0005	15.2
91	1.00	172.6	-	0.0000	-	-	0.0283	-	0.0283	0.0000	14.2
92	1.00	230.1	0.0000	0.0002	-	-	13.3	-	13.3	0.0002	15.2
93	0.54	222.4	30.9	0.0066	-	-	0.625	-	31.5	0.0066	208
94	1.00	198.6	-	0.0001	-	-	6.36	-	6.36	0.0001	15.2
95	1.00	236.9	-	-	-	-	-	-	-	-	-
96	1.00	175.1	-	-	-	-	-	-	-	-	-
97	1.00	276.6	-	0.0004	-	-	29.7	-	29.7	0.0004	15.1
98	2.49	141.5	-	0.0005	-	-	14.4	-	14.4	0.0005	37.7
99	1.00	171.2	-	-	-	-	3.06	0.0034	3.06	0.0034	1,098
100	1.00	319.5	-	0.0001	-	-	8.69	0.0002	8.69	0.0004	40.5
101	1.00	66.2	-	-	-	-	0.997	-	0.997	-	-
102	1.00	573.0	-	-	-	-	286	-	286	-	-
103	1.00	214.2	-	-	-	-	66.0	-	66.0	-	-

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
104	1.00	134.6	-	-	-	-	-	-	-	-	-
105	1.00	307.0	-	0.0005	-	-	234	-	234	0.0005	2.02
106	1.00	172.2	-	-	24.8	0.0636	0.0909	-	24.9	0.0636	2,558
107	1.00	95.6	3.48	0.0010	-	-	55.5	0.0608	58.9	0.0618	1,049
108	1.00	66.1	4.98	0.0014	-	-	1.34	-	6.32	0.0014	218
109	1.00	155.1	17.7	0.0145	-	-	91.1	0.100	109	0.115	1,054
110	1.00	218.5	6.93	0.0088	-	-	39.7	0.0001	46.6	0.0089	191
111	1.00	73.4	18.2	0.0300	-	-	14.2	0.0095	32.4	0.0394	1,217
112	1.00	139.0	0.618	0.0002	-	-	-	-	0.618	0.0002	277
113	1.00	158.8	59.1	0.0258	-	-	12.8	-	71.9	0.0258	358
114	1.00	112.9	14.5	0.0040	-	-	-	-	14.5	0.0040	277
115	1.00	145.3	4.57	0.0013	-	-	0.946	-	5.51	0.0013	230
116	1.00	52.3	14.5	0.0293	-	-	21.5	0.0169	36.0	0.0462	1,282
117	1.00	75.9	15.4	0.0043	-	-	13.0	-	28.4	0.0043	150
118	1.00	180.0	33.1	0.0317	-	-	8.16	-	41.3	0.0317	768
119	1.00	122.2	73.2	0.0331	-	-	49.0	0.0539	122	0.0870	712
120	1.00	54.1	14.6	0.0040	-	-	0.171	-	14.7	0.0040	274
121	1.00	150.8	31.0	0.0397	-	-	-	-	31.0	0.0397	1,279
122	1.00	53.9	15.0	0.0113	-	-	18.7	0.0205	33.7	0.0318	945
123	1.00	35.0	24.9	0.0069	-	-	5.57	-	30.5	0.0069	226
124	1.00	99.1	30.9	0.0086	-	-	0.796	-	31.7	0.0086	270
125	1.00	93.1	13.1	0.0036	-	-	1.85	-	14.9	0.0036	243
126	1.00	191.2	17.3	0.0048	-	-	0.0048	-	17.3	0.0048	277
127	1.00	36.2	31.3	0.0087	-	-	0.0835	-	31.4	0.0087	276
128	1.00	43.1	23.3	0.0280	-	-	13.8	0.0152	37.1	0.0432	1,164
129	1.00	57.0	23.7	0.0066	-	-	10.4	0.0114	34.1	0.0180	527
130	1.00	106.3	20.5	0.0095	-	-	-	-	20.5	0.0095	462
131	1.00	78.7	-	-	17.2	0.0440	6.32	0.0059	23.5	0.0499	2,125
132	1.00	71.4	35.7	0.0168	9.49	0.0244	1.92	-	47.1	0.0412	873
133	1.00	72.7	14.1	0.0117	39.0	0.100	1.62	-	54.8	0.112	2,043
134	1.00	101.6	11.9	0.0033	-	-	0.997	-	12.9	0.0033	256
135	1.00	123.5	16.2	0.0045	-	-	1.12	-	17.4	0.0045	259
136	1.00	84.7	33.2	0.0092	-	-	-	-	33.2	0.0092	277
137	1.00	43.8	27.7	0.0130	-	-	-	-	27.7	0.0130	472
138	1.00	51.7	18.2	0.0050	-	-	2.51	-	20.7	0.0050	244
139	1.00	179.7	95.8	0.0639	25.2	0.0645	6.23	0.0011	127	0.129	1,018
140	1.00	114.1	14.7	0.0081	-	-	-	-	14.7	0.0081	554
141	1.00	65.8	3.52	0.0010	-	-	9.63	0.0106	13.1	0.0116	880
142	1.00	111.5	33.7	0.0093	-	-	-	-	33.7	0.0093	277
143	1.00	135.3	67.0	0.0320	5.63	0.0084	-	-	72.6	0.0403	555
144	1.00	125.5	15.6	0.0160	87.5	0.225	17.7	0.0195	121	0.260	2,153
145	1.00	96.9	26.5	0.0108	1.85	0.0026	0.390	-	28.7	0.0134	465
146	1.00	97.4	10.9	0.0030	0.193	0.0005	1.50	-	12.6	0.0035	279
147	1.00	160.2	19.2	0.0274	5.45	0.0076	10.1	0.0062	34.8	0.0412	1,184
148	1.00	60.5	1.20	0.0003	2.32	0.0059	1.84	-	5.36	0.0063	1,171
149	1.00	60.0	7.64	0.0089	8.60	0.0221	1.45	-	17.7	0.0310	1,753
150	1.00	132.0	13.3	0.0143	-	-	18.1	0.0199	31.4	0.0342	1,088
151	1.00	106.9	28.0	0.0371	-	-	20.5	0.0226	48.5	0.0597	1,229
152	1.00	152.9	21.1	0.0058	-	-	4.95	0.0054	26.0	0.0113	434
153	1.00	86.7	4.13	0.0011	-	-	-	-	4.13	0.0011	277
154	1.00	110.5	9.14	0.0025	-	-	-	-	9.14	0.0025	277
155	1.00	135.7	35.5	0.0098	-	-	-	-	35.5	0.0098	277
156	1.00	158.6	22.6	0.0063	-	-	-	-	22.6	0.0063	277
157	1.00	117.6	8.07	0.0047	7.11	0.0183	-	-	15.2	0.0229	1,511
158	1.00	114.9	53.8	0.127	0.503	0.0007	3.59	0.0039	57.9	0.132	2,281
159	1.00	149.4	126	0.0359	-	-	4.09	0.0045	130	0.0404	311
160	1.00	264.3	203	0.0658	-	-	11.2	0.0124	214	0.0782	365
161	1.00	146.9	32.3	0.0090	-	-	-	-	32.3	0.0090	277
162	1.00	209.5	86.7	0.0423	-	-	2.86	-	89.6	0.0423	472
163	1.00	194.2	182	0.122	2.29	0.0032	3.12	-	187	0.125	670
164	1.00	91.1	86.3	0.0337	-	-	-	-	86.3	0.0337	391
165	1.00	107.7	63.8	0.0251	-	-	-	-	63.8	0.0251	394
166	0.54	133.1	90.0	0.0236	-	-	33.7	0.0201	124	0.0438	354
167	0.54	109.2	-	-	-	-	0.0004	0.0000	0.0004	0.0000	597
168	0.54	155.1	-	-	-	-	31.9	0.0190	31.9	0.0190	597
169	0.54	137.1	112	0.108	-	-	9.73	0.0058	122	0.114	932
170	0.54	153.4	-	-	-	-	153	0.0916	153	0.0916	597
171	1.06	114.5	27.7	0.0086	-	-	-	-	27.7	0.0086	311
172	1.06	111.0	35.0	0.0124	-	-	-	-	35.0	0.0124	354
173	1.06	85.3	75.9	0.0364	-	-	-	-	75.9	0.0364	479
174	1.00	93.3	76.0	0.0330	-	-	-	-	76.0	0.0330	435
175	1.00	230.6	100	0.0386	-	-	8.95	0.0098	109	0.0485	445
176	1.00	135.2	24.7	0.0097	-	-	-	-	24.7	0.0097	391
177	1.00	261.5	12.6	0.0049	-	-	2.27	0.0025	14.9	0.0074	499
178	1.00	115.1	80.0	0.0862	-	-	21.8	0.0240	102	0.110	1,082
179	1.06	142.7	60.2	0.0183	-	-	-	-	60.2	0.0183	305
180	1.00	102.1	42.7	0.0255	-	-	3.88	0.0043	46.6	0.0297	638
181	0.68	195.2	53.4	0.0665	-	-	86.5	0.0645	140	0.131	937
182	0.68	284.0	-	-	-	-	24.9	0.0185	24.9	0.0185	746
183	0.68	268.5	0.0000	0.0000	-	-	22.7	0.0169	22.7	0.0169	746
184	1.00	238.0	22.8	0.0308	-	-	0.196	0.0002	23.0	0.0310	1,349
185	0.68	285.9	47.9	0.0147	-	-	14.2	0.0106	62.1	0.0253	407
186	0.68	227.2	-	-	-	-	114	0.0847	114	0.0847	746
187	1.00	329.4	-	-	-	-	21.0	0.0230	21.0	0.0230	1,100
188	1.00	122.0	40.5	0.0207	-	-	-	-	40.5	0.0207	512
189	1.00	49.8	34.0	0.0206	-	-	4.94	-	38.9	0.0206	528
190	1.00	60.4	38.7	0.0210	-	-	2.22	-	41.0	0.0210	512
191	1.00	77.7	32.3	0.0650	-	-	22.7	0.0192	55.0	0.0842	1,530
192	1.00	121.6	-	-	-	-	49.7	0.0547	49.7	0.0547	1,100
193	1.00	195.9	36.1	0.0303	-	-	5.72	-	41.8	0.0303	725
194	1.00	104.7	34.8	0.0178	-	-	9.11	-	43.9	0.0178	406
195	1.00	204.3	18.5	0.0095	-	-	1.91	-	20.4	0.0095	464
196	0.68	55.2	47.9	0.0167	-	-	2.15	-	50.0	0.0167	333
197	0.68	132.9	31.4	0.0364	-	-	8.37	-	39.8	0.0364	915
198	0.68	80.7	10.9	0.0026	-	-	-	-	10.9	0.0026	242
199	1.06	97.3	-	-	-	-	12.9	0.0150	12.9	0.0150	1,166
200	1.06	218.5	18.8	0.0112	-	-	-	-	18.8	0.0112	595
201	1.06	153.9	50.6	0.0149	-	-	-	-	50.6	0.0149	294
202	1.00	178.2	-	-	-	-	83.7	0.0920	83.7	0.0920	1,099
203	1.00	203.2	-	-	-	-	87.0	0.0934	87.0	0.0934	1,073
204	1.00	124.3	-	-	5.39	0.0138	-	-	5.39	0.0138	2,568
205	1.00	181.3	-	-	57.3	0.147	2.84	0.0000	60.1	0.147	2,447
206	1.00	88.2	-	-	68.2	0.175	11.2	-	79.4	0.175	2,205

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
207	0.69	96.5	0.146	0.0003	0.146	0.0004	50.0	0.109	50.3	0.110	2,180
208	1.00	71.2	-	-	28.2	0.0725	3.79	-	32.0	0.0725	2,264
209	1.00	94.8	-	-	16.0	0.0411	4.69	-	20.7	0.0411	1,986
210	1.00	137.4	95.8	0.410	4.18	0.0107	31.5	0.0000	131	0.421	3,202
211	1.00	84.3	-	-	-	-	-	-	-	-	-
212	1.00	141.0	-	-	98.6	0.253	-	-	98.6	0.253	2,568
213	1.00	117.9	-	-	26.0	0.0668	-	-	26.0	0.0668	2,568
214	1.00	119.3	33.9	0.0276	17.6	0.0451	19.8	0.0050	71.3	0.0777	1,090
215	1.00	81.6	-	-	60.3	0.155	2.76	-	63.1	0.155	2,456
216	0.54	196.8	23.4	0.0256	-	-	0.0006	0.0000	23.4	0.0256	1,093
217	0.54	187.8	23.7	0.0050	-	-	93.9	0.0561	118	0.0611	520
218	0.68	143.2	0.0058	0.0000	0.0061	0.0000	26.1	0.0573	26.1	0.0573	2,199
219	0.95	84.7	8.58	0.0027	33.0	0.0846	21.7	0.0187	63.2	0.106	1,677
220	1.00	140.7	4.36	0.0088	49.6	0.123	1.54	-	55.5	0.132	2,378
221	1.00	65.2	27.7	0.105	-	-	19.7	0.0217	47.4	0.127	2,670
222	1.00	168.0	63.3	0.238	43.0	0.0821	51.8	0.0569	158	0.377	2,382
223	1.00	110.8	0.278	0.0012	0.920	0.0013	11.4	0.0117	12.6	0.0142	1,127
224	1.00	119.3	-	-	-	-	32.8	0.0247	32.8	0.0247	755
225	0.54	144.9	55.6	0.0185	-	-	0.0003	0.0000	55.6	0.0185	332
226	1.00	102.1	7.32	0.0023	-	-	64.0	0.0354	71.3	0.0377	529
227	1.00	53.9	18.5	0.0095	0.0041	0.0000	-	-	18.5	0.0095	512
228	1.00	59.8	31.6	0.0109	-	-	-	-	31.6	0.0109	344
229	1.00	124.3	17.3	0.0114	-	-	-	-	17.3	0.0114	659
230	1.00	139.1	60.1	0.0876	-	-	-	-	60.1	0.0876	1,456
231	1.00	61.7	-	-	-	-	61.7	0.0679	61.7	0.0679	1,100
232	0.54	119.3	-	-	-	-	0.0083	0.0000	0.0083	0.0000	547
233	0.54	79.4	65.5	0.0457	-	-	10.6	0.0063	76.2	0.0521	684
234	0.54	77.6	45.0	0.0096	-	-	6.61	0.0039	51.7	0.0135	262
235	0.54	77.0	-	-	-	-	73.4	0.0438	73.4	0.0438	597
236	1.00	63.1	-	-	-	-	54.7	0.0600	54.7	0.0600	1,098
237	0.54	197.7	57.7	0.0123	-	-	44.1	0.0263	102	0.0386	379
238	0.54	65.7	51.5	0.0099	-	-	0.262	0.0002	51.7	0.0101	195
239	0.54	143.0	69.8	0.0219	-	-	73.0	0.0436	143	0.0655	459
240	0.54	60.9	60.9	0.0129	-	-	0.0001	0.0000	60.9	0.0129	212
241	0.54	172.6	158	0.0266	-	-	-	-	158	0.0266	168
242	1.06	230.1	161	0.0501	-	-	-	-	161	0.0501	311
243	1.06	222.4	119	0.0428	-	-	2.04	0.0024	121	0.0452	372
244	1.00	198.6	187	0.0800	-	-	-	-	187	0.0800	428
245	1.00	236.9	193	0.0698	-	-	8.32	0.0091	202	0.0789	391
246	0.68	180.8	159	0.0442	0.464	0.0004	13.8	0.0103	173	0.0550	317
247	0.68	276.6	207	0.0470	-	-	10.1	0.0076	217	0.0545	251
248	0.68	105.3	42.4	0.0747	-	-	61.6	0.0459	104	0.121	1,160
249	1.00	53.2	31.3	0.140	0.701	0.0010	0.0011	0.0000	32.0	0.141	4,405
250	1.00	76.0	16.0	0.0704	-	-	1.37	0.0015	17.4	0.0719	4,139
251	1.00	184.0	9.75	0.0048	-	-	38.6	0.0425	48.4	0.0473	977
252	1.00	105.4	83.3	0.0463	-	-	8.29	0.0091	91.6	0.0554	604
253	1.00	136.1	40.7	0.0631	-	-	92.8	0.102	134	0.165	1,237
254	1.00	122.5	33.1	0.0130	-	-	19.8	0.0217	52.9	0.0347	656
255	1.00	124.8	28.5	0.0157	-	-	19.0	0.0209	47.5	0.0366	770
256	1.00	146.3	20.9	0.0376	-	-	6.46	0.0071	27.3	0.0448	1,637
257	1.00	293.7	59.0	0.0871	-	-	13.3	0.0146	72.3	0.102	1,407
258	1.00	196.1	-	-	3.10	0.0043	42.9	0.0472	46.0	0.0515	1,120
259	1.00	170.9	0.0013	0.0000	6.52	0.0168	2.24	0.0025	8.77	0.0192	2,192
260	1.00	218.5	0.0828	0.0002	-	-	218	-	219	0.0002	0.880
261	1.00	141.3	61.5	0.275	-	-	3.23	-	64.8	0.275	4,249
262	1.00	255.1	113	0.0802	-	-	9.59	0.0105	123	0.0908	740
263	1.00	158.8	139	0.125	-	-	0.518	0.0006	140	0.125	899
264	1.00	112.9	69.1	0.181	-	-	27.1	0.0298	96.2	0.211	2,190
265	1.00	273.1	33.9	0.0439	-	-	3.81	0.0006	37.7	0.0445	1,182
266	1.00	166.8	32.9	0.0249	-	-	-	-	32.9	0.0249	757
267	1.00	305.9	68.6	0.0843	-	-	0.972	0.0005	69.6	0.0848	1,219
268	1.24	147.8	23.3	0.129	10.5	0.0332	20.7	0.0281	54.5	0.190	3,484
269	1.24	174.3	46.0	0.119	-	-	33.6	0.0456	79.6	0.165	2,074
270	1.24	62.2	20.9	0.0809	-	-	2.82	-	23.7	0.0809	3,412
271	1.24	92.6	70.7	0.130	-	-	0.0711	0.0001	70.8	0.130	1,835
272	1.00	148.3	-	-	-	-	53.9	0.0593	53.9	0.0593	1,100
273	1.00	172.1	-	-	-	-	17.9	0.0035	17.9	0.0035	193
274	1.00	99.1	39.9	0.178	-	-	53.4	0.0539	93.3	0.232	2,489
275	1.00	58.1	13.2	0.0589	-	-	3.42	0.0038	16.6	0.0627	3,776
276	1.00	162.1	31.7	0.110	79.1	0.187	37.3	0.0410	148	0.338	2,283
277	1.00	169.9	-	-	36.2	0.0928	-	-	36.2	0.0928	2,568
278	1.00	92.6	0.0010	0.0000	-	-	8.60	0.0095	8.60	0.0095	1,100
279	1.24	61.8	56.2	0.0605	-	-	0.370	0.0005	56.6	0.0610	1,077
280	0.31	106.3	88.8	0.0111	-	-	14.5	0.0050	103	0.0161	156
281	1.00	100.6	12.2	0.0048	-	-	35.1	0.0386	47.3	0.0434	917
282	1.00	151.9	28.9	0.0346	-	-	-	-	28.9	0.0346	1,196
283	1.00	104.7	50.0	0.0195	-	-	18.0	0.0198	68.0	0.0394	578
284	1.00	134.0	50.7	0.0410	-	-	48.7	0.0492	99.5	0.0902	907
285	1.00	238.4	105	0.0412	-	-	16.4	0.0180	121	0.0592	489
286	1.00	84.7	49.8	0.0558	-	-	29.3	0.0323	79.1	0.0880	1,112
287	1.00	175.4	9.40	0.0037	-	-	-	-	9.40	0.0037	391
288	1.00	156.9	24.6	0.0092	-	-	27.1	0.0298	51.7	0.0390	755
289	1.00	91.7	46.0	0.0152	-	-	3.50	0.0038	49.5	0.0191	385
290	0.31	114.1	91.2	0.0194	-	-	0.0003	0.0000	91.2	0.0194	213
291	0.31	217.1	33.1	0.0208	-	-	9.78	0.0034	42.8	0.0242	565
292	0.31	126.4	83.8	0.0188	-	-	8.21	0.0028	92.0	0.0216	235
293	0.31	151.5	-	-	-	-	38.1	0.0131	38.1	0.0131	344
294	0.31	81.3	8.55	0.0054	-	-	19.4	0.0067	27.9	0.0121	432
295	1.00	230.3	30.7	0.0389	-	-	3.68	0.0040	34.4	0.0429	1,248
296	1.00	49.2	12.8	0.0050	-	-	17.1	0.0188	29.9	0.0238	797
297	0.31	160.2	106	0.0279	-	-	44.6	0.0154	151	0.0432	287
298	1.00	298.2	54.0	0.0211	-	-	-	-	54.0	0.0211	391
299	1.00	193.4	41.4	0.0162	-	-	17.0	0.0187	58.4	0.0349	597
300	0.31	320.6	0.368	0.0002	-	-	17.0	0.0058	17.3	0.0061	350
301	1.00	142.4	79.4	0.0460	-	-	6.17	0.0068	85.6	0.0528	617
302	1.00	262.6	49.2	0.0704	-	-	9.11	0.0100	58.3	0.0805	1,381
303	1.00	86.7	61.2	0.0564	-	-	14.3	0.0158	75.5	0.0722	956
304	1.00	88.0	53.9	0.0520	-	-	8.41	0.0092	62.3	0.0613	984
305	1.00	135.7	96.7	0.138	2.40	0.0062	9.70	0.0107	109	0.155	1,422
306	1.00	158.6	96.4	0.0401	-	-	17.0	-	113	0.0401	354
307	1.00	171.2	67.9	0.0513	-	-	15.8	0.0125	83.7	0.0638	762
308	1.00	196.4	30.8	0.0433	-	-	-	-	30.8	0.0433	1,405
309	1.00	30.0	28.7	0.0107	-	-	-	-	28.7	0.0107	374

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
310	1.00	136.3	36.0	0.0164	-	-	2.66	-	38.7	0.0164	425
311	1.00	146.9	133	0.0571	-	-	11.5	0.0126	144	0.0697	483
312	1.00	94.9	54.1	0.0277	-	-	-	-	54.1	0.0277	512
313	1.24	136.1	86.4	0.115	-	-	-	-	86.4	0.115	1,331
314	1.00	85.4	67.5	0.0408	-	-	15.3	0.0000	82.8	0.0408	492
315	1.00	107.7	70.8	0.0369	-	-	31.2	-	102	0.0369	362
316	1.00	108.1	101	0.0530	-	-	4.54	-	105	0.0530	503
317	1.00	109.2	91.0	0.0516	-	-	14.8	-	106	0.0516	488
318	1.24	155.1	116	0.0828	-	-	29.5	0.0000	146	0.0828	567
319	1.24	118.7	118	0.0866	-	-	-	-	118	0.0866	731
320	1.00	191.9	32.0	0.0156	-	-	-	-	32.0	0.0156	487
321	1.00	114.5	108	0.0856	-	-	3.66	0.0040	112	0.0896	802
322	1.00	113.7	59.2	0.0166	-	-	-	-	59.2	0.0166	281
323	1.00	186.7	23.3	0.0469	-	-	-	-	23.3	0.0469	2,013
324	1.00	108.7	56.5	0.0246	-	-	13.9	0.0152	70.3	0.0398	567
325	1.00	230.6	173	0.0563	-	-	8.29	0.0091	181	0.0654	361
326	1.00	135.2	118	0.0390	-	-	5.05	0.0055	123	0.0445	362
327	1.00	261.5	215	0.101	-	-	32.8	0.0270	248	0.128	514
328	1.00	115.1	115	0.0803	-	-	-	-	115	0.0803	701
329	1.00	116.5	102	0.0531	-	-	2.97	0.0033	105	0.0564	539
330	1.00	68.3	25.6	0.0276	-	-	21.1	0.0232	46.7	0.0508	1,089
331	1.00	72.3	72.3	0.0278	-	-	0.0001	0.0000	72.3	0.0278	385
332	1.00	71.7	53.9	0.0211	-	-	3.49	0.0038	57.4	0.0249	434
333	1.00	152.4	137	0.0919	-	-	8.27	0.0091	145	0.101	697
334	1.00	147.6	57.5	0.0681	-	-	5.35	0.0059	62.9	0.0740	1,176
335	1.00	167.6	33.7	0.0302	-	-	0.937	0.0010	34.6	0.0312	902
336	1.00	67.4	51.3	0.0309	-	-	6.85	0.0075	58.2	0.0385	661
337	1.00	134.8	124	0.0712	-	-	7.18	0.0076	132	0.0788	599
338	1.24	106.5	68.6	0.0982	-	-	7.23	0.0000	75.8	0.0982	1,294
339	1.24	48.9	33.3	0.0441	-	-	14.9	0.0202	48.1	0.0643	1,335
340	1.00	93.1	21.7	0.0116	-	-	20.9	0.0230	42.6	0.0346	812
341	1.00	77.7	77.7	0.0304	-	-	-	-	77.7	0.0304	391
342	1.00	114.9	91.1	0.0476	-	-	23.8	0.0261	115	0.0738	642
343	1.24	74.6	59.3	0.0712	1.22	0.0039	0.572	0.0008	61.0	0.0758	1,242
344	1.24	150.5	85.4	0.135	-	-	5.15	0.0069	90.6	0.141	1,562
345	1.00	204.3	134	0.0757	44.7	0.115	7.16	0.0000	185	0.190	1,027
346	1.00	139.2	20.0	0.0332	-	-	18.1	0.0153	38.1	0.0485	1,273
347	1.00	366.8	98.6	0.0414	-	-	15.6	0.0000	114	0.0414	363
348	1.00	184.8	32.5	0.0823	0.0001	0.0000	12.4	0.0137	44.9	0.0960	2,138
349	1.00	195.1	19.2	0.0281	-	-	21.2	0.0234	40.4	0.0514	1,271
350	1.00	95.6	33.6	0.0317	-	-	3.83	0.0042	37.5	0.0359	959
351	1.00	181.5	27.7	0.0427	5.34	0.0137	43.7	0.0481	76.8	0.104	1,361
352	1.00	255.1	78.7	0.0975	-	-	-	-	78.7	0.0975	1,239
353	1.00	111.5	58.6	0.0233	-	-	-	-	58.6	0.0233	398
354	1.00	71.1	66.2	0.0322	-	-	-	-	66.2	0.0322	486
355	1.00	181.3	169	0.0661	-	-	3.79	0.0042	173	0.0703	407
356	1.00	149.9	29.0	0.0114	-	-	0.0002	0.0000	29.0	0.0114	391
357	1.00	96.1	20.5	0.0080	-	-	-	-	20.5	0.0080	391
358	1.00	52.2	28.2	0.0205	-	-	-	-	28.2	0.0205	728
359	1.00	109.1	6.32	0.0025	-	-	0.0001	0.0000	6.32	0.0025	391
360	1.00	79.8	57.3	0.0331	-	-	0.0000	0.0000	57.3	0.0331	577
361	1.00	43.9	28.7	0.0112	-	-	-	-	28.7	0.0112	391
362	0.68	177.4	79.9	0.0385	-	-	2.05	0.0015	81.9	0.0400	489
363	0.68	117.9	64.8	0.0225	-	-	-	-	64.8	0.0225	347
364	0.68	97.9	40.5	0.107	-	-	35.2	0.0263	75.7	0.133	1,762
365	1.00	81.6	74.4	0.0240	-	-	-	-	74.4	0.0240	322
366	1.00	41.2	24.0	0.0094	-	-	9.08	0.0100	33.1	0.0194	586
367	1.00	187.8	5.48	0.0245	49.2	0.103	116	0.128	171	0.256	1,493
368	0.68	143.2	128	0.133	4.75	0.0046	2.86	0.0008	135	0.138	1,022
369	1.00	55.1	9.98	0.0033	1.28	0.0033	1.44	-	12.7	0.0066	522
370	1.00	110.4	79.1	0.0957	11.6	0.0297	15.8	0.0155	107	0.141	1,323
371	0.54	38.9	-	-	-	-	18.6	0.0025	18.6	0.0025	132
372	0.32	127.2	-	-	-	-	24.2	0.0266	24.2	0.0266	1,098
373	0.54	116.8	-	-	-	-	75.0	0.0823	75.0	0.0823	1,098
374	1.00	157.3	36.8	0.0506	-	-	4.19	0.0046	41.0	0.0552	1,346
375	1.00	126.7	41.8	0.0233	-	-	9.58	0.0005	51.3	0.0238	463
376	1.00	33.8	12.3	0.0034	-	-	7.79	0.0086	20.0	0.0120	597
377	1.00	53.9	28.3	0.0494	-	-	3.07	-	31.3	0.0494	1,576
378	1.00	195.5	21.5	0.0060	-	-	-	-	21.5	0.0060	277
379	1.00	124.3	-	-	96.7	0.248	2.59	0.0028	99.2	0.251	2,525
380	1.00	136.2	61.6	0.0540	13.2	0.0339	35.4	0.0382	110	0.126	1,144
381	1.00	137.5	32.1	0.0645	-	-	-	-	32.1	0.0645	2,010
382	1.00	108.2	0.269	0.0005	-	-	88.7	0.0974	89.0	0.0979	1,100
383	1.06	178.6	52.2	0.0359	-	-	4.39	0.0051	56.5	0.0410	726
384	0.54	77.6	77.2	0.0151	-	-	-	-	77.2	0.0151	196
385	1.00	111.7	9.02	0.0025	-	-	0.0004	0.0000	9.02	0.0025	277
386	1.00	45.9	22.6	0.0123	-	-	19.5	0.0215	42.1	0.0338	802
387	0.54	61.1	47.7	0.0101	-	-	13.4	0.0080	61.1	0.0181	296
388	0.54	330.5	16.0	0.0024	-	-	-	-	16.0	0.0024	151
389	1.00	238.2	2.14	0.0006	-	-	55.2	0.0607	57.3	0.0613	1,069
390	1.00	275.4	31.1	0.0433	0.0063	0.0000	21.6	0.0189	52.7	0.0622	1,180
391	1.00	160.2	18.9	0.0380	-	-	33.1	0.0364	52.0	0.0744	1,431
392	1.00	310.3	38.4	0.0774	-	-	0.0017	0.0000	38.4	0.0774	2,013
393	1.00	81.5	24.7	0.0261	-	-	43.3	0.0462	68.0	0.0723	1,063
394	1.00	105.4	79.2	0.0414	-	-	15.7	0.0144	95.0	0.0558	588
395	1.00	136.0	90.6	0.0391	-	-	22.0	0.0191	113	0.0582	517
396	1.00	47.2	36.5	0.0952	-	-	2.62	0.0024	39.1	0.0976	2,497
397	1.00	55.1	31.9	0.0089	-	-	0.0187	-	32.0	0.0089	277
398	1.00	86.2	66.8	0.0229	-	-	0.0352	-	66.9	0.0229	342
399	1.00	24.9	18.3	0.0051	-	-	-	-	18.3	0.0051	277
400	1.00	76.0	36.2	0.0112	-	-	9.19	-	45.4	0.0112	247
401	1.00	73.0	22.8	0.0376	6.69	0.0172	-	-	29.5	0.0548	1,859
402	1.00	101.6	41.8	0.0116	-	-	15.3	-	57.2	0.0116	203
403	0.54	59.5	-	-	-	-	25.1	0.0150	25.1	0.0150	597
404	1.00	122.5	-	-	-	-	32.2	0.0353	32.2	0.0353	1,098
405	1.00	76.3	-	-	-	-	23.6	0.0259	23.6	0.0259	1,098
406	1.00	91.5	71.3	0.0511	-	-	17.1	0.0188	88.4	0.0699	790
407	1.00	293.7	257	0.158	-	-	12.6	0.0138	270	0.172	637
408	1.00	156.0	111	0.0566	-	-	17.2	-	128	0.0566	441
409	1.00	170.9	77.7	0.0537	25.3	0.0650	8.63	0.0041	112	0.123	1,101
410	1.00	61.9	-	-	54.2	0.139	-	-	54.2	0.139	2,568
411	1.00	134.9	28.8	0.0080	76.9	0.198	-	-	106	0.206	1,944
412	0.32	255.1	-	-	-	-	255	0.280	255	0.280	1,098

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
413	1.00	213.8	-	-	-	-	111	0.122	111	0.122	1,098
414	1.00	72.0	-	-	-	-	15.1	0.0166	15.1	0.0166	1,100
415	1.00	52.9	-	-	-	-	21.2	0.0233	21.2	0.0233	1,100
416	0.55	151.7	-	-	12.4	0.0318	137	0.302	150	0.334	2,230
417	1.00	86.8	-	-	11.3	0.0291	0.257	-	11.6	0.0291	2,511
418	1.00	134.6	-	-	9.31	0.0239	-	-	9.31	0.0239	2,568
419	1.00	87.3	5.55	0.0055	47.1	0.121	14.7	-	67.3	0.126	1,878
420	1.00	62.2	25.9	0.0359	10.7	0.0275	2.06	-	38.7	0.0635	1,640
421	1.00	47.9	-	-	29.0	0.0744	0.299	-	29.3	0.0744	2,541
422	1.00	148.3	-	-	1.63	0.0042	126	0.123	127	0.127	997
423	1.00	79.6	23.6	0.0066	-	-	0.905	-	24.5	0.0066	267
424	1.00	87.3	14.3	0.0040	-	-	-	-	14.3	0.0040	277
425	1.00	26.8	12.3	0.0034	-	-	-	-	12.3	0.0034	277
426	1.00	24.9	24.9	0.0069	-	-	-	-	24.9	0.0069	277
427	1.00	23.2	19.3	0.0054	-	-	3.86	-	23.2	0.0054	231
428	1.00	31.8	14.4	0.0040	-	-	10.0	0.0110	24.4	0.0150	614
429	1.00	80.0	11.3	0.0031	-	-	-	-	11.3	0.0031	277
430	1.00	69.0	6.32	0.0018	-	-	0.101	-	6.42	0.0018	273
431	1.00	120.9	-	-	-	-	0.396	0.0004	0.396	0.0004	1,100
432	1.00	107.7	-	-	-	-	97.3	0.107	97.3	0.107	1,098
433	1.00	104.7	45.4	0.0775	38.5	0.0987	6.65	-	90.6	0.176	1,946
434	1.00	126.2	114	0.0407	-	-	-	-	114	0.0407	358
435	1.00	94.5	93.8	0.0345	-	-	0.116	0.0001	93.9	0.0346	369
436	1.00	52.8	7.18	0.0028	-	-	-	-	7.18	0.0028	391
437	1.00	84.8	10.7	0.0215	-	-	1.50	0.0016	12.2	0.0232	1,901
438	1.06	156.9	135	0.0889	-	-	9.99	0.0116	145	0.101	694
439	0.54	127.6	90.1	0.0136	-	-	-	-	90.1	0.0136	151
440	0.54	81.9	81.1	0.0140	-	-	-	-	81.1	0.0140	172
441	0.54	124.9	115	0.0181	-	-	-	-	115	0.0181	158
442	0.54	81.2	74.2	0.0258	-	-	-	-	74.2	0.0258	348
443	1.06	151.5	134	0.221	-	-	5.64	0.0066	140	0.227	1,622
444	0.54	49.2	48.5	0.0175	-	-	-	-	48.5	0.0175	361
445	0.54	78.7	77.5	0.0358	-	-	-	-	77.5	0.0358	462
446	1.00	49.2	-	0.0007	-	-	44.4	-	44.4	0.0007	15.2
447	1.00	44.0	-	-	-	-	-	-	-	-	-
448	1.00	298.2	0.0000	0.0008	-	-	99.9	0.0040	99.9	0.0048	47.9
449	0.54	193.4	-	0.0001	-	-	19.9	0.0006	19.9	0.0007	35.2
450	1.00	320.6	273	0.108	-	-	2.51	-	275	0.108	391
451	1.00	142.4	122	0.0471	0.0000	0.0000	-	-	122	0.0471	387
452	1.00	262.6	80.4	0.0285	1.71	0.0024	1.44	0.0000	83.6	0.0309	370
453	1.00	90.7	27.5	0.0093	-	-	-	-	27.5	0.0093	338
454	1.00	97.7	28.2	0.0110	-	-	0.0000	0.0000	28.2	0.0110	391
455	1.00	52.4	24.4	0.0726	-	-	24.1	0.0265	48.5	0.0990	2,043
456	1.00	52.0	33.1	0.0399	-	-	-	-	33.1	0.0399	1,207
457	1.00	49.6	-	-	-	-	-	-	-	-	-
458	1.00	56.8	-	-	-	-	55.9	0.0614	55.9	0.0614	1,098
459	1.00	61.7	-	-	-	-	21.1	-	21.1	-	-
460	0.24	76.2	-	-	-	-	26.1	0.0140	26.1	0.0140	537
461	0.49	83.5	-	0.0005	-	-	72.6	-	72.6	0.0005	7.06
462	0.62	94.9	-	0.0001	-	-	94.9	0.117	94.9	0.118	1,239
463	0.62	35.6	6.68	0.0012	-	-	1.26	0.0001	7.94	0.0013	164
464	0.61	60.7	10.8	0.0019	-	-	1.23	-	12.0	0.0019	156
465	0.49	126.7	-	0.0005	-	-	74.0	-	74.0	0.0005	7.36
466	0.49	43.5	-	-	12.1	0.0152	4.27	0.0023	16.3	0.0174	1,067
467	1.61	84.4	20.5	0.0091	-	-	5.53	-	26.0	0.0091	351
468	0.62	58.0	15.5	0.0046	-	-	42.4	0.0515	58.0	0.0560	966
469	0.62	82.8	47.8	0.0271	-	-	35.0	0.0390	82.8	0.0661	799
470	0.49	27.4	3.85	0.0021	-	-	2.16	-	6.01	0.0021	342
471	0.49	93.0	-	-	-	-	6.45	0.0035	6.45	0.0035	537
472	0.49	40.6	-	-	-	-	10.5	0.0053	10.5	0.0053	504
473	0.49	186.7	5.94	0.0005	-	-	2.43	-	8.37	0.0005	57.7
474	0.49	60.9	0.622	0.0001	-	-	2.38	-	3.00	0.0001	16.9
475	1.00	52.4	-	-	-	-	-	-	-	-	-
476	0.49	105.1	10.7	0.0009	-	-	0.0000	-	10.7	0.0009	81.3
477	0.49	70.2	5.67	0.0005	-	-	0.0229	-	5.69	0.0005	81.0
478	1.00	114.3	-	-	-	-	2.12	-	2.12	-	-
479	1.00	42.2	-	-	-	-	-	-	-	-	-
480	1.61	46.0	36.5	0.0163	-	-	9.31	0.0165	45.8	0.0327	715
481	0.89	52.0	38.6	0.0134	-	-	1.25	0.0012	39.9	0.0147	368
482	0.89	49.2	12.3	0.0043	-	-	36.8	0.0360	49.2	0.0403	820
483	0.38	65.7	29.1	0.0131	-	-	30.0	0.0161	59.2	0.0292	494
484	0.89	51.0	7.23	0.0025	-	-	0.0018	-	7.23	0.0025	348
485	0.36	23.1	9.16	0.0159	-	-	2.02	-	11.2	0.0159	1,422
486	0.89	50.9	9.85	0.0034	-	-	0.448	-	10.3	0.0034	333
487	0.89	35.6	12.4	0.0043	-	-	-	-	12.4	0.0043	348
488	0.89	47.9	18.6	0.0028	-	-	8.89	0.0087	27.5	0.0114	416
489	0.89	31.3	30.1	0.0058	-	-	0.0021	0.0000	30.1	0.0059	195
490	0.89	71.5	46.2	0.0161	-	-	5.96	0.0000	52.2	0.0161	308
491	0.89	33.9	2.27	0.0008	-	-	17.3	0.0169	19.6	0.0177	905
492	0.89	42.8	0.720	0.0003	-	-	11.1	-	11.8	0.0003	21.1
493	0.89	31.0	15.4	0.0054	-	-	-	-	15.4	0.0054	348
494	0.89	89.1	61.4	0.0214	-	-	10.7	-	72.1	0.0214	296
495	0.89	53.1	23.4	0.0081	-	-	2.49	-	25.9	0.0081	314
496	0.89	70.3	13.4	0.0047	-	-	0.0020	0.0000	13.4	0.0047	348
497	0.89	78.5	13.1	0.0045	-	-	0.414	-	13.5	0.0045	337
498	0.89	49.9	16.5	0.0057	-	-	0.0038	-	16.5	0.0057	348
499	0.89	107.9	13.3	0.0080	-	-	6.25	0.0061	19.6	0.0141	718
500	0.89	63.8	3.71	0.0013	-	-	14.7	-	18.4	0.0013	70.2
501	0.56	62.0	30.1	0.0092	-	-	0.194	0.0000	30.3	0.0092	304
502	0.89	79.5	54.4	0.0189	-	-	0.0098	0.0000	54.4	0.0189	348
503	0.89	102.5	23.6	0.0082	-	-	0.549	0.0000	24.1	0.0082	340
504	0.89	94.3	17.9	0.0062	-	-	6.48	0.0000	24.4	0.0062	255
505	0.89	58.6	15.1	0.0135	-	-	-	-	15.1	0.0135	892
506	0.89	97.4	14.3	0.0147	-	-	0.0287	-	14.4	0.0147	1,020
507	0.89	36.7	18.3	0.0305	-	-	-	-	18.3	0.0305	1,665
508	0.89	52.2	35.9	0.0643	-	-	5.61	0.0014	41.5	0.0657	1,583
509	0.89	49.3	-	-	-	-	7.28	0.0071	7.28	0.0071	977
510	0.89	105.8	-	0.0000	-	-	7.85	0.0148	7.85	0.0148	1,885
511	0.49	359.3	0.0001	0.0002	-	-	22.5	0.0009	22.5	0.0011	47.8
512	1.40	133.8	-	-	-	-	134	0.237	134	0.237	1,769
513	1.48	59.4	1.69	0.0055	-	-	4.33	0.0077	6.02	0.0131	2,180
514	0.49	108.5	5.02	0.0049	-	-	92.6	-	97.7	0.0049	50.6
515	0.49	34.7	15.5	0.0067	4.82	0.0060	14.0	-	34.3	0.0128	372

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
516	1.61	62.3	31.2	0.0445	-	-	8.04	-	39.3	0.0445	1,133
517	1.61	36.2	14.9	0.0067	-	-	9.31	0.0000	24.3	0.0067	275
518	1.61	26.8	17.1	0.0214	-	-	1.92	0.0000	19.1	0.0214	1,122
519	1.61	97.6	36.8	0.0331	-	-	9.71	0.0172	46.6	0.0503	1,079
520	1.61	119.9	24.8	0.0218	-	-	-	-	24.8	0.0218	878
521	1.61	168.8	38.2	0.0442	-	-	0.0065	0.0000	38.2	0.0442	1,157
522	1.61	66.6	36.2	0.0161	-	-	15.1	0.0266	51.3	0.0428	834
523	1.61	21.0	14.2	0.0387	-	-	-	-	14.2	0.0387	2,728
524	1.61	130.3	28.1	0.0135	-	-	-	-	28.1	0.0135	479
525	1.61	48.0	47.6	0.0212	-	-	-	-	47.6	0.0212	446
526	1.61	159.8	31.7	0.0141	-	-	-	-	31.7	0.0141	446
527	1.61	96.5	36.2	0.0161	-	-	-	-	36.2	0.0161	446
528	1.61	129.7	17.2	0.0422	-	-	0.833	-	18.0	0.0422	2,341
529	1.61	127.6	38.2	0.0219	-	-	3.67	-	41.9	0.0219	524
530	1.61	58.1	13.3	0.0096	-	-	0.333	-	13.7	0.0096	702
531	1.61	75.2	39.9	0.0279	-	-	12.5	0.0168	52.4	0.0447	854
532	1.61	20.9	14.0	0.0062	-	-	1.63	-	15.6	0.0062	399
533	1.61	96.0	12.0	0.0090	-	-	2.62	-	14.6	0.0090	617
534	1.61	36.8	5.34	0.0173	-	-	24.8	-	30.2	0.0173	574
535	0.49	40.5	-	-	4.71	0.0059	24.9	0.0134	29.6	0.0193	651
536	0.49	37.5	-	-	-	-	28.2	0.0152	28.2	0.0152	537
537	0.49	43.5	-	-	-	-	30.9	0.0166	30.9	0.0166	537
538	0.49	55.8	-	-	8.08	0.0101	-	-	8.08	0.0101	1,255
539	1.48	85.7	6.70	0.0215	-	-	14.4	0.0249	21.1	0.0463	2,192
540	1.61	100.6	6.10	0.0196	-	-	-	-	6.10	0.0196	3,206
541	1.61	52.1	38.8	0.0660	-	-	1.86	-	40.6	0.0660	1,624
542	1.61	64.4	10.2	0.0290	15.3	0.0633	2.12	0.0038	27.7	0.0961	3,470
543	0.49	90.7	-	-	-	-	5.40	0.0029	5.40	0.0029	537
544	0.49	48.9	-	-	10.5	0.0131	3.89	0.0021	14.4	0.0152	1,061
545	0.49	45.8	2.62	0.0026	3.70	0.0046	3.42	0.0018	9.74	0.0091	930
546	0.49	53.9	-	-	22.8	0.0286	0.555	0.0003	23.3	0.0289	1,238
547	0.49	51.7	-	-	19.6	0.0247	1.70	0.0009	21.3	0.0256	1,198
548	0.49	36.2	-	-	35.6	0.0447	-	-	35.6	0.0447	1,255
549	0.49	24.9	11.6	0.0114	-	-	6.11	0.0031	17.7	0.0145	819
550	0.49	153.9	-	-	6.98	0.0088	-	-	6.98	0.0088	1,255
551	0.49	131.5	-	-	26.1	0.0328	-	-	26.1	0.0328	1,255
552	0.49	148.8	-	-	31.6	0.0397	-	-	31.6	0.0397	1,255
553	0.49	111.7	-	-	25.3	0.0317	-	-	25.3	0.0317	1,255
554	0.49	94.6	6.40	0.0009	9.27	0.0116	0.0001	0.0000	15.7	0.0125	798
555	0.49	101.3	16.1	0.0022	6.41	0.0080	-	-	22.5	0.0102	454
556	0.49	114.9	0.142	0.0001	9.01	0.0113	-	-	9.15	0.0114	1,251
557	1.61	85.8	35.3	0.0211	-	-	1.72	0.0000	37.0	0.0211	571
558	1.61	55.7	6.16	0.0199	-	-	41.3	0.0634	47.4	0.0833	1,756
559	1.61	79.6	63.5	0.0382	-	-	13.8	-	77.2	0.0382	495
560	1.61	58.1	43.2	0.0193	-	-	9.98	0.0176	53.2	0.0369	694
561	1.61	107.7	18.3	0.0082	-	-	-	-	18.3	0.0082	446
562	1.61	66.5	24.0	0.0248	-	-	-	-	24.0	0.0248	1,037
563	1.61	84.0	84.0	0.107	-	-	-	-	84.0	0.107	1,275
564	1.61	96.1	39.6	0.0272	-	-	4.50	-	44.1	0.0272	618
565	1.61	203.9	22.2	0.0126	-	-	3.28	-	25.4	0.0126	495
566	1.49	79.3	52.8	0.0480	-	-	26.4	0.0466	79.2	0.0946	1,195
567	1.00	31.7	-	-	-	-	-	-	-	-	-
568	0.49	27.1	3.77	0.0005	-	-	3.13	-	6.91	0.0005	74.0
569	0.49	99.5	-	-	30.5	0.0382	-	-	30.5	0.0382	1,255
570	1.00	31.5	-	-	-	-	-	-	-	-	-
571	0.89	47.9	5.41	0.0019	-	-	0.152	-	5.56	0.0019	339
572	0.89	95.4	33.0	0.0583	-	-	1.57	0.0031	34.6	0.0614	1,776
573	0.97	62.5	43.4	0.0901	-	-	9.62	0.0206	53.0	0.111	2,088
574	1.03	87.3	56.1	0.0316	-	-	12.5	0.0024	68.6	0.0340	496
575	0.89	29.9	6.18	0.0016	-	-	-	-	6.18	0.0016	253
576	0.89	55.1	13.9	0.0048	-	-	0.0004	-	13.9	0.0048	348
577	0.27	53.3	9.07	0.0032	-	-	0.0117	0.0000	9.08	0.0032	348
578	0.49	42.6	-	-	4.52	0.0057	-	-	4.52	0.0057	1,255
579	0.49	80.0	14.3	0.0021	-	-	27.2	-	41.5	0.0021	51.6
580	0.62	85.6	51.4	0.0332	-	-	17.6	0.0097	69.0	0.0429	621
581	0.62	120.9	65.2	0.0511	-	-	55.7	0.0455	121	0.0966	799
582	0.89	79.0	24.2	0.0062	-	-	0.0054	-	24.2	0.0062	255
583	0.49	113.0	-	-	15.1	0.0189	-	-	15.1	0.0189	1,255
584	1.61	115.7	18.6	0.0668	17.5	0.0722	-	-	36.1	0.139	3,854
585	1.61	58.3	25.0	0.0276	-	-	0.0306	-	25.1	0.0276	1,101
586	0.49	143.5	-	-	28.7	0.0360	-	-	28.7	0.0360	1,255
587	0.49	110.2	-	-	-	-	71.8	0.0289	71.8	0.0289	402
588	0.85	108.6	47.8	0.0118	-	-	60.8	0.0664	109	0.0782	720
589	0.84	127.6	38.9	0.0123	-	-	88.7	0.0522	128	0.0645	505
590	1.61	108.8	2.24	0.0010	-	-	1.70	-	3.94	0.0010	253
591	0.49	65.7	7.06	0.0069	15.2	0.0190	5.95	0.0032	28.2	0.0292	1,036
592	0.12	160.9	12.2	0.0023	-	-	-	-	12.2	0.0023	191
593	0.49	168.3	-	-	-	-	6.01	0.0012	6.01	0.0012	197
594	1.00	101.5	-	-	-	-	-	-	-	-	-
595	1.00	69.3	-	-	-	-	3.95	-	3.95	-	-
596	1.00	129.6	-	-	-	-	-	-	-	-	-
597	0.49	91.0	-	0.0001	-	-	8.59	-	8.59	0.0001	7.42
598	0.49	30.7	-	0.0000	-	-	2.05	-	2.05	0.0000	7.42
599	0.49	69.7	1.94	0.0004	-	-	0.989	-	2.93	0.0004	127
600	1.00	201.5	-	-	-	-	-	-	-	-	-
601	0.49	184.5	-	-	-	-	38.4	0.0000	38.4	0.0000	0.0123
602	1.00	138.7	-	-	-	-	27.9	-	27.9	-	-
603	0.49	172.6	0.350	0.0001	-	-	90.4	-	90.7	0.0001	0.624
604	0.49	107.9	-	0.0000	-	-	2.29	-	2.29	0.0000	7.42
605	1.00	82.1	-	-	-	-	-	-	-	-	-
606	0.49	73.4	0.0055	0.0000	-	-	1.22	-	1.23	0.0000	0.613
607	1.00	64.3	-	-	-	-	3.21	-	3.21	-	-
608	1.00	67.7	-	-	-	-	2.59	-	2.59	-	-
609	1.00	97.4	-	-	-	-	-	-	-	-	-
610	0.49	119.9	-	0.0000	-	-	21.6	-	21.6	0.0000	1.44
611	0.49	103.9	-	0.0000	-	-	35.9	-	35.9	0.0000	1.03
612	1.00	197.7	-	-	-	-	-	-	-	-	-
613	1.00	35.6	-	-	-	-	0.329	-	0.329	-	-
614	1.00	176.6	-	-	-	-	-	-	-	-	-
615	0.49	126.7	9.11	0.0017	-	-	1.57	-	10.7	0.0017	163
616	1.00	141.9	-	-	-	-	-	-	-	-	-
617	1.00	185.6	-	-	-	-	-	-	-	-	-
618	0.17	129.6	47.1	0.0132	-	-	-	-	47.1	0.0132	280

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
619	1.69	23.0	1.05	0.0007	-	-	11.2	0.0207	12.2	0.0214	1,750
620	0.52	99.8	10.2	0.0021	-	-	2.40	0.0014	12.6	0.0035	276
621	0.52	111.3	36.1	0.0253	3.68	0.0027	19.5	0.0128	59.2	0.0408	689
622	0.52	40.6	17.7	0.0036	-	-	19.8	0.0114	37.5	0.0150	401
623	0.52	98.9	8.41	0.0017	-	-	-	-	8.41	0.0017	205
624	0.52	92.8	22.6	0.0046	-	-	0.797	0.0005	23.4	0.0051	218
625	1.69	125.6	-	-	-	-	7.47	0.0277	7.47	0.0277	3,704
626	1.00	176.7	-	-	-	-	-	-	-	-	-
627	1.00	125.4	-	-	-	-	3.68	-	3.68	-	-
628	1.00	97.0	-	-	-	-	-	-	-	-	-
629	0.53	110.2	1.17	0.0002	-	-	-	-	1.17	0.0002	207
630	1.46	124.2	-	-	-	-	4.49	0.0083	4.49	0.0083	1,852
631	1.69	151.3	3.65	0.0124	-	-	13.5	0.0373	17.1	0.0497	2,905
632	0.53	179.9	2.22	0.0013	-	-	7.39	0.0086	9.61	0.0098	1,022
633	1.69	121.9	2.51	0.0073	-	-	-	-	2.51	0.0073	2,907
634	0.52	51.0	50.8	0.0255	-	-	0.0001	0.0000	50.8	0.0255	502
635	0.52	46.3	13.8	0.0028	-	-	-	-	13.8	0.0028	205
636	0.52	64.0	25.3	0.0162	-	-	16.4	0.0118	41.8	0.0280	671
637	0.52	115.0	29.5	0.0124	-	-	5.79	0.0033	35.3	0.0157	446
638	0.52	36.5	25.3	0.0090	-	-	6.78	0.0078	32.1	0.0168	524
639	0.52	20.9	7.41	0.0078	-	-	9.32	0.0107	16.7	0.0186	1,109
640	0.52	161.2	30.9	0.0326	2.39	0.0018	26.9	0.0216	60.3	0.0560	929
641	0.52	151.2	18.8	0.0069	-	-	0.565	0.0003	19.3	0.0072	373
642	0.52	167.5	18.0	0.0037	-	-	-	-	18.0	0.0037	205
643	1.69	136.0	0.664	0.0023	-	-	4.19	0.0078	4.85	0.0100	2,063
644	0.52	83.0	13.3	0.0027	-	-	-	-	13.3	0.0027	205
645	1.69	53.1	2.31	0.0016	-	-	46.5	0.0107	48.9	0.0123	251
646	1.69	128.0	-	-	-	-	28.6	0.0941	28.6	0.0941	3,293
647	1.69	98.5	64.4	0.0615	-	-	8.09	0.0112	72.5	0.0728	1,004
648	1.69	67.4	4.04	0.0027	-	-	-	-	4.04	0.0027	659
649	1.69	51.5	5.04	0.0033	-	-	-	-	5.04	0.0033	659
650	0.53	29.7	16.4	0.0175	-	-	12.9	0.0126	29.3	0.0301	1,027
651	0.53	127.6	10.9	0.0023	-	-	0.294	0.0002	11.2	0.0024	217
652	1.69	80.8	19.5	0.0606	-	-	12.0	0.0156	31.6	0.0762	2,413
653	1.69	49.2	25.6	0.0169	-	-	4.44	0.0082	30.0	0.0251	835
654	1.69	114.8	11.3	0.0139	-	-	5.73	0.0106	17.1	0.0245	1,437
655	1.55	238.6	-	-	-	-	55.7	0.184	55.7	0.184	3,307
656	1.50	89.3	36.2	0.0383	-	-	7.95	0.0135	44.1	0.0518	1,174
657	1.69	36.7	32.4	0.0280	-	-	4.29	-	36.7	0.0280	765
658	1.69	100.0	15.4	0.0101	-	-	13.2	0.0244	28.6	0.0346	1,210
659	1.17	128.5	3.79	0.0053	-	-	28.1	0.0440	31.9	0.0493	1,547
660	0.53	105.8	51.9	0.0542	-	-	50.5	0.0278	102	0.0820	800
661	1.69	359.3	0.0000	0.0000	-	-	180	0.333	180	0.333	1,852
662	0.53	50.9	33.8	0.0105	-	-	12.9	0.0054	46.7	0.0159	341
663	1.69	67.9	-	-	-	-	8.89	0.0328	8.89	0.0328	3,687
664	0.53	47.1	8.27	0.0088	-	-	37.8	0.0232	46.1	0.0320	694
665	1.68	127.9	26.1	0.0172	-	-	0.0431	0.0002	26.1	0.0174	664
666	0.53	84.8	23.8	0.0253	-	-	15.2	0.0140	39.0	0.0393	1,009
667	0.53	55.4	4.10	0.0044	-	-	11.2	0.0055	15.3	0.0098	642
668	1.69	88.1	26.5	0.0175	-	-	-	-	26.5	0.0175	659
669	0.53	200.2	30.8	0.0275	-	-	34.8	0.0203	65.7	0.0478	728
670	0.53	70.0	54.5	0.0537	-	-	13.3	0.0078	67.8	0.0614	905
671	0.53	390.2	7.52	0.0080	-	-	49.5	0.0356	57.0	0.0436	765
672	0.53	157.2	1.23	0.0008	-	-	0.0000	-	1.23	0.0008	680
673	1.69	148.8	3.90	0.0026	-	-	0.117	-	4.01	0.0026	640
674	0.52	184.1	96.9	0.0283	-	-	19.1	0.0110	116	0.0393	339
675	0.52	57.0	5.81	0.0018	6.72	0.0049	26.6	0.0153	39.1	0.0220	564
676	1.40	172.3	34.4	0.0227	-	-	68.7	0.127	103	0.150	1,452
677	1.69	143.3	-	-	-	-	11.4	0.0423	11.4	0.0423	3,704
678	1.69	180.4	3.59	0.0122	-	-	33.3	0.0617	36.9	0.0738	2,002
679	1.50	120.1	4.48	0.0030	-	-	2.19	0.0041	6.68	0.0070	1,051
680	1.69	212.4	26.4	0.0402	-	-	14.4	0.0266	40.7	0.0668	1,640
681	2.49	72.4	0.216	0.0007	-	-	-	-	0.216	0.0007	3,305
682	2.49	197.7	3.28	0.0023	-	-	-	-	3.28	0.0023	688
683	2.49	167.7	-	0.0033	-	-	87.9	-	87.9	0.0033	37.7
684	2.49	139.1	-	0.0012	-	-	32.7	-	32.7	0.0012	37.7
685	2.49	73.5	-	0.0011	-	-	29.3	-	29.3	0.0011	37.7
686	2.49	172.1	-	0.0007	-	-	17.3	-	17.3	0.0007	37.7
687	2.49	169.7	-	0.0013	-	-	35.4	-	35.4	0.0013	37.7
688	2.49	145.6	-	0.0010	-	-	26.8	-	26.8	0.0010	37.7
689	0.00	133.4	0.879	0.0018	-	-	36.0	0.0144	36.9	0.0162	438
690	2.49	193.6	7.56	0.0065	-	-	34.9	-	42.5	0.0065	154
691	2.49	71.0	-	0.0002	-	-	5.15	0.0000	5.15	0.0002	39.5
692	2.49	143.1	-	0.0001	-	-	1.91	-	1.91	0.0001	37.7
693	2.49	171.6	-	0.0000	-	-	0.517	-	0.517	0.0000	37.7
694	2.49	118.9	-	0.0001	-	-	1.90	-	1.90	0.0001	37.7
695	2.49	93.9	-	-	-	-	38.0	0.0960	38.0	0.0960	2,523
696	2.49	70.8	4.17	0.0223	-	-	16.1	0.0158	20.2	0.0381	1,881
697	1.19	99.6	36.7	0.0417	-	-	-	-	36.7	0.0417	1,136
698	1.19	85.7	22.8	0.0461	7.08	0.0216	-	-	29.9	0.0677	2,262
699	1.00	107.6	-	-	-	-	-	-	-	-	-
700	2.49	153.9	-	0.0024	-	-	66.7	0.0102	66.7	0.0126	189
701	2.49	143.5	-	0.0014	-	-	41.5	0.0124	41.5	0.0139	334
702	1.00	220.5	-	-	-	-	28.0	-	28.0	-	-
703	1.00	111.7	-	-	-	-	12.0	-	12.0	-	-
704	0.52	104.1	-	0.0001	-	-	8.08	-	8.08	0.0001	7.81
705	2.49	59.8	-	0.0001	-	-	41.2	-	41.2	0.0001	1.63
706	2.05	114.9	32.6	0.0468	-	-	1.52	-	34.2	0.0468	1,370
707	1.00	203.8	-	-	-	-	0.0675	-	0.0675	-	-
708	2.49	156.0	-	0.0005	-	-	12.8	-	12.8	0.0005	37.7
709	2.49	60.3	-	0.0000	-	-	1.03	-	1.03	0.0000	37.7
710	0.76	103.6	-	0.0000	-	-	0.0001	-	0.0001	0.0000	11.6
711	0.76	142.2	-	-	-	-	104	0.0684	104	0.0684	660
712	0.76	118.4	48.0	0.0101	-	-	14.0	0.0116	62.0	0.0218	351
713	0.23	122.4	39.1	0.0026	-	-	-	-	39.1	0.0026	66.7
714	0.23	96.1	79.6	0.0054	-	-	8.68	0.0022	88.3	0.0075	85.3
715	0.34	203.9	1.22	0.0003	-	-	88.2	0.0614	89.4	0.0617	690
716	0.34	213.7	30.4	0.0063	-	-	32.7	0.0122	63.1	0.0184	292
717	0.76	161.5	-	-	-	-	5.25	0.0044	5.25	0.0044	838
718	0.76	131.8	14.7	0.0044	-	-	4.83	0.0040	19.5	0.0084	432
719	0.76	147.8	77.1	0.0232	-	-	13.5	0.0065	90.6	0.0297	328
720	0.76	137.9	31.5	0.0097	-	-	-	-	31.5	0.0097	309
721	0.76	177.7	42.3	0.0144	-	-	1.67	0.0014	43.9	0.0158	359

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
722	1.19	218.9	22.6	0.0105	-	-	1.45	0.0019	24.1	0.0124	516
723	0.76	142.5	7.86	0.0268	12.6	0.0247	-	-	20.5	0.0515	2,513
724	0.76	45.7	14.9	0.0149	-	-	0.554	-	15.4	0.0149	968
725	1.19	87.9	-	-	15.2	0.0460	-	-	15.2	0.0460	3,022
726	1.19	81.3	-	-	11.0	0.0325	-	-	11.0	0.0325	2,943
727	1.19	135.2	0.361	0.0019	-	-	11.6	0.0152	12.0	0.0171	1,429
728	1.19	57.4	12.9	0.0688	-	-	-	-	12.9	0.0688	5,322
729	1.19	34.7	-	-	21.4	0.0654	3.19	0.0042	24.6	0.0696	2,829
730	0.80	77.3	10.6	0.0033	-	-	-	-	10.6	0.0033	313
731	1.19	28.8	0.501	0.0027	14.4	0.0441	-	-	14.9	0.0467	3,130
732	0.80	79.0	39.9	0.0347	-	-	33.6	0.0296	73.5	0.0643	875
733	0.80	125.1	29.2	0.0136	-	-	33.2	0.0292	62.4	0.0428	686
734	0.80	115.7	68.8	0.0585	-	-	8.08	0.0071	76.9	0.0656	853
735	0.76	59.0	13.0	0.0080	-	-	1.35	0.0011	14.4	0.0092	636
736	0.76	143.5	109	0.0333	-	-	-	-	109	0.0333	306
737	0.76	95.7	8.49	0.0018	-	-	46.2	0.0248	54.7	0.0266	486
738	0.52	80.1	23.8	0.0182	-	-	9.14	0.0052	32.9	0.0234	711
739	0.52	133.8	64.6	0.0120	-	-	31.1	0.0176	95.6	0.0296	309
740	0.52	143.1	38.7	0.0212	-	-	59.3	0.0335	98.0	0.0547	558
741	0.52	65.7	-	-	-	-	16.7	0.0141	16.7	0.0141	843
742	0.52	160.9	120	0.0151	-	-	0.685	0.0004	121	0.0154	128
743	0.76	168.3	-	-	0.0027	0.0000	168	0.0687	168	0.0687	410
744	0.76	101.5	87.2	0.0463	-	-	9.45	-	96.7	0.0463	479
745	0.76	233.8	56.3	0.0804	-	-	4.00	0.0034	60.3	0.0837	1,389
746	0.76	129.6	129	0.0513	-	-	-	-	129	0.0513	396
747	0.76	172.6	87.0	0.0638	-	-	3.36	-	90.4	0.0638	706
748	0.76	158.0	8.47	0.0033	-	-	16.6	0.0139	25.0	0.0172	686
749	0.76	69.7	56.8	0.0479	0.0980	0.0002	12.9	0.0108	69.7	0.0588	844
750	0.76	201.5	101	0.0840	72.5	0.139	10.8	0.0091	184	0.232	1,262
751	0.76	93.9	50.3	0.0150	-	-	0.0000	0.0000	50.3	0.0150	298
752	0.76	138.7	127	0.0498	-	-	1.37	0.0011	128	0.0509	397
753	0.76	172.6	-	-	23.3	0.0455	148	0.124	172	0.170	990
754	0.76	137.9	101	0.0341	-	-	-	-	101	0.0341	338
755	0.76	154.8	75.9	0.0263	0.257	0.0003	-	-	76.2	0.0266	349
756	0.76	121.2	23.7	0.0097	-	-	-	-	23.7	0.0097	410
757	0.76	175.5	54.7	0.0163	-	-	1.77	0.0015	56.5	0.0178	315
758	0.76	222.7	53.7	0.0191	-	-	1.93	0.0016	55.6	0.0207	372
759	0.34	259.4	-	-	-	-	62.5	0.0281	62.5	0.0281	450
760	0.34	119.9	-	-	-	-	79.8	0.0299	79.8	0.0299	374
761	1.95	479.9	51.2	0.0950	-	-	24.6	0.0692	75.9	0.164	2,164
762	0.34	197.7	-	-	-	-	157	0.107	157	0.107	684
763	2.29	202.9	9.54	0.0477	-	-	11.0	0.0101	20.5	0.0578	2,812
764	0.34	219.2	51.5	0.0442	-	-	27.8	0.0007	79.3	0.0449	567
765	0.34	95.5	7.43	0.0025	-	-	43.0	0.0300	50.4	0.0325	644
766	0.34	213.0	-	-	-	-	38.3	0.0235	38.3	0.0235	615
767	2.49	185.6	129	0.113	-	-	20.3	-	149	0.113	758
768	2.49	218.7	117	0.176	-	-	9.91	-	127	0.176	1,385
769	1.27	133.6	0.991	0.0015	-	-	22.0	0.0662	23.0	0.0677	2,946
770	2.49	261.8	-	-	-	-	47.2	0.109	47.2	0.109	2,320
771	2.49	111.3	103	0.190	-	-	2.61	0.0070	105	0.196	1,867
772	0.34	125.0	28.2	0.0058	-	-	-	-	28.2	0.0058	206
773	2.49	136.9	20.2	0.0303	-	-	0.554	-	20.8	0.0303	1,462
774	2.49	171.7	91.8	0.138	-	-	0.964	0.0000	92.8	0.138	1,487
775	0.52	134.0	80.8	0.0335	-	-	3.49	0.0019	84.2	0.0354	420
776	0.52	176.7	153	0.0383	-	-	19.0	0.0107	172	0.0490	285
777	0.52	209.9	116	0.0298	-	-	1.87	0.0011	118	0.0309	262
778	0.52	180.0	79.2	0.0183	-	-	16.4	0.0093	95.6	0.0276	289
779	0.52	157.1	-	-	-	-	81.8	0.0925	81.8	0.0925	1,131
780	0.52	127.9	8.96	0.0070	-	-	22.5	0.0127	31.5	0.0197	626
781	0.52	151.3	82.9	0.0648	-	-	65.7	0.0372	149	0.102	686
782	0.52	179.9	114	0.0163	-	-	29.1	0.0084	143	0.0247	173
783	0.52	121.9	99.5	0.0218	-	-	-	-	99.5	0.0218	219
784	0.34	101.5	-	-	-	-	20.0	0.0094	20.0	0.0094	470
785	0.34	36.6	-	-	-	-	23.5	0.0176	23.5	0.0176	749
786	0.34	72.4	22.6	0.0046	-	-	41.4	0.0131	64.0	0.0178	278
787	0.34	117.2	-	-	-	-	74.6	0.0559	74.6	0.0559	749
788	0.34	56.6	-	-	-	-	17.8	0.0133	17.8	0.0133	749
789	0.34	67.4	-	-	-	-	13.3	0.0100	13.3	0.0100	748
790	0.34	113.4	-	-	-	-	40.6	0.0299	40.6	0.0299	738
791	0.34	62.9	-	-	-	-	21.8	0.0152	21.8	0.0152	697
792	1.00	69.6	-	-	-	-	-	-	-	-	-
793	0.52	106.2	-	-	-	-	80.4	0.0846	80.4	0.0846	1,052
794	0.34	75.2	-	-	-	-	33.3	0.0240	33.3	0.0240	721
795	0.34	62.9	-	-	-	-	40.3	0.0293	40.3	0.0293	728
796	0.34	91.1	5.37	0.0011	-	-	-	-	5.37	0.0011	206
797	0.34	52.0	16.3	0.0034	-	-	0.860	-	17.1	0.0034	195
798	0.34	66.2	43.3	0.0089	-	-	22.0	-	65.2	0.0089	136
799	0.34	91.6	25.4	0.0052	-	-	2.00	-	27.4	0.0052	191
800	0.34	122.2	17.7	0.0036	-	-	3.59	-	21.3	0.0036	171
801	0.34	272.7	12.3	0.0025	-	-	-	-	12.3	0.0025	206
802	0.34	147.0	16.8	0.0035	-	-	-	-	16.8	0.0035	206
803	0.34	143.2	43.7	0.0090	-	-	-	-	43.7	0.0090	206
804	0.34	78.2	-	-	-	-	56.5	0.0212	56.5	0.0212	374
805	0.34	87.0	-	-	-	-	33.2	0.0210	33.2	0.0210	634
806	2.44	32.8	-	-	-	-	31.3	0.0970	31.3	0.0970	3,104
807	1.53	186.8	0.560	0.0028	-	-	21.4	0.0584	22.0	0.0612	2,789
808	2.49	120.8	91.4	0.184	-	-	7.47	0.0106	98.9	0.194	1,967
809	2.49	184.5	15.2	0.0761	-	-	18.9	0.0481	34.2	0.124	3,637
810	2.49	162.7	-	-	-	-	36.5	0.0949	36.5	0.0949	2,597
811	2.49	42.3	-	-	-	-	31.7	0.0863	31.7	0.0863	2,720
812	2.49	71.3	0.741	0.0011	-	-	10.4	0.0274	11.1	0.0285	2,555
813	2.49	100.0	60.6	0.195	-	-	7.35	0.0195	67.9	0.214	3,155
814	2.49	60.9	2.09	0.0031	-	-	44.4	0.121	46.5	0.124	2,676
815	0.76	127.9	88.1	0.0218	-	-	31.5	0.0264	120	0.0482	403
816	0.76	84.8	56.5	0.0145	4.92	0.0096	7.33	0.0040	68.7	0.0281	409
817	0.76	79.9	2.53	0.0007	31.9	0.0625	-	-	34.5	0.0632	1,835
818	0.76	97.3	54.7	0.0269	19.2	0.0375	4.78	0.0040	78.7	0.0685	870
819	0.76	200.2	113	0.0345	-	-	71.0	0.0424	184	0.0769	419
820	0.76	65.7	40.3	0.0085	-	-	19.2	0.0160	59.4	0.0245	413
821	0.76	390.2	292	0.0686	-	-	49.5	0.0234	341	0.0920	270
822	2.49	157.2	126	0.189	-	-	18.3	-	144	0.189	1,311
823	2.49	105.6	0.189	0.0003	-	-	82.6	-	82.8	0.0003	3.43
824	2.39	184.1	121	0.0998	-	-	52.7	0.144	174	0.244	1,400

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
825	2.49	57.0	18.6	0.0154	-	-	33.8	0.0025	52.4	0.0179	342
826	0.76	172.3	139	0.0318	-	-	-	-	139	0.0318	229
827	0.23	149.4	129	0.0083	-	-	8.01	0.0020	137	0.0103	75.6
828	0.76	180.4	164	0.0441	-	-	-	-	164	0.0441	269
829	0.76	158.1	77.2	0.0437	-	-	5.03	0.0000	82.2	0.0437	532
830	0.76	212.4	142	0.0989	-	-	-	-	142	0.0989	694
831	0.23	72.4	69.4	0.0044	-	-	-	-	69.4	0.0044	63.3
832	0.23	104.8	70.0	0.0050	-	-	16.6	0.0042	86.6	0.0092	106
833	0.23	108.7	52.0	0.0045	-	-	-	-	52.0	0.0045	87.0
834	2.05	139.1	70.4	0.0507	-	-	35.3	-	106	0.0507	479
835	0.80	234.4	0.786	0.0013	-	-	6.68	0.0059	7.46	0.0071	958
836	2.05	121.9	33.5	0.0415	-	-	13.7	0.0310	47.3	0.0725	1,533
837	2.05	222.5	133	0.0799	-	-	0.655	0.0015	134	0.0814	608
838	0.23	145.6	71.1	0.0053	-	-	-	-	71.1	0.0053	74.4
839	2.05	164.3	85.4	0.197	-	-	33.9	0.0764	119	0.274	2,295
840	2.05	121.3	72.4	0.162	-	-	8.47	0.0129	80.9	0.175	2,167
841	2.05	93.0	34.4	0.0758	-	-	25.6	0.0577	60.0	0.133	2,223
842	2.05	80.9	39.3	0.0934	-	-	-	-	39.3	0.0934	2,376
843	2.05	176.9	11.2	0.0462	-	-	19.4	0.0436	30.6	0.0898	2,937
844	2.05	167.1	72.8	0.175	-	-	0.0001	0.0000	72.8	0.175	2,410
845	2.05	71.4	20.4	0.0379	-	-	-	-	20.4	0.0379	1,861
846	2.05	70.8	68.9	0.168	-	-	0.232	-	69.1	0.168	2,425
847	1.97	205.6	76.2	0.0944	-	-	16.4	0.0132	92.6	0.108	1,162
848	2.05	278.0	26.5	0.0329	-	-	-	-	26.5	0.0329	1,238
849	2.05	79.0	25.4	0.0315	-	-	9.15	-	34.6	0.0315	910
850	0.76	155.8	56.5	0.0443	-	-	3.22	0.0000	59.7	0.0443	742
851	0.76	71.6	32.2	0.0196	-	-	0.0004	0.0000	32.2	0.0196	609
852	0.76	127.8	39.3	0.0181	-	-	22.4	0.0159	61.7	0.0340	552
853	0.76	179.8	57.6	0.0266	-	-	-	-	57.6	0.0266	461
854	0.76	162.3	38.7	0.0178	-	-	26.1	0.0219	64.8	0.0397	613
855	0.76	106.6	44.3	0.151	0.0009	0.0000	0.0084	-	44.3	0.151	3,408
856	0.76	68.9	64.6	0.0520	-	-	-	-	64.6	0.0520	805
857	0.76	145.8	27.5	0.0127	-	-	7.19	-	34.7	0.0127	365
858	0.76	89.4	26.2	0.0121	-	-	0.0008	-	26.2	0.0121	460
859	0.76	176.1	58.2	0.0268	-	-	0.297	-	58.5	0.0268	458
860	0.76	138.6	86.0	0.0394	-	-	7.38	-	93.4	0.0394	422
861	0.76	86.8	22.3	0.0103	-	-	12.7	-	35.0	0.0103	294
862	0.76	151.2	80.3	0.0187	2.26	0.0044	35.7	0.0092	118	0.0323	273
863	0.76	180.5	101	0.0225	-	-	8.49	0.0002	109	0.0226	207
864	0.76	65.0	-	-	0.0000	0.0000	62.7	0.0525	62.7	0.0525	838
865	0.76	161.3	7.04	0.0015	-	-	72.2	0.0388	79.3	0.0403	509
866	0.23	119.0	18.9	0.0012	-	-	-	-	18.9	0.0012	63.3
867	0.76	161.5	129	0.117	7.14	0.0076	18.5	-	154	0.125	807
868	0.76	89.9	85.3	0.0465	-	-	2.23	-	87.5	0.0465	532
869	0.76	147.8	113	0.0682	-	-	21.9	0.0054	135	0.0736	545
870	0.76	137.9	111	0.0237	-	-	25.3	0.0088	136	0.0326	239
871	0.76	40.0	15.5	0.0529	-	-	2.44	0.0020	18.0	0.0550	3,059
872	0.76	64.3	61.6	0.116	-	-	2.68	0.0022	64.3	0.118	1,837
873	0.76	122.9	29.1	0.0339	-	-	-	-	29.1	0.0339	1,165
874	0.76	62.2	43.4	0.0320	-	-	2.32	0.0019	45.7	0.0339	743
875	0.76	87.9	83.9	0.0370	-	-	0.508	0.0004	84.4	0.0375	444
876	0.76	36.7	35.5	0.0138	-	-	-	-	35.5	0.0138	390
877	0.76	109.6	63.4	0.0255	-	-	-	-	63.4	0.0255	403
878	0.76	57.4	57.3	0.0224	-	-	-	-	57.3	0.0224	392
879	0.76	59.4	34.5	0.0149	-	-	-	-	34.5	0.0149	433
880	0.76	49.1	37.8	0.0390	-	-	5.85	0.0001	43.6	0.0391	896
881	0.76	82.5	28.8	0.0354	-	-	0.0010	0.0000	28.8	0.0354	1,230
882	0.76	100.2	49.5	0.120	0.249	0.0003	-	-	49.7	0.121	2,424
883	0.76	62.2	44.7	0.0094	-	-	5.34	0.0000	50.0	0.0095	189
884	0.76	83.5	11.1	0.0026	42.4	0.0830	28.9	-	82.4	0.0857	1,040
885	0.76	47.1	10.9	0.0031	1.79	0.0035	20.6	0.0102	33.3	0.0168	504
886	0.76	52.7	-	-	0.148	0.0003	-	-	0.148	0.0003	1,957
887	0.76	47.8	-	-	0.0002	0.0000	19.4	0.0163	19.4	0.0163	838
888	0.76	77.7	0.0447	0.0000	77.7	0.152	-	-	77.7	0.152	1,956
889	0.76	133.8	28.4	0.0081	-	-	74.3	0.0402	103	0.0483	470
890	0.76	143.1	14.5	0.0093	5.17	0.0101	114	0.133	133	0.152	1,143
891	0.76	339.5	16.4	0.0104	-	-	3.40	0.0028	19.8	0.0132	669
892	0.76	63.6	34.1	0.0216	-	-	15.6	0.0131	49.7	0.0347	698
893	0.76	71.2	0.123	0.0000	-	-	70.4	0.0590	70.5	0.0590	837
894	0.76	66.7	-	-	-	-	65.0	0.0479	65.0	0.0479	738
895	0.76	233.8	97.5	0.0439	-	-	121	0.0815	219	0.125	572
896	0.76	96.7	3.64	0.0008	-	-	78.3	0.0656	82.0	0.0664	810
897	0.76	172.6	131	0.0347	-	-	2.47	0.0000	133	0.0347	261
898	2.39	74.2	-	-	-	-	70.8	0.193	70.8	0.193	2,725
899	2.49	55.0	41.3	0.0284	-	-	10.7	0.0194	51.9	0.0478	922
900	0.68	56.5	-	-	-	-	33.3	0.182	33.3	0.182	5,463
901	0.76	93.9	55.7	0.0353	-	-	37.3	0.0177	93.0	0.0530	570
902	2.41	176.0	43.6	0.0301	-	-	28.2	0.0567	71.8	0.0867	1,207
903	2.34	155.8	12.6	0.0170	7.42	0.0473	120	0.223	140	0.287	2,050
904	0.76	137.9	122	0.0261	-	-	-	-	122	0.0261	214
905	0.76	164.8	17.4	0.0044	-	-	2.30	0.0019	19.7	0.0063	322
906	0.76	52.9	40.6	0.0121	-	-	6.61	0.0055	47.2	0.0176	374
907	0.76	175.5	101	0.0507	12.9	0.0252	43.2	0.0362	157	0.112	713
908	0.76	222.7	3.49	0.0016	58.0	0.114	99.2	0.0831	161	0.198	1,234
909	0.76	83.8	79.0	0.0173	-	-	-	-	79.0	0.0173	219
910	0.76	104.1	12.5	0.0026	-	-	83.0	0.0611	95.6	0.0637	667
911	0.76	54.6	49.3	0.0147	-	-	-	-	49.3	0.0147	298
912	0.76	116.7	74.2	0.0263	-	-	21.5	-	95.8	0.0263	275
913	0.76	202.9	139	0.0678	-	-	1.62	0.0011	141	0.0688	489
914	0.76	166.7	105	0.0841	2.86	0.0030	14.2	0.0119	122	0.0991	809
915	0.76	95.5	40.9	0.0163	2.75	0.0029	44.1	0.0370	87.8	0.0562	640
916	0.76	50.5	16.7	0.0050	-	-	-	-	16.7	0.0050	298
917	0.76	191.2	106	0.0316	-	-	40.2	0.0260	146	0.0575	395
918	0.76	122.0	54.1	0.0341	-	-	-	-	54.1	0.0341	630
919	0.76	133.6	120	0.0342	1.83	0.0036	7.21	0.0060	129	0.0438	340
920	0.76	128.8	96.9	0.0447	-	-	3.66	0.0031	101	0.0478	475
921	0.80	70.1	62.4	0.0210	-	-	7.12	0.0063	69.5	0.0273	392
922	0.80	125.0	80.7	0.0391	-	-	38.3	0.0292	119	0.0684	575
923	0.76	136.9	135	0.0413	-	-	0.0001	0.0000	135	0.0413	306
924	0.92	72.3	45.4	0.0286	-	-	-	-	45.4	0.0286	630
925	0.92	134.0	108	0.0748	-	-	16.3	0.0165	125	0.0914	734
926	0.80	97.3	63.1	0.0264	-	-	26.0	0.0229	89.1	0.0493	553
927	0.80	198.6	61.1	0.0208	-	-	0.446	0.0004	61.6	0.0212	345

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
928	0.76	86.6	23.2	0.0280	-	-	33.2	0.0263	56.4	0.0543	962
929	0.76	159.4	57.0	0.0216	-	-	0.236	0.0002	57.2	0.0218	381
930	0.92	131.2	36.2	0.0324	-	-	5.45	0.0055	41.7	0.0379	910
931	0.92	47.6	9.37	0.0137	-	-	30.6	0.0310	40.0	0.0447	1,118
932	0.80	62.9	14.4	0.0152	-	-	-	-	14.4	0.0152	1,054
933	0.80	94.5	51.0	0.0264	-	-	16.3	0.0143	67.3	0.0407	605
934	1.00	28.7	2.58	0.0052	2.93	0.0075	21.4	0.0235	26.9	0.0361	1,345
935	0.76	78.8	33.6	0.0281	-	-	0.0001	-	33.6	0.0281	837
936	1.19	36.0	-	-	-	-	36.0	0.0471	36.0	0.0471	1,308
937	0.93	101.2	-	-	-	-	29.1	0.0380	29.1	0.0380	1,308
938	0.76	56.6	3.26	0.0021	30.8	0.0601	-	-	34.0	0.0622	1,828
939	1.19	35.6	11.9	0.0635	17.7	0.0542	-	-	29.7	0.118	3,967
940	0.76	32.3	15.3	0.0060	-	-	-	-	15.3	0.0060	394
941	0.76	62.9	0.0023	0.0000	0.0002	0.0000	61.1	0.0471	61.1	0.0471	770
942	0.76	45.1	-	-	-	-	36.6	0.0284	36.6	0.0284	775
943	0.76	28.4	9.36	0.0036	-	-	2.99	0.0025	12.4	0.0062	498
944	0.76	57.3	-	-	-	-	57.3	0.0481	57.3	0.0481	838
945	0.76	17.0	-	-	-	-	4.81	0.0040	4.81	0.0040	838
946	0.76	19.4	12.8	0.0150	-	-	6.57	0.0055	19.4	0.0205	1,057
947	0.76	39.1	0.0021	0.0000	-	-	36.8	0.0257	36.8	0.0257	700
948	0.76	159.5	38.6	0.0153	-	-	0.0326	0.0000	38.7	0.0153	395
949	0.76	131.3	84.2	0.0535	-	-	6.18	0.0030	90.3	0.0566	626
950	1.19	46.2	-	-	14.8	0.0454	-	-	14.8	0.0454	3,055
951	2.05	272.7	182	0.329	-	-	74.1	0.1000	256	0.429	1,679
952	0.76	27.1	-	-	15.5	0.0303	-	-	15.5	0.0303	1,957
953	0.76	39.8	-	-	22.4	0.0438	-	-	22.4	0.0438	1,957
954	0.76	42.9	-	-	35.9	0.0703	-	-	35.9	0.0703	1,957
955	1.19	152.9	38.3	0.0475	-	-	3.54	0.0046	41.8	0.0521	1,246
956	1.19	84.8	6.10	0.0325	-	-	2.69	0.0035	8.79	0.0360	4,094
957	1.19	91.6	89.0	0.143	-	-	2.44	-	91.5	0.143	1,559
958	0.76	32.4	-	-	26.7	0.0518	-	-	26.7	0.0518	1,942
959	1.19	96.7	-	-	14.3	0.0435	0.161	0.0002	14.4	0.0437	3,031
960	1.19	26.5	12.8	0.0385	9.98	0.0305	0.0160	0.0000	22.8	0.0690	3,021
961	1.19	7.6	-	-	6.88	0.0209	0.164	0.0002	7.05	0.0211	2,999
962	1.19	37.0	29.8	0.120	-	-	6.53	0.0085	36.4	0.129	3,533
963	0.76	164.7	90.9	0.0511	-	-	0.0151	0.0000	90.9	0.0511	562
964	0.76	41.2	0.0056	0.0000	-	-	27.0	0.0167	27.0	0.0167	616
965	0.92	32.3	31.9	0.0150	-	-	0.168	0.0002	32.1	0.0152	474
966	0.76	23.9	-	-	-	-	13.1	0.0110	13.1	0.0110	838
967	0.76	141.4	2.99	0.0012	-	-	32.8	0.0275	35.8	0.0286	800
968	0.76	97.3	-	-	-	-	93.0	0.0779	93.0	0.0779	838
969	0.76	69.8	-	-	-	-	64.1	0.0537	64.1	0.0537	838
970	0.76	31.4	-	-	-	-	2.62	0.0022	2.62	0.0022	838
971	0.92	156.4	29.3	0.0390	-	-	0.266	0.0003	29.6	0.0393	1,329
972	2.05	52.4	16.0	0.0126	-	-	1.21	-	17.2	0.0126	735
973	1.19	105.6	97.3	0.0906	-	-	3.43	0.0045	101	0.0951	945
974	1.19	124.2	122	0.0628	-	-	1.27	0.0017	124	0.0645	522
975	1.19	71.0	-	-	-	-	23.6	0.0309	23.6	0.0309	1,308
976	0.80	60.3	11.0	0.0084	-	-	28.7	0.0253	39.7	0.0336	848
977	0.80	149.4	130	0.0654	-	-	10.2	0.0090	140	0.0744	532
978	0.80	98.8	89.1	0.0330	-	-	7.51	0.0066	96.6	0.0396	410
979	0.76	135.6	17.1	0.0222	5.64	0.0110	31.3	0.0262	54.0	0.0594	1,100
980	0.76	105.7	98.2	0.0307	-	-	2.18	0.0018	100	0.0325	324
981	0.76	36.4	36.1	0.0141	-	-	0.0008	0.0000	36.1	0.0141	390
982	0.76	104.8	85.6	0.0293	-	-	13.2	0.0111	98.8	0.0404	409
983	0.76	76.9	45.5	0.0320	-	-	26.0	0.0218	71.5	0.0538	753
984	0.76	67.8	-	-	-	-	64.8	0.0543	64.8	0.0543	838
985	0.92	104.2	28.7	0.0104	-	-	-	-	28.7	0.0104	360
986	0.92	78.2	54.9	0.0253	-	-	-	-	54.9	0.0253	461
987	0.80	154.5	126	0.0611	-	-	7.60	0.0021	133	0.0632	475
988	0.80	82.2	51.6	0.0294	-	-	6.44	0.0057	58.1	0.0351	605
989	0.80	164.3	118	0.149	-	-	22.5	0.0198	141	0.169	1,197
990	0.76	114.9	85.5	0.0658	14.1	0.0151	0.788	-	100	0.0808	805
991	0.76	48.8	27.1	0.0104	-	-	11.2	-	38.3	0.0104	271
992	0.76	197.8	40.6	0.0312	-	-	1.51	0.0010	42.1	0.0322	764
993	2.49	92.3	16.4	0.169	10.9	0.0377	0.499	-	27.7	0.207	7,462
994	0.52	92.3	-	-	-	-	4.24	0.0024	4.24	0.0024	566
995	0.52	158.1	-	-	-	-	57.5	0.0651	57.5	0.0651	1,131
996	0.52	46.0	4.41	0.0019	-	-	-	-	4.41	0.0019	428
997	0.52	173.2	61.8	0.0104	-	-	8.80	0.0050	70.6	0.0154	218
998	0.52	39.5	25.2	0.0140	-	-	1.02	0.0006	26.2	0.0146	556
999	0.34	20.6	15.3	0.0032	-	-	-	-	15.3	0.0032	206
1000	0.34	28.4	-	-	-	-	24.8	0.0093	24.8	0.0093	374
1001	0.34	57.9	-	-	-	-	57.9	0.0217	57.9	0.0217	374
1002	0.34	45.1	-	-	-	-	45.1	0.0338	45.1	0.0338	749
1003	0.34	23.8	-	-	-	-	23.8	0.0172	23.8	0.0172	723
1004	1.00	7.6	-	-	-	-	0.625	-	0.625	-	-
1005	2.05	1.1	1.06	0.0013	-	-	-	-	1.06	0.0013	1,238
1006	2.05	11.5	5.56	0.0069	-	-	5.97	-	11.5	0.0069	599
1007	1.00	16.7	16.7	0.0065	-	-	-	-	16.7	0.0065	390
1008	0.76	89.4	-	-	73.5	0.144	11.6	0.0097	85.1	0.153	1,804
1009	0.76	108.8	91.7	0.0194	-	-	-	-	91.7	0.0194	211
1010	0.76	34.1	22.6	0.0048	-	-	-	-	22.6	0.0048	211
1011	0.76	36.7	14.6	0.0031	-	-	-	-	14.6	0.0031	211
1012	0.76	19.5	8.56	0.0118	-	-	7.82	-	16.4	0.0118	721
1013	0.76	2.7	2.73	0.0011	-	-	-	-	2.73	0.0011	390
1014	1.19	19.2	2.96	0.0124	12.0	0.0365	2.42	0.0031	17.3	0.0520	3,002
1015	0.80	133.6	104	0.0472	-	-	11.6	0.0102	116	0.0574	495
1016	0.80	76.2	34.4	0.0348	-	-	40.3	0.0355	74.6	0.0702	941
1017	1.19	11.8	-	-	-	-	11.8	0.0154	11.8	0.0154	1,308
1018	1.19	9.9	5.22	0.0278	4.73	0.0144	-	-	9.95	0.0422	4,245
1019	1.19	80.4	-	-	10.7	0.0327	44.6	0.0581	55.3	0.0908	1,642
1020	0.76	6.3	2.05	0.0008	-	-	2.78	0.0023	4.83	0.0031	648
1021	1.00	-	-	-	-	-	-	-	-	-	-
1022	0.76	17.9	8.50	0.0084	-	-	7.69	0.0039	16.2	0.0123	758
1023	0.34	122.9	90.0	0.0185	-	-	1.01	-	91.0	0.0185	204
1024	0.08	62.2	28.0	0.0058	-	-	0.518	-	28.6	0.0058	202
1025	2.49	11.9	-	0.0000	-	-	2.55	0.0066	2.55	0.0066	2,588
1026	0.34	28.5	2.28	0.0005	-	-	6.06	-	8.34	0.0005	56.2
1027	2.49	109.6	61.3	0.0921	-	-	17.9	0.0488	79.2	0.141	1,779
1028	2.49	25.7	0.106	0.0002	-	-	16.6	0.0095	16.7	0.0097	577
1029	2.49	59.4	0.363	0.0006	-	-	4.79	-	5.15	0.0006	123
1030	2.49	28.5	0.598	0.0013	-	-	14.9	-	15.5	0.0013	83.2

Table E-1. Average Dry Weather Flows by Land Use Area - Existing Conditions (2006)

Land Use Polygon ID	ADWF Calibration Factor	Gross Acreage	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
			Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
1031	2.49	82.5	45.8	0.0687	-	-	36.7	-	82.5	0.0687	834
1032	2.49	42.3	16.6	0.0250	-	-	25.6	-	42.3	0.0250	592
1033	2.49	62.2	25.3	0.0380	-	-	5.54	-	30.9	0.0380	1,232
1034	2.49	46.5	43.1	0.0696	-	-	0.0002	0.0000	43.1	0.0696	1,616
1035	2.03	47.1	0.0001	0.0000	-	-	45.1	0.123	45.1	0.123	2,732
1036	1.37	52.7	-	-	-	-	50.2	0.197	50.2	0.197	3,924
1037	2.05	43.7	33.2	0.0636	-	-	3.51	0.0079	36.7	0.0715	1,950
1038	0.76	41.4	-	-	-	-	25.0	0.0204	25.0	0.0204	814
1039	2.05	121.5	71.0	0.0405	-	-	17.6	0.0395	88.5	0.0800	904
1040	1.00	-	-	-	-	-	-	-	-	-	-
1041	0.76	8.4	7.28	0.0015	-	-	-	-	7.28	0.0015	211
1042	2.05	58.0	44.4	0.0860	-	-	0.0054	-	44.4	0.0860	1,937
1043	2.05	18.1	18.1	0.0103	-	-	-	-	18.1	0.0103	568
1044	2.05	39.0	37.8	0.0246	-	-	-	-	37.8	0.0246	650
1045	2.05	92.0	91.4	0.0519	-	-	-	-	91.4	0.0519	568
1046	2.49	69.7	-	0.0006	-	-	14.9	-	14.9	0.0006	37.7
1047	1.00	68.4	-	-	-	-	0.0215	-	0.0215	-	-
1048	2.05	62.2	50.3	0.0285	-	-	-	-	50.3	0.0285	568
1049	2.49	24.0	-	0.0003	-	-	8.69	-	8.69	0.0003	37.7
1050	2.05	56.5	52.1	0.0320	-	-	-	-	52.1	0.0320	613
1051	2.49	36.2	-	0.0004	-	-	11.7	-	11.7	0.0004	37.7
1052	1.00	176.0	33.4	0.0102	-	-	62.1	-	95.4	0.0102	106
1053	1.00	76.9	2.11	0.0004	-	-	0.0001	-	2.11	0.0004	166
1054	1.00	-	-	-	-	-	-	-	-	-	-
1055	0.55	164.8	-	-	-	-	158	0.207	158	0.207	1,308
1056	2.49	35.1	22.2	0.0333	-	-	7.27	-	29.5	0.0333	1,131
9999	2.49	173.2	88.4	0.1327	-	-	5.43	0.000	93.8	0.1327	1,415

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
0									
1	25.9	0.0389	-	-	7.04	-	33.0	0.0389	1,181
2	44.5	0.154	-	-	25.8	0.0536	70.2	0.207	2,953
3	-	-	-	-	-	-	-	-	-
4	21.0	0.0797	-	-	-	-	21.0	0.0797	3,800
5	-	-	-	-	0.963	0.0036	0.963	0.0036	3,779
6	28.3	0.0371	-	-	46.6	0.0264	74.9	0.0635	847
7	74.0	0.0394	-	-	40.0	0.0461	114	0.0855	749
8	15.5	0.0022	-	-	-	-	15.5	0.0022	143
9	-	-	-	-	-	-	-	-	-
10	-	-	-	-	-	-	-	-	-
11	9.66	0.0367	-	-	7.94	0.0291	17.6	0.0658	3,736
12	11.9	0.0248	-	-	26.1	0.116	37.9	0.141	3,704
13	86.9	0.323	-	-	0.0015	0.0000	86.9	0.323	3,719
14	0.338	0.0004	-	-	4.87	0.0043	5.21	0.0046	891
15	-	-	-	-	62.9	0.176	62.9	0.176	2,800
16	45.7	0.0415	-	-	13.2	0.0129	58.9	0.0544	924
17	41.8	0.0251	-	-	85.4	0.0503	127	0.0754	593
18	-	-	-	-	33.9	0.187	33.9	0.187	5,502
19	6.92	0.0124	-	-	17.3	-	24.2	0.0124	514
20	-	-	-	-	16.7	0.122	16.7	0.122	7,315
21	-	-	-	-	5.75	0.0102	5.75	0.0102	1,769
22	47.1	0.179	-	-	-	-	47.1	0.179	3,800
23	39.4	0.150	-	-	-	-	39.4	0.150	3,800
24	-	-	-	-	0.766	0.0010	0.766	0.0010	1,343
25	-	-	-	-	2.10	0.0199	2.10	0.0199	9,500
26	-	-	-	-	1.10	0.0104	1.10	0.0104	9,426
27	-	-	-	-	-	-	-	-	-
28	0.159	0.0006	-	-	0.587	0.0065	0.747	0.0071	9,500
29	6.36	0.0242	-	-	(3.8134)	-	2.54	0.0242	9,500
30	1.76	0.0067	-	-	(1.0581)	-	0.705	0.0067	9,500
31	7.79	0.0296	-	-	(4.0067)	0.0063	3.78	0.0359	9,500
32	3.66	0.0139	-	-	(2.1953)	-	1.46	0.0139	9,500
33	6.78	0.0257	-	-	(4.0649)	0.0000	2.71	0.0257	9,500
34	0.0000	0.0000	-	-	3.66	0.0348	3.66	0.0348	9,500
35	-	-	-	-	7.05	0.0068	7.05	0.0068	964
36	-	-	-	-	9.14	0.0017	9.14	0.0017	182
37	-	-	-	-	429	0.743	429	0.743	1,731
38	-	-	-	-	24.7	0.0436	24.7	0.0436	1,769
39	-	-	-	-	34.6	0.0379	34.6	0.0379	1,098
40	-	-	-	-	23.5	0.0837	23.5	0.0837	3,561
41	-	-	-	-	36.4	0.0183	36.4	0.0183	503
42	64.3	0.0365	-	-	0.297	0.0007	64.6	0.0372	575
43	-	-	-	-	-	-	-	-	-
44	0.0490	0.0002	-	-	19.2	0.0211	19.2	0.0213	1,106
45	0.0002	0.0000	-	-	46.8	0.0514	46.8	0.0514	1,100
46	7.37	0.0280	-	-	-	-	7.37	0.0280	3,800
47	-	-	-	-	8.58	0.0168	8.58	0.0168	1,955
48	244	0.0730	-	-	-	-	244	0.0730	299
49	45.7	0.0127	-	-	9.82	0.0094	55.5	0.0220	397
50	10.1	0.0073	-	-	121	0.0942	131	0.102	772
51	2.82	0.0008	-	-	41.9	0.0084	44.7	0.0091	204
52	-	-	-	-	49.2	0.0242	49.2	0.0242	493
53	-	-	-	-	25.2	0.0135	25.2	0.0135	537
54	0.686	0.0001	-	-	199	0.0015	199	0.0016	8
55	29.4	0.112	-	-	8.37	0.0306	37.8	0.142	3,769
56	4.18	0.0159	-	-	7.20	0.0263	11.4	0.0422	3,711
57	58.7	0.178	1.20	0.0017	63.8	0.183	124	0.363	2,932
58	13.5	0.0145	-	-	0.0065	0.0000	13.5	0.0145	1,073
59	9.02	0.0343	-	-	0.0004	0.0000	9.02	0.0343	3,800
60	32.6	0.112	-	-	-	-	32.6	0.112	3,440
61	-	-	-	-	5.84	0.0064	5.84	0.0064	1,098
62	-	-	-	-	28.4	0.0311	28.4	0.0311	1,098
63	-	-	-	-	9.04	0.0099	9.04	0.0099	1,098
64	-	-	-	-	5.13	0.0031	5.13	0.0031	597
65	0.0067	0.0000	-	-	23.3	0.0139	23.3	0.0139	598
66	139	0.0449	-	-	1.00	0.0011	140	0.0460	328
67	73.6	0.0284	-	-	-	-	73.6	0.0284	385
68	44.1	0.0130	-	-	0.0050	0.0000	44.1	0.0130	294
69	-	-	-	-	33.3	0.0366	33.3	0.0366	1,098
70	-	-	8.98	0.0230	-	-	8.98	0.0230	2,563
71	30.7	0.0085	-	-	3.59	0.0000	34.3	0.0085	248
72	2.36	0.0007	-	-	8.03	0.0088	10.4	0.0095	913
73	50.3	0.0734	-	-	0.0004	0.0000	50.3	0.0734	1,458
74	6.80	0.0019	-	-	-	-	6.80	0.0019	277
75	-	-	-	-	-	-	-	-	-
76	21.9	0.0832	-	-	-	-	21.9	0.0832	3,800
77	41.4	0.157	-	-	-	-	41.4	0.157	3,795
78	23.8	0.0904	-	-	0.0342	0.0001	23.9	0.0906	3,794
79	10.9	0.0119	-	-	6.80	0.0041	17.7	0.0160	903
80	1.15	0.0047	-	-	-	-	1.15	0.0047	4,076
81	16.5	0.0331	-	-	2.37	0.0026	18.8	0.0358	1,898
82	-	-	7.03	0.0181	7.36	-	14.4	0.0181	1,255
83	-	-	-	-	12.6	0.0098	12.6	0.0098	777
84	22.7	0.0204	17.8	0.0457	3.84	-	44.3	0.0661	1,493
85	-	-	-	-	41.4	0.0454	41.4	0.0454	1,098
86	-	-	-	-	2.89	0.0017	2.89	0.0017	597
87	21.2	0.0807	-	-	-	-	21.2	0.0807	3,800
88	-	-	-	-	-	-	-	-	-
89	9.66	0.0367	-	-	-	-	9.66	0.0367	3,800
90	31.0	0.118	-	-	-	-	31.0	0.118	3,800
91	0.0265	0.0001	-	-	0.0018	0.0000	0.0283	0.0001	3,800
92	13.3	0.0506	-	-	-	-	13.3	0.0506	3,800
93	31.5	0.0089	-	-	-	-	31.5	0.0089	284
94	6.36	0.0242	-	-	-	-	6.36	0.0242	3,800

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
95	-	-	-	-	116	0.880	116	0.880	7,600
96	1.63	0.0062	-	-	12.9	0.0488	14.5	0.0550	3,800
97	33.9	0.129	-	-	4.32	0.0164	38.3	0.145	3,800
98	14.4	0.0548	-	-	-	-	14.4	0.0548	3,800
99	-	-	-	-	1.22	0.0034	1.22	0.0034	2,744
100	10.6	0.0404	-	-	0.203	0.0002	10.8	0.0406	3,749
101	-	-	-	-	32.1	0.122	32.1	0.122	3,800
102	-	-	-	-	-	-	-	-	-
103	-	-	-	-	46.0	0.175	46.0	0.175	3,800
104	-	-	-	-	94.2	0.512	94.2	0.512	5,429
105	31.2	0.118	-	-	163	0.933	194	1.05	5,429
106	-	-	24.8	0.0636	0.0909	-	24.9	0.0636	2,558
107	3.48	0.0010	-	-	60.9	0.0687	64.4	0.0697	1,082
108	4.98	0.0014	-	-	1.66	-	6.65	0.0014	208
109	18.9	0.0152	-	-	91.1	0.100	110	0.115	1,049
110	6.93	0.0088	-	-	39.7	0.0001	46.6	0.0089	191
111	18.2	0.0300	-	-	15.8	0.0152	34.0	0.0451	1,329
112	0.618	0.0002	-	-	-	-	0.618	0.0002	277
113	59.1	0.0258	-	-	13.1	-	72.2	0.0258	357
114	14.5	0.0040	-	-	-	-	14.5	0.0040	277
115	5.94	0.0021	-	-	0.946	-	6.89	0.0021	300
116	14.5	0.0293	-	-	21.5	0.0169	36.0	0.0462	1,282
117	15.4	0.0043	-	-	13.0	-	28.4	0.0043	150
118	33.1	0.0317	-	-	8.16	-	41.3	0.0317	768
119	73.2	0.0331	-	-	49.0	0.0539	122	0.0870	712
120	14.6	0.0040	-	-	0.171	-	14.7	0.0040	274
121	31.0	0.0397	-	-	-	-	31.0	0.0397	1,279
122	15.3	0.0115	-	-	18.7	0.0205	34.0	0.0320	942
123	27.1	0.0082	-	-	5.57	-	32.7	0.0082	251
124	30.9	0.0086	-	-	0.796	-	31.7	0.0086	270
125	13.1	0.0036	-	-	3.14	-	16.2	0.0036	223
126	17.3	0.0048	-	-	0.0048	-	17.3	0.0048	277
127	31.9	0.0090	-	-	0.864	-	32.8	0.0090	276
128	23.3	0.0280	-	-	13.8	0.0152	37.1	0.0432	1,164
129	23.7	0.0066	-	-	10.4	0.0114	34.1	0.0180	527
130	20.5	0.0095	-	-	-	-	20.5	0.0095	462
131	-	-	17.2	0.0440	9.71	0.0059	26.9	0.0499	1,857
132	35.7	0.0168	9.49	0.0244	1.92	-	47.1	0.0412	873
133	14.1	0.0117	39.0	0.100	1.62	-	54.8	0.112	2,043
134	11.9	0.0033	-	-	0.997	-	12.9	0.0033	256
135	16.2	0.0045	-	-	1.12	-	17.4	0.0045	259
136	33.2	0.0092	-	-	-	-	33.2	0.0092	277
137	27.7	0.0130	-	-	-	-	27.7	0.0130	472
138	18.2	0.0050	-	-	2.51	-	20.7	0.0050	244
139	95.8	0.0645	25.2	0.0645	9.00	0.0011	130	0.130	1,001
140	14.7	0.0081	-	-	-	-	14.7	0.0081	554
141	3.52	0.0010	-	-	9.63	0.0106	13.1	0.0116	880
142	33.7	0.0093	-	-	-	-	33.7	0.0093	277
143	67.3	0.0321	5.63	0.0084	-	-	72.9	0.0405	555
144	15.6	0.0160	87.5	0.225	19.7	0.0216	123	0.262	2,136
145	27.7	0.0115	1.85	0.0026	1.08	-	30.6	0.0141	459
146	10.9	0.0030	0.193	0.0005	1.50	-	12.6	0.0035	279
147	21.3	0.0286	5.45	0.0076	10.1	0.0062	36.9	0.0424	1,151
148	1.20	0.0003	2.32	0.0059	1.84	-	5.36	0.0063	1,171
149	7.64	0.0089	8.60	0.0221	1.45	-	17.7	0.0310	1,753
150	13.3	0.0143	-	-	18.1	0.0199	31.4	0.0342	1,088
151	28.0	0.0371	-	-	20.5	0.0226	48.5	0.0597	1,229
152	21.1	0.0058	-	-	4.95	0.0054	26.0	0.0113	434
153	4.13	0.0011	-	-	-	-	4.13	0.0011	277
154	9.14	0.0025	-	-	-	-	9.14	0.0025	277
155	35.5	0.0098	-	-	-	-	35.5	0.0098	277
156	22.6	0.0063	-	-	-	-	22.6	0.0063	277
157	8.07	0.0047	7.11	0.0183	-	-	15.2	0.0229	1,511
158	54.4	0.128	0.503	0.0007	3.59	0.0039	58.5	0.133	2,270
159	126	0.0359	-	-	4.09	0.0045	130	0.0404	311
160	203	0.0658	-	-	11.2	0.0124	214	0.0782	365
161	32.3	0.0090	-	-	-	-	32.3	0.0090	277
162	98.2	0.0860	-	-	-	-	98.2	0.0860	875
163	182	0.122	2.29	0.0032	3.12	-	187	0.125	671
164	86.3	0.0337	-	-	-	-	86.3	0.0337	391
165	63.8	0.0251	-	-	-	-	63.8	0.0251	394
166	90.0	0.0236	-	-	33.7	0.0201	124	0.0438	354
167	-	-	-	-	0.0004	0.0000	0.0004	0.0000	597
168	-	-	-	-	31.9	0.0190	31.9	0.0190	597
169	112	0.108	-	-	9.73	0.0058	122	0.114	932
170	-	-	-	-	153	0.0916	153	0.0916	597
171	27.7	0.0086	-	-	-	-	27.7	0.0086	311
172	37.3	0.0142	-	-	-	-	37.3	0.0142	382
173	75.9	0.0364	-	-	-	-	75.9	0.0364	479
174	76.0	0.0330	-	-	-	-	76.0	0.0330	435
175	100	0.0386	-	-	8.95	0.0098	109	0.0485	445
176	24.7	0.0097	-	-	-	-	24.7	0.0097	391
177	14.6	0.0065	-	-	2.41	0.0030	17.0	0.0095	562
178	80.1	0.0863	-	-	24.7	0.0345	105	0.121	1,152
179	60.2	0.0183	-	-	-	-	60.2	0.0183	305
180	42.7	0.0255	-	-	3.88	0.0043	46.6	0.0297	638
181	53.4	0.0665	-	-	86.5	0.0645	140	0.131	937
182	-	-	-	-	24.9	0.0185	24.9	0.0185	746
183	0.0000	0.0000	-	-	22.7	0.0169	22.7	0.0169	746
184	22.9	0.0309	-	-	0.315	0.0007	23.2	0.0315	1,360
185	54.5	0.0206	-	-	14.6	0.0118	69.1	0.0324	470
186	-	-	-	-	117	0.0984	117	0.0984	839
187	-	-	-	-	21.0	0.0230	21.0	0.0230	1,100
188	40.5	0.0207	-	-	1.18	-	41.7	0.0207	497
189	34.2	0.0208	-	-	4.94	-	39.1	0.0208	532

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
190	38.7	0.0210	-	-	2.22	-	41.0	0.0210	512
191	32.3	0.0650	-	-	29.8	0.0448	62.0	0.110	1,770
192	-	-	-	-	49.7	0.0547	49.7	0.0547	1,100
193	36.1	0.0303	-	-	5.72	-	41.8	0.0303	725
194	35.0	0.0180	-	-	9.11	-	44.1	0.0180	409
195	19.1	0.0100	-	-	1.91	-	21.0	0.0100	479
196	48.7	0.0176	-	-	3.43	-	52.2	0.0176	337
197	31.4	0.0364	-	-	8.37	-	39.8	0.0364	915
198	10.9	0.0026	-	-	-	-	10.9	0.0026	242
199	-	-	-	-	16.3	0.0275	16.3	0.0275	1,690
200	18.8	0.0112	-	-	-	-	18.8	0.0112	595
201	50.6	0.0149	-	-	-	-	50.6	0.0149	294
202	-	-	-	-	83.7	0.0920	83.7	0.0920	1,099
203	-	-	-	-	87.0	0.0934	87.0	0.0934	1,073
204	-	-	5.39	0.0138	-	-	5.39	0.0138	2,568
205	-	-	57.3	0.147	2.84	0.0000	60.1	0.147	2,447
206	-	-	68.2	0.177	11.2	-	79.4	0.177	2,229
207	0.146	0.0003	0.146	0.0004	54.8	0.109	55.1	0.110	1,993
208	-	-	28.2	0.0734	3.79	-	32.0	0.0734	2,289
209	-	-	16.0	0.0411	4.69	-	20.7	0.0411	1,986
210	95.8	0.410	4.18	0.0107	32.3	0.0000	132	0.421	3,181
211	-	-	-	-	-	-	-	-	-
212	-	-	98.6	0.253	-	-	98.6	0.253	2,568
213	-	-	26.0	0.0668	-	-	26.0	0.0668	2,568
214	46.5	0.0350	17.6	0.0451	20.4	0.0054	84.5	0.0855	1,011
215	-	-	60.3	0.155	2.86	-	63.2	0.155	2,452
216	23.4	0.0256	-	-	0.0006	0.0000	23.4	0.0256	1,093
217	23.7	0.0050	-	-	93.9	0.0561	118	0.0611	520
218	0.0058	0.0000	0.0061	0.0000	26.1	0.0573	26.1	0.0573	2,199
219	8.59	0.0027	33.0	0.0846	22.7	0.0187	64.2	0.106	1,651
220	4.36	0.0088	49.6	0.123	5.34	-	59.3	0.132	2,226
221	27.7	0.105	-	-	19.7	0.0217	47.4	0.127	2,670
222	63.3	0.238	43.0	0.0821	52.6	0.0571	159	0.377	2,372
223	0.278	0.0012	0.920	0.0013	14.6	0.0117	15.8	0.0141	898
224	-	-	-	-	32.8	0.0247	32.8	0.0247	755
225	56.5	0.0192	-	-	0.0003	0.0000	56.5	0.0192	340
226	7.32	0.0023	-	-	64.0	0.0354	71.3	0.0377	529
227	18.7	0.0097	0.0041	0.0000	-	-	18.7	0.0097	517
228	31.6	0.0109	-	-	-	-	31.6	0.0109	344
229	17.4	0.0119	-	-	-	-	17.4	0.0119	682
230	61.2	0.0921	-	-	-	-	61.2	0.0921	1,505
231	-	-	-	-	61.7	0.0679	61.7	0.0679	1,100
232	-	-	-	-	0.0083	0.0000	0.0083	0.0000	547
233	65.5	0.0457	-	-	10.6	0.0063	76.2	0.0521	684
234	45.0	0.0096	-	-	6.61	0.0039	51.7	0.0135	262
235	-	-	-	-	73.4	0.0438	73.4	0.0438	597
236	-	-	-	-	55.2	0.0619	55.2	0.0619	1,122
237	57.8	0.0124	-	-	44.2	0.0268	102	0.0392	384
238	51.5	0.0099	-	-	0.262	0.0002	51.7	0.0101	195
239	69.8	0.0219	-	-	73.0	0.0436	143	0.0655	459
240	60.9	0.0129	-	-	0.0001	0.0000	60.9	0.0129	212
241	158	0.0266	-	-	-	-	158	0.0266	168
242	161	0.0501	-	-	-	-	161	0.0501	311
243	119	0.0428	-	-	2.04	0.0024	121	0.0452	372
244	187	0.0800	-	-	-	-	187	0.0800	428
245	193	0.0698	-	-	8.32	0.0091	202	0.0789	391
246	159	0.0442	0.464	0.0004	13.8	0.0103	173	0.0550	317
247	207	0.0470	-	-	10.9	0.0103	218	0.0572	263
248	42.4	0.0747	-	-	61.6	0.0459	104	0.121	1,160
249	31.4	0.141	0.701	0.0010	0.0011	0.0000	32.1	0.142	4,428
250	16.0	0.0704	-	-	1.37	0.0015	17.4	0.0719	4,139
251	10.0	0.0072	-	-	38.6	0.0425	48.6	0.0497	1,021
252	83.3	0.0463	-	-	8.29	0.0091	91.6	0.0554	604
253	41.7	0.0641	-	-	92.8	0.102	134	0.166	1,236
254	33.1	0.0130	-	-	19.8	0.0217	52.9	0.0347	656
255	28.5	0.0157	-	-	19.0	0.0209	47.5	0.0366	770
256	20.9	0.0376	-	-	6.46	0.0071	27.3	0.0448	1,637
257	59.0	0.0871	-	-	13.3	0.0146	72.3	0.102	1,407
258	-	-	3.10	0.0043	49.0	0.0694	52.1	0.0737	1,415
259	0.0013	0.0000	6.52	0.0168	4.09	0.0092	10.6	0.0260	2,447
260	0.0828	0.0002	-	-	218	-	219	0.0002	1
261	61.5	0.275	-	-	3.23	-	64.8	0.275	4,249
262	113	0.0802	-	-	9.59	0.0105	123	0.0908	740
263	139	0.125	-	-	0.518	0.0006	140	0.125	899
264	69.1	0.181	-	-	27.4	0.0307	96.5	0.212	2,194
265	33.9	0.0439	-	-	7.61	0.0145	41.5	0.0584	1,409
266	32.9	0.0249	-	-	-	-	32.9	0.0249	757
267	68.6	0.0843	-	-	0.972	0.0005	69.6	0.0848	1,219
268	23.3	0.129	10.5	0.0332	21.2	0.0300	55.0	0.192	3,486
269	46.0	0.119	-	-	33.6	0.0456	79.6	0.165	2,074
270	20.9	0.0809	-	-	2.82	-	23.7	0.0809	3,412
271	70.7	0.130	-	-	0.0711	0.0001	70.8	0.130	1,835
272	-	-	-	-	53.9	0.0593	53.9	0.0593	1,100
273	-	-	-	-	23.1	0.0226	23.1	0.0226	979
274	39.9	0.178	-	-	54.3	0.0570	94.1	0.235	2,500
275	13.2	0.0589	-	-	3.42	0.0038	16.6	0.0627	3,776
276	31.7	0.110	79.1	0.187	37.3	0.0410	148	0.338	2,283
277	-	-	36.2	0.0928	-	-	36.2	0.0928	2,568
278	0.0010	0.0000	-	-	26.3	0.0741	26.3	0.0741	2,821
279	56.6	0.0608	-	-	0.370	0.0005	57.0	0.0613	1,076
280	88.8	0.0111	-	-	14.5	0.0050	103	0.0161	156
281	12.2	0.0048	-	-	35.1	0.0386	47.3	0.0434	917
282	28.9	0.0346	-	-	-	-	28.9	0.0346	1,196
283	50.0	0.0195	-	-	18.0	0.0198	68.0	0.0394	578
284	50.8	0.0412	-	-	49.4	0.0668	100	0.108	1,077

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
285	105	0.0412	-	-	16.4	0.0180	121	0.0592	489
286	49.8	0.0558	-	-	29.3	0.0323	79.1	0.0880	1,112
287	9.40	0.0037	-	-	-	-	9.40	0.0037	391
288	24.6	0.0092	-	-	27.1	0.0298	51.7	0.0390	755
289	46.0	0.0152	-	-	3.50	0.0038	49.5	0.0191	385
290	91.2	0.0194	-	-	0.0003	0.0000	91.2	0.0194	213
291	33.1	0.0208	-	-	9.78	0.0034	42.8	0.0242	565
292	83.9	0.0189	-	-	8.21	0.0028	92.1	0.0217	236
293	-	-	-	-	38.1	0.0131	38.1	0.0131	344
294	8.55	0.0054	-	-	21.4	0.0139	29.9	0.0193	646
295	30.7	0.0389	-	-	3.68	0.0040	34.4	0.0429	1,248
296	12.8	0.0050	-	-	17.1	0.0188	29.9	0.0238	797
297	106	0.0279	-	-	45.4	0.0180	151	0.0458	303
298	54.0	0.0211	-	-	-	-	54.0	0.0211	391
299	41.4	0.0162	-	-	17.0	0.0187	58.4	0.0349	597
300	0.368	0.0002	-	-	17.7	0.0084	18.0	0.0087	480
301	79.4	0.0460	-	-	6.17	0.0068	85.6	0.0528	617
302	49.2	0.0704	-	-	9.11	0.0100	58.3	0.0805	1,381
303	61.2	0.0564	-	-	14.3	0.0158	75.5	0.0722	956
304	53.9	0.0520	-	-	8.41	0.0092	62.3	0.0613	984
305	96.7	0.138	2.40	0.0062	9.70	0.0107	109	0.155	1,422
306	96.4	0.0401	-	-	17.0	-	113	0.0401	354
307	67.9	0.0513	-	-	15.8	0.0125	83.7	0.0638	762
308	30.8	0.0433	-	-	-	-	30.8	0.0433	1,405
309	28.7	0.0107	-	-	-	-	28.7	0.0107	374
310	36.0	0.0164	-	-	2.66	-	38.7	0.0164	425
311	133	0.0571	-	-	11.5	0.0126	144	0.0697	483
312	54.1	0.0277	-	-	-	-	54.1	0.0277	512
313	86.4	0.115	-	-	-	-	86.4	0.115	1,331
314	67.5	0.0408	-	-	15.3	0.0000	82.8	0.0408	492
315	70.8	0.0369	-	-	31.2	-	102	0.0369	362
316	101	0.0530	-	-	4.54	-	105	0.0530	503
317	91.0	0.0516	-	-	14.8	-	106	0.0516	488
318	116	0.0828	-	-	29.5	0.0000	146	0.0828	567
319	118	0.0866	-	-	-	-	118	0.0866	731
320	32.0	0.0156	-	-	-	-	32.0	0.0156	487
321	108	0.0856	-	-	4.10	0.0056	112	0.0912	813
322	59.2	0.0166	-	-	-	-	59.2	0.0166	281
323	23.3	0.0469	-	-	-	-	23.3	0.0469	2,013
324	56.5	0.0246	-	-	13.9	0.0152	70.3	0.0398	567
325	173	0.0563	-	-	8.68	0.0105	182	0.0668	368
326	118	0.0390	-	-	5.05	0.0055	123	0.0445	362
327	215	0.101	-	-	32.8	0.0270	248	0.128	514
328	115	0.0803	-	-	-	-	115	0.0803	701
329	102	0.0531	-	-	4.31	0.0082	106	0.0613	578
330	25.6	0.0276	-	-	21.1	0.0232	46.7	0.0508	1,089
331	72.3	0.0278	-	-	0.0001	0.0000	72.3	0.0278	385
332	53.9	0.0211	-	-	3.49	0.0038	57.4	0.0249	434
333	137	0.0919	-	-	8.27	0.0091	145	0.101	697
334	57.5	0.0681	-	-	5.35	0.0059	62.9	0.0740	1,176
335	33.7	0.0302	-	-	0.937	0.0010	34.6	0.0312	902
336	51.3	0.0309	-	-	6.85	0.0075	58.2	0.0385	661
337	124	0.0712	-	-	7.18	0.0076	132	0.0788	599
338	69.6	0.0990	-	-	7.23	0.0000	76.8	0.0990	1,289
339	33.3	0.0441	-	-	15.4	0.0222	48.7	0.0663	1,362
340	21.7	0.0116	-	-	20.9	0.0230	42.6	0.0346	812
341	77.7	0.0304	-	-	-	-	77.7	0.0304	391
342	91.1	0.0476	-	-	23.8	0.0261	115	0.0738	642
343	60.4	0.0726	1.22	0.0039	0.572	0.0008	62.1	0.0772	1,243
344	85.7	0.136	-	-	5.15	0.0069	90.9	0.143	1,571
345	134	0.0757	44.7	0.115	7.61	0.0000	186	0.190	1,024
346	25.1	0.0362	-	-	18.3	0.0154	43.4	0.0516	1,189
347	105	0.0451	-	-	16.1	0.0000	121	0.0451	373
348	33.2	0.0892	0.0001	0.0000	23.9	0.0556	57.1	0.145	2,536
349	19.4	0.0296	-	-	21.6	0.0246	40.9	0.0542	1,323
350	33.6	0.0317	-	-	3.94	0.0046	37.6	0.0363	967
351	30.2	0.0662	5.34	0.0137	52.7	0.0787	88.2	0.159	1,798
352	79.4	0.104	-	-	-	-	79.4	0.104	1,310
353	58.6	0.0233	-	-	-	-	58.6	0.0233	398
354	66.3	0.0328	-	-	-	-	66.3	0.0328	495
355	169	0.0661	-	-	3.79	0.0042	173	0.0703	407
356	29.0	0.0114	-	-	0.0002	0.0000	29.0	0.0114	391
357	20.5	0.0080	-	-	-	-	20.5	0.0080	391
358	28.2	0.0205	-	-	-	-	28.2	0.0205	728
359	6.32	0.0025	-	-	0.0001	0.0000	6.32	0.0025	391
360	60.6	0.0358	-	-	0.0000	0.0000	60.6	0.0358	591
361	29.2	0.0117	-	-	-	-	29.2	0.0117	401
362	89.5	0.0464	-	-	2.37	0.0027	91.9	0.0491	535
363	64.8	0.0225	-	-	-	-	64.8	0.0225	347
364	40.5	0.107	-	-	35.8	0.0282	76.2	0.135	1,776
365	74.4	0.0240	-	-	1.26	-	75.6	0.0240	317
366	24.0	0.0094	-	-	9.08	0.0100	33.1	0.0194	586
367	5.48	0.0245	49.2	0.103	126	0.163	181	0.291	1,609
368	128	0.133	4.75	0.0046	3.96	0.0008	136	0.138	1,014
369	9.98	0.0033	1.28	0.0033	1.44	-	12.7	0.0066	522
370	79.1	0.0957	11.6	0.0297	15.8	0.0155	107	0.141	1,323
371	-	-	-	-	18.6	0.0576	18.6	0.0576	3,093
372	-	-	-	-	24.2	0.0266	24.2	0.0266	1,098
373	-	-	-	-	75.0	0.0823	75.0	0.0823	1,098
374	36.8	0.0506	-	-	4.19	0.0046	41.0	0.0552	1,346
375	41.8	0.0233	-	-	9.58	0.0005	51.3	0.0238	463
376	12.3	0.0034	-	-	7.79	0.0086	20.0	0.0120	597
377	28.3	0.0494	-	-	5.14	-	33.4	0.0494	1,478
378	21.5	0.0060	-	-	-	-	21.5	0.0060	277
379	-	-	96.7	0.248	4.87	0.0028	102	0.251	2,468

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
380	61.6	0.0540	13.2	0.0339	45.9	0.0667	121	0.155	1,281
381	32.1	0.0645	-	-	-	-	32.1	0.0645	2,010
382	0.269	0.0005	-	-	88.7	0.0974	89.0	0.0979	1,100
383	52.2	0.0359	-	-	4.39	0.0051	56.5	0.0410	726
384	77.2	0.0151	-	-	-	-	77.2	0.0151	196
385	9.02	0.0025	-	-	0.0004	0.0000	9.02	0.0025	277
386	22.6	0.0123	-	-	19.5	0.0215	42.1	0.0338	802
387	47.7	0.0101	-	-	13.4	0.0080	61.1	0.0181	296
388	16.0	0.0024	-	-	-	-	16.0	0.0024	151
389	2.62	0.0009	-	-	55.2	0.0607	57.8	0.0616	1,065
390	31.1	0.0433	0.0063	0.0000	23.0	0.0189	54.1	0.0622	1,149
391	18.9	0.0380	-	-	33.1	0.0364	52.0	0.0744	1,431
392	38.4	0.0774	-	-	0.0017	0.0000	38.4	0.0774	2,013
393	24.7	0.0261	-	-	43.3	0.0462	68.0	0.0723	1,063
394	79.2	0.0414	-	-	15.7	0.0144	95.0	0.0558	588
395	90.6	0.0391	-	-	28.1	0.0413	119	0.0803	677
396	37.8	0.0960	-	-	2.62	0.0024	40.4	0.0984	2,437
397	33.0	0.0094	-	-	0.0187	0.0001	33.0	0.0095	288
398	68.4	0.0238	-	-	0.0352	0.0000	68.5	0.0238	348
399	18.3	0.0051	-	-	-	-	18.3	0.0051	277
400	36.2	0.0112	-	-	12.0	-	48.2	0.0112	233
401	22.8	0.0376	6.69	0.0172	-	-	29.5	0.0548	1,859
402	41.8	0.0116	-	-	15.3	-	57.2	0.0116	203
403	-	-	-	-	25.1	0.0150	25.1	0.0150	597
404	-	-	-	-	37.3	0.0353	37.3	0.0353	948
405	-	-	-	-	23.6	0.0259	23.6	0.0259	1,098
406	71.3	0.0511	-	-	17.1	0.0188	88.4	0.0699	790
407	257	0.158	-	-	22.0	0.0483	279	0.206	739
408	111	0.0566	-	-	17.2	-	128	0.0566	441
409	77.7	0.0537	25.3	0.0650	8.63	0.0041	112	0.123	1,101
410	-	-	54.2	0.139	-	-	54.2	0.139	2,568
411	28.8	0.0080	76.9	0.198	-	-	106	0.206	1,944
412	-	-	-	-	255	0.280	255	0.280	1,098
413	-	-	-	-	111	0.122	111	0.122	1,098
414	-	-	-	-	15.1	0.0166	15.1	0.0166	1,100
415	-	-	-	-	22.8	0.0233	22.8	0.0233	1,021
416	-	-	12.4	0.0318	139	0.302	152	0.334	2,205
417	-	-	11.3	0.0291	19.1	-	30.4	0.0291	955
418	-	-	9.31	0.0239	1.72	-	11.0	0.0239	2,167
419	7.48	0.0066	47.1	0.121	24.4	-	79.0	0.128	1,616
420	25.9	0.0359	10.7	0.0275	2.14	-	38.8	0.0635	1,637
421	-	-	29.0	0.0744	0.349	-	29.3	0.0744	2,537
422	-	-	1.63	0.0042	134	0.123	135	0.127	937
423	23.6	0.0066	-	-	0.905	-	24.5	0.0066	267
424	14.3	0.0040	-	-	-	-	14.3	0.0040	277
425	12.3	0.0034	-	-	-	-	12.3	0.0034	277
426	24.9	0.0069	-	-	-	-	24.9	0.0069	277
427	19.3	0.0054	-	-	3.86	-	23.2	0.0054	231
428	14.4	0.0040	-	-	10.0	0.0110	24.4	0.0150	614
429	11.3	0.0031	-	-	-	-	11.3	0.0031	277
430	6.32	0.0018	-	-	0.309	-	6.63	0.0018	264
431	-	-	-	-	0.396	0.0004	0.396	0.0004	1,100
432	-	-	-	-	97.3	0.107	97.3	0.107	1,098
433	50.8	0.0810	38.5	0.0987	14.9	-	104	0.180	1,726
434	121	0.0456	-	-	-	-	121	0.0456	376
435	93.8	0.0345	-	-	0.116	0.0001	93.9	0.0346	369
436	7.18	0.0028	-	-	-	-	7.18	0.0028	391
437	10.7	0.0215	-	-	5.79	0.0173	16.5	0.0389	2,359
438	135	0.0889	-	-	9.99	0.0116	145	0.101	694
439	90.1	0.0136	-	-	-	-	90.1	0.0136	151
440	81.1	0.0140	-	-	-	-	81.1	0.0140	172
441	115	0.0181	-	-	-	-	115	0.0181	158
442	74.2	0.0258	-	-	-	-	74.2	0.0258	348
443	134	0.221	-	-	5.64	0.0066	140	0.227	1,622
444	48.5	0.0175	-	-	-	-	48.5	0.0175	361
445	77.5	0.0358	-	-	-	-	77.5	0.0358	462
446	44.4	0.169	-	-	-	-	44.4	0.169	3,800
447	-	-	-	-	-	-	-	-	-
448	54.1	0.206	-	-	91.5	0.338	146	0.544	3,733
449	17.4	0.0661	-	-	2.51	0.0065	19.9	0.0727	3,650
450	280	0.127	-	-	-	-	280	0.127	452
451	122	0.0471	0.0000	0.0000	-	-	122	0.0471	387
452	80.4	0.0285	1.71	0.0024	1.44	0.0000	83.6	0.0309	370
453	27.5	0.0093	-	-	-	-	27.5	0.0093	338
454	28.2	0.0110	-	-	0.0000	0.0000	28.2	0.0110	391
455	24.4	0.0726	-	-	24.1	0.0265	48.5	0.0990	2,043
456	33.1	0.0399	-	-	-	-	33.1	0.0399	1,207
457	-	-	-	-	-	-	-	-	-
458	-	-	-	-	55.9	0.0614	55.9	0.0614	1,098
459	-	-	-	-	21.1	0.0802	21.1	0.0802	3,800
460	-	-	-	-	26.1	0.0140	26.1	0.0140	537
461	69.0	0.262	-	-	(59.5908)	0.0136	9.44	0.276	29,231
462	7.80	0.0297	-	-	87.1	0.123	94.9	0.152	1,607
463	7.12	0.0028	-	-	0.828	0.0025	7.94	0.0053	664
464	12.0	0.0064	-	-	0.0338	0.0001	12.0	0.0065	544
465	73.4	0.279	-	-	(47.5093)	0.0024	25.9	0.281	10,857
466	-	-	12.1	0.0152	4.27	0.0023	16.3	0.0174	1,067
467	20.5	0.0091	-	-	5.53	0.0038	26.0	0.0129	498
468	15.5	0.0046	-	-	42.4	0.0515	58.0	0.0560	966
469	47.8	0.0271	-	-	35.0	0.0390	82.8	0.0661	799
470	3.85	0.0021	-	-	2.16	-	6.01	0.0021	342
471	-	-	-	-	6.45	0.0035	6.45	0.0035	537
472	-	-	-	-	24.3	0.0603	24.3	0.0603	2,479
473	2.15	0.0008	-	-	40.3	0.153	42.5	0.154	3,626
474	0.553	0.0002	-	-	13.2	0.0501	13.7	0.0503	3,662

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	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
475	13.1	0.0046	-	-	0.0000	0.0000	13.1	0.0046	352
476	41.9	0.0155	-	-	0.0028	0.0000	41.9	0.0155	369
477	29.4	0.0116	-	-	0.0486	0.0002	29.4	0.0118	400
478	-	-	-	-	27.5	0.105	27.5	0.105	3,800
479	-	-	-	-	-	-	-	-	-
480	36.5	0.0163	-	-	9.31	0.0165	45.8	0.0327	715
481	38.6	0.0134	-	-	1.25	0.0012	39.9	0.0147	368
482	12.3	0.0043	-	-	36.8	0.0360	49.2	0.0403	820
483	29.1	0.0131	-	-	30.0	0.0161	59.2	0.0292	494
484	7.23	0.0025	-	-	-	-	7.23	0.0025	349
485	9.16	0.0159	-	-	2.02	-	11.2	0.0159	1,422
486	9.85	0.0034	-	-	0.448	-	10.3	0.0034	333
487	12.4	0.0043	-	-	-	-	12.4	0.0043	348
488	18.6	0.0028	-	-	8.89	0.0087	27.5	0.0114	416
489	30.1	0.0058	-	-	0.0021	0.0000	30.1	0.0059	195
490	46.2	0.0161	-	-	6.14	0.0007	52.4	0.0168	320
491	2.27	0.0008	-	-	17.3	0.0169	19.6	0.0177	905
492	0.720	0.0003	-	-	11.1	-	11.8	0.0003	21
493	15.4	0.0054	-	-	-	-	15.4	0.0054	348
494	61.4	0.0214	-	-	10.7	0.0001	72.1	0.0214	297
495	23.4	0.0081	-	-	2.49	-	25.9	0.0081	314
496	13.4	0.0047	-	-	0.0020	0.0000	13.4	0.0047	348
497	13.1	0.0045	-	-	0.414	-	13.5	0.0045	337
498	16.5	0.0057	-	-	0.0038	-	16.5	0.0057	348
499	13.4	0.0082	-	-	6.20	0.0061	19.6	0.0142	726
500	3.84	0.0018	-	-	14.6	-	18.4	0.0018	97
501	30.3	0.0098	-	-	0.0398	0.0000	30.3	0.0098	323
502	31.4	0.0109	-	-	0.0063	0.0000	31.4	0.0109	348
503	23.6	0.0082	-	-	0.549	0.0000	24.1	0.0082	340
504	17.9	0.0062	-	-	6.48	0.0000	24.4	0.0062	255
505	15.1	0.0135	-	-	-	-	15.1	0.0135	892
506	14.4	0.0148	-	-	0.0002	-	14.4	0.0148	1,027
507	18.3	0.0305	-	-	-	-	18.3	0.0305	1,665
508	35.9	0.0644	-	-	5.58	0.0014	41.5	0.0658	1,585
509	-	-	-	-	49.2	0.314	49.2	0.314	6,382
510	0.256	0.0010	-	-	33.0	0.196	33.2	0.197	5,919
511	20.8	0.0790	-	-	1.71	0.0009	22.5	0.0799	3,551
512	-	-	-	-	134	0.237	134	0.237	1,769
513	1.69	0.0055	-	-	4.33	0.0077	6.02	0.0131	2,180
514	5.02	0.0049	-	-	92.6	-	97.7	0.0049	51
515	15.5	0.0067	4.82	0.0060	14.0	-	34.3	0.0128	372
516	31.2	0.0445	-	-	8.04	-	39.3	0.0445	1,133
517	14.9	0.0067	-	-	9.31	0.0000	24.3	0.0067	275
518	17.1	0.0214	-	-	1.92	0.0000	19.1	0.0214	1,122
519	36.8	0.0331	-	-	9.71	0.0172	46.6	0.0503	1,079
520	24.8	0.0218	-	-	-	-	24.8	0.0218	878
521	38.2	0.0442	-	-	0.0065	0.0000	38.2	0.0442	1,157
522	36.2	0.0161	-	-	15.1	0.0266	51.3	0.0428	834
523	14.2	0.0387	-	-	-	-	14.2	0.0387	2,728
524	28.1	0.0135	-	-	-	-	28.1	0.0135	479
525	47.6	0.0212	-	-	-	-	47.6	0.0212	446
526	31.7	0.0141	-	-	-	-	31.7	0.0141	446
527	36.2	0.0161	-	-	-	-	36.2	0.0161	446
528	17.2	0.0422	-	-	0.833	-	18.0	0.0422	2,341
529	38.2	0.0219	-	-	3.67	-	41.9	0.0219	524
530	13.3	0.0096	-	-	0.333	-	13.7	0.0096	702
531	39.9	0.0279	-	-	12.7	0.0177	52.6	0.0456	867
532	14.0	0.0062	-	-	1.63	-	15.6	0.0062	399
533	12.0	0.0090	-	-	2.62	-	14.6	0.0090	617
534	5.34	0.0173	-	-	24.8	0.0004	30.2	0.0177	587
535	-	-	4.71	0.0059	24.9	0.0134	29.6	0.0193	651
536	-	-	-	-	28.2	0.0152	28.2	0.0152	537
537	-	-	-	-	32.5	0.0224	32.5	0.0224	692
538	-	-	8.41	0.0119	-	-	8.41	0.0119	1,419
539	6.70	0.0215	-	-	14.4	0.0249	21.1	0.0463	2,192
540	6.10	0.0196	-	-	-	-	6.10	0.0196	3,206
541	38.8	0.0660	-	-	1.86	-	40.6	0.0660	1,624
542	10.2	0.0290	15.3	0.0633	2.12	0.0038	27.7	0.0961	3,470
543	-	-	-	-	5.40	0.0029	5.40	0.0029	537
544	-	-	10.5	0.0131	3.89	0.0021	14.4	0.0152	1,061
545	2.62	0.0026	3.70	0.0046	3.42	0.0018	9.74	0.0091	930
546	-	-	22.8	0.0286	0.555	0.0003	23.3	0.0289	1,238
547	-	-	19.6	0.0247	1.70	0.0009	21.3	0.0256	1,198
548	-	-	35.6	0.0447	-	-	35.6	0.0447	1,255
549	11.6	0.0114	-	-	6.11	0.0031	17.7	0.0145	819
550	-	-	6.98	0.0088	-	-	6.98	0.0088	1,255
551	-	-	26.1	0.0328	-	-	26.1	0.0328	1,255
552	-	-	31.6	0.0397	-	-	31.6	0.0397	1,255
553	-	-	25.3	0.0317	-	-	25.3	0.0317	1,255
554	6.40	0.0009	9.27	0.0116	0.0001	0.0000	15.7	0.0125	798
555	16.1	0.0022	6.41	0.0080	-	-	22.5	0.0102	454
556	0.142	0.0001	9.01	0.0113	-	-	9.15	0.0114	1,251
557	35.3	0.0211	-	-	1.72	0.0000	37.0	0.0211	571
558	6.16	0.0199	-	-	41.3	0.0634	47.4	0.0833	1,756
559	63.5	0.0382	-	-	13.8	-	77.2	0.0382	495
560	43.2	0.0193	-	-	9.98	0.0176	53.2	0.0369	694
561	18.3	0.0082	-	-	-	-	18.3	0.0082	446
562	24.0	0.0248	-	-	-	-	24.0	0.0248	1,037
563	84.0	0.107	-	-	-	-	84.0	0.107	1,275
564	39.6	0.0272	-	-	4.57	0.0003	44.2	0.0275	623
565	22.2	0.0126	-	-	3.59	0.0020	25.7	0.0146	566
566	52.8	0.0480	-	-	26.4	0.0466	79.2	0.0946	1,195
567	-	-	-	-	-	-	-	-	-
568	6.11	0.0019	-	-	3.13	-	9.24	0.0019	203
569	-	-	30.5	0.0382	-	-	30.5	0.0382	1,255

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
570	-	-	-	-	25.5	0.0969	25.5	0.0969	3,800
571	5.56	0.0025	-	-	0.160	0.0006	5.72	0.0031	536
572	33.0	0.0584	-	-	17.7	0.115	50.7	0.173	3,407
573	43.4	0.0901	-	-	9.62	0.0206	53.0	0.111	2,088
574	66.5	0.0709	-	-	2.12	0.0024	68.6	0.0733	1,069
575	6.18	0.0016	-	-	-	-	6.18	0.0016	253
576	13.9	0.0048	-	-	0.0004	-	13.9	0.0048	348
577	9.06	0.0032	-	-	0.0015	0.0000	9.06	0.0032	348
578	-	-	4.52	0.0057	-	-	4.52	0.0057	1,255
579	41.5	0.105	-	-	0.0014	0.0000	41.5	0.105	2,536
580	56.6	0.0529	-	-	12.4	0.0173	69.0	0.0702	1,017
581	68.7	0.0642	-	-	52.3	0.0482	121	0.112	929
582	24.2	0.0062	-	-	0.0054	-	24.2	0.0062	255
583	-	-	15.1	0.0189	-	-	15.1	0.0189	1,255
584	18.6	0.0668	17.5	0.0722	-	-	36.1	0.139	3,854
585	25.0	0.0276	-	-	0.0306	-	25.1	0.0276	1,101
586	-	-	28.7	0.0360	-	-	28.7	0.0360	1,255
587	-	-	-	-	75.1	0.0417	75.1	0.0417	555
588	47.8	0.0118	-	-	60.8	0.0664	109	0.0782	720
589	38.9	0.0123	-	-	88.7	0.251	128	0.263	2,064
590	2.24	0.0010	-	-	1.70	0.0023	3.94	0.0033	842
591	7.06	0.0069	15.2	0.0190	5.95	0.0032	28.2	0.0292	1,036
592	12.2	0.0023	-	-	-	-	12.2	0.0023	191
593	-	-	-	-	11.9	0.0452	11.9	0.0452	3,800
594	-	-	-	-	6.68	0.0254	6.68	0.0254	3,800
595	-	-	-	-	4.21	0.0160	4.21	0.0160	3,800
596	-	-	-	-	0.985	0.0037	0.985	0.0037	3,800
597	-	-	-	-	-	-	-	-	-
598	1.13	0.0043	-	-	-	-	1.13	0.0043	3,800
599	0.0172	0.0001	-	-	9.71	0.0369	9.73	0.0370	3,800
600	-	-	-	-	-	-	-	-	-
601	-	-	-	-	38.4	0.146	38.4	0.146	3,800
602	-	-	-	-	27.9	0.106	27.9	0.106	3,800
603	1.59	0.0048	-	-	89.1	0.327	90.7	0.331	3,653
604	2.29	0.0087	-	-	-	-	2.29	0.0087	3,800
605	-	-	-	-	-	-	-	-	-
606	0.0055	0.0000	-	-	1.22	0.0046	1.23	0.0046	3,783
607	-	-	-	-	10.8	0.0411	10.8	0.0411	3,800
608	-	-	-	-	7.91	0.0301	7.91	0.0301	3,800
609	-	-	-	-	2.07	0.0079	2.07	0.0079	3,800
610	2.65	0.0101	-	-	5.60	0.0213	8.25	0.0314	3,800
611	2.91	0.0111	-	-	0.0000	0.0000	2.91	0.0111	3,800
612	-	-	-	-	9.48	0.0360	9.48	0.0360	3,800
613	-	-	-	-	35.6	0.135	35.6	0.135	3,800
614	-	-	-	-	30.3	0.115	30.3	0.115	3,800
615	24.1	0.0913	-	-	28.6	0.109	52.7	0.200	3,796
616	-	-	-	-	-	-	-	-	-
617	-	-	-	-	-	-	-	-	-
618	47.1	0.0132	-	-	(42.3551)	-	4.71	0.0132	2,801
619	1.05	0.0007	-	-	11.2	0.0207	12.2	0.0214	1,750
620	10.2	0.0021	-	-	2.40	0.0014	12.6	0.0035	276
621	36.1	0.0253	3.68	0.0027	19.5	0.0128	59.2	0.0408	689
622	17.7	0.0036	-	-	19.8	0.0114	37.5	0.0150	401
623	8.41	0.0017	-	-	-	-	8.41	0.0017	205
624	22.6	0.0046	-	-	0.797	0.0005	23.4	0.0051	218
625	-	-	-	-	35.4	0.232	35.4	0.232	6,554
626	-	-	-	-	4.62	0.0176	4.62	0.0176	3,800
627	-	-	-	-	27.7	0.105	27.7	0.105	3,800
628	-	-	-	-	0.483	0.0035	0.483	0.0035	7,318
629	1.17	0.0002	-	-	-	-	1.17	0.0002	207
630	-	-	-	-	4.61	0.0088	4.61	0.0088	1,900
631	3.65	0.0124	-	-	19.6	0.0710	23.2	0.0834	3,590
632	2.22	0.0013	-	-	11.3	0.0374	13.5	0.0386	2,850
633	2.51	0.0073	-	-	-	-	2.51	0.0073	2,907
634	50.8	0.0255	-	-	0.0001	0.0000	50.8	0.0255	502
635	13.8	0.0028	-	-	7.84	0.0298	21.6	0.0326	1,507
636	25.3	0.0162	-	-	16.4	0.0353	41.8	0.0514	1,231
637	29.5	0.0124	-	-	5.79	0.0033	35.3	0.0157	446
638	25.3	0.0090	-	-	6.78	0.0078	32.1	0.0168	524
639	7.41	0.0078	-	-	9.81	0.0126	17.2	0.0204	1,186
640	30.9	0.0326	2.39	0.0018	27.2	0.0234	60.5	0.0578	955
641	18.8	0.0069	-	-	0.565	0.0003	19.3	0.0072	373
642	18.0	0.0037	-	-	-	-	18.0	0.0037	205
643	0.664	0.0023	-	-	4.86	0.0102	5.52	0.0125	2,257
644	13.3	0.0027	-	-	-	-	13.3	0.0027	205
645	3.64	0.0066	-	-	46.1	0.150	49.7	0.157	3,151
646	-	-	-	-	70.3	0.317	70.3	0.317	4,513
647	64.4	0.0615	-	-	10.3	0.0194	74.7	0.0809	1,083
648	4.04	0.0027	-	-	-	-	4.04	0.0027	659
649	5.04	0.0033	-	-	-	-	5.04	0.0033	659
650	16.4	0.0175	-	-	12.9	0.0127	29.3	0.0302	1,029
651	10.9	0.0023	-	-	0.294	0.0002	11.2	0.0024	217
652	19.7	0.0607	-	-	12.3	0.0167	32.0	0.0774	2,419
653	25.6	0.0169	-	-	4.44	0.0082	30.0	0.0251	835
654	11.3	0.0139	-	-	5.73	0.0106	17.1	0.0245	1,437
655	-	-	-	-	56.6	0.191	56.6	0.191	3,369
656	36.2	0.0383	-	-	7.95	0.0135	44.1	0.0518	1,174
657	32.4	0.0280	-	-	4.29	0.0000	36.7	0.0280	765
658	15.4	0.0101	-	-	17.2	0.0392	32.6	0.0493	1,513
659	3.79	0.0053	-	-	28.1	0.0503	31.9	0.0556	1,745
660	51.9	0.0542	-	-	51.9	0.0326	104	0.0868	837
661	-	-	-	-	0.0035	0.0000	0.0035	0.0000	3,800
662	38.0	0.0140	-	-	12.9	0.0054	50.9	0.0194	380
663	-	-	-	-	15.9	0.0840	15.9	0.0840	5,286
664	8.27	0.0088	-	-	38.8	0.0267	47.1	0.0355	754

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
665	26.9	0.0179	-	-	0.0431	0.0002	27.0	0.0180	669
666	23.8	0.0254	-	-	15.4	0.0159	39.2	0.0413	1,053
667	4.10	0.0044	-	-	11.2	0.0055	15.3	0.0098	642
668	26.5	0.0175	-	-	-	-	26.5	0.0175	659
669	30.8	0.0275	-	-	40.3	0.0552	71.1	0.0827	1,163
670	54.5	0.0537	-	-	13.3	0.0078	67.8	0.0614	905
671	7.52	0.0080	-	-	49.8	0.0380	57.3	0.0460	803
672	1.23	0.0008	-	-	0.215	0.0009	1.44	0.0018	1,229
673	3.90	0.0026	-	-	0.117	0.0004	4.01	0.0030	751
674	96.9	0.0283	-	-	19.8	0.0135	117	0.0418	358
675	5.81	0.0018	6.72	0.0049	26.6	0.0153	39.1	0.0220	564
676	34.4	0.0227	-	-	69.0	0.129	103	0.151	1,463
677	-	-	-	-	18.0	0.0908	18.0	0.0908	5,031
678	3.59	0.0122	-	-	33.3	0.0617	36.9	0.0738	2,002
679	4.48	0.0030	-	-	2.19	0.0041	6.68	0.0070	1,051
680	26.4	0.0402	-	-	21.8	0.0538	48.2	0.0940	1,952
681	0.216	0.0007	-	-	-	-	0.216	0.0007	3,305
682	3.28	0.0023	-	-	-	-	3.28	0.0023	688
683	87.9	0.334	-	-	-	-	87.9	0.334	3,800
684	32.7	0.124	-	-	-	-	32.7	0.124	3,800
685	29.3	0.111	-	-	0.0506	0.0002	29.3	0.111	3,800
686	18.5	0.0702	-	-	0.0991	0.0004	18.6	0.0706	3,800
687	35.4	0.134	-	-	-	-	35.4	0.134	3,800
688	26.7	0.102	-	-	0.0522	0.0002	26.8	0.102	3,800
689	9.61	0.0347	-	-	2.59	0.0095	12.2	0.0442	3,624
690	13.7	0.0427	-	-	0.880	0.0033	14.5	0.0461	3,168
691	5.15	0.0196	-	-	0.0034	0.0000	5.15	0.0196	3,799
692	15.6	0.0593	-	-	-	-	15.6	0.0593	3,800
693	12.8	0.0488	-	-	-	-	12.8	0.0488	3,800
694	7.12	0.0271	-	-	-	-	7.12	0.0271	3,800
695	-	-	-	-	38.0	0.0960	38.0	0.0960	2,523
696	4.17	0.0223	-	-	30.4	0.0682	34.6	0.0905	2,613
697	36.7	0.0417	-	-	-	-	36.7	0.0417	1,136
698	22.8	0.0461	7.08	0.0216	-	-	29.9	0.0677	2,262
699	-	-	-	-	-	-	-	-	-
700	62.9	0.239	-	-	4.30	0.0124	67.2	0.251	3,740
701	38.2	0.145	-	-	43.4	0.169	81.6	0.314	3,846
702	-	-	-	-	147	0.557	147	0.557	3,800
703	-	-	-	-	78.5	0.298	78.5	0.298	3,800
704	8.08	0.0307	-	-	-	-	8.08	0.0307	3,800
705	3.17	0.0076	-	-	46.9	0.178	50.1	0.186	3,711
706	61.2	0.0971	-	-	0.0570	-	61.3	0.0971	1,584
707	53.6	0.204	-	-	0.132	0.0005	53.7	0.204	3,800
708	12.8	0.0488	-	-	0.0236	0.0001	12.9	0.0488	3,800
709	1.03	0.0039	-	-	-	-	1.03	0.0039	3,800
710	0.0001	0.0000	-	-	-	-	0.0001	0.0000	3,800
711	-	-	-	-	104	0.0684	104	0.0684	660
712	48.0	0.0101	-	-	14.0	0.0116	62.0	0.0218	351
713	39.1	0.0026	-	-	-	-	39.1	0.0026	67
714	79.6	0.0054	-	-	8.71	0.0023	88.3	0.0076	87
715	1.22	0.0003	-	-	107	0.200	108	0.201	1,850
716	30.4	0.0063	-	-	32.7	0.0122	63.1	0.0184	292
717	-	-	-	-	5.25	0.0044	5.25	0.0044	838
718	14.7	0.0044	-	-	4.83	0.0040	19.5	0.0084	432
719	77.1	0.0232	-	-	13.5	0.0066	90.7	0.0297	328
720	31.5	0.0097	-	-	-	-	31.5	0.0097	309
721	42.3	0.0144	-	-	1.67	0.0014	43.9	0.0158	359
722	22.6	0.0105	-	-	1.45	0.0019	24.1	0.0124	516
723	7.86	0.0268	12.6	0.0247	-	-	20.5	0.0515	2,513
724	14.9	0.0149	-	-	0.981	0.0016	15.8	0.0165	1,040
725	-	-	15.2	0.0460	-	-	15.2	0.0460	3,022
726	-	-	11.0	0.0325	-	-	11.0	0.0325	2,943
727	0.361	0.0019	-	-	11.6	0.0152	12.0	0.0171	1,429
728	12.9	0.0688	-	-	-	-	12.9	0.0688	5,322
729	-	-	21.4	0.0654	3.19	0.0042	24.6	0.0696	2,829
730	10.6	0.0033	-	-	-	-	10.6	0.0033	313
731	0.501	0.0027	14.4	0.0441	-	-	14.9	0.0467	3,130
732	40.0	0.0354	-	-	33.6	0.0296	73.5	0.0649	883
733	29.2	0.0136	-	-	33.2	0.0292	62.4	0.0428	686
734	68.8	0.0585	-	-	8.08	0.0071	76.9	0.0656	853
735	13.0	0.0080	-	-	1.35	0.0011	14.4	0.0092	636
736	109	0.0333	-	-	-	-	109	0.0333	306
737	8.49	0.0018	-	-	79.9	0.148	88.4	0.150	1,696
738	23.8	0.0182	-	-	13.1	0.0196	36.8	0.0378	1,026
739	64.6	0.0120	-	-	31.1	0.0176	95.6	0.0296	309
740	38.7	0.0212	-	-	59.3	0.0335	98.0	0.0547	558
741	-	-	-	-	16.7	0.0141	16.7	0.0141	843
742	120	0.0151	-	-	1.74	0.0044	122	0.0195	160
743	-	-	0.0027	0.0000	168	0.0687	168	0.0687	410
744	87.2	0.0463	-	-	9.45	-	96.7	0.0463	479
745	56.3	0.0804	-	-	4.00	0.0034	60.3	0.0837	1,389
746	129	0.0513	-	-	-	-	129	0.0513	396
747	87.0	0.0638	-	-	3.36	-	90.4	0.0638	706
748	8.47	0.0033	-	-	16.6	0.0139	25.0	0.0172	686
749	56.8	0.0479	0.0980	0.0002	12.9	0.0108	69.7	0.0588	844
750	114	0.125	72.5	0.139	10.8	0.0091	198	0.273	1,383
751	52.7	0.0170	-	-	0.0000	0.0000	52.7	0.0170	323
752	127	0.0498	-	-	1.37	0.0011	128	0.0509	397
753	-	-	23.3	0.0455	148	0.124	172	0.170	990
754	101	0.0341	-	-	-	-	101	0.0341	338
755	75.9	0.0263	0.257	0.0003	-	-	76.2	0.0266	349
756	23.7	0.0097	-	-	-	-	23.7	0.0097	410
757	54.7	0.0163	-	-	1.77	0.0015	56.5	0.0178	315
758	61.7	0.0257	-	-	1.93	0.0016	63.7	0.0273	430
759	-	-	-	-	70.8	0.0581	70.8	0.0581	821

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
760	-	-	-	-	120	0.177	120	0.177	1,473
761	56.6	0.0995	-	-	30.9	0.0919	87.5	0.191	2,188
762	-	-	-	-	167	0.146	167	0.146	873
763	9.54	0.0477	-	-	11.0	0.0101	20.5	0.0578	2,812
764	51.5	0.0442	-	-	28.2	0.0022	79.8	0.0464	582
765	7.43	0.0025	-	-	46.8	0.0441	54.3	0.0466	858
766	-	-	-	-	38.3	0.0235	38.3	0.0235	615
767	129	0.114	-	-	19.9	-	149	0.114	767
768	117	0.176	-	-	9.91	-	127	0.176	1,385
769	0.991	0.0015	-	-	22.0	0.0662	23.0	0.0677	2,946
770	-	-	-	-	54.2	0.135	54.2	0.135	2,486
771	103	0.190	-	-	2.61	0.0070	105	0.196	1,867
772	28.2	0.0058	-	-	-	-	28.2	0.0058	206
773	20.2	0.0303	-	-	0.554	-	20.8	0.0303	1,462
774	91.8	0.138	-	-	0.964	0.0000	92.8	0.138	1,487
775	80.8	0.0335	-	-	3.49	0.0027	84.2	0.0362	429
776	153	0.0384	-	-	19.0	0.0107	172	0.0492	286
777	116	0.0298	-	-	1.87	0.0011	118	0.0309	262
778	79.2	0.0183	-	-	16.4	0.0094	95.6	0.0278	290
779	-	-	-	-	81.8	0.0925	81.8	0.0925	1,131
780	8.96	0.0070	-	-	22.5	0.0127	31.5	0.0197	626
781	82.9	0.0648	-	-	66.1	0.0384	149	0.103	693
782	129	0.0709	-	-	28.1	0.0570	157	0.128	817
783	99.5	0.0218	-	-	1.91	0.0070	101	0.0288	284
784	-	-	-	-	22.2	0.0253	22.2	0.0253	1,143
785	-	-	-	-	33.3	0.0893	33.3	0.0893	2,684
786	22.6	0.0046	-	-	41.4	0.0131	64.0	0.0178	278
787	-	-	-	-	92.5	0.144	92.5	0.144	1,559
788	-	-	-	-	31.0	0.110	31.0	0.110	3,546
789	-	-	-	-	13.5	0.0100	13.5	0.0100	738
790	-	-	-	-	61.3	0.162	61.3	0.162	2,646
791	-	-	-	-	21.8	0.0152	21.8	0.0152	694
792	-	-	-	-	59.4	0.435	59.4	0.435	7,318
793	0.789	0.0030	-	-	102	0.232	103	0.235	2,281
794	-	-	-	-	37.6	0.0495	37.6	0.0495	1,315
795	-	-	-	-	50.1	0.101	50.1	0.101	2,019
796	5.37	0.0011	-	-	-	-	5.37	0.0011	206
797	16.3	0.0034	-	-	0.860	-	17.1	0.0034	195
798	43.3	0.0089	-	-	22.0	-	65.2	0.0089	136
799	25.4	0.0052	-	-	2.00	-	27.4	0.0052	191
800	17.7	0.0036	-	-	3.59	-	21.3	0.0036	171
801	12.3	0.0025	-	-	-	-	12.3	0.0025	206
802	16.8	0.0035	-	-	-	-	16.8	0.0035	206
803	43.7	0.0090	-	-	-	-	43.7	0.0090	206
804	-	-	-	-	65.5	0.0539	65.5	0.0539	823
805	-	-	-	-	33.2	0.0210	33.2	0.0210	634
806	-	-	-	-	32.8	0.108	32.8	0.108	3,300
807	0.560	0.0028	-	-	21.4	0.0584	22.0	0.0612	2,789
808	91.4	0.184	-	-	7.47	0.0106	98.9	0.194	1,967
809	15.2	0.0761	-	-	18.9	0.0481	34.2	0.124	3,637
810	-	-	-	-	39.0	0.0972	39.0	0.0972	2,491
811	-	-	-	-	32.6	0.0893	32.6	0.0893	2,742
812	0.741	0.0011	-	-	13.8	0.0383	14.5	0.0394	2,712
813	60.6	0.195	-	-	7.35	0.0195	67.9	0.214	3,155
814	2.09	0.0031	-	-	44.4	0.121	46.5	0.124	2,676
815	88.1	0.0218	-	-	32.3	0.0294	120	0.0512	425
816	56.5	0.0145	4.92	0.0096	7.41	0.0043	68.8	0.0284	413
817	2.53	0.0007	31.9	0.0625	-	-	34.5	0.0632	1,835
818	54.9	0.0283	19.2	0.0375	4.78	0.0040	78.8	0.0698	886
819	113	0.0345	-	-	76.0	0.0435	188	0.0780	414
820	40.3	0.0085	-	-	20.1	0.0196	60.4	0.0281	465
821	292	0.0686	-	-	49.5	0.0234	341	0.0920	270
822	126	0.189	-	-	18.3	-	144	0.189	1,311
823	0.189	0.0003	-	-	82.6	-	82.8	0.0003	3
824	121	0.0998	-	-	52.7	0.144	174	0.244	1,400
825	18.6	0.0154	-	-	38.5	0.0196	57.0	0.0350	614
826	139	0.0318	-	-	-	-	139	0.0318	229
827	129	0.0083	-	-	8.01	0.0020	137	0.0104	76
828	164	0.0441	-	-	-	-	164	0.0441	269
829	82.2	0.0628	-	-	0.0000	0.0000	82.2	0.0628	764
830	142	0.0989	-	-	-	-	142	0.0989	694
831	69.4	0.0044	-	-	-	-	69.4	0.0044	63
832	70.0	0.0050	-	-	16.9	0.0053	86.9	0.0103	118
833	52.0	0.0045	-	-	-	-	52.0	0.0045	87
834	71.3	0.0538	-	-	35.1	-	106	0.0538	506
835	0.786	0.0013	-	-	6.68	0.0059	7.46	0.0071	958
836	33.5	0.0415	-	-	13.7	0.0310	47.3	0.0725	1,533
837	133	0.0800	-	-	0.655	0.0015	134	0.0814	608
838	85.8	0.0174	-	-	-	-	85.8	0.0174	203
839	85.4	0.197	-	-	33.9	0.0764	119	0.274	2,295
840	72.7	0.164	-	-	8.17	0.0129	80.9	0.176	2,181
841	34.4	0.0758	-	-	25.6	0.0577	60.0	0.133	2,223
842	39.3	0.0934	-	-	-	-	39.3	0.0934	2,376
843	11.2	0.0462	-	-	21.1	0.0499	32.3	0.0961	2,976
844	72.8	0.175	-	-	0.0001	0.0000	72.8	0.175	2,410
845	21.8	0.0391	-	-	-	-	21.8	0.0391	1,794
846	69.1	0.168	-	-	-	-	69.1	0.168	2,438
847	76.2	0.0944	-	-	16.6	0.0132	92.8	0.108	1,160
848	26.5	0.0329	-	-	-	-	26.5	0.0329	1,238
849	25.4	0.0315	-	-	9.15	-	34.6	0.0315	910
850	56.5	0.0443	-	-	3.22	0.0000	59.7	0.0443	742
851	32.2	0.0196	-	-	0.0004	0.0000	32.2	0.0196	609
852	39.3	0.0181	-	-	22.4	0.0159	61.7	0.0340	552
853	57.6	0.0266	-	-	-	-	57.6	0.0266	461
854	38.7	0.0178	-	-	26.1	0.0219	64.8	0.0397	613

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
855	44.3	0.151	0.0009	0.0000	0.0084	-	44.3	0.151	3,408
856	64.6	0.0520	-	-	-	-	64.6	0.0520	805
857	27.5	0.0127	-	-	7.19	-	34.7	0.0127	365
858	26.2	0.0121	-	-	0.0008	-	26.2	0.0121	460
859	58.5	0.0280	-	-	-	-	58.5	0.0280	478
860	86.0	0.0394	-	-	7.38	-	93.4	0.0394	422
861	22.4	0.0105	-	-	12.6	-	35.0	0.0105	301
862	80.3	0.0187	2.26	0.0044	35.8	0.0092	118	0.0323	273
863	103	0.0239	-	-	8.50	0.0002	112	0.0240	215
864	-	-	0.0000	0.0000	62.7	0.0525	62.7	0.0525	838
865	7.04	0.0015	-	-	72.2	0.0388	79.3	0.0403	509
866	18.9	0.0012	-	-	-	-	18.9	0.0012	63
867	129	0.117	7.14	0.0076	18.5	-	154	0.125	807
868	85.3	0.0465	-	-	2.23	-	87.5	0.0465	532
869	113	0.0682	-	-	22.0	0.0054	135	0.0736	545
870	111	0.0237	-	-	25.3	0.0088	136	0.0326	239
871	15.5	0.0529	-	-	2.44	0.0020	18.0	0.0550	3,059
872	61.6	0.116	-	-	2.68	0.0022	64.3	0.118	1,837
873	29.1	0.0339	-	-	-	-	29.1	0.0339	1,165
874	43.4	0.0320	-	-	2.32	0.0019	45.7	0.0339	743
875	83.9	0.0370	-	-	0.508	0.0004	84.4	0.0375	444
876	35.5	0.0138	-	-	-	-	35.5	0.0138	390
877	63.4	0.0255	-	-	-	-	63.4	0.0255	403
878	57.3	0.0224	-	-	-	-	57.3	0.0224	392
879	34.5	0.0149	-	-	-	-	34.5	0.0149	433
880	37.8	0.0390	-	-	5.85	0.0001	43.6	0.0391	896
881	28.8	0.0354	-	-	0.0010	0.0000	28.8	0.0354	1,230
882	49.5	0.120	0.249	0.0003	1.79	0.0065	51.5	0.127	2,467
883	44.7	0.0094	-	-	5.34	0.0000	50.0	0.0095	189
884	11.1	0.0026	42.4	0.0830	28.9	-	82.4	0.0857	1,040
885	10.9	0.0031	1.79	0.0035	20.6	0.0102	33.3	0.0168	504
886	-	-	0.148	0.0003	-	-	0.148	0.0003	1,957
887	-	-	0.0002	0.0000	25.2	0.0376	25.2	0.0376	1,488
888	0.0447	0.0000	77.7	0.152	-	-	77.7	0.152	1,956
889	28.4	0.0081	-	-	74.6	0.0412	103	0.0493	478
890	14.5	0.0093	5.17	0.0101	115	0.136	134	0.156	1,161
891	16.4	0.0104	-	-	3.40	0.0028	19.8	0.0132	669
892	34.1	0.0216	-	-	15.6	0.0131	49.7	0.0347	698
893	0.123	0.0000	-	-	70.4	0.0590	70.5	0.0590	837
894	-	-	-	-	65.0	0.0479	65.0	0.0479	738
895	97.5	0.0439	-	-	123	0.0882	221	0.132	598
896	3.64	0.0008	-	-	80.1	0.0720	83.7	0.0728	869
897	131	0.0347	-	-	2.47	0.0000	133	0.0347	261
898	-	-	-	-	70.8	0.193	70.8	0.193	2,725
899	41.3	0.0284	-	-	13.8	0.0308	55.0	0.0592	1,076
900	-	-	-	-	33.3	0.182	33.3	0.182	5,463
901	55.7	0.0353	-	-	37.3	0.0177	93.0	0.0530	570
902	43.6	0.0301	-	-	28.9	0.0593	72.6	0.0894	1,232
903	12.6	0.0170	7.42	0.0473	123	0.234	143	0.298	2,084
904	126	0.0289	-	-	-	-	126	0.0289	230
905	17.4	0.0044	-	-	2.30	0.0019	19.7	0.0063	322
906	45.4	0.0160	-	-	6.61	0.0055	52.0	0.0216	415
907	101	0.0507	12.9	0.0252	44.0	0.0393	158	0.115	729
908	3.49	0.0016	68.1	0.168	99.2	0.0831	171	0.253	1,480
909	79.0	0.0173	-	-	-	-	79.0	0.0173	219
910	13.3	0.0031	-	-	85.9	0.0717	99.3	0.0748	753
911	49.4	0.0148	-	-	-	-	49.4	0.0148	299
912	74.2	0.0263	-	-	21.5	-	95.8	0.0263	275
913	139	0.0678	-	-	1.62	0.0011	141	0.0688	489
914	105	0.0841	2.86	0.0030	16.5	0.0205	125	0.108	863
915	40.9	0.0163	2.75	0.0029	44.1	0.0370	87.8	0.0562	640
916	16.7	0.0050	-	-	-	-	16.7	0.0050	298
917	106	0.0316	-	-	41.5	0.0310	147	0.0626	425
918	54.1	0.0341	-	-	-	-	54.1	0.0341	630
919	120	0.0347	1.83	0.0036	10.0	0.0164	132	0.0547	414
920	109	0.0544	-	-	3.66	0.0031	112	0.0575	512
921	62.4	0.0210	-	-	7.12	0.0063	69.5	0.0273	392
922	81.1	0.0396	-	-	38.7	0.0309	120	0.0704	588
923	135	0.0413	-	-	0.0001	0.0000	135	0.0413	306
924	45.4	0.0286	-	-	-	-	45.4	0.0286	630
925	108	0.0748	-	-	16.3	0.0165	125	0.0914	734
926	64.0	0.0271	-	-	28.0	0.0304	92.0	0.0575	625
927	64.1	0.0233	-	-	0.446	0.0004	64.6	0.0237	367
928	23.2	0.0280	-	-	37.6	0.0422	60.8	0.0702	1,155
929	57.0	0.0216	-	-	0.236	0.0002	57.2	0.0218	381
930	36.2	0.0324	-	-	5.45	0.0055	41.7	0.0379	910
931	9.63	0.0140	-	-	30.6	0.0310	40.2	0.0450	1,119
932	14.4	0.0152	-	-	-	-	14.4	0.0152	1,054
933	51.0	0.0264	-	-	16.3	0.0143	67.3	0.0407	605
934	2.58	0.0052	2.93	0.0075	23.2	0.0303	28.7	0.0430	1,494
935	33.6	0.0281	-	-	0.0001	-	33.6	0.0281	837
936	-	-	-	-	36.0	0.0471	36.0	0.0471	1,308
937	-	-	-	-	34.0	0.0494	34.0	0.0494	1,455
938	3.26	0.0021	30.8	0.0601	-	-	34.0	0.0622	1,828
939	11.9	0.0635	17.7	0.0542	-	-	29.7	0.118	3,967
940	15.3	0.0060	-	-	-	-	15.3	0.0060	394
941	0.0023	0.0000	0.0002	0.0000	61.1	0.0471	61.1	0.0471	770
942	-	-	-	-	36.7	0.0287	36.7	0.0287	782
943	9.36	0.0036	-	-	2.99	0.0025	12.4	0.0062	498
944	-	-	-	-	57.3	0.0481	57.3	0.0481	838
945	-	-	-	-	4.81	0.0040	4.81	0.0040	838
946	12.8	0.0150	-	-	6.57	0.0055	19.4	0.0205	1,057
947	0.0021	0.0000	-	-	36.8	0.0257	36.8	0.0257	700
948	38.6	0.0153	-	-	0.0326	0.0000	38.7	0.0153	395
949	84.2	0.0535	-	-	6.59	0.0045	90.7	0.0580	640

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	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
950	-	-	14.8	0.0454	-	-	14.8	0.0454	3,055
951	182	0.329	-	-	75.4	0.105	257	0.434	1,689
952	-	-	15.5	0.0303	-	-	15.5	0.0303	1,957
953	-	-	22.4	0.0438	-	-	22.4	0.0438	1,957
954	-	-	35.9	0.0703	-	-	35.9	0.0703	1,957
955	38.3	0.0475	-	-	3.54	0.0046	41.8	0.0521	1,246
956	6.10	0.0325	-	-	2.69	0.0035	8.79	0.0360	4,094
957	89.0	0.143	-	-	2.44	-	91.5	0.143	1,559
958	-	-	26.7	0.0518	5.77	0.0211	32.4	0.0729	2,248
959	-	-	14.3	0.0435	0.161	0.0002	14.4	0.0437	3,031
960	12.8	0.0385	9.98	0.0305	0.0160	0.0000	22.8	0.0690	3,021
961	-	-	6.88	0.0209	0.164	0.0002	7.05	0.0211	2,999
962	30.5	0.123	-	-	6.53	0.0085	37.0	0.131	3,545
963	91.3	0.0516	-	-	0.0151	0.0000	91.3	0.0516	565
964	0.0056	0.0000	-	-	27.0	0.0167	27.0	0.0167	616
965	31.9	0.0150	-	-	0.168	0.0002	32.1	0.0152	474
966	-	-	-	-	13.1	0.0110	13.1	0.0110	838
967	2.99	0.0012	-	-	32.8	0.0275	35.8	0.0286	800
968	-	-	-	-	96.9	0.0922	96.9	0.0922	952
969	-	-	-	-	64.1	0.0537	64.1	0.0537	838
970	-	-	-	-	2.62	0.0022	2.62	0.0022	838
971	29.3	0.0390	-	-	0.266	0.0003	29.6	0.0393	1,329
972	16.0	0.0126	-	-	1.21	-	17.2	0.0126	735
973	97.3	0.0906	-	-	3.43	0.0045	101	0.0951	945
974	122	0.0628	-	-	1.27	0.0017	124	0.0645	522
975	-	-	-	-	23.6	0.0309	23.6	0.0309	1,308
976	11.0	0.0084	-	-	28.7	0.0253	39.7	0.0336	848
977	130	0.0654	-	-	10.2	0.0090	140	0.0744	532
978	89.1	0.0330	-	-	7.51	0.0066	96.6	0.0396	410
979	17.1	0.0222	5.64	0.0110	31.3	0.0262	54.0	0.0594	1,100
980	98.2	0.0307	-	-	2.18	0.0018	100	0.0325	324
981	36.1	0.0141	-	-	0.0008	0.0000	36.1	0.0141	390
982	91.2	0.0340	-	-	13.2	0.0111	104	0.0450	431
983	46.3	0.0402	-	-	26.0	0.0218	72.4	0.0620	857
984	-	-	-	-	67.8	0.0652	67.8	0.0652	962
985	28.7	0.0104	-	-	-	-	28.7	0.0104	360
986	55.5	0.0258	-	-	-	-	55.5	0.0258	465
987	126	0.0611	-	-	7.60	0.0021	133	0.0632	475
988	51.6	0.0294	-	-	6.44	0.0057	58.1	0.0351	605
989	118	0.149	-	-	22.5	0.0198	141	0.169	1,197
990	85.5	0.0658	14.1	0.0151	0.788	-	100	0.0808	805
991	38.3	0.0527	-	-	-	-	38.3	0.0527	1,377
992	40.9	0.0322	-	-	4.70	0.0137	45.6	0.0460	1,008
993	16.4	0.169	10.9	0.0377	0.499	-	27.7	0.207	7,462
994	-	-	-	-	4.24	0.0024	4.24	0.0024	566
995	-	-	-	-	71.4	0.167	71.4	0.167	2,336
996	4.41	0.0019	-	-	-	-	4.41	0.0019	428
997	61.8	0.0104	-	-	13.8	0.0233	75.6	0.0336	445
998	25.2	0.0140	-	-	1.02	0.0006	26.2	0.0146	556
999	15.3	0.0032	-	-	-	-	15.3	0.0032	206
1000	-	-	-	-	28.4	0.0225	28.4	0.0225	791
1001	-	-	-	-	57.9	0.0217	57.9	0.0217	374
1002	-	-	-	-	45.1	0.0338	45.1	0.0338	749
1003	-	-	-	-	23.8	0.0172	23.8	0.0172	724
1004	-	-	-	-	0.841	-	0.841	-	-
1005	1.06	0.0013	-	-	-	-	1.06	0.0013	1,238
1006	6.16	0.0091	-	-	5.37	-	11.5	0.0091	793
1007	16.7	0.0065	-	-	-	-	16.7	0.0065	390
1008	-	-	75.6	0.155	11.6	0.0097	87.2	0.165	1,893
1009	91.7	0.0194	-	-	-	-	91.7	0.0194	211
1010	22.6	0.0048	-	-	-	-	22.6	0.0048	211
1011	14.6	0.0031	-	-	-	-	14.6	0.0031	211
1012	8.56	0.0118	-	-	7.82	-	16.4	0.0118	721
1013	2.73	0.0011	-	-	-	-	2.73	0.0011	390
1014	2.96	0.0124	12.0	0.0365	2.42	0.0031	17.3	0.0520	3,002
1015	115	0.0559	-	-	11.6	0.0102	126	0.0661	524
1016	34.4	0.0348	-	-	41.2	0.0390	75.6	0.0738	976
1017	-	-	-	-	11.8	0.0154	11.8	0.0154	1,308
1018	5.22	0.0278	4.73	0.0144	-	-	9.95	0.0422	4,245
1019	-	-	10.7	0.0327	54.3	0.0934	65.0	0.126	1,941
1020	2.05	0.0008	-	-	2.79	0.0023	4.83	0.0031	650
1021	-	-	-	-	-	-	-	-	-
1022	8.50	0.0084	-	-	7.69	0.0039	16.2	0.0123	758
1023	90.0	0.0185	-	-	1.01	-	91.0	0.0185	204
1024	0.332	0.0004	-	-	0.932	-	1.26	0.0004	335
1025	0.136	0.0005	-	-	1.71	0.0063	1.85	0.0068	3,669
1026	2.73	0.0035	-	-	0.235	-	2.97	0.0035	1,173
1027	61.3	0.0921	-	-	17.9	0.0488	79.2	0.141	1,779
1028	0.106	0.0002	-	-	18.4	0.0095	18.5	0.0097	522
1029	13.1	0.0487	-	-	-	-	13.1	0.0487	3,729
1030	16.5	0.0610	-	-	-	-	16.5	0.0610	3,706
1031	45.8	0.0687	-	-	36.7	-	82.5	0.0687	834
1032	16.6	0.0250	-	-	25.6	-	42.3	0.0250	592
1033	25.3	0.0380	-	-	5.54	-	30.9	0.0380	1,232
1034	43.1	0.0696	-	-	0.0002	0.0000	43.1	0.0696	1,616
1035	0.0001	0.0000	-	-	47.1	0.131	47.1	0.131	2,771
1036	-	-	-	-	52.5	0.206	52.5	0.206	3,912
1037	33.2	0.0636	-	-	9.43	0.0296	42.6	0.0932	2,187
1038	-	-	-	-	25.0	0.0204	25.0	0.0204	814
1039	71.0	0.0405	-	-	17.6	0.0395	88.5	0.0800	904
1040	-	-	-	-	-	-	-	-	-
1041	7.28	0.0015	-	-	-	-	7.28	0.0015	211
1042	44.4	0.0860	-	-	-	-	44.4	0.0860	1,938
1043	18.1	0.0103	-	-	-	-	18.1	0.0103	568
1044	37.9	0.0247	-	-	-	-	37.9	0.0247	651

Table E-2. Average Dry Weather Flows by Land Use Area - 2015

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
1045	91.4	0.0519	-	-	-	-	91.4	0.0519	568
1046	49.2	0.187	-	-	-	-	49.2	0.187	3,800
1047	-	-	-	-	0.0215	0.0001	0.0215	0.0001	3,800
1048	50.3	0.0285	-	-	-	-	50.3	0.0285	568
1049	8.69	0.0330	-	-	-	-	8.69	0.0330	3,800
1050	52.9	0.0326	-	-	-	-	52.9	0.0326	616
1051	27.0	0.103	-	-	-	-	27.0	0.103	3,800
1052	55.1	0.0190	-	-	61.7	-	117	0.0190	163
1053	29.8	0.0101	-	-	0.0093	0.0000	29.8	0.0101	338
1054	-	-	-	-	-	-	-	-	-
1055	-	-	-	-	158	0.207	158	0.207	1,308
1056	22.2	0.0333	-	-	7.27	-	29.5	0.0333	1,131
9999	88.4	0.1327	-	-	5.43	-	93.8	0.1327	1,415

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
1	25.9	0.0389	-	-	7.04	-	33.0	0.0389	1,181
2	44.6	0.154	-	-	42.1	0.0662	86.7	0.220	2,541
3	-	-	-	-	6.75	0.0247	6.75	0.0247	3,659
4	21.0	0.0797	-	-	14.6	0.0536	35.6	0.133	3,743
5	6.48	0.0246	-	-	0.963	0.0036	7.44	0.0283	3,797
6	45.2	0.105	-	-	106	0.243	151	0.348	2,306
7	84.6	0.0601	-	-	47.7	0.0743	132	0.134	1,016
8	15.5	0.0022	-	-	-	-	15.5	0.0022	143
9	3.11	0.0118	-	-	28.6	0.109	31.7	0.121	3,800
10	16.4	0.0625	-	-	7.70	0.0293	24.1	0.0917	3,800
11	50.3	0.191	-	-	31.8	0.116	82.1	0.307	3,745
12	17.5	0.0281	-	-	30.2	0.145	47.7	0.173	3,628
13	198	0.722	-	-	0.0015	0.0000	198	0.722	3,638
14	2.68	0.0103	-	-	21.0	0.0795	23.6	0.0898	3,799
15	0.0574	0.0002	-	-	96.4	0.399	96.5	0.399	4,134
16	50.2	0.0604	-	-	13.2	0.0129	63.3	0.0733	1,157
17	50.8	0.0631	-	-	85.4	0.0506	136	0.114	835
18	0.0431	0.0002	-	-	39.6	0.187	39.7	0.187	4,707
19	6.93	0.0124	-	-	17.9	-	24.9	0.0124	500
20	0.0067	0.0000	-	-	23.8	0.174	23.8	0.174	7,315
21	-	-	-	-	25.9	0.0837	25.9	0.0837	3,238
22	59.6	0.226	-	-	-	-	59.6	0.226	3,800
23	63.9	0.243	-	-	-	-	63.9	0.243	3,800
24	-	-	-	-	39.6	0.119	39.6	0.119	2,998
25	-	-	-	-	34.0	0.129	34.0	0.129	3,800
26	-	-	-	-	70.2	0.267	70.2	0.267	3,799
27	-	-	-	-	74.2	0.282	74.2	0.282	3,800
28	0.159	0.0006	-	-	25.7	0.0975	25.8	0.0981	3,800
29	33.5	0.127	-	-	-	-	33.5	0.127	3,800
30	22.2	0.0843	-	-	33.9	0.129	56.1	0.213	3,800
31	49.4	0.188	-	-	24.0	0.0910	73.4	0.279	3,800
32	30.3	0.115	-	-	-	-	30.3	0.115	3,800
33	24.6	0.0935	-	-	13.4	0.0510	38.0	0.145	3,800
34	0.966	0.0037	-	-	20.5	0.0779	21.5	0.0816	3,800
35	-	-	-	-	8.73	0.0068	8.73	0.0068	778
36	-	-	-	-	58.4	0.127	58.4	0.127	2,180
37	-	-	-	-	447	0.808	447	0.808	1,807
38	-	-	-	-	112	0.363	112	0.363	3,242
39	-	-	-	-	45.4	0.0777	45.4	0.0777	1,710
40	-	-	-	-	23.5	0.0837	23.5	0.0837	3,561
41	-	-	-	-	61.5	0.0896	61.5	0.0896	1,458
42	78.5	0.0448	-	-	0.297	0.0007	78.8	0.0455	577
43	14.7	0.0186	-	-	2.09	-	16.8	0.0186	1,104
44	0.0490	0.0002	-	-	19.2	0.0211	19.2	0.0213	1,106
45	0.0002	0.0000	-	-	46.8	0.0514	46.8	0.0514	1,100
46	42.1	0.160	-	-	0.0029	0.0000	42.1	0.160	3,800
47	-	-	-	-	13.8	0.0359	13.8	0.0359	2,600
48	324	0.169	-	-	-	-	324	0.169	522
49	52.8	0.0168	-	-	14.7	0.0094	67.5	0.0262	388
50	10.7	0.0099	-	-	185	0.327	196	0.337	1,723
51	10.2	0.0051	-	-	45.8	0.0084	56.0	0.0135	240
52	-	-	-	-	66.0	0.0860	66.0	0.0860	1,302
53	-	-	-	-	42.4	0.0602	42.4	0.0602	1,421
54	0.686	0.0001	-	-	199	0.0015	199	0.0016	7.97
55	145	0.552	-	-	34.7	0.126	180	0.678	3,767
56	18.4	0.0701	-	-	142	0.416	161	0.486	3,020
57	123	0.441	4.81	0.0123	69.7	0.193	198	0.647	3,273
58	14.0	0.0165	-	-	0.0065	0.0000	14.0	0.0165	1,183
59	12.0	0.0455	-	-	0.0004	0.0000	12.0	0.0455	3,800
60	37.2	0.130	-	-	-	-	37.2	0.130	3,485
61	-	-	-	-	5.84	0.0064	5.84	0.0064	1,098
62	-	-	-	-	69.2	0.181	69.2	0.181	2,609
63	-	-	-	-	9.04	0.0099	9.04	0.0099	1,098
64	-	-	-	-	10.0	0.0193	10.0	0.0193	1,928
65	0.0075	0.0000	-	-	118	0.362	118	0.362	3,057
66	177	0.0672	-	-	1.02	0.0012	178	0.0684	384
67	102	0.0512	-	-	-	-	102	0.0512	503
68	64.1	0.0246	-	-	0.0050	0.0000	64.1	0.0247	385
69	-	-	-	-	53.2	0.109	53.2	0.109	2,054
70	-	-	11.3	0.0354	-	-	11.3	0.0354	3,141
71	30.7	0.0085	-	-	3.59	0.0000	34.3	0.0085	248
72	2.36	0.0007	-	-	8.03	0.0088	10.4	0.0095	913
73	50.3	0.0734	-	-	0.0004	0.0000	50.3	0.0734	1,458
74	8.09	0.0023	-	-	-	-	8.09	0.0023	286
75	1.81	0.0069	-	-	11.0	0.0419	12.8	0.0488	3,800
76	36.0	0.137	-	-	-	-	36.0	0.137	3,800
77	65.7	0.249	-	-	-	-	65.7	0.249	3,797
78	40.1	0.152	-	-	0.0342	0.0001	40.2	0.152	3,783
79	21.3	0.0560	-	-	6.80	0.0041	28.1	0.0601	2,138
80	4.91	0.0206	-	-	-	-	4.91	0.0206	4,202
81	17.3	0.0360	-	-	2.37	0.0026	19.7	0.0386	1,962
82	-	-	7.03	0.0181	7.36	-	14.4	0.0181	1,255
83	-	-	-	-	22.4	0.0455	22.4	0.0455	2,035
84	22.7	0.0204	36.8	0.149	3.84	-	63.3	0.169	2,671
85	-	-	-	-	41.9	0.0472	41.9	0.0472	1,129
86	-	-	-	-	9.66	0.0265	9.66	0.0265	2,745
87	28.2	0.107	-	-	-	-	28.2	0.107	3,800
88	9.72	0.0369	-	-	-	-	9.72	0.0369	3,800
89	52.1	0.198	-	-	-	-	52.1	0.198	3,800
90	211	0.803	-	-	0.751	0.0029	212	0.806	3,800
91	95.1	0.361	-	-	0.0091	0.0000	95.1	0.361	3,800
92	59.7	0.227	-	-	-	-	59.7	0.227	3,800
93	102	0.0671	-	-	-	-	102	0.0671	657
94	36.8	0.140	-	-	-	-	36.8	0.140	3,800
95	-	-	-	-	232	0.880	232	0.880	3,800

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
96	12.6	0.0477	-	-	12.9	0.0488	25.4	0.0965	3,800
97	67.4	0.256	-	-	4.32	0.0164	71.7	0.272	3,800
98	18.7	0.0707	-	-	-	-	18.7	0.0707	3,776
99	-	-	-	-	135	0.487	135	0.487	3,601
100	25.0	0.0951	-	-	11.5	0.0416	36.5	0.137	3,741
101	-	-	-	-	66.2	0.252	66.2	0.252	3,800
102	-	-	-	-	573	2.18	573	2.18	3,800
103	-	-	-	-	158	0.601	158	0.601	3,800
104	0.0003	0.0000	-	-	135	0.512	135	0.512	3,800
105	57.1	0.217	-	-	250	0.949	307	1.17	3,800
106	-	-	25.4	0.0671	0.0909	-	25.5	0.0671	2,630
107	3.48	0.0010	-	-	75.7	0.0994	79.2	0.100	1,268
108	4.98	0.0014	-	-	2.56	-	7.54	0.0014	183
109	19.9	0.0194	-	-	106	0.155	126	0.175	1,386
110	6.93	0.0088	-	-	39.9	0.0001	46.9	0.0089	190
111	19.2	0.0341	-	-	17.2	0.0152	36.4	0.0492	1,355
112	0.929	0.0004	-	-	44.5	-	45.4	0.0004	7.77
113	67.2	0.0304	-	-	16.5	-	83.7	0.0304	364
114	14.5	0.0040	-	-	-	-	14.5	0.0040	277
115	7.37	0.0029	-	-	1.50	-	8.87	0.0029	327
116	14.9	0.0309	-	-	37.4	0.0224	52.3	0.0534	1,020
117	15.4	0.0043	-	-	13.0	-	28.4	0.0043	150
118	33.1	0.0317	-	-	8.16	-	41.3	0.0317	768
119	73.2	0.0331	-	-	49.0	0.0539	122	0.0870	712
120	14.8	0.0042	-	-	0.171	-	15.0	0.0042	280
121	31.1	0.0398	-	-	-	-	31.1	0.0398	1,282
122	15.3	0.0115	-	-	18.7	0.0207	34.0	0.0321	945
123	29.4	0.0095	-	-	5.57	-	35.0	0.0095	273
124	30.9	0.0086	-	-	2.41	-	33.3	0.0086	257
125	13.1	0.0036	-	-	4.79	-	17.9	0.0036	203
126	17.5	0.0049	-	-	0.574	-	18.1	0.0049	273
127	32.8	0.0096	-	-	2.64	-	35.5	0.0096	270
128	24.2	0.0285	-	-	13.8	0.0152	38.0	0.0437	1,149
129	23.7	0.0066	-	-	10.4	0.0114	34.1	0.0180	527
130	20.5	0.0095	-	-	-	-	20.5	0.0095	462
131	-	-	62.3	0.288	16.3	0.0059	78.7	0.294	3,739
132	35.9	0.0169	9.49	0.0244	4.09	-	49.4	0.0412	834
133	14.6	0.0120	39.3	0.102	2.35	-	56.3	0.114	2,022
134	12.8	0.0038	-	-	1.92	-	14.7	0.0038	259
135	16.2	0.0045	-	-	1.12	-	17.4	0.0045	259
136	33.2	0.0092	-	-	-	-	33.2	0.0092	277
137	29.2	0.0150	-	-	-	-	29.2	0.0150	512
138	21.1	0.0067	-	-	3.66	-	24.8	0.0067	272
139	127	0.105	25.2	0.0645	27.2	0.0352	180	0.205	1,141
140	14.7	0.0081	-	-	-	-	14.7	0.0081	554
141	3.52	0.0010	-	-	9.63	0.0106	13.1	0.0116	880
142	33.7	0.0093	-	-	-	-	33.7	0.0093	277
143	69.5	0.0334	5.63	0.0084	-	-	75.1	0.0418	556
144	15.6	0.0160	87.5	0.225	22.4	0.0216	125	0.262	2,090
145	30.2	0.0148	2.15	0.0034	2.83	-	35.2	0.0182	518
146	13.0	0.0043	0.193	0.0005	3.24	-	16.5	0.0048	289
147	26.7	0.0377	5.45	0.0076	10.1	0.0062	42.3	0.0515	1,218
148	1.69	0.0006	2.32	0.0059	3.06	-	7.07	0.0066	929
149	7.74	0.0090	8.83	0.0233	2.43	-	19.0	0.0323	1,700
150	13.7	0.0156	-	-	18.1	0.0199	31.7	0.0355	1,118
151	28.3	0.0383	-	-	20.5	0.0226	48.8	0.0608	1,246
152	21.1	0.0058	-	-	4.95	0.0054	26.0	0.0113	434
153	4.13	0.0011	-	-	-	-	4.13	0.0011	277
154	9.14	0.0025	-	-	-	-	9.14	0.0025	277
155	36.0	0.0101	-	-	-	-	36.0	0.0101	281
156	23.0	0.0065	-	-	-	-	23.0	0.0065	282
157	8.07	0.0047	7.32	0.0194	-	-	15.4	0.0241	1,565
158	110	0.567	0.949	0.0020	3.95	0.0053	115	0.575	4,999
159	145	0.0474	-	-	4.09	0.0045	149	0.0519	347
160	253	0.0993	-	-	11.2	0.0124	264	0.112	422
161	39.9	0.0138	-	-	-	-	39.9	0.0138	344
162	125	0.135	-	-	1.72	-	127	0.135	1,059
163	189	0.137	2.29	0.0032	3.19	-	194	0.141	724
164	91.1	0.0378	-	-	-	-	91.1	0.0378	414
165	64.6	0.0258	-	-	-	-	64.6	0.0258	399
166	90.6	0.0241	-	-	42.5	0.0521	133	0.0762	572
167	-	-	-	-	52.3	0.191	52.3	0.191	3,659
168	-	-	-	-	53.1	0.0966	53.1	0.0966	1,820
169	126	0.148	-	-	10.9	0.0101	137	0.158	1,150
170	-	-	-	-	153	0.0916	153	0.0916	597
171	27.9	0.0088	-	-	-	-	27.9	0.0088	314
172	38.0	0.0147	-	-	-	-	38.0	0.0147	386
173	76.8	0.0375	-	-	-	-	76.8	0.0375	489
174	76.0	0.0330	-	-	-	-	76.0	0.0330	435
175	101	0.0389	-	-	8.95	0.0098	109	0.0487	445
176	29.2	0.0134	-	-	-	-	29.2	0.0134	458
177	14.6	0.0065	-	-	2.41	0.0030	17.0	0.0095	562
178	89.7	0.109	-	-	24.9	0.0353	115	0.145	1,261
179	83.2	0.0318	-	-	-	-	83.2	0.0318	383
180	43.0	0.0258	-	-	3.88	0.0043	46.8	0.0301	642
181	54.2	0.0698	-	-	86.5	0.0645	141	0.134	955
182	-	-	-	-	24.9	0.0185	24.9	0.0185	746
183	0.0000	0.0000	-	-	22.7	0.0169	22.7	0.0169	746
184	23.0	0.0309	-	-	0.315	0.0007	23.3	0.0316	1,358
185	54.6	0.0207	-	-	17.6	0.0229	72.2	0.0436	604
186	-	-	-	-	151	0.220	151	0.220	1,461
187	-	-	-	-	21.0	0.0230	21.0	0.0230	1,100
188	40.5	0.0207	-	-	1.18	-	41.7	0.0207	497
189	34.4	0.0210	-	-	4.94	-	39.3	0.0210	535
190	39.1	0.0214	-	-	2.22	-	41.3	0.0214	518

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
191	32.3	0.0650	-	-	29.8	0.0448	62.0	0.110	1,770
192	-	-	-	-	57.5	0.0832	57.5	0.0832	1,446
193	37.7	0.0370	-	-	5.72	-	43.4	0.0370	852
194	35.0	0.0180	-	-	9.72	0.0022	44.7	0.0203	454
195	19.1	0.0100	-	-	1.91	-	21.0	0.0100	479
196	50.6	0.0196	-	-	4.61	-	55.2	0.0196	355
197	31.4	0.0364	-	-	8.37	-	39.8	0.0364	915
198	14.1	0.0046	-	-	-	-	14.1	0.0046	325
199	-	-	-	-	16.3	0.0275	16.3	0.0275	1,690
200	29.3	0.0461	-	-	-	-	29.3	0.0461	1,570
201	51.0	0.0151	-	-	-	-	51.0	0.0151	296
202	-	-	-	-	83.7	0.0920	83.7	0.0920	1,099
203	-	-	-	-	117	0.205	117	0.205	1,743
204	-	-	5.39	0.0138	-	-	5.39	0.0138	2,568
205	-	-	83.5	0.289	3.51	0.0025	87.0	0.291	3,348
206	-	-	77.0	0.225	11.2	-	88.2	0.225	2,546
207	0.147	0.0003	0.147	0.0004	63.2	0.171	63.5	0.172	2,703
208	-	-	42.3	0.149	3.79	-	46.1	0.149	3,241
209	-	-	21.4	0.0702	4.69	-	26.1	0.0702	2,692
210	95.8	0.410	4.68	0.0134	36.9	0.0168	137	0.440	3,205
211	-	-	-	-	-	-	-	-	-
212	-	-	117	0.353	23.9	0.0874	141	0.441	3,126
213	-	-	45.1	0.170	-	-	45.1	0.170	3,770
214	46.5	0.0350	28.5	0.104	32.5	0.0054	108	0.145	1,346
215	-	-	75.6	0.238	5.17	-	80.8	0.238	2,941
216	26.1	0.0370	-	-	0.0006	0.0000	26.1	0.0370	1,419
217	23.7	0.0050	-	-	93.9	0.0561	118	0.0611	520
218	0.0058	0.0000	0.0061	0.0000	38.6	0.149	38.6	0.149	3,858
219	8.62	0.0029	33.8	0.0893	42.3	0.162	84.7	0.254	3,002
220	4.86	0.0113	53.3	0.137	5.34	-	63.6	0.148	2,328
221	27.7	0.105	-	-	37.5	0.0867	65.2	0.192	2,939
222	67.7	0.280	45.6	0.0927	54.7	0.0649	168	0.437	2,603
223	7.61	0.0701	3.38	0.0085	14.6	0.0117	25.5	0.0903	3,537
224	-	-	-	-	37.0	0.0401	37.0	0.0401	1,085
225	58.4	0.0208	-	-	0.0003	0.0000	58.4	0.0208	356
226	7.32	0.0023	-	-	64.9	0.0382	72.2	0.0405	560
227	18.7	0.0097	0.0041	0.0000	-	-	18.7	0.0097	517
228	31.6	0.0109	-	-	-	-	31.6	0.0109	344
229	21.8	0.0186	-	-	-	-	21.8	0.0186	855
230	67.0	0.111	-	-	-	-	67.0	0.111	1,652
231	-	-	-	-	61.7	0.0679	61.7	0.0679	1,100
232	-	-	-	-	0.0083	0.0000	0.0083	0.0000	547
233	65.5	0.0457	-	-	10.6	0.0063	76.2	0.0521	684
234	45.0	0.0096	-	-	6.61	0.0039	51.7	0.0135	262
235	-	-	-	-	77.0	0.0571	77.0	0.0571	742
236	-	-	-	-	63.1	0.0908	63.1	0.0908	1,440
237	58.0	0.0125	-	-	44.2	0.0268	102	0.0393	384
238	56.4	0.0128	-	-	0.262	0.0002	56.7	0.0130	229
239	70.1	0.0221	-	-	73.0	0.0436	143	0.0657	459
240	60.9	0.0129	-	-	0.0001	0.0000	60.9	0.0129	212
241	173	0.0352	-	-	-	-	173	0.0352	204
242	230	0.0937	-	-	-	-	230	0.0937	407
243	218	0.104	-	-	4.61	0.0118	222	0.116	523
244	199	0.0894	-	-	-	-	199	0.0894	450
245	229	0.0910	-	-	8.32	0.0091	237	0.100	423
246	161	0.0456	0.464	0.0004	13.8	0.0103	175	0.0563	322
247	264	0.0877	-	-	12.7	0.0169	277	0.105	378
248	42.9	0.0794	-	-	62.4	0.0491	105	0.129	1,221
249	35.1	0.176	18.0	0.0520	0.0011	0.0000	53.2	0.228	4,295
250	16.0	0.0704	-	-	1.37	0.0015	17.4	0.0719	4,139
251	17.3	0.0684	-	-	38.6	0.0425	55.9	0.111	1,982
252	83.3	0.0463	-	-	8.29	0.0091	91.6	0.0554	604
253	43.3	0.0672	-	-	92.8	0.102	136	0.169	1,243
254	33.2	0.0131	-	-	19.8	0.0217	53.0	0.0348	656
255	31.4	0.0181	-	-	19.0	0.0209	50.4	0.0390	773
256	22.6	0.0444	-	-	6.46	0.0071	29.1	0.0515	1,771
257	82.3	0.236	-	-	13.3	0.0146	95.6	0.250	2,619
258	-	-	8.85	0.0213	49.0	0.0694	57.8	0.0906	1,567
259	0.0013	0.0000	78.7	0.407	4.09	0.0092	82.8	0.416	5,029
260	0.0828	0.0002	-	-	218	-	219	0.0002	0.880
261	61.5	0.275	-	-	11.9	-	73.4	0.275	3,748
262	121	0.0925	-	-	18.2	0.0421	139	0.135	968
263	158	0.146	-	-	0.518	0.0006	159	0.147	926
264	85.5	0.250	-	-	27.4	0.0307	113	0.281	2,490
265	46.4	0.0599	-	-	11.3	0.0279	57.7	0.0878	1,522
266	33.1	0.0250	-	-	-	-	33.1	0.0250	757
267	74.9	0.0895	-	-	0.972	0.0005	75.9	0.0900	1,186
268	26.7	0.148	10.6	0.0338	21.2	0.0300	58.6	0.211	3,609
269	46.6	0.122	-	-	35.5	0.0525	82.1	0.175	2,127
270	20.9	0.0809	-	-	3.37	0.0020	24.3	0.0829	3,418
271	71.2	0.132	-	-	0.0711	0.0001	71.3	0.132	1,854
272	-	-	-	-	53.9	0.0593	53.9	0.0593	1,100
273	-	-	-	-	23.1	0.0226	23.1	0.0226	979
274	39.9	0.178	5.00	0.0270	54.3	0.0570	99.1	0.262	2,647
275	17.1	0.0955	-	-	3.43	0.0038	20.5	0.0993	4,846
276	39.8	0.151	84.8	0.206	37.5	0.0418	162	0.399	2,461
277	-	-	36.2	0.0928	-	-	36.2	0.0928	2,568
278	0.0010	0.0000	-	-	26.3	0.0741	26.3	0.0741	2,821
279	56.6	0.0608	-	-	0.370	0.0005	57.0	0.0613	1,076
280	91.8	0.0136	-	-	14.5	0.0050	106	0.0186	175
281	12.2	0.0048	-	-	35.1	0.0386	47.3	0.0434	917
282	29.4	0.0365	-	-	-	-	29.4	0.0365	1,243
283	54.7	0.0234	-	-	18.0	0.0198	72.7	0.0432	594
284	52.2	0.0471	-	-	49.4	0.0668	102	0.114	1,121
285	107	0.0432	-	-	16.4	0.0180	123	0.0612	496

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
286	51.3	0.0622	-	-	33.4	0.0471	84.7	0.109	1,290
287	11.0	0.0050	-	-	-	-	11.0	0.0050	454
288	24.6	0.0092	-	-	27.1	0.0298	51.7	0.0390	755
289	47.5	0.0164	-	-	3.50	0.0038	51.0	0.0202	397
290	114	0.0594	-	-	0.0003	0.0000	114	0.0594	520
291	36.9	0.0372	-	-	9.78	0.0034	46.7	0.0405	868
292	84.8	0.0228	-	-	8.21	0.0028	93.1	0.0256	275
293	-	-	-	-	38.1	0.0131	38.1	0.0131	344
294	8.55	0.0054	-	-	21.4	0.0139	29.9	0.0193	646
295	39.5	0.0526	-	-	3.68	0.0040	43.2	0.0566	1,312
296	14.0	0.0092	-	-	17.1	0.0188	31.1	0.0280	901
297	114	0.0561	-	-	46.0	0.0202	160	0.0762	476
298	54.0	0.0211	-	-	-	-	54.0	0.0211	391
299	43.0	0.0175	-	-	17.0	0.0187	60.0	0.0362	603
300	0.368	0.0002	-	-	17.7	0.0084	18.0	0.0087	480
301	99.9	0.0778	-	-	6.60	0.0084	107	0.0862	810
302	55.7	0.0980	-	-	9.92	0.0130	65.6	0.111	1,692
303	69.9	0.0655	-	-	16.8	0.0249	86.7	0.0903	1,042
304	58.5	0.0634	-	-	8.41	0.0092	66.9	0.0727	1,086
305	122	0.284	3.37	0.0114	10.6	0.0138	136	0.309	2,275
306	137	0.0789	-	-	21.1	0.0111	159	0.0900	568
307	78.2	0.0717	-	-	15.8	0.0125	94.0	0.0842	896
308	47.8	0.0621	-	-	-	-	47.8	0.0621	1,299
309	30.0	0.0113	-	-	-	-	30.0	0.0113	376
310	42.5	0.0204	-	-	2.66	-	45.2	0.0204	452
311	135	0.0588	-	-	11.5	0.0126	147	0.0715	486
312	62.1	0.0364	-	-	18.0	-	80.2	0.0364	454
313	86.9	0.120	-	-	-	-	86.9	0.120	1,381
314	70.1	0.0436	-	-	15.3	0.0000	85.4	0.0436	511
315	76.5	0.0439	-	-	31.2	-	108	0.0439	407
316	104	0.0562	-	-	4.54	-	108	0.0562	520
317	91.6	0.0524	-	-	17.6	-	109	0.0524	480
318	126	0.0927	-	-	29.5	0.0000	155	0.0927	598
319	119	0.0878	-	-	-	-	119	0.0878	739
320	32.0	0.0156	-	-	-	-	32.0	0.0156	487
321	110	0.0896	-	-	4.10	0.0056	115	0.0952	832
322	111	0.0468	-	-	-	-	111	0.0468	422
323	25.0	0.0529	-	-	-	-	25.0	0.0529	2,112
324	57.2	0.0252	-	-	13.9	0.0152	71.1	0.0404	569
325	221	0.114	-	-	9.10	0.0121	231	0.126	546
326	130	0.0462	-	-	5.05	0.0055	135	0.0518	383
327	229	0.110	-	-	32.8	0.0270	262	0.137	522
328	115	0.0811	-	-	-	-	115	0.0811	704
329	112	0.0658	-	-	4.31	0.0082	117	0.0740	635
330	27.8	0.0371	-	-	21.1	0.0232	48.9	0.0603	1,232
331	72.3	0.0278	-	-	0.0001	0.0000	72.3	0.0278	385
332	53.9	0.0211	-	-	3.49	0.0038	57.4	0.0249	434
333	144	0.0961	-	-	8.27	0.0091	152	0.105	690
334	58.7	0.0729	-	-	5.35	0.0059	64.0	0.0787	1,230
335	41.8	0.0497	-	-	0.937	0.0010	42.7	0.0507	1,188
336	60.6	0.0426	-	-	6.85	0.0075	67.4	0.0502	744
337	128	0.0748	-	-	7.18	0.0076	135	0.0824	611
338	70.2	0.102	-	-	7.23	0.0000	77.4	0.102	1,312
339	33.5	0.0451	-	-	15.4	0.0222	48.9	0.0674	1,377
340	39.5	0.0843	-	-	20.9	0.0230	60.4	0.107	1,776
341	77.7	0.0304	-	-	-	-	77.7	0.0304	391
342	91.1	0.0476	-	-	23.8	0.0261	115	0.0738	642
343	61.3	0.0765	1.42	0.0050	0.572	0.0008	63.3	0.0823	1,300
344	99.6	0.156	-	-	5.15	0.0069	105	0.163	1,560
345	142	0.0996	54.7	0.169	7.61	0.0000	204	0.268	1,314
346	29.1	0.0532	-	-	21.7	0.0160	50.8	0.0692	1,361
347	105	0.0451	-	-	28.0	0.0000	133	0.0451	339
348	56.0	0.293	0.761	0.0022	23.9	0.0556	80.7	0.351	4,343
349	23.5	0.0684	1.01	0.0030	21.6	0.0246	46.1	0.0960	2,083
350	35.8	0.0335	-	-	3.94	0.0046	39.7	0.0381	959
351	95.5	0.661	5.34	0.0137	53.1	0.0787	154	0.753	4,894
352	106	0.275	-	-	-	-	106	0.275	2,589
353	64.4	0.0281	-	-	-	-	64.4	0.0281	436
354	71.1	0.0512	-	-	-	-	71.1	0.0512	720
355	178	0.0731	-	-	3.79	0.0042	181	0.0773	426
356	29.4	0.0117	-	-	0.0002	0.0000	29.4	0.0117	397
357	20.5	0.0080	-	-	-	-	20.5	0.0080	391
358	28.2	0.0205	-	-	-	-	28.2	0.0205	728
359	6.32	0.0025	-	-	0.0001	0.0000	6.32	0.0025	391
360	62.0	0.0370	-	-	0.0002	0.0000	62.0	0.0370	596
361	30.3	0.0129	-	-	-	-	30.3	0.0129	427
362	95.4	0.0553	-	-	2.37	0.0027	97.7	0.0580	594
363	118	0.0409	-	-	-	-	118	0.0409	347
364	40.5	0.107	-	-	35.8	0.0282	76.2	0.135	1,776
365	79.2	0.0268	-	-	2.43	-	81.6	0.0268	328
366	24.0	0.0094	-	-	9.08	0.0100	33.1	0.0194	586
367	6.34	0.0326	55.3	0.123	126	0.163	188	0.319	1,698
368	133	0.138	4.75	0.0046	5.79	0.0008	143	0.144	1,004
369	12.4	0.0056	1.90	0.0066	1.44	-	15.7	0.0122	780
370	80.5	0.0968	13.7	0.0413	16.2	0.0168	110	0.155	1,403
371	-	-	-	-	30.7	0.102	30.7	0.102	3,315
372	-	-	-	-	48.0	0.114	48.0	0.114	2,367
373	-	-	-	-	111	0.213	111	0.213	1,926
374	38.5	0.0523	-	-	4.19	0.0046	42.7	0.0569	1,332
375	41.9	0.0234	-	-	9.58	0.0005	51.5	0.0239	464
376	12.4	0.0040	-	-	10.3	0.0177	22.7	0.0217	957
377	41.0	0.100	-	-	12.8	-	53.9	0.100	1,863
378	21.7	0.0061	-	-	-	-	21.7	0.0061	280
379	-	-	115	0.347	9.34	0.0028	124	0.350	2,813
380	69.8	0.0887	13.2	0.0339	53.2	0.0743	136	0.197	1,445

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
381	32.3	0.0655	-	-	-	-	32.3	0.0655	2,026
382	1.29	0.0049	-	-	88.7	0.0974	90.0	0.102	1,136
383	75.0	0.0496	-	-	4.39	0.0051	79.4	0.0547	689
384	77.6	0.0155	-	-	-	-	77.6	0.0155	199
385	9.02	0.0025	-	-	0.0004	0.0000	9.02	0.0025	277
386	22.6	0.0123	-	-	19.5	0.0215	42.1	0.0338	802
387	47.7	0.0101	-	-	13.4	0.0080	61.1	0.0181	296
388	16.0	0.0024	-	-	-	-	16.0	0.0024	151
389	3.13	0.0012	-	-	55.2	0.0607	58.3	0.0619	1,061
390	31.1	0.0433	0.0063	0.0000	23.8	0.0215	54.8	0.0647	1,181
391	18.9	0.0380	-	-	33.8	0.0389	52.7	0.0768	1,459
392	38.4	0.0774	-	-	0.0017	0.0000	38.4	0.0774	2,013
393	24.7	0.0261	-	-	56.8	0.0497	81.5	0.0758	930
394	87.1	0.0460	-	-	18.3	0.0144	105	0.0604	573
395	103	0.0463	-	-	33.0	0.0413	136	0.0876	644
396	44.6	0.129	-	-	2.62	0.0024	47.2	0.131	2,776
397	33.2	0.0096	-	-	21.9	0.0001	55.1	0.0097	176
398	68.4	0.0238	-	-	17.8	0.0000	86.2	0.0238	276
399	18.3	0.0051	-	-	-	-	18.3	0.0051	277
400	51.6	0.0292	-	-	24.4	-	76.0	0.0292	384
401	23.3	0.0398	6.69	0.0172	-	-	30.0	0.0569	1,899
402	44.8	0.0133	-	-	19.7	-	64.5	0.0133	207
403	-	-	-	-	59.5	0.118	59.5	0.118	1,985
404	-	-	-	-	122	0.311	122	0.311	2,537
405	-	-	-	-	23.6	0.0259	23.6	0.0259	1,098
406	74.4	0.0529	-	-	17.1	0.0188	91.5	0.0717	783
407	272	0.176	-	-	22.0	0.0483	294	0.224	763
408	137	0.0715	-	-	19.3	-	156	0.0715	459
409	103	0.0682	37.2	0.129	31.2	0.0289	171	0.226	1,323
410	-	-	61.9	0.181	-	-	61.9	0.181	2,921
411	33.2	0.0105	102	0.332	-	-	135	0.342	2,536
412	-	-	-	-	255	0.280	255	0.280	1,098
413	-	-	-	-	111	0.122	111	0.122	1,098
414	-	-	-	-	15.1	0.0166	15.1	0.0166	1,100
415	-	-	-	-	22.8	0.0233	22.8	0.0233	1,021
416	-	-	12.5	0.0323	139	0.302	152	0.335	2,207
417	-	-	67.8	0.334	19.1	-	86.8	0.334	3,849
418	-	-	12.0	0.0383	1.72	-	13.7	0.0383	2,797
419	7.92	0.0085	51.8	0.146	27.6	-	87.3	0.155	1,772
420	29.0	0.0467	29.2	0.128	3.95	-	62.2	0.174	2,805
421	-	-	31.2	0.0864	1.48	-	32.7	0.0864	2,645
422	-	-	1.63	0.0042	147	0.170	148	0.174	1,173
423	24.1	0.0068	-	-	0.905	-	25.0	0.0068	272
424	14.3	0.0040	-	-	-	-	14.3	0.0040	277
425	12.3	0.0034	-	-	-	-	12.3	0.0034	277
426	24.9	0.0069	-	-	-	-	24.9	0.0069	277
427	19.3	0.0054	-	-	3.86	-	23.2	0.0054	231
428	14.4	0.0040	-	-	10.0	0.0110	24.4	0.0150	614
429	11.3	0.0031	-	-	-	-	11.3	0.0031	277
430	6.72	0.0020	-	-	0.717	-	7.44	0.0020	267
431	-	-	-	-	0.396	0.0004	0.396	0.0004	1,100
432	-	-	-	-	108	0.145	108	0.145	1,345
433	51.3	0.0814	38.5	0.0987	14.9	-	105	0.180	1,722
434	126	0.0492	-	-	-	-	126	0.0492	390
435	94.4	0.0349	-	-	0.116	0.0001	94.5	0.0350	370
436	35.1	0.0727	-	-	-	-	35.1	0.0727	2,072
437	10.7	0.0215	-	-	5.79	0.0173	16.5	0.0389	2,359
438	147	0.100	-	-	10.1	0.0119	157	0.112	715
439	91.7	0.0145	-	-	-	-	91.7	0.0145	158
440	81.9	0.0145	-	-	-	-	81.9	0.0145	177
441	125	0.0240	-	-	-	-	125	0.0240	192
442	81.2	0.0557	-	-	-	-	81.2	0.0557	686
443	146	0.269	-	-	5.64	0.0066	152	0.276	1,819
444	49.2	0.0180	-	-	-	-	49.2	0.0180	366
445	78.7	0.0376	-	-	-	-	78.7	0.0376	478
446	49.2	0.187	-	-	-	-	49.2	0.187	3,800
447	44.0	0.167	-	-	-	-	44.0	0.167	3,800
448	166	0.633	-	-	132	0.490	298	1.12	3,764
449	61.8	0.235	-	-	132	0.497	193	0.732	3,782
450	321	0.166	-	-	-	-	321	0.166	517
451	142	0.0638	0.337	0.0010	-	-	142	0.0648	455
452	259	0.168	1.89	0.0029	1.44	0.0000	263	0.171	653
453	29.7	0.0111	-	-	-	-	29.7	0.0111	373
454	29.9	0.0124	-	-	0.0000	0.0000	29.9	0.0124	415
455	25.7	0.0799	-	-	26.7	0.0362	52.4	0.116	2,213
456	37.7	0.0584	-	-	-	-	37.7	0.0584	1,550
457	-	-	-	-	30.9	0.113	30.9	0.113	3,659
458	-	-	-	-	56.8	0.0648	56.8	0.0648	1,140
459	-	-	-	-	21.1	0.0802	21.1	0.0802	3,800
460	-	-	-	-	26.1	0.0140	26.1	0.0140	537
461	69.0	0.262	-	-	3.59	0.0136	72.6	0.276	3,800
462	7.80	0.0297	-	-	87.1	0.123	94.9	0.152	1,607
463	7.12	0.0028	-	-	0.828	0.0025	7.94	0.0053	664
464	12.0	0.0064	-	-	0.0338	0.0001	12.0	0.0065	544
465	73.4	0.279	-	-	0.620	0.0024	74.0	0.281	3,800
466	-	-	12.2	0.0160	4.27	0.0023	16.5	0.0183	1,111
467	40.7	0.0260	-	-	43.8	0.0157	84.4	0.0417	494
468	15.5	0.0046	-	-	42.4	0.0515	58.0	0.0560	966
469	47.8	0.0271	-	-	35.0	0.0390	82.8	0.0661	799
470	4.05	0.0029	-	-	2.16	-	6.21	0.0029	466
471	-	-	-	-	14.3	0.0322	14.3	0.0322	2,251
472	-	-	-	-	29.8	0.0802	29.8	0.0802	2,695
473	20.5	0.0041	-	-	166	0.632	187	0.636	3,405
474	3.40	0.0009	-	-	57.5	0.218	60.9	0.219	3,604
475	52.4	0.0184	-	-	0.0000	0.0000	52.4	0.0184	352

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
476	105	0.0326	-	-	0.0055	0.0000	105	0.0327	311
477	70.1	0.0243	-	-	0.0972	0.0004	70.2	0.0246	351
478	-	-	-	-	114	0.434	114	0.434	3,800
479	-	-	-	-	-	-	-	-	-
480	36.7	0.0164	-	-	9.31	0.0165	46.0	0.0329	714
481	39.5	0.0141	-	-	1.25	0.0012	40.7	0.0154	377
482	12.3	0.0043	-	-	36.8	0.0360	49.2	0.0403	820
483	29.2	0.0132	-	-	36.5	0.0398	65.7	0.0530	806
484	14.6	0.0086	-	-	-	-	14.6	0.0086	589
485	11.0	0.0184	-	-	2.02	-	13.0	0.0184	1,410
486	14.6	0.0073	-	-	8.57	-	23.2	0.0073	316
487	12.4	0.0043	-	-	-	-	12.4	0.0043	348
488	18.9	0.0029	-	-	8.89	0.0087	27.8	0.0115	415
489	31.3	0.0063	-	-	0.0021	0.0000	31.3	0.0063	200
490	46.7	0.0164	-	-	6.14	0.0007	52.8	0.0171	325
491	2.27	0.0008	-	-	17.3	0.0169	19.6	0.0177	905
492	28.9	0.0235	-	-	11.1	0.0000	40.0	0.0235	587
493	25.8	0.0140	-	-	-	-	25.8	0.0140	540
494	78.4	0.0353	-	-	10.7	0.0001	89.1	0.0354	397
495	23.6	0.0083	-	-	2.49	-	26.1	0.0083	319
496	47.6	0.0329	-	-	0.0020	0.0000	47.6	0.0329	690
497	56.5	0.0403	-	-	0.460	-	56.9	0.0403	708
498	19.4	0.0081	-	-	0.0038	-	19.4	0.0081	419
499	19.3	0.0296	-	-	9.16	0.0169	28.5	0.0465	1,634
500	33.0	0.0259	-	-	15.4	0.0030	48.4	0.0290	599
501	61.8	0.0234	-	-	0.148	0.0004	62.0	0.0238	384
502	79.5	0.0287	-	-	0.0132	0.0000	79.5	0.0287	361
503	24.6	0.0091	-	-	0.549	0.0000	25.2	0.0091	360
504	17.9	0.0062	-	-	6.48	0.0000	24.4	0.0062	255
505	15.1	0.0135	-	-	-	-	15.1	0.0135	892
506	18.8	0.0329	-	-	0.0015	-	18.8	0.0329	1,751
507	19.8	0.0368	-	-	-	-	19.8	0.0368	1,856
508	46.6	0.110	-	-	5.58	0.0014	52.2	0.111	2,127
509	0.0023	0.0000	-	-	49.3	0.314	49.3	0.314	6,382
510	0.261	0.0010	-	-	35.0	0.196	35.3	0.197	5,572
511	33.7	0.128	-	-	4.41	0.0108	38.1	0.139	3,643
512	-	-	-	-	134	0.237	134	0.237	1,769
513	1.69	0.0055	-	-	4.33	0.0077	6.02	0.0131	2,180
514	5.26	0.0060	-	-	92.6	-	97.9	0.0060	61.0
515	15.8	0.0084	4.82	0.0060	14.0	-	34.7	0.0144	415
516	31.4	0.0446	-	-	9.74	-	41.2	0.0446	1,084
517	14.9	0.0067	-	-	9.31	0.0000	24.3	0.0067	275
518	17.2	0.0214	-	-	1.92	0.0000	19.1	0.0214	1,119
519	45.4	0.0380	-	-	9.71	0.0172	55.1	0.0552	1,003
520	26.4	0.0227	-	-	-	-	26.4	0.0227	861
521	38.9	0.0454	-	-	0.0065	0.0000	38.9	0.0454	1,168
522	39.4	0.0180	-	-	15.1	0.0266	54.4	0.0446	820
523	14.2	0.0387	-	-	-	-	14.2	0.0387	2,728
524	43.1	0.0222	-	-	-	-	43.1	0.0222	516
525	48.0	0.0215	-	-	-	-	48.0	0.0215	447
526	33.8	0.0154	-	-	-	-	33.8	0.0154	454
527	36.2	0.0161	-	-	-	-	36.2	0.0161	446
528	17.5	0.0424	-	-	0.833	-	18.3	0.0424	2,316
529	54.2	0.0315	-	-	5.71	-	59.9	0.0315	526
530	15.5	0.0108	-	-	6.14	-	21.6	0.0108	502
531	42.1	0.0292	-	-	33.1	0.0177	75.2	0.0469	624
532	14.7	0.0067	-	-	6.15	-	20.9	0.0067	320
533	14.1	0.0102	-	-	3.09	-	17.2	0.0102	596
534	5.34	0.0173	-	-	24.8	0.0004	30.2	0.0177	587
535	-	-	4.71	0.0059	27.0	0.0209	31.7	0.0268	847
536	-	-	-	-	37.5	0.0493	37.5	0.0493	1,312
537	-	-	-	-	32.5	0.0224	32.5	0.0224	692
538	-	-	8.41	0.0119	-	-	8.41	0.0119	1,419
539	6.70	0.0215	-	-	27.2	0.0258	33.9	0.0472	1,391
540	6.10	0.0196	-	-	-	-	6.10	0.0196	3,206
541	39.0	0.0670	-	-	1.86	-	40.9	0.0670	1,639
542	10.2	0.0290	16.0	0.0667	2.12	0.0038	28.3	0.0995	3,513
543	-	-	-	-	5.40	0.0029	5.40	0.0029	537
544	-	-	10.5	0.0131	3.89	0.0021	14.4	0.0152	1,061
545	6.61	0.0195	4.45	0.0087	4.04	0.0018	15.1	0.0300	1,990
546	-	-	22.8	0.0286	0.774	0.0011	23.6	0.0297	1,260
547	-	-	19.6	0.0247	1.70	0.0009	21.3	0.0256	1,198
548	-	-	35.7	0.0449	-	-	35.7	0.0449	1,259
549	12.0	0.0132	-	-	12.9	0.0067	24.9	0.0198	798
550	-	-	6.98	0.0088	-	-	6.98	0.0088	1,255
551	-	-	26.1	0.0328	-	-	26.1	0.0328	1,255
552	-	-	32.1	0.0422	-	-	32.1	0.0422	1,316
553	-	-	25.3	0.0317	-	-	25.3	0.0317	1,255
554	6.40	0.0009	9.27	0.0116	0.0001	0.0000	15.7	0.0125	798
555	16.3	0.0023	6.41	0.0080	-	-	22.7	0.0103	455
556	0.142	0.0001	9.67	0.0149	-	-	9.81	0.0150	1,531
557	35.5	0.0213	-	-	1.72	0.0000	37.2	0.0213	571
558	6.16	0.0199	-	-	41.3	0.0634	47.4	0.0833	1,756
559	65.5	0.0467	-	-	14.1	-	79.6	0.0467	588
560	48.1	0.0221	-	-	9.98	0.0176	58.1	0.0398	684
561	18.3	0.0082	-	-	-	-	18.3	0.0082	446
562	30.2	0.0508	-	-	-	-	30.2	0.0508	1,684
563	84.0	0.107	-	-	-	-	84.0	0.107	1,275
564	43.7	0.0302	-	-	28.2	0.0027	72.0	0.0329	458
565	23.6	0.0135	-	-	14.1	0.0020	37.7	0.0155	411
566	52.9	0.0484	-	-	26.4	0.0466	79.3	0.0950	1,199
567	-	-	-	-	10.0	0.0025	10.0	0.0025	250
568	8.52	0.0121	-	-	18.6	-	27.1	0.0121	447
569	-	-	30.5	0.0382	-	-	30.5	0.0382	1,255
570	-	-	-	-	25.5	0.0969	25.5	0.0969	3,800

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Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
571	26.1	0.0195	-	-	21.8	0.0774	47.9	0.0969	2,021
572	71.8	0.212	-	-	23.6	0.115	95.4	0.327	3,427
573	52.8	0.129	-	-	9.62	0.0206	62.5	0.149	2,388
574	85.1	0.101	-	-	2.12	0.0024	87.3	0.103	1,183
575	26.8	0.0181	-	-	-	-	26.8	0.0181	678
576	13.9	0.0048	-	-	0.0004	-	13.9	0.0048	348
577	9.91	0.0038	-	-	12.1	0.0443	22.0	0.0482	2,186
578	-	-	4.72	0.0068	-	-	4.72	0.0068	1,433
579	62.6	0.182	-	-	17.4	0.0658	80.0	0.248	3,099
580	56.6	0.0529	-	-	12.4	0.0173	69.0	0.0702	1,017
581	68.7	0.0642	-	-	52.3	0.0482	121	0.112	929
582	24.6	0.0063	-	-	0.0054	-	24.7	0.0063	257
583	-	-	15.1	0.0189	-	-	15.1	0.0189	1,255
584	20.8	0.0761	17.6	0.0731	-	-	38.4	0.149	3,882
585	30.2	0.0312	-	-	0.0306	-	30.2	0.0312	1,033
586	-	-	29.1	0.0380	-	-	29.1	0.0380	1,308
587	-	-	-	-	84.8	0.0609	84.8	0.0609	718
588	47.8	0.0118	-	-	60.8	0.0664	109	0.0782	720
589	38.9	0.0123	-	-	88.7	0.251	128	0.263	2,064
590	6.62	0.0036	-	-	7.17	0.0096	13.8	0.0131	952
591	7.06	0.0069	15.2	0.0190	5.95	0.0032	28.2	0.0292	1,036
592	15.9	0.0055	-	-	-	-	15.9	0.0055	347
593	-	-	-	-	59.6	0.212	59.6	0.212	3,558
594	-	-	-	-	26.7	0.102	26.7	0.102	3,800
595	-	-	-	-	24.7	0.0940	24.7	0.0940	3,800
596	-	-	-	-	3.94	0.0150	3.94	0.0150	3,800
597	17.2	0.0652	-	-	-	-	17.2	0.0652	3,800
598	8.63	0.0328	-	-	-	-	8.63	0.0328	3,800
599	3.95	0.0010	-	-	40.8	0.155	44.8	0.156	3,488
600	-	-	-	-	-	-	-	-	-
601	-	-	-	-	38.4	0.146	38.4	0.146	3,800
602	-	-	-	-	27.9	0.106	27.9	0.106	3,800
603	1.59	0.0048	-	-	89.1	0.327	90.7	0.331	3,653
604	2.29	0.0087	-	-	-	-	2.29	0.0087	3,800
605	-	-	-	-	-	-	-	-	-
606	0.0055	0.0000	-	-	1.22	0.0046	1.23	0.0046	3,783
607	-	-	-	-	49.6	0.189	49.6	0.189	3,800
608	-	-	-	-	36.8	0.140	36.8	0.140	3,800
609	-	-	-	-	8.28	0.0315	8.28	0.0315	3,800
610	19.0	0.0721	-	-	57.3	0.218	76.2	0.290	3,800
611	21.6	0.0822	-	-	61.8	0.235	83.5	0.317	3,800
612	-	-	-	-	37.9	0.144	37.9	0.144	3,800
613	-	-	-	-	35.6	0.135	35.6	0.135	3,799
614	-	-	-	-	60.7	0.231	60.7	0.231	3,800
615	67.3	0.190	-	-	59.4	0.226	127	0.415	3,278
616	-	-	-	-	-	-	-	-	-
617	-	-	-	-	-	-	-	-	-
618	47.1	0.0132	-	-	-	-	47.1	0.0132	280
619	1.05	0.0007	-	-	11.2	0.0207	12.2	0.0214	1,750
620	12.0	0.0090	-	-	2.41	0.0014	14.4	0.0105	726
621	36.6	0.0274	3.68	0.0027	20.7	0.0216	61.0	0.0517	848
622	20.8	0.0062	-	-	19.8	0.0114	40.6	0.0176	434
623	10.9	0.0110	-	-	0.0355	0.0001	10.9	0.0112	1,024
624	25.3	0.0069	-	-	0.797	0.0005	26.1	0.0074	282
625	-	-	-	-	35.4	0.232	35.4	0.232	6,554
626	-	-	-	-	4.62	0.0176	4.62	0.0176	3,800
627	-	-	-	-	27.7	0.105	27.7	0.105	3,800
628	-	-	-	-	0.483	0.0035	0.483	0.0035	7,318
629	1.49	0.0005	-	-	-	-	1.49	0.0005	339
630	-	-	-	-	4.61	0.0088	4.61	0.0088	1,900
631	3.65	0.0124	-	-	21.5	0.0782	25.2	0.0906	3,596
632	8.30	0.0270	-	-	13.7	0.0384	22.0	0.0655	2,973
633	3.86	0.0105	-	-	-	-	3.86	0.0105	2,724
634	51.0	0.0267	-	-	0.0007	0.0000	51.0	0.0267	522
635	15.3	0.0041	-	-	7.84	0.0298	23.1	0.0339	1,463
636	34.5	0.0306	-	-	16.4	0.0353	50.9	0.0659	1,294
637	29.8	0.0127	-	-	5.79	0.0033	35.6	0.0160	449
638	26.0	0.0096	-	-	6.78	0.0078	32.8	0.0174	531
639	8.43	0.0121	-	-	9.81	0.0126	18.2	0.0247	1,356
640	34.7	0.0487	2.39	0.0018	34.4	0.0592	71.5	0.110	1,533
641	19.1	0.0084	-	-	1.66	0.0043	20.8	0.0128	614
642	18.1	0.0038	-	-	-	-	18.1	0.0038	208
643	0.664	0.0023	-	-	4.86	0.0102	5.52	0.0125	2,257
644	13.5	0.0029	-	-	-	-	13.5	0.0029	213
645	6.92	0.0094	-	-	46.1	0.150	53.1	0.159	3,006
646	-	-	-	-	70.3	0.317	70.3	0.317	4,513
647	65.9	0.0653	-	-	12.6	0.0278	78.5	0.0932	1,187
648	4.04	0.0027	-	-	-	-	4.04	0.0027	659
649	5.04	0.0033	-	-	-	-	5.04	0.0033	659
650	16.8	0.0189	-	-	12.9	0.0127	29.7	0.0317	1,067
651	11.0	0.0023	-	-	0.294	0.0002	11.3	0.0025	221
652	20.2	0.0630	-	-	12.5	0.0175	32.7	0.0804	2,457
653	26.0	0.0172	-	-	4.44	0.0082	30.5	0.0254	835
654	12.4	0.0184	-	-	5.73	0.0106	18.1	0.0290	1,599
655	-	-	-	-	58.6	0.198	58.6	0.198	3,379
656	36.2	0.0383	-	-	7.95	0.0135	44.1	0.0518	1,174
657	32.4	0.0280	-	-	4.29	0.0000	36.7	0.0280	765
658	15.4	0.0101	-	-	17.2	0.0392	32.6	0.0493	1,513
659	3.79	0.0053	-	-	28.1	0.0503	31.9	0.0556	1,745
660	53.2	0.0595	-	-	52.7	0.0356	106	0.0951	898
661	0.0000	0.0000	-	-	359	0.666	359	0.666	1,852
662	38.0	0.0140	-	-	12.9	0.0054	50.9	0.0194	381
663	-	-	-	-	21.7	0.0840	21.7	0.0840	3,874
664	8.27	0.0088	-	-	38.8	0.0267	47.1	0.0355	754
665	26.9	0.0179	-	-	0.0431	0.0002	27.0	0.0180	669

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
666	40.1	0.0946	-	-	22.2	0.0407	62.3	0.135	2,171
667	4.10	0.0044	-	-	11.2	0.0055	15.3	0.0098	642
668	26.8	0.0177	-	-	-	-	26.8	0.0177	661
669	34.7	0.0441	-	-	42.0	0.0614	76.7	0.105	1,375
670	56.6	0.0626	-	-	13.4	0.0080	70.0	0.0706	1,009
671	8.08	0.0104	-	-	51.4	0.0438	59.4	0.0542	911
672	66.4	0.277	-	-	0.216	0.0009	66.6	0.278	4,175
673	4.37	0.0030	-	-	0.119	0.0005	4.49	0.0034	760
674	107	0.0375	-	-	22.8	0.0246	130	0.0621	476
675	6.34	0.0023	9.16	0.0121	30.6	0.0301	46.1	0.0444	964
676	34.7	0.0230	-	-	125	0.334	160	0.357	2,232
677	-	-	-	-	18.0	0.0908	18.0	0.0908	5,031
678	3.59	0.0122	-	-	33.3	0.0617	36.9	0.0738	2,002
679	4.48	0.0030	-	-	2.19	0.0041	6.68	0.0070	1,051
680	26.4	0.0402	-	-	31.7	0.0900	58.1	0.130	2,243
681	9.90	0.0278	-	-	-	-	9.90	0.0278	2,813
682	6.56	0.0057	-	-	-	-	6.56	0.0057	872
683	96.0	0.365	-	-	-	-	96.0	0.365	3,800
684	36.8	0.140	-	-	-	-	36.8	0.140	3,800
685	40.5	0.154	-	-	0.0506	0.0002	40.5	0.154	3,800
686	26.4	0.100	-	-	0.0991	0.0004	26.5	0.101	3,800
687	43.5	0.165	-	-	-	-	43.5	0.165	3,800
688	55.7	0.212	-	-	0.0522	0.0002	55.8	0.212	3,800
689	70.1	0.256	-	-	15.6	0.0523	85.7	0.309	3,602
690	97.1	0.309	-	-	3.52	0.0134	101	0.322	3,201
691	52.1	0.198	-	-	0.0118	0.0000	52.1	0.198	3,800
692	64.4	0.245	-	-	-	-	64.4	0.245	3,800
693	51.9	0.197	-	-	-	-	51.9	0.197	3,800
694	30.4	0.115	-	-	-	-	30.4	0.115	3,800
695	0.647	0.0027	-	-	38.0	0.0960	38.7	0.0987	2,552
696	4.17	0.0223	-	-	30.7	0.0682	34.9	0.0905	2,594
697	36.7	0.0417	-	-	-	-	36.7	0.0417	1,136
698	23.3	0.0482	8.11	0.0272	-	-	31.4	0.0754	2,397
699	6.98	0.0089	-	-	-	-	6.98	0.0089	1,274
700	150	0.568	-	-	4.30	0.0124	154	0.581	3,774
701	88.1	0.335	-	-	43.4	0.169	132	0.504	3,829
702	-	-	-	-	149	0.565	149	0.565	3,800
703	-	-	-	-	112	0.424	112	0.424	3,800
704	61.2	0.233	-	-	-	-	61.2	0.233	3,800
705	7.35	0.0100	-	-	46.9	0.178	54.2	0.188	3,470
706	101	0.142	-	-	14.0	-	115	0.142	1,237
707	85.6	0.325	-	-	0.132	0.0005	85.8	0.326	3,800
708	55.6	0.211	-	-	0.175	0.0007	55.7	0.212	3,800
709	27.1	0.103	-	-	-	-	27.1	0.103	3,800
710	12.4	0.0527	-	-	-	-	12.4	0.0527	4,240
711	-	-	-	-	108	0.0688	108	0.0688	639
712	52.6	0.0128	-	-	14.0	0.0116	66.5	0.0244	367
713	42.4	0.0053	-	-	-	-	42.4	0.0053	125
714	87.4	0.0101	-	-	8.71	0.0023	96.1	0.0124	129
715	4.38	0.0043	-	-	200	0.821	204	0.826	4,048
716	35.7	0.0129	-	-	41.4	0.0396	77.1	0.0526	682
717	-	-	-	-	5.25	0.0044	5.25	0.0044	838
718	14.7	0.0044	-	-	4.83	0.0040	19.5	0.0084	432
719	86.0	0.0309	-	-	13.5	0.0066	99.5	0.0375	377
720	31.5	0.0097	-	-	-	-	31.5	0.0097	309
721	42.9	0.0149	-	-	1.67	0.0014	44.6	0.0163	366
722	22.8	0.0107	-	-	1.45	0.0019	24.3	0.0126	519
723	7.86	0.0268	13.2	0.0278	-	-	21.0	0.0545	2,592
724	15.2	0.0153	-	-	2.25	0.0016	17.4	0.0168	966
725	-	-	16.1	0.0510	-	-	16.1	0.0510	3,157
726	-	-	17.1	0.0652	-	-	17.1	0.0652	3,815
727	0.361	0.0019	-	-	11.6	0.0152	12.0	0.0171	1,429
728	12.9	0.0688	-	-	-	-	12.9	0.0688	5,322
729	-	-	23.0	0.0740	3.19	0.0042	26.2	0.0782	2,985
730	11.6	0.0041	-	-	-	-	11.6	0.0041	357
731	0.501	0.0027	14.8	0.0459	-	-	15.3	0.0485	3,180
732	45.5	0.0547	-	-	33.6	0.0296	79.0	0.0842	1,066
733	79.9	0.119	-	-	33.2	0.0292	113	0.149	1,314
734	108	0.154	-	-	8.08	0.0071	116	0.161	1,390
735	13.0	0.0080	-	-	1.35	0.0011	14.4	0.0092	636
736	143	0.0605	-	-	-	-	143	0.0605	422
737	8.49	0.0018	-	-	87.2	0.148	95.7	0.150	1,567
738	47.9	0.101	-	-	13.1	0.0196	60.9	0.121	1,981
739	67.1	0.0152	-	-	31.1	0.0176	98.2	0.0328	334
740	49.2	0.0493	-	-	59.7	0.0349	109	0.0842	773
741	-	-	-	-	65.7	0.193	65.7	0.193	2,943
742	159	0.0291	-	-	1.74	0.0044	161	0.0335	208
743	-	-	0.0027	0.0000	168	0.0712	168	0.0712	423
744	92.1	0.0515	-	-	9.45	-	102	0.0515	507
745	57.1	0.0837	-	-	4.00	0.0034	61.1	0.0871	1,426
746	130	0.0515	-	-	-	-	130	0.0515	398
747	87.6	0.0644	-	-	3.36	-	91.0	0.0644	708
748	9.18	0.0041	-	-	18.8	0.0220	28.0	0.0261	932
749	56.8	0.0479	0.0980	0.0002	12.9	0.0108	69.7	0.0588	844
750	115	0.125	76.2	0.159	10.8	0.0091	201	0.293	1,456
751	53.0	0.0173	-	-	0.0000	0.0000	53.0	0.0173	326
752	137	0.0584	-	-	1.37	0.0011	139	0.0595	429
753	-	-	24.3	0.0509	148	0.124	173	0.175	1,015
754	108	0.0402	-	-	-	-	108	0.0402	372
755	81.8	0.0314	0.257	0.0003	-	-	82.1	0.0317	386
756	24.5	0.0106	-	-	-	-	24.5	0.0106	432
757	62.5	0.0227	-	-	1.77	0.0015	64.3	0.0242	377
758	65.8	0.0291	-	-	1.93	0.0016	67.7	0.0307	453
759	-	-	-	-	84.3	0.0581	84.3	0.0581	689
760	-	-	-	-	120	0.177	120	0.177	1,473

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Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
761	71.8	0.127	-	-	32.1	0.0919	104	0.219	2,107
762	-	-	-	-	198	0.296	198	0.296	1,497
763	9.54	0.0477	-	-	11.0	0.0101	20.5	0.0578	2,812
764	53.4	0.0574	-	-	28.5	0.0022	81.8	0.0596	728
765	7.43	0.0025	-	-	46.8	0.0441	54.3	0.0466	858
766	-	-	-	-	38.3	0.0235	38.3	0.0235	615
767	166	0.143	-	-	20.0	-	186	0.143	768
768	120	0.179	-	-	9.91	-	130	0.179	1,383
769	0.991	0.0015	-	-	22.0	0.0662	23.0	0.0677	2,946
770	-	-	-	-	56.1	0.135	56.1	0.135	2,402
771	106	0.195	-	-	5.43	0.0173	111	0.212	1,903
772	28.2	0.0058	-	-	-	-	28.2	0.0058	206
773	20.2	0.0303	-	-	0.554	-	20.8	0.0303	1,462
774	91.8	0.138	-	-	0.964	0.0000	92.8	0.138	1,487
775	90.2	0.0395	-	-	35.4	0.119	126	0.159	1,266
776	156	0.0415	-	-	20.6	0.0167	177	0.0583	330
777	121	0.0355	-	-	4.93	0.0123	125	0.0478	381
778	80.6	0.0191	-	-	16.4	0.0094	97.0	0.0286	295
779	-	-	-	-	81.8	0.0925	81.8	0.0925	1,131
780	14.0	0.0285	-	-	22.5	0.0127	36.6	0.0413	1,128
781	84.0	0.0694	-	-	67.3	0.0429	151	0.112	742
782	152	0.0847	-	-	28.1	0.0570	180	0.142	788
783	120	0.0626	-	-	1.91	0.0070	122	0.0696	571
784	-	-	-	-	22.2	0.0253	22.2	0.0253	1,140
785	-	-	-	-	33.3	0.0893	33.3	0.0893	2,684
786	22.6	0.0046	-	-	41.4	0.0131	64.0	0.0178	278
787	-	-	-	-	115	0.144	115	0.144	1,254
788	-	-	-	-	31.0	0.110	31.0	0.110	3,546
789	-	-	-	-	20.9	0.0205	20.9	0.0205	981
790	-	-	-	-	73.5	0.171	73.5	0.171	2,329
791	-	-	-	-	24.4	0.0152	24.4	0.0152	620
792	-	-	-	-	59.4	0.435	59.4	0.435	7,318
793	2.94	0.0112	-	-	103	0.240	106	0.251	2,365
794	-	-	-	-	40.9	0.0495	40.9	0.0495	1,211
795	-	-	-	-	50.1	0.101	50.1	0.101	2,019
796	5.37	0.0011	-	-	-	-	5.37	0.0011	206
797	16.3	0.0034	-	-	0.860	-	17.1	0.0034	195
798	44.2	0.0101	-	-	22.0	-	66.2	0.0101	153
799	25.4	0.0052	-	-	2.00	-	27.4	0.0052	191
800	17.7	0.0036	-	-	3.59	-	21.3	0.0036	171
801	12.3	0.0025	-	-	-	-	12.3	0.0025	206
802	17.7	0.0046	-	-	-	-	17.7	0.0046	261
803	43.7	0.0091	-	-	0.179	-	43.9	0.0091	206
804	-	-	-	-	65.5	0.0539	65.5	0.0539	823
805	-	-	-	-	33.2	0.0210	33.2	0.0210	634
806	-	-	-	-	32.8	0.108	32.8	0.108	3,300
807	0.560	0.0028	-	-	21.4	0.0584	22.0	0.0612	2,789
808	92.3	0.186	-	-	7.74	0.0106	100	0.197	1,970
809	15.2	0.0761	-	-	18.9	0.0481	34.2	0.124	3,637
810	-	-	-	-	46.2	0.0972	46.2	0.0972	2,102
811	-	-	-	-	32.6	0.0893	32.6	0.0893	2,738
812	0.741	0.0011	-	-	15.4	0.0383	16.1	0.0394	2,446
813	60.6	0.195	-	-	7.35	0.0195	67.9	0.214	3,155
814	2.09	0.0031	-	-	44.4	0.121	46.5	0.124	2,676
815	95.1	0.0262	-	-	32.9	0.0314	128	0.0576	450
816	66.2	0.0219	5.41	0.0123	13.2	0.0074	84.8	0.0416	491
817	2.72	0.0009	52.7	0.175	-	-	55.4	0.176	3,168
818	56.8	0.0296	26.5	0.0771	4.78	0.0040	88.1	0.111	1,257
819	122	0.0410	-	-	77.9	0.0435	200	0.0845	422
820	45.2	0.0114	-	-	20.5	0.0210	65.7	0.0324	493
821	341	0.0987	-	-	49.5	0.0234	390	0.122	313
822	139	0.206	-	-	18.3	-	157	0.206	1,308
823	0.189	0.0003	-	-	82.6	-	82.8	0.0003	3.43
824	131	0.108	-	-	52.7	0.144	184	0.252	1,368
825	18.6	0.0154	-	-	38.5	0.0196	57.0	0.0350	614
826	172	0.0559	-	-	-	-	172	0.0559	325
827	135	0.0121	-	-	8.01	0.0020	143	0.0142	99.0
828	180	0.0544	-	-	-	-	180	0.0544	302
829	88.5	0.0665	-	-	0.0000	0.0000	88.5	0.0665	751
830	212	0.177	-	-	-	-	212	0.177	832
831	72.4	0.0062	-	-	-	-	72.4	0.0062	85.2
832	73.7	0.0072	-	-	16.9	0.0053	90.6	0.0125	137
833	60.6	0.0106	-	-	-	-	60.6	0.0106	174
834	98.4	0.0866	-	-	40.7	-	139	0.0866	622
835	0.786	0.0013	-	-	6.68	0.0059	7.46	0.0071	958
836	36.0	0.0447	-	-	13.9	0.0310	49.9	0.0757	1,517
837	169	0.101	-	-	0.655	0.0015	170	0.102	603
838	145	0.0594	-	-	0.444	0.0016	146	0.0610	419
839	99.5	0.220	-	-	33.9	0.0764	133	0.296	2,219
840	112	0.243	-	-	9.10	0.0163	121	0.260	2,141
841	34.5	0.0758	-	-	25.6	0.0577	60.1	0.134	2,222
842	44.8	0.100	-	-	-	-	44.8	0.100	2,242
843	13.4	0.0553	-	-	21.1	0.0499	34.5	0.105	3,054
844	74.5	0.179	-	-	0.0001	0.0000	74.5	0.179	2,408
845	26.1	0.0477	-	-	-	-	26.1	0.0477	1,826
846	70.8	0.176	-	-	-	-	70.8	0.176	2,481
847	82.4	0.102	-	-	17.2	0.0132	99.6	0.116	1,159
848	28.4	0.0353	-	-	-	-	28.4	0.0353	1,241
849	48.0	0.0602	-	-	9.15	-	57.1	0.0602	1,054
850	85.0	0.0806	-	-	3.22	0.0000	88.2	0.0806	914
851	45.9	0.0368	-	-	0.942	0.0000	46.9	0.0368	786
852	39.3	0.0181	-	-	22.4	0.0159	61.7	0.0340	552
853	58.8	0.0280	-	-	-	-	58.8	0.0280	477
854	41.1	0.0209	-	-	26.1	0.0219	67.2	0.0428	636
855	52.9	0.232	0.0009	0.0000	0.0084	-	52.9	0.232	4,386

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
856	68.9	0.0668	-	-	-	-	68.9	0.0668	969
857	27.5	0.0127	-	-	20.6	-	48.1	0.0127	264
858	33.5	0.0213	-	-	0.0008	-	33.5	0.0213	637
859	60.3	0.0324	-	-	-	-	60.3	0.0324	537
860	96.2	0.0524	-	-	7.38	-	104	0.0524	506
861	23.7	0.0134	-	-	12.6	-	36.3	0.0134	369
862	80.3	0.0187	2.26	0.0044	35.8	0.0092	118	0.0323	273
863	114	0.0304	-	-	8.51	0.0002	122	0.0306	250
864	-	-	0.0000	0.0000	62.7	0.0525	62.7	0.0525	838
865	9.10	0.0027	-	-	74.1	0.0388	83.2	0.0415	499
866	22.5	0.0033	-	-	-	-	22.5	0.0033	145
867	136	0.147	7.14	0.0076	18.5	-	162	0.155	957
868	87.7	0.0479	-	-	2.23	-	89.9	0.0479	533
869	125	0.117	-	-	23.0	0.0054	148	0.122	827
870	112	0.0245	-	-	25.8	0.0088	138	0.0333	241
871	15.5	0.0529	-	-	2.44	0.0020	18.0	0.0550	3,059
872	61.6	0.116	-	-	2.68	0.0022	64.3	0.118	1,837
873	29.1	0.0339	-	-	-	-	29.1	0.0339	1,165
874	43.4	0.0320	-	-	2.32	0.0019	45.7	0.0339	743
875	87.4	0.0409	-	-	0.508	0.0004	87.9	0.0413	470
876	36.7	0.0151	-	-	-	-	36.7	0.0151	412
877	63.4	0.0255	-	-	-	-	63.4	0.0255	403
878	57.4	0.0226	-	-	-	-	57.4	0.0226	393
879	34.7	0.0151	-	-	-	-	34.7	0.0151	437
880	43.0	0.0583	-	-	6.16	0.0001	49.1	0.0584	1,189
881	28.8	0.0354	-	-	0.0010	0.0000	28.8	0.0354	1,230
882	50.9	0.127	0.705	0.0016	1.79	0.0065	53.4	0.135	2,529
883	44.7	0.0094	-	-	5.34	0.0000	50.0	0.0095	189
884	11.1	0.0026	43.6	0.0893	28.9	-	83.5	0.0919	1,101
885	11.7	0.0036	1.79	0.0035	20.6	0.0102	34.0	0.0173	508
886	-	-	0.148	0.0003	-	-	0.148	0.0003	1,957
887	-	-	0.0002	0.0000	25.2	0.0376	25.2	0.0376	1,488
888	0.0447	0.0000	77.7	0.152	-	-	77.7	0.152	1,956
889	28.9	0.0085	-	-	105	0.0825	134	0.0910	680
890	14.5	0.0093	14.0	0.0581	115	0.136	143	0.204	1,424
891	16.4	0.0104	-	-	3.40	0.0028	19.8	0.0132	669
892	48.0	0.0458	-	-	15.6	0.0131	63.6	0.0589	925
893	0.123	0.0000	-	-	71.0	0.0614	71.2	0.0615	864
894	-	-	-	-	66.7	0.0493	66.7	0.0493	739
895	101	0.0468	-	-	133	0.119	234	0.165	708
896	8.58	0.0036	-	-	88.1	0.0720	96.7	0.0756	782
897	164	0.0592	-	-	8.57	0.0010	173	0.0601	348
898	-	-	-	-	74.2	0.205	74.2	0.205	2,768
899	41.3	0.0284	-	-	13.8	0.0308	55.0	0.0592	1,076
900	-	-	-	-	33.3	0.182	33.3	0.182	5,463
901	56.5	0.0367	-	-	37.4	0.0182	93.9	0.0549	584
902	47.4	0.0323	-	-	28.9	0.0593	76.4	0.0916	1,199
903	21.8	0.0227	7.42	0.0473	127	0.241	156	0.311	1,998
904	138	0.0360	-	-	-	-	138	0.0360	261
905	24.7	0.0104	-	-	2.30	0.0019	27.0	0.0123	456
906	46.3	0.0168	-	-	6.61	0.0055	52.9	0.0223	422
907	108	0.0593	23.6	0.0832	44.0	0.0393	176	0.182	1,035
908	3.49	0.0016	68.1	0.168	151	0.273	223	0.443	1,988
909	83.8	0.0185	-	-	-	-	83.8	0.0185	221
910	16.2	0.0048	-	-	87.9	0.0730	104	0.0778	747
911	54.6	0.0190	-	-	-	-	54.6	0.0190	349
912	94.6	0.0434	-	-	22.1	-	117	0.0434	371
913	201	0.133	-	-	1.97	0.0023	203	0.136	668
914	126	0.115	2.86	0.0030	16.5	0.0205	145	0.139	956
915	48.6	0.0235	2.75	0.0029	44.1	0.0370	95.5	0.0635	665
916	16.9	0.0052	-	-	-	-	16.9	0.0052	305
917	110	0.0347	-	-	41.5	0.0310	151	0.0657	435
918	55.0	0.0354	-	-	-	-	55.0	0.0354	644
919	121	0.0352	2.54	0.0074	10.0	0.0164	134	0.0589	441
920	109	0.0545	-	-	3.66	0.0031	112	0.0576	512
921	63.0	0.0215	-	-	7.12	0.0063	70.1	0.0278	396
922	86.3	0.0453	-	-	38.7	0.0309	125	0.0762	609
923	137	0.0431	-	-	0.0001	0.0000	137	0.0431	315
924	45.4	0.0286	-	-	-	-	45.4	0.0286	630
925	118	0.1000	-	-	16.3	0.0165	134	0.117	870
926	68.8	0.0360	-	-	28.6	0.0323	97.3	0.0684	702
927	69.2	0.0275	-	-	0.446	0.0004	69.6	0.0279	400
928	23.4	0.0282	-	-	37.6	0.0422	61.0	0.0704	1,155
929	57.1	0.0217	-	-	0.236	0.0002	57.3	0.0219	382
930	36.5	0.0327	-	-	5.45	0.0055	41.9	0.0382	911
931	12.4	0.0175	-	-	31.0	0.0324	43.4	0.0498	1,149
932	14.6	0.0153	-	-	-	-	14.6	0.0153	1,050
933	51.4	0.0267	-	-	16.9	0.0167	68.3	0.0435	636
934	2.58	0.0052	2.93	0.0075	23.2	0.0303	28.7	0.0430	1,494
935	34.5	0.0309	-	-	2.16	-	36.6	0.0309	844
936	-	-	-	-	36.0	0.0471	36.0	0.0471	1,308
937	-	-	-	-	36.7	0.0494	36.7	0.0494	1,348
938	8.77	0.0204	47.8	0.0984	-	-	56.6	0.119	2,098
939	11.9	0.0635	23.7	0.0727	-	-	35.6	0.136	3,821
940	15.3	0.0060	-	-	-	-	15.3	0.0060	394
941	0.0023	0.0000	0.0002	0.0000	62.9	0.0471	62.9	0.0471	749
942	-	-	-	-	37.5	0.0294	37.5	0.0294	783
943	9.36	0.0036	-	-	2.99	0.0025	12.4	0.0062	498
944	-	-	-	-	57.3	0.0481	57.3	0.0481	838
945	-	-	-	-	17.0	0.0486	17.0	0.0486	2,861
946	12.8	0.0150	-	-	6.57	0.0055	19.4	0.0205	1,057
947	0.0021	0.0000	-	-	39.1	0.0342	39.1	0.0342	874
948	39.8	0.0168	-	-	0.0326	0.0000	39.9	0.0168	421
949	85.0	0.0544	-	-	6.59	0.0045	91.6	0.0590	644
950	-	-	14.8	0.0454	-	-	14.8	0.0454	3,055

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
951	197	0.364	-	-	75.6	0.105	273	0.469	1,720
952	-	-	16.9	0.0378	-	-	16.9	0.0378	2,241
953	-	-	39.8	0.0778	-	-	39.8	0.0778	1,957
954	-	-	36.7	0.0726	-	-	36.7	0.0726	1,977
955	38.6	0.0482	-	-	3.54	0.0046	42.1	0.0528	1,255
956	6.10	0.0325	-	-	2.69	0.0035	8.79	0.0360	4,094
957	89.1	0.143	-	-	2.44	-	91.6	0.143	1,559
958	-	-	26.7	0.0518	5.77	0.0211	32.4	0.0729	2,248
959	-	-	14.3	0.0435	0.161	0.0002	14.4	0.0437	3,031
960	12.9	0.0388	9.98	0.0305	0.0160	0.0000	22.9	0.0693	3,026
961	-	-	6.88	0.0209	0.164	0.0002	7.05	0.0211	2,999
962	30.5	0.123	-	-	6.53	0.0085	37.0	0.131	3,548
963	99.9	0.0743	-	-	0.0151	0.0000	100.0	0.0743	744
964	0.0056	0.0000	-	-	27.0	0.0167	27.0	0.0167	616
965	32.1	0.0152	-	-	0.168	0.0002	32.3	0.0154	477
966	-	-	-	-	13.1	0.0110	13.1	0.0110	838
967	3.11	0.0013	-	-	32.8	0.0275	35.9	0.0288	801
968	-	-	-	-	97.3	0.0935	97.3	0.0935	962
969	-	-	-	-	64.1	0.0537	64.1	0.0537	838
970	-	-	-	-	2.62	0.0022	2.62	0.0022	838
971	29.3	0.0390	-	-	0.266	0.0003	29.6	0.0393	1,329
972	21.9	0.0175	-	-	1.21	-	23.1	0.0175	758
973	102	0.0947	-	-	3.43	0.0045	106	0.0992	939
974	122	0.0629	-	-	1.78	0.0035	124	0.0664	534
975	-	-	-	-	24.1	0.0329	24.1	0.0329	1,361
976	13.6	0.0110	-	-	33.0	0.0290	46.6	0.0400	860
977	139	0.0750	-	-	10.2	0.0090	149	0.0840	562
978	91.3	0.0350	-	-	7.51	0.0066	98.8	0.0416	421
979	17.1	0.0222	7.04	0.0138	31.3	0.0262	55.4	0.0622	1,121
980	104	0.0348	-	-	2.18	0.0018	106	0.0366	346
981	36.4	0.0143	-	-	0.0008	0.0000	36.4	0.0143	394
982	91.6	0.0356	-	-	13.2	0.0111	105	0.0467	446
983	50.0	0.0671	-	-	26.9	0.0249	76.9	0.0920	1,197
984	-	-	-	-	67.8	0.0652	67.8	0.0652	962
985	29.8	0.0112	-	-	-	-	29.8	0.0112	377
986	55.5	0.0258	-	-	-	-	55.5	0.0258	465
987	144	0.0765	-	-	10.0	0.0043	155	0.0808	523
988	75.8	0.0469	-	-	6.44	0.0057	82.2	0.0526	640
989	142	0.185	-	-	22.5	0.0198	164	0.205	1,246
990	99.5	0.167	14.1	0.0151	1.35	-	115	0.182	1,580
991	48.8	0.0914	-	-	-	-	48.8	0.0914	1,873
992	45.3	0.0385	-	-	5.51	0.0168	50.8	0.0553	1,088
993	45.7	0.441	24.0	0.0763	0.499	-	70.2	0.517	7,366
994	-	-	-	-	4.24	0.0024	4.24	0.0024	566
995	-	-	-	-	71.4	0.167	71.4	0.167	2,336
996	4.41	0.0019	-	-	-	-	4.41	0.0019	428
997	64.9	0.0191	-	-	13.8	0.0233	78.7	0.0423	538
998	37.4	0.0453	-	-	2.12	0.0046	39.5	0.0499	1,263
999	19.6	0.0086	-	-	1.04	-	20.6	0.0086	415
1000	-	-	-	-	28.4	0.0225	28.4	0.0225	791
1001	-	-	-	-	57.9	0.0217	57.9	0.0217	374
1002	-	-	-	-	45.1	0.0338	45.1	0.0338	749
1003	-	-	-	-	23.8	0.0172	23.8	0.0172	724
1004	-	-	-	-	7.57	-	7.57	-	-
1005	1.06	0.0013	-	-	-	-	1.06	0.0013	1,238
1006	6.16	0.0091	-	-	5.37	-	11.5	0.0091	793
1007	16.7	0.0065	-	-	-	-	16.7	0.0065	390
1008	-	-	77.8	0.167	11.7	0.0100	89.4	0.177	1,979
1009	109	0.0293	-	-	-	-	109	0.0293	270
1010	34.1	0.0115	-	-	-	-	34.1	0.0115	337
1011	36.7	0.0160	-	-	-	-	36.7	0.0160	435
1012	11.7	0.0250	-	-	7.82	-	19.5	0.0250	1,284
1013	2.73	0.0011	-	-	-	-	2.73	0.0011	390
1014	4.13	0.0234	12.6	0.0401	2.42	0.0031	19.2	0.0667	3,478
1015	121	0.0591	-	-	12.4	0.0109	134	0.0700	524
1016	34.9	0.0350	-	-	41.2	0.0390	76.2	0.0740	972
1017	-	-	-	-	11.8	0.0154	11.8	0.0154	1,308
1018	5.22	0.0278	4.73	0.0144	-	-	9.95	0.0422	4,245
1019	-	-	13.2	0.0463	67.2	0.141	80.4	0.187	2,326
1020	2.05	0.0008	-	-	4.29	0.0078	6.33	0.0086	1,363
1021	-	-	-	-	-	-	-	-	-
1022	8.50	0.0084	-	-	9.42	0.0039	17.9	0.0123	685
1023	119	0.0558	-	-	3.68	-	123	0.0558	454
1024	57.4	0.0132	-	-	4.77	-	62.2	0.0132	213
1025	0.191	0.0007	-	-	11.7	0.0382	11.9	0.0390	3,284
1026	15.5	0.0149	-	-	13.1	-	28.5	0.0149	520
1027	84.2	0.121	-	-	25.4	0.0488	110	0.170	1,551
1028	0.444	0.0006	-	-	25.3	0.0095	25.7	0.0101	392
1029	59.4	0.198	-	-	-	-	59.4	0.198	3,337
1030	27.6	0.0867	-	-	0.889	-	28.5	0.0867	3,041
1031	45.8	0.0687	-	-	36.7	-	82.5	0.0687	834
1032	16.6	0.0250	-	-	25.6	-	42.3	0.0250	592
1033	45.5	0.0637	-	-	16.7	-	62.2	0.0637	1,025
1034	46.5	0.0724	-	-	0.0002	0.0000	46.5	0.0724	1,557
1035	0.0001	0.0000	-	-	47.1	0.131	47.1	0.131	2,771
1036	0.150	0.0002	-	-	52.5	0.206	52.7	0.206	3,903
1037	34.3	0.0683	-	-	9.43	0.0296	43.7	0.0979	2,240
1038	-	-	-	-	41.4	0.0505	41.4	0.0505	1,219
1039	104	0.0597	-	-	17.6	0.0395	122	0.0993	817
1040	-	-	-	-	-	-	-	-	-
1041	8.38	0.0022	-	-	-	-	8.38	0.0022	260
1042	58.0	0.0942	-	-	0.0043	0.0000	58.0	0.0942	1,625
1043	18.1	0.0103	-	-	-	-	18.1	0.0103	568
1044	39.0	0.0254	-	-	-	-	39.0	0.0254	651
1045	92.0	0.0522	-	-	-	-	92.0	0.0522	568

Table E-3. Average Dry Weather Flows by Land Use Area - Buildout

Land Use Polygon ID	Residential		Mixed Use Commercial		Other Non-Residential		Totals		Aggregate Unit Flow Factor, gpd/acre
	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	Net Upstream Acres	ADWF, mgd	
1046	69.7	0.265	-	-	-	-	69.7	0.265	3,800
1047	68.4	0.260	-	-	0.0457	0.0002	68.4	0.260	3,800
1048	62.2	0.0360	-	-	0.0019	0.0000	62.2	0.0360	578
1049	24.0	0.0911	-	-	0.0354	0.0001	24.0	0.0912	3,800
1050	56.5	0.0351	-	-	-	-	56.5	0.0351	621
1051	36.1	0.137	-	-	0.0047	0.0000	36.2	0.137	3,800
1052	107	0.0447	-	-	69.1	-	176	0.0447	254
1053	76.9	0.0265	-	-	0.0093	0.0000	76.9	0.0266	346
1054	-	-	-	-	-	-	-	-	-
1055	-	-	-	-	165	0.231	165	0.231	1,403
1056	22.2	0.0334	-	-	12.9	-	35.1	0.0334	950
9999	90.0	0.1348	-	-	5.43	-	95.4	0.1348	1,413

APPENDIX F

General Flow Data Analysis Approach (Excerpt from the 1995 *Collection System Needs Analysis Report*)

APPENDIX B-2
DRY SEASON FLOW DATA ANALYSIS
EXCERPT FROM
1995 COLLECTION SYSTEM NEEDS ANALYSIS REPORT

DRY-SEASON FLOW DATA ANALYSIS
Excerpt from Section 4 of the *1995 Collection System Needs Analysis Report*
Prepared by HDR Engineering, Inc.

GENERAL APPROACH

To conduct a collection system analysis, there are three basic flow components that must be evaluated and characterized:

- **Dry Weather Flow (DFW)** is the collection system base flow or the sanitary flow component. Typically, this base flow has consistent, predictable daily and weekly flow patterns. These flow patterns are dictated by the land use contributing to the flow.
- **Wet Weather Infiltration (WWI)** is assumed to be a constant flow during the wet weather season. WWI is site specific and depends on the ground water elevation and the physical condition of the collection system. Infiltration into the collection system is only possible in sewers and laterals with defects such as cracks and open joints.
- **Storm-Related Infiltration and Inflow (SRI/I)** is infrequent flow that is closely correlated to specific storm events in the service area. The storm-related infiltration portion is caused by pipe defects coupled with temporary changes in the ground water elevation resulting from a storm. Storm-related inflow results from interconnections between the storm and sanitary sewer collection systems, or direct inflows into the sewer system through manholes and broken pipes. Isolating storm-related infiltration from inflows is difficult; however, the flow response time to a storm event is significantly shorter for inflows than for infiltration, and is typically used as an indicator parameter.

For USA's collection system, these flow components were defined by analyzing flow data collected at 123 monitoring stations and rainfall data collected at 14 locations throughout the study area. The general approach to the flow data analysis (shown in Figure 4-1) included the following steps:

- **Dry Weather Data Analysis.** Unit flow factors for average dry weather flow (ADWF) and diurnal flow curves were developed for model input.
- **Wet Weather Data Analysis.** The WWI flow component was assessed using flow data on non-storm days (i.e., flow data that is not influenced by a specific storm event).
- **Storm-Related Flow Data Analysis.** Storm-related flow responses were analyzed to determine the volume and pattern of flow into the collection system.

- **Unit Flow Generation Factors Development.** A set of unit flow factors was developed based on the ADWF, WWI and SRI/I data. These factors were used to extrapolate flow conditions for unmonitored basins and for future conditions.
- **Plant Influent Analysis.** Flow records from the treatment plants were analyzed to define wet and dry weather seasons for the above analysis. The records also were used to determine the average dry and wet weather flows and hourly flow patterns for model calibration purposes.
- **Point Source Flow Contributions.** Point source flows, such as large industries, were identified and site-specific data were collected. These data were used to define average daily flows and diurnal flow patterns for point sources.

The following discussion outlines the methods used to analyze flow data, identify flow characteristics, and predict specific hydraulic conditions that will occur in the collection system.

Analysis of Flow Monitor Data --

Figure 4-2 is a schematic flow diagram of the analytical procedure used to analyze the DWF data. There are two components to this procedure: analysis of ADWFs, and definition of diurnal curves.

Average Dry Weather Flow --

The ADWF data from the flow monitoring stations were combined in a single database, which included land use data for each monitored basin. The land use data, extracted from the Block Group Database, are expressed in terms of development units, either dwelling units (DU) or 1,000 square foot of commercial and industrial development. The land use information is divided into 15 land use categories.

The objective of the analysis was to define the unit flow factors to be used to generate flow assignments for the collection system model. These unit flow factors predict the wastewater contribution per development unit for each land use category (e.g., the land use factor for weekday flows from the Single Family Residential No. 1 (SFRI) category is approximately 143 gpd/DU). Using multiple regression analysis, units flow factors for both weekday and weekend flows were defined for each land use category. These are summarized in Table 4-1.

Table 4-1. Unit Flow Factors for ADWF Assignment

Land Use Category		Population Density (cap/DU) [5]	Weekday Unit Flow Factors		Weekend Unit Flow Factors		Units
Acronym	Description		Median	STD [4]	Median	STD [4]	
SFR1	Single Family Residential (1-3/acre)	2.4	160	14.46	171	14.07	gpd/DU
SFR2	Single Family Residential (3-4/acre)	2.4	160	14.46	171	14.07	gpd/DU
SFR3	Single Family Residential (4-6/acre)	2.4	160	14.46	171	14.07	gpd/DU
MFR1	Multi Family Residential (2-25/acre)	2.3	200	18.08	213	17.58	gpd/DU
MFR2	Multi Family Residential (>25/acre)	2.3	200	18.08	213	17.58	gpd/DU
RR	Rural Residential	2.3	160	14.46	171	14.07	gpd/DU
CN	Neighborhood Commercial	n.a.	84	21.66	65	21.05	gpd/1000 sf
CG	General commercial	n.a.	84	21.66	65	21.05	gpd/1000 sf
CC	Central Commercial	n.a.	84	21.66	65	21.05	gpd/1000 sf
CO	Office Commercial	n.a.	84	21.66	65	21.05	gpd/1000 sf
IL	Light Industry	n.a.	84	21.66	65	21.05	gpd/1000 sf
IMU	Multi-use Industrial	n.a.	84	21.66	65	21.05	gpd/1000 sf
IH	Heavy Industrial [1]	n.a.	168	43.3	130	42.1	gpd/1000 sf
PF	Public Facilities [2]	n.a.					
NZ	Not Zoned Areas [3]	n.a.					

Notes:
1) Excluding identified "wet" industries.
2) Public facilities with significant inflow should be treated as point inflows.
3) Not zoned areas such as highway right of ways.
4) Standard deviation.
5) Assumed target population densities from demographics study.

The correlation between the recorded and predicted flows using the unit flow factors for the flow monitor basins is illustrated in Figure 4-3. The following assumptions were made in the unit flow factor analysis:

- 1992 flow monitoring data were used to match the 1992 land use/demographic data.
- All single-family residential categories, including the rural residential land use categories, were grouped together as category SFR.
- All multiple family categories were grouped together as category MFR.
- All commercial, light industrial and multi-use industrial categories were grouped together and called CO/IL.
- Trial runs proved that a better correlation can be obtained by assuming a SFR to MFR unit flow factor ratio of 1.25, and a CO/IL to IH (heavy industrial) flow factor ratio of 2.0. These ratios correspond to typical observed ratios in other collection systems.
- Flow contributions from "wet" industries were deducted from the total basin flows, but the development area for the particular industry was not deducted from the land use database. This approach was adopted by assuming that the "wet" flow is a process-related flow, and that the industry still contributes to the base ADWF.
- In the multiple regression analysis, it was assumed that all cross correlation between factors was negligible.

Diurnal Flow Patterns --

Diurnal flow patterns are defined as a dimensionless hourly flow with a daily average of 1.0. Diurnal flow is calculated by dividing the hourly flow by the average flow for that day. The approach for defining typical diurnal flow patterns is shown in Figure 4-2. The objectives of the analysis were to categorize the flow patterns according to land use, and to define the anticipated variation in the peak flow conditions. An analysis of the diurnal curves at USA's subbasin monitoring stations indicated that four basic curve patterns occur. These are illustrated in Figure 4-4 for average weekday and weekend conditions.

The factors most likely to influence diurnal curve patterns are basin size, basin configuration and land use. A comparison of data for the four curve types shown in Figure 4-4 proved land use to be the predominant factor, which is consistent with previous experience classifying diurnal curves. Four land use parameters were used to define the relationship between land use and diurnal curve type. These parameters were then used to assign curve types to subbasins for which monitoring data were not available.

The following is a description of the land use parameters and their influence on the diurnal curve pattern:

- **Ratio of Single Family Residential to Multi-Family Residential (SFR/MFR).** Experience showed that basins with a higher ratio of single family residential dwelling units to multi-family residential units are likely to have higher morning peaks and lower mid-afternoon lows.
- **Ratio of Residential Dwellings to Commercial and Industrial Development (RES/COM).** Basins with higher RES/COM ratios proved to have higher morning peaks and lower mid-afternoon lows.
- **Ratio of Industrial to Commercial Development (IND/COM).** Basins with high ratios of industrial to commercial development in combination with low RES/COM ratios proved to have relatively flat diurnal curves.
- **Industrial Development per Acre (IND/acre).** Basins with IND/acre values of more than 1,000 ft^2/acre in combination with low RES/COM values proved to have very flat curves. This illustrates a predominantly industrial flow component.

Table 4-2 summarizes information for each curve type with respect to diurnal peak and land use characteristics. Figure 4-5 summarizes information on the land use parameter ratios for each curve type.

Table 4-2. Diurnal Curve Category Definitions

Parameter	Diurnal Curve Category			
	Type 1	Type 2	Type 3	Type 4
Weekly Peak Occurrence Time	6:00 a.m. to 8:00 a.m.	6:00 a.m. to 8:00 a.m.	6:00 a.m. to 8:00 a.m.	9:00 a.m. to 11:00
Weekday Peak	1.75 to 2.2	1.50 to 1.75	1.25 to 1.50	1.10 to 1.50
SFR/MFR	>2	>2	<2	N/A
RES/COM	2 to 20	>20	2 to 20	<2
IND/COM	<3	<3	<3	>3
IND/acre	<1	<1	<1	>1
Other Characteristics	Low early morning and mid-afternoon lows.	Medium early morning and mid-afternoon lows.	Medium early morning and mid-afternoon lows.	High early morning low and almost no mid-afternoon low

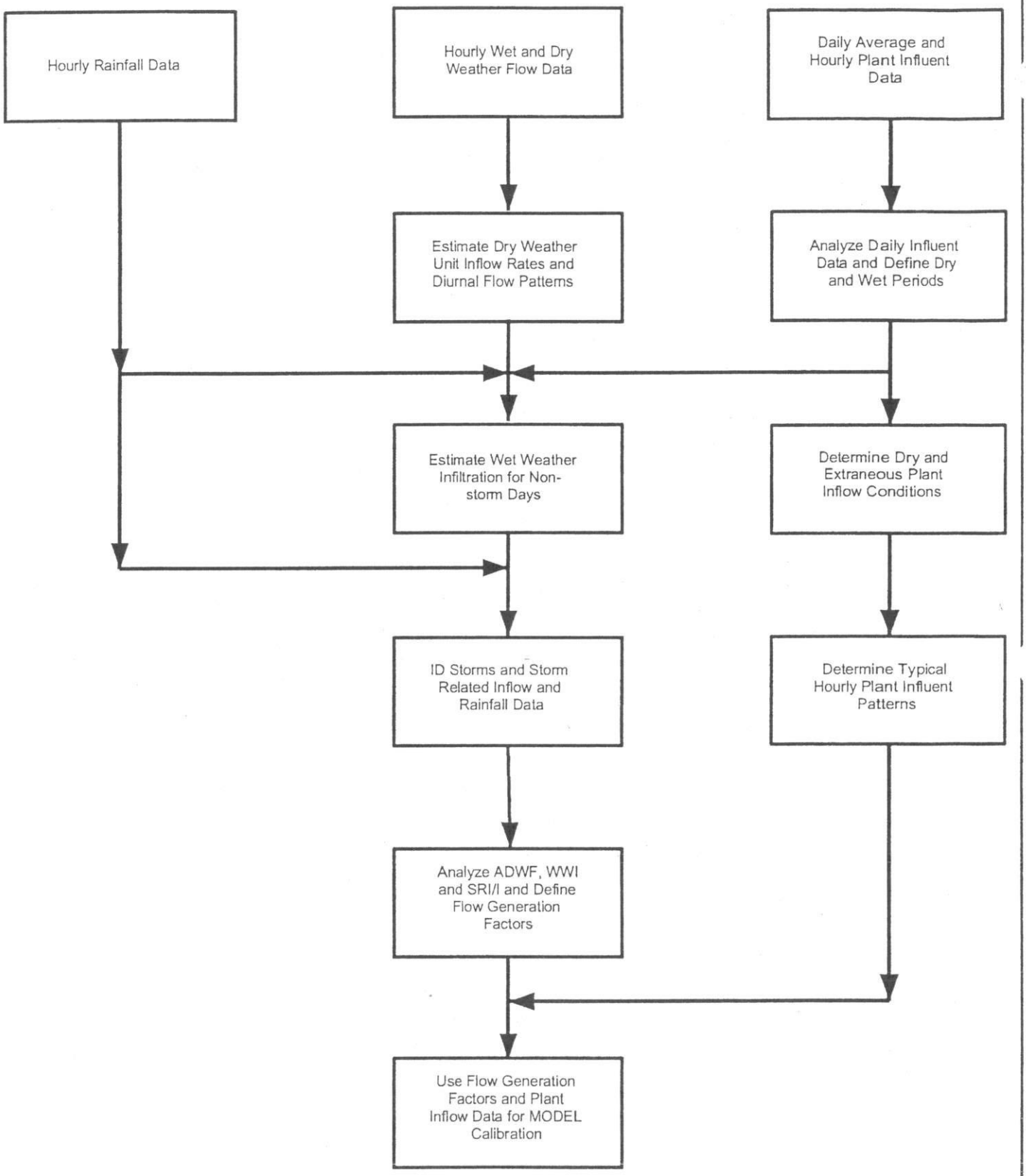
Diurnal Curve Peaking Factor Adjustments --

The curves shown in Figure 4-4 represent average diurnal flow patterns from the drainage basins. When combined with the ADWF from the basins, they simulate ADWF conditions in the collection system. However, for collection system evaluation purposes, flow conditions other than the average daily flows (e.g., maximum-day flows) may be needed. To simulate these flow conditions, the peaking factor for the diurnal curves must be adjusted. This was accomplished by preparing a log-normal distribution analysis on the peaking factors for each diurnal curve category to predict the maximum-day peaking factor (the 99.7 percentile). Based on this analysis, each value in the diurnal curve was adjusted proportionately to increase the steepness of the curve, while maintaining a unit average daily flow.

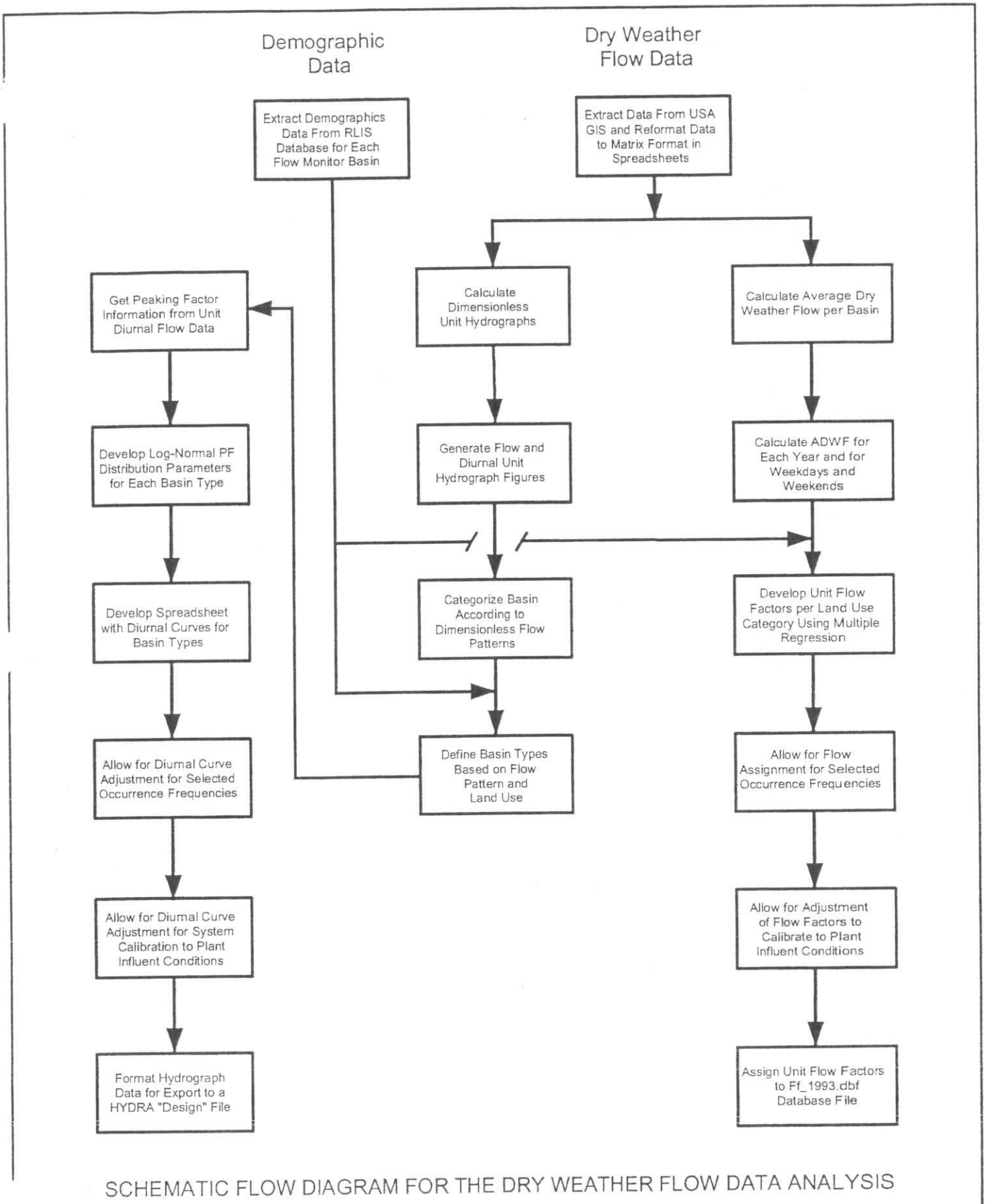
A second adjustment was to calibrate the diurnal curves for the individual collection systems. In this step, the steepness of the diurnal curves within a particular collection system (such as Forest Grove) was adjusted to match the observed diurnal flow pattern at the downstream treatment plant. This step was necessary to calibrate the flow patterns generated from "typical" curves to the basin-wide characteristics of the particular collection system.

Two additional diurnal curve adjustments were considered, a lag time adjustment and a basin size adjustment. The lag time adjustment could be applied to compensate for the time of concentration between the point of entry and the flow monitor station. In the model, flow is routed into the furthest upstream point in the collection system. This results in a lag between the observed flows and the model prediction. The diurnal curve timing can be corrected to compensate for the lag time. However, a lag in the diurnal curve will not influence the design flows predicted by the model. Therefore, the lag time adjustment was not considered essential and was ignored.

The average size of the sanitary service area used in the model is smaller than that of the flow monitoring basins. It is expected that the diurnal curve peak at the point of entry for the smaller service area will be higher than what is observed at the downstream flow monitor. An evaluation of the influence of basin size on the peaking factors showed that the increase is relatively small. It was concluded that if such an adjustment were needed, it would be incorporated in the calibration adjustment factor. Thus, no separate basin size adjustment was applied.

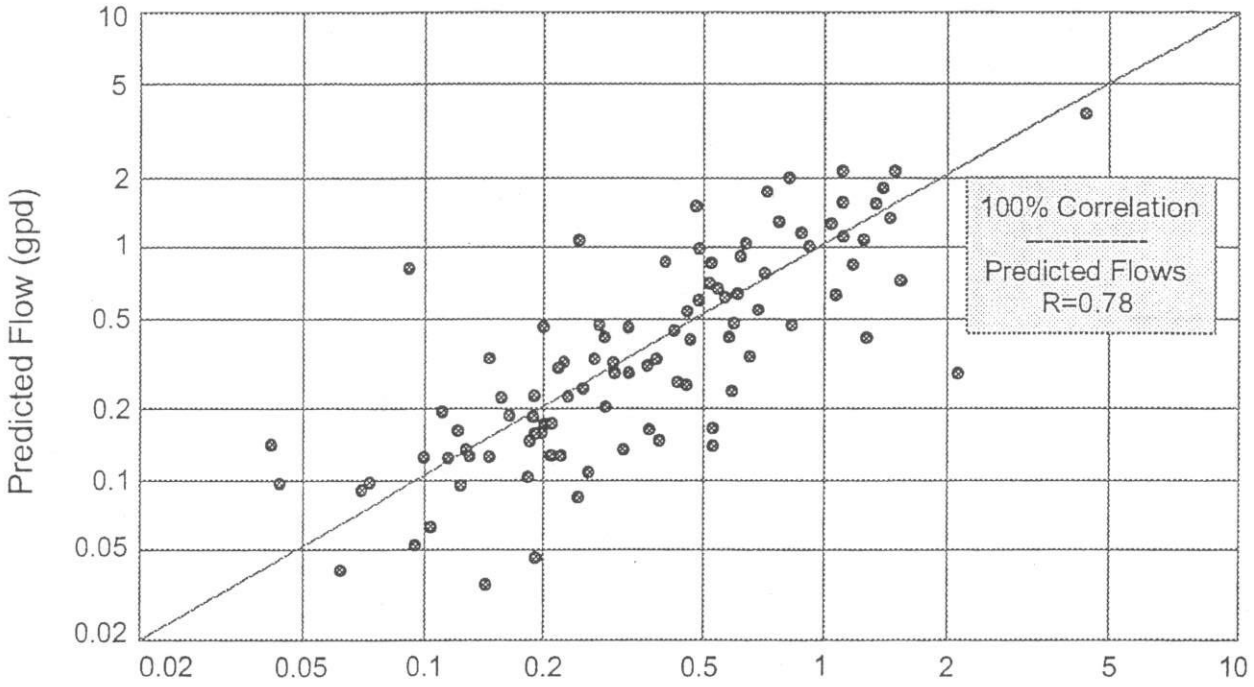


SCHEMATIC FLOW DIAGRAM OF THE GENERAL DATA ANALYSIS APPROACH

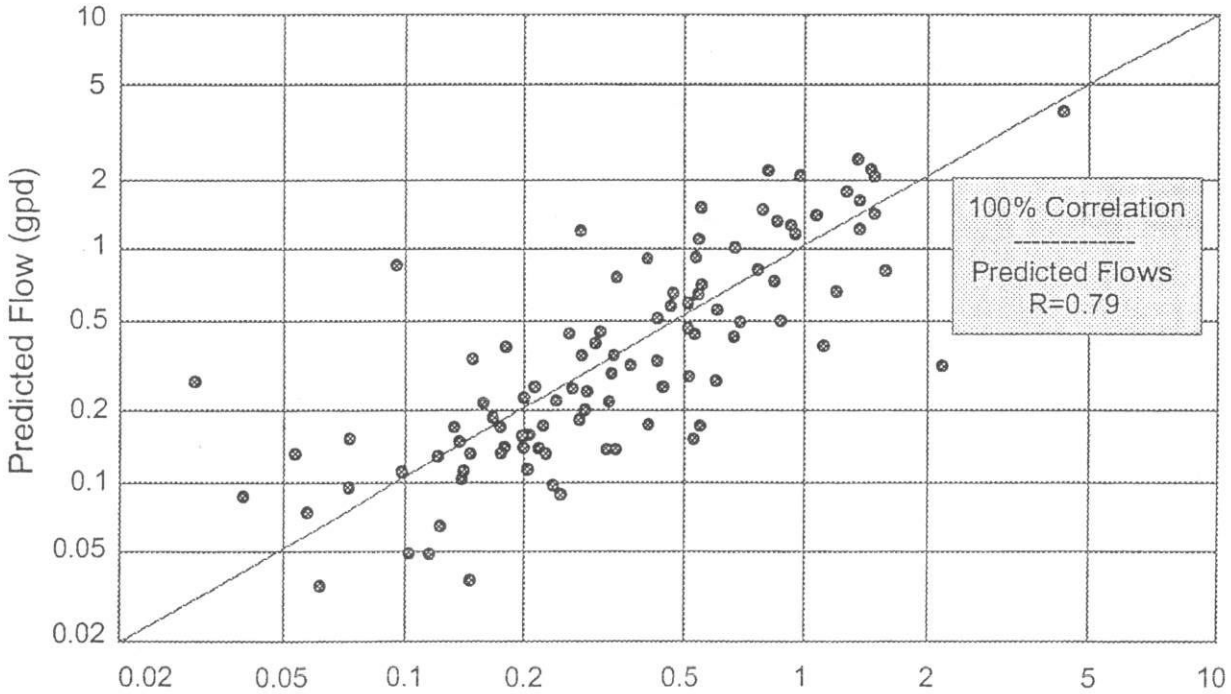


SCHEMATIC FLOW DIAGRAM FOR THE DRY WEATHER FLOW DATA ANALYSIS

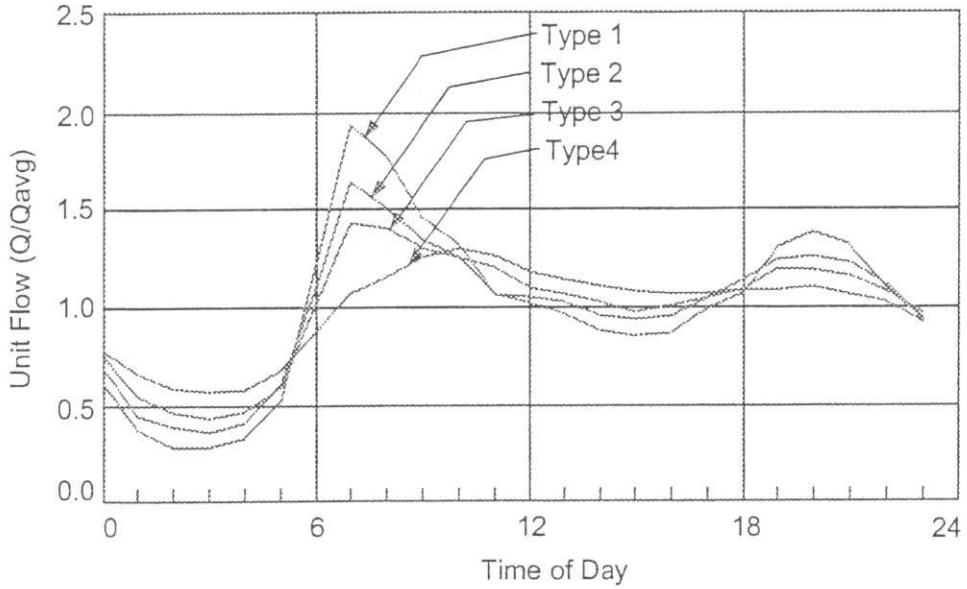
Appendix B-2
Figure 4-2



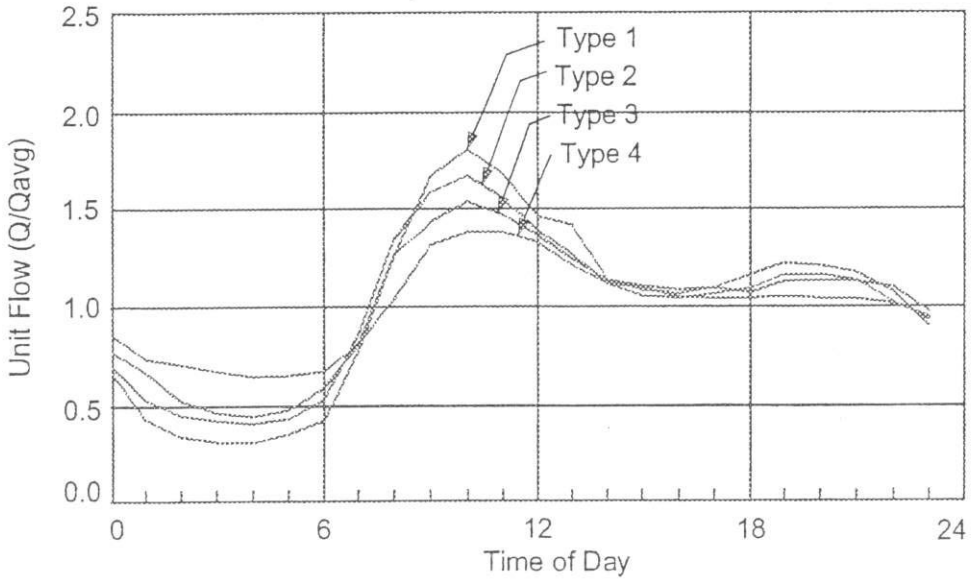
(a) COMPARISON BETWEEN OBSERVED AND PREDICTED WEEKDAY FLOWS USING GENERATED UNIT FLOW FACTORS



(b) COMPARISON BETWEEN OBSERVED AND PREDICTED WEEKEND FLOWS USING GENERATED UNIT FLOW FACTORS



(a) AVERAGE WEEKDAY UNIT DIURNAL FLOW CURVES FOR BASIN TYPES



(b) AVERAGE WEEKEND UNIT DIURNAL FLOW CURVES FOR BASIN TYPES

APPENDIX G

***Flow Monitoring Data Analysis* (I&I Analysis; Chapter 4 from the 2000 MP)**

4. Flow Monitoring Data Analysis

The update and analysis of flow monitoring data focused on defining input parameters to the Hydra defects database for each of the basin models. Previous collection system evaluations developed inflow/infiltration hydrographs outside of the Hydra software that were injected into the sewer system as point flows. Therefore, a new approach to wet-season data analysis was needed to convert flow-monitoring information into Hydra *Defects.dbf* file inputs. Dry-season flow monitoring data were also updated, but only for the purpose of separating base sanitary flows from wet-season flow data. This chapter describes the methods used to define extraneous flows and to estimate system responses for the 5-year 24-hour design storm.

4.1. Approach

The approach to generating inflow and infiltration focused on setting up Hydra's *Defects.dbf* database for each of the four basin models. Two I/I components were modeled: average wet season infiltration (WWI) and storm-responsive inflow/infiltration (SRI). The average wet seasonal rate was modeled using the *WET_Q* parameter, which is input in gallons per day. The latter was modeled using the rapid infiltration parameters as follows:

- *RAP_AREA* field: Area in square feet that generates stormwater, which enters the system through major defects. The model imposes a rainfall hyetograph (contained in a storm or **.STO* file) onto this area to compute a stormwater runoff volume.
- *RAP_BEGIN* field: Beginning hour when SRI is "seen" by the system relative to the beginning of the storm.
- *RAP_MAX* field: Time between maximum rainfall intensity and maximum rapid infiltration response.
- *RAP_END* field: Time from the ending of the storm to the end of significant infiltration.

Rapid infiltration is normally delayed behind the rainfall and will continue to contribute flow to the sewer system after the storm has ended. The beginning, maximum and ending times and the storm hyetograph form the SRI hydrograph shape.

The Hydra defects database also provides a method for simulating direct storm flow into the system (*STO* fields). However, storm inflow from direct connections to the sewer system, such as roof drains, is difficult to separate from storm-responsive infiltration in analyzing flow monitoring data. Generally, it is necessary to obtain sufficient field information on direct-connection problems to justify the use of storm inflow parameters. In addition, the flow monitoring data indicates that there is generally a lag between rainfall and SRI. Therefore, the quantification of direct storm inflow was not included in this analysis.

Recently collected flow data (since that used in the 1995 work), along with hourly rainfall, was added to the flow monitoring data analysis worksheets. The current analysis of flow monitoring data more closely relates rainfall to SRI response than previous planning efforts.

Defects databases were set up for the four treatment plant basins based on the flow monitoring data analysis results. Also, unique *Defects.dbf* files were needed for the buildout condition, since the service areas that were added (e.g. URAs) will only contribute I/I and sanitary flow when developed.

These data analysis procedures resulted in a revised definition of defect flows, and were closely related to USA's 5-year 24-hour design storm. Figure 4-1 shows the location of USA's temporary flow monitors that were installed between 1990 and 1997.

4.2. Design Storm Criterion

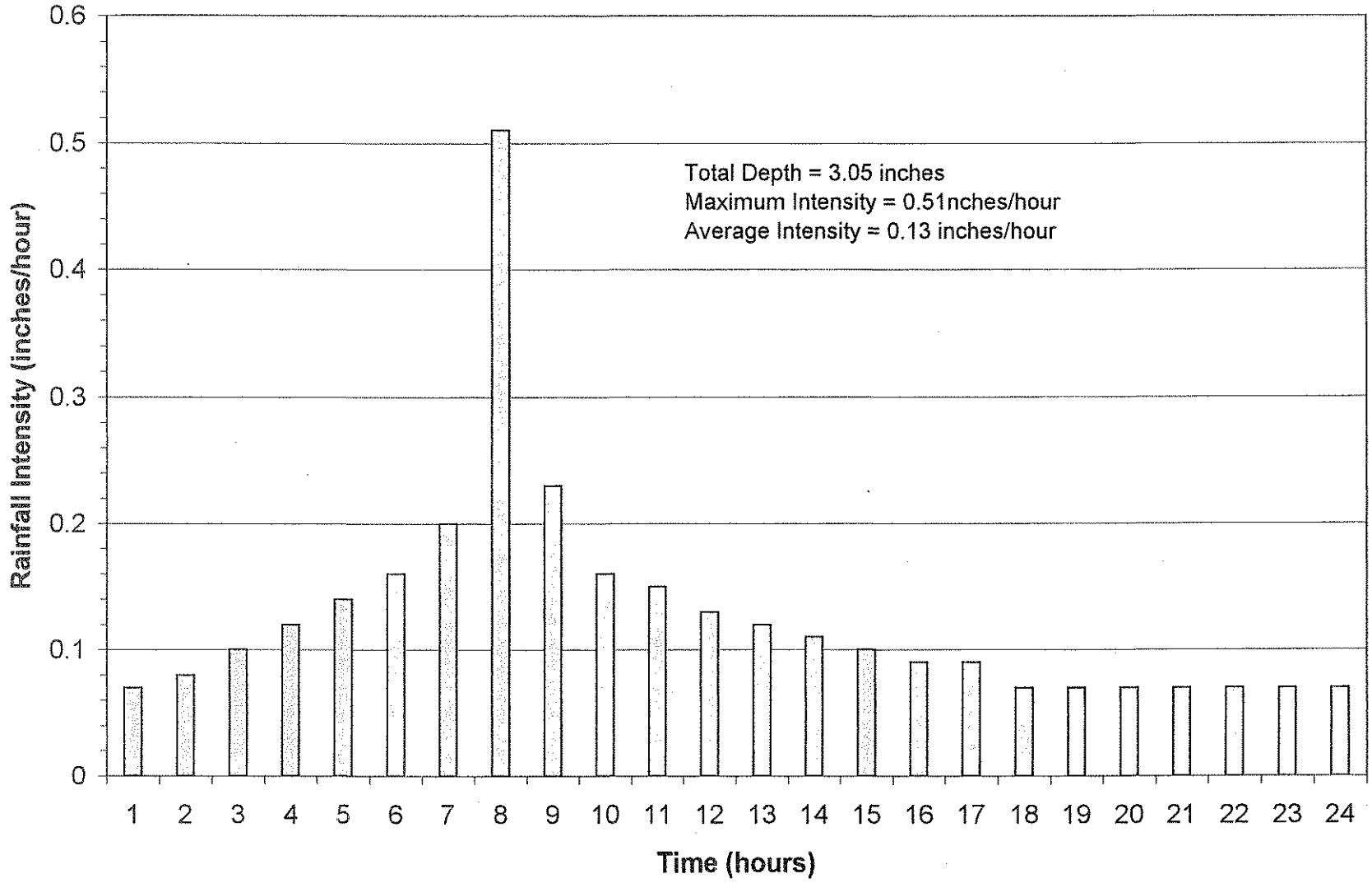
USA's NPDES permit requires that the Agency control sanitary sewer overflows (SSOs) in response to a 5-year event. SSOs include flow bypassed at the treatment plant, overflows to streams, flooded manholes and basement backups. Recent mandates by the Environmental Protection Agency have identified a receiving water-quality based approach to determining SSO control criteria. However, an SSO-control criterion is already included in USA's NPDES permit that defines the control level and compliance schedule.

The 1995 work adopted a statistical approach to I/I analysis that equated the peak 5-year response to a 20-percent frequency, or 80-percentile probability. The approach used in this analysis involves a more literal interpretation of the 5-year 24-hour storm response. In addition, a comprehensive review of the flow-monitoring data revealed that the meters did not always capture flows in response to significant rainfall events. This is because the meters were moved throughout the collection system, so the flow monitoring periods for one meter may not have coincided with the period for another located nearby. These types of inconsistencies presented problems in implementing a statistical approach to wet-season data analysis. Instead, representative wet-season SRI events were selected for each monitor and analyzed. Those events caused by rainfall events approximating the 5-year 24-hour storm, which is shown in Figure 4-2, were selected for characterizing rapid infiltration parameters. This is a synthetic rainfall event and was not derived specifically from rainfall records for the Washington County area. Synthetic rainfall events derived from regional NOAA parameters are generally less representative than events derived from local rainfall data.

An important consideration in screening the SRI representative events was antecedent conditions. In this case, the presence of wet antecedent conditions refers to the decay of the SRI response during the wet season. For instance, certain monitors show a long response to rainfall. So if a rainfall event occurs within one or two days, the SRI response may not have receded between events. This was found to be especially true in the Rock Creek system, due to the presence of a layer of clay soils that causes groundwater to be perched for long periods of time.

Determining input parameters to the defects database would be different for various design storm and antecedent conditions. The Hydra model input files are prepared from the monitoring data, and should reflect the system response that approximates the selected design event. The sewer system will respond differently under wet versus dry antecedent conditions, and under a 3-month versus a 5-year storm. Based on a comprehensive review of the available data, the USA collection system exhibits a significantly greater response to wet antecedent conditions.

Figure 4-2. 5-Year 24-Hour Design Storm



These issues were presented to USA staff for consideration. Based on USA staff and consultant discussions, it was decided that USA's 5-year 24-hour design storm would be used, and that the SRI events selected for establishing the rapid infiltration parameters would assume dry antecedent conditions (during the wet season) to the degree possible. Therefore, SRI events nested within long periods of rainfall were not used as representative of the design condition response.

4.3. Data Collection and Update

4.3.1. Seasonality

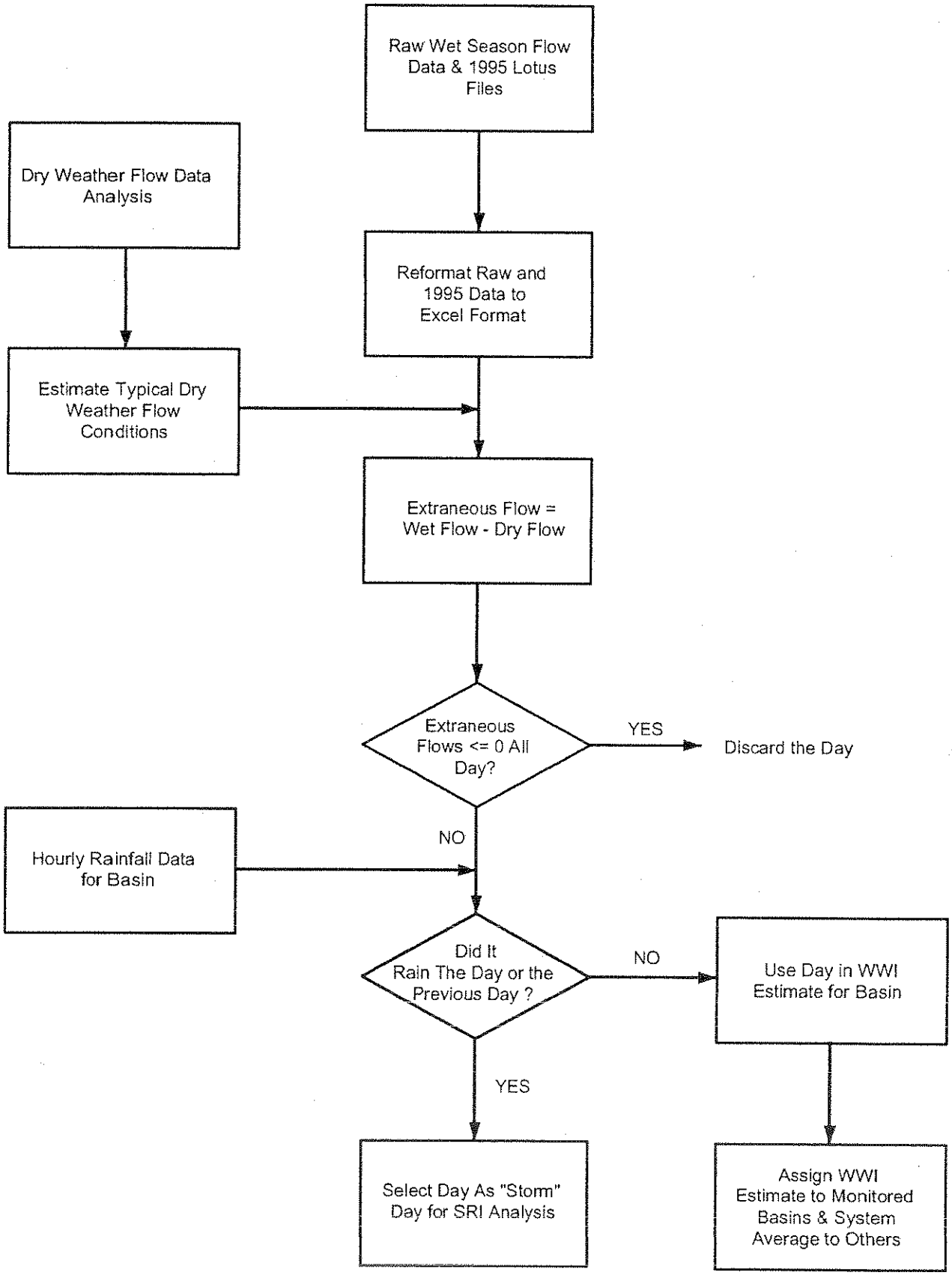
An analysis of seasonality was conducted in order to separate dry- from wet-season flows, for data added to the flow monitoring data analysis spreadsheets. The analysis method was adopted from the 1995 work, and involves creating a mass plot for each treatment plant and then identifying inflection points on the graph. The inflection points are an indication of increases and decreases in I/I flow contribution. Only recent treatment plant flows (from 1996) were analyzed. Previous definitions of dry- and wet-season changes were used for the years 1990-1995. The resulting mass plots are included in Appendix C-1, and season definition dates are summarized in Table 4-1.

4.3.2. Flow Data Update and Worksheet Templates

In order to facilitate the data update process, Excel worksheet templates and instructions were prepared for converting the 1995 Lotus worksheets. Flow and rainfall data collected since that time were added, and worksheet calculations were modified. USA staff developed procedures to convert and transpose flow and rainfall data from the flow monitor and rainfall records stored on the main computer system to the spreadsheets. Appendix C-2 contains the spreadsheet templates and instructions, and a brief memorandum providing additional details on the analysis process. Figure 4-3 is an overview of the wet-season data analysis process, and was partially adopted from the 1995 *Collection System Needs Analysis*.

Table 4-1. Unified Sewerage Agency Flow Monitoring Season Definition

Treatment Plant	Year	Dry Season End	Wet Season Start	Wet Season End	Dry Season Start
Durham	1990-1991	11-Nov-90	12-Nov-90	23-May-91	24-May-91
	1991-1992	29-Oct-91	30-Oct-90	08-May-92	09-May-92
	1992-1993	20-Nov-92	21-Nov-92	06-May-93	07-May-93
	1993-1994	05-Dec-93	06-Dec-93	14-Apr-94	15-Apr-94
	1994-1995	24-Oct-94	25-Oct-94	27-Mar-95	28-Mar-95
	1995-1996	09-Nov-95	10-Nov-95	26-May-96	27-May-95
	1996-1997	14-Nov-96	15-Nov-96	27-Mar-97	28-Mar-97
	1997-1998	10-Nov-97	11-Nov-97	05-Apr-98	06-Apr-98
	1998-1999	28-Nov-98	29-Nov-98	17-Apr-99	18-Apr-99
Rock Creek	1990-1991	09-Nov-90	10-Nov-90	25-May-91	26-May-91
	1991-1992	15-Nov-91	16-Nov-91	12-May-92	13-May-92
	1992-1993	28-Oct-92	29-Oct-92	28-Apr-93	29-Apr-93
	1993-1994	07-Dec-93	08-Dec-93	27-Apr-94	28-Apr-94
	1994-1995	24-Oct-94	25-Oct-94	01-Apr-95	02-Apr-95
	1995-1996	08-Nov-95	09-Nov-95	28-May-96	29-May-95
	1996-1997	17-Nov-96	18-Nov-96	27-Mar-97	28-Mar-97
	1997-1998	09-Nov-97	10-Nov-97	27-Mar-98	28-Mar-98
	1998-1999	18-Nov-98	19-Nov-98	28-Apr-99	29-Apr-99
Forest Grove	1990-1991	28-Nov-90	29-Nov-90	18-Apr-91	19-Apr-91
	1991-1992	14-Nov-91	15-Nov-91	02-May-92	03-May-92
	1992-1993	28-Oct-92	29-Oct-92	16-Jun-93	17-Jun-93
	1993-1994	28-Nov-93	29-Nov-93	21-Apr-94	22-Apr-94
	1994-1995	24-Oct-94	25-Oct-94	19-May-95	20-May-95
	1995-1996	08-Nov-95	09-Nov-95	02-Jun-96	03-Jun-96
	1996-1997	17-Nov-96	18-Nov-96	26-Mar-96	27-Mar-96
	1997-1998	16-Nov-97	17-Nov-97	17-Apr-98	18-Apr-98
	1998-1999	20-Nov-98	21-Nov-98	22-Apr-99	23-Apr-99
Hillsboro	1990-1991	28-Nov-90	29-Nov-90	23-May-91	24-May-91
	1991-1992	15-Nov-91	16-Nov-91	02-May-92	03-May-92
	1992-1993	19-Nov-92	20-Nov-92	12-May-93	13-May-93
	1993-1994	05-Dec-93	06-Dec-93	11-Mar-94	12-Mar-94
	1994-1995	24-Oct-94	25-Oct-94	25-Mar-95	26-Mar-95
	1995-1996	07-Nov-95	08-Nov-95	24-May-96	25-May-95
	1996-1997	15-Nov-96	16-Nov-96	27-Mar-97	28-Mar-97
	1997-1998	09-Nov-97	10-Nov-97	27-Mar-98	28-Mar-98
	1998-1999	18-Nov-98	19-Nov-98	28-Apr-99	29-Apr-99
	Shaded dates indicate that values for Rock Creek WWTP were used due to data inconsistencies.				



SCHEMATIC FLOW DIAGRAM FOR WET-SEASON INFILTRATION DATA ANALYSIS

Partially adopted from the 1995 Collection System Analysis

Figure 4-3

4.3.3. Sewer Rehabilitation Flow Data

Flow monitors that collected data downstream of sewer rehabilitation areas were subdivided according to rehabilitation project schedules. Based on construction dates provided by USA staff, the monitoring data were separated into "before" and "after" rehabilitation project periods. Table 4-2 summarizes the rehabilitation monitors and dates when work was completed.

Table 4-2. Summary of Sewer Rehabilitation Monitors

Monitor	Rehabilitation Project	Scope and Date of Work
F005	Forest Grove	Mains completed October 1993; Laterals summer 1995
D033	Cedar Hills	Mains and laterals began November 1991 and completed summer 1995
B003	Banks	Mains completed spring 1995; laterals summer 1999
H004	Hillsboro	Mains completed June 1995; no lateral rehabilitation
F001	Cornelius	Mains completed spring 1995; laterals summer 1999

In addition to those listed in the table, there were numerous temporary flow monitors set up in the rehabilitation project collection systems. These data were not used primarily because the flow monitoring data were collected only before or after the completion of construction but not both, and would therefore not provide for an analysis of I/I reduction. Most of the monitoring periods were also relatively short. For these reasons, and because a detailed analysis of sewer rehabilitation effectiveness was not part of the project scope, the temporary monitoring data were not used.

As shown in Table 4-2 rehabilitation construction was mostly accomplished in phases, which presented difficulties in separating and analyzing the flow data, and in determining effectiveness. Use of rehabilitation monitoring data is discussed further in Section 4.4.

4.3.4. Monitor Selection

Based upon a thorough review of all available data, a few of the monitors were eliminated from further analysis due to siting or data inconsistency problems. For instance, meter D035 was located on a cross-connection between the Beaverton Lateral and the Fanno Creek Interceptor, so it measured only flow diverted from the Beaverton Lateral and does not have a definitive

collection area. Other monitors such as D013B, D027A and D029A, were eliminated for data inconsistency reasons or because there were numerous upstream diversions such that the collection area could not be defined. The matrix in Appendix C-3 was created from USA's flow monitoring site database, and was enhanced to refine monitor site locations and provide a record of data use.

4.3.5. Monitor Overlap and Data Concurrency

One of the objectives in improving the system characterization of I/I flows was to separate flow data for overlapping meters. This would allow for a more accurate I/I definition for service areas between monitor sites, but requires that monitoring periods be concurrent for the meters that have been installed in sequence. For instance, monitor D017A collects 801 acres and overlaps the 496-acre area of D017B. If the records for D017B could be subtracted from D017A, then the residual data could be used to define I/I rates for the 305-acre area between the meter sites.

Worksheets were set up to sort all monitoring periods of record for the dry and wet seasons. Based on a review of the results, it was concluded that the majority of records for overlapping meters lacked concurrency. A significant amount of data would have been eliminated in order to subtract flow records and improve the characterization of I/I in areas between meter sites.

The only exception was for monitors R002A and R002B, which were installed on parallel lines. Although the monitoring periods for these meters were not entirely concurrent, the coincident flows were added together to generate a dataset that could be analyzed. Otherwise, these monitors would have been eliminated from the analysis.

4.3.6. Flow Monitor Basin Definition

Flow monitor collection areas were re-defined by USA staff using sewer and parcel information in the Agency's GIS. To the degree possible, the monitor basins were delineated to include only developed areas, since it is the existing sewer collection system that generates I/I flow. Unfortunately, area definitions were based on current parcel and sewer information, which were related to flows collected between 1990 and 1997. This meant that the area-flow relationships were not as accurate for the older flow monitoring data.

The basins that extend into the Portland system were especially difficult to define because USA has no sewer information in its GIS. Although most of these service areas were removed from the model due to the construction of the Fanno Creek Pumping Station, the monitor basins still needed to be defined, since the area computations were necessary to characterize flows collected at downstream monitors.

The results generated by USA staff were compared to the monitor acreages used in the 1995 work, and to the sum of the 1995 service areas upstream of each monitor. In many cases, the 1995 areas for these monitors, or the total area of Hydra service areas collecting to the monitors was used. In other cases, the "working" collection system and service area maps were used to make adjustments.

For the purposes of defining monitor collection areas and overlapping monitors, a spreadsheet was created to compare monitoring areas from various sources and to tabulate overlapping meter areas. This table is presented in Appendix C-4.

4.3.7. Representative Monitor Assignments

There are many approaches for quantifying and simulating I/I. The method used for analyzing the USA collection system assigns I/I rates to service areas that are connected to the modeled sewer system. The 1995 work assigned a representative monitor to each service area, and unmonitored areas were assigned typical values based on the monitored areas. This approach was adopted for the *2000 Master Plan Update*. However, a review of the 1995 monitor assignments indicated a need for refinement.

The first step was to prepare a table of Hydra service areas within monitor basins. This table was used to compare areas computed by USA, and to assign defect database input values to the service areas. Defect flow parameters (seasonal infiltration and storm-responsive infiltration) were assigned to the service areas on this basis. The tables included in Appendix C-5 were used for this purpose.

4.3.8. Data Quality and Consistency Issues

The following summarizes issues relating to the flow monitoring data available for use in preparing this *2000 Master Plan Update*:

- Rainfall data were missing for critical periods for which wet-season flow data were collected. Adjacent rain gauges were used to fill in for missing periods where possible, but it appears that there are periods when several gauges were off-line. Accurate, representative rainfall is critical in the analysis of wet weather data, since it is used to determine the difference between non-storm (WWI) and storm-related (SRI) infiltration, and to derive relationships between rainfall and SRI.
- The flow data worksheets are set up to define a storm day as having at least 0.2 inches of rain on that day or the prior day. Based on a review of the data, it appears that different areas of the system exhibit different SRI recession patterns. That is, some areas take longer than others for the SRI portion of the hydrograph to become insignificant. A uniform storm-day criterion was used for all monitors because of data reliability and consistency issues.
- The amount of flow data that have been collected concurrently is limited. Ideally, all of the monitors should be running concurrently so that records for overlapping monitors can be subtracted. This is the only way to accurately quantify I/I rates for areas in-between monitors. Dry- and wet-season monitoring periods were analyzed for all monitors to determine whether there was enough concurrency to difference records.
- Dry-season flows are subtracted from wet-season flows in order to determine I/I quantities. For each year of wet-season data, weekday and weekend dry-season flows are required. This is because dry-season flows will change over time as development occurs and changes to the sewer system take place. In many cases, average annual dry-season flows had to be estimated due to the lack of data.
- Measuring the sewered area upstream of the monitors was difficult. A measured collection area is necessary to compute unit I/I rates in terms of gallons per acre per day. The high rate of development in Washington County over this period of time has significantly changed the collection system.
- The portable monitors previously used by USA had data compilation limitations. Once the pipe surcharged, the monitor continued to record depth above the crown of the pipe and did

not have the ability to differentiate surcharge from gravity flow, thus giving erroneous values under surcharged conditions. The Badger meters installed at the permanent sites have the ability to differentiate between these two conditions.

- Several of the monitors have significant diversions upstream, and were therefore eliminated from the analysis.

An attempt was made to account for such problems by carefully selecting representative events. Unfortunately, characterizing SRI inputs to the model relies heavily on the larger wet-season events (during which the monitor manholes may be surcharged), because the design event is also large (a 5-year, 24-hour storm). Additional issues and recommendations are provided in Appendix C-8.

4.4. Definition of Wet-Season and Storm-Responsive Infiltration

Within the wet-season data worksheets, the two I/I components are separated: the average wet season rate (WWI) and the storm-responsive component (SRI), which is hydrographic. From the SRI dataset, representative "events" were selected for plotting. From these graphs, parameters were estimated that would approximate the system response to a 5-year 24-hour storm.

The following summarizes the method used to derive defect database parameters:

1. It was concluded that the flow datasets are not sufficiently consistent to allow for a statistical analysis. Therefore, the analysis of wet-season SRI was based on selected events representative of the design storm and antecedent conditions.
2. Two components of the Hydra defects database were used to model I/I flows. First, the *WET_Q* field, entered in gallons per day, was used to simulate average wet-season I/I. These values were taken from Section 3 of the wet-season spreadsheets, which averages I/I flows for non-storm days. Second, the rapid infiltration method was used to simulate SRI. The fields required are *RAP_AREA*, *RAP_BEG*, *RAP_MAX* and *RAP_END*. The *RAP_AREA* is the equivalent area of paved surface in square feet that would result in a total volume of rapid infiltration for SRI defects. The *RAP_BEG*, *RAP_MAX* and *RAP_END* are the times from the start, peak and ending times of the storm to the corresponding times of the rapid

infiltration response. A storm hyetograph is also set up in a *.*STO* file. The storm "rains" on the rapid infiltration area and generates an infiltration volume that is distributed according to the pattern defined by the beginning, maximum and ending times.

3. Graphs of SRI flows versus rainfall were prepared to define the timing pattern of SRI flows and to derive relationships between rainfall and SRI volume. The latter was used to compute *RAP_AREA* for each monitor and the former for establishing *RAP_BEG*, *RAP_MAX* and *RAP_END* hours. The rapid area is the volume of the SRI flow divided by depth of rainfall that caused the SRI response. A ratio was then computed that is the rapid area divided by the monitored basin area. This ratio was then used to determine the rapid area for each service area (sanitary subbasin) in the model.
4. For each service area, a representative monitor was selected, and the characteristics of that monitor were assigned to the service area.

Test runs of this approach were made for selected areas within the Forest Grove. The method appeared to work well, although the resulting model hydrographs exhibited less fluctuation than the monitoring data.

4.4.1. Example Monitor Data Analysis

This section provides specific examples of the methods used derive average season and rapid infiltration, or SRI, parameters. Monitor D001C, which has a collection area of 968 acres, was selected as an example. A representative rapid infiltration event for monitor D033, which collected flows from the Cedar Hills rehabilitation project, is also provided.

There are five sections to the wet-season worksheets:

Section 1: Raw wet-season flow monitoring data for a particular monitor location.

Section 2: The "residual" total flow data. Values in this section are computed from the raw monitor data less the flows for the upstream monitor or monitors, if appropriate.

Section 3: Wet-season inflow and infiltration rates, or WWI. These are the total monitored flow rates less dry-season flow, using the average yearly flow rate and the dry-season diurnal curve. Storm days are also separated from non-storm days in this section.

Section 4: Storm-responsive I/I flows. SRI flows are computed in this section from the Section 3 values less the average WWI rate for "storm" days.

Section 5: Hourly rainfall. Hourly rainfall is necessary to develop relationships between SRI flows and rainfall, and to define "storm" days.

Appendix C-2 contains further documentation on the flow data worksheets.

Average Wet Season Infiltration

Table 4-3 presents an excerpt from Section 3 of the wet-season flow worksheet for D001C. As shown in Table 4-3, the infiltration rate for this monitor is relatively low at 50 gallons per acre per day (gpad). This 50-gpad value was then assigned to the subbasins represented by this monitor, specifically, service area Nos. 8 and 105 in the Durham system.

Records identified as "Storm" days are considered to be rapid infiltration "events" and are further analyzed in Section 4 of the worksheets. The WWI rate is subtracted from the hourly I/I values in Section 3, leaving only the rapid infiltration flows.

Storm-Responsive Infiltration

Table 4-4 presents an excerpt from Section 4 of the data analysis worksheet for monitor D001C, which includes only rapid infiltration hydrographs. The representative days selected for further review and analysis are highlighted in blue. For each of these events, graphs of SRI flow (in gpm) and rainfall (in inches) versus time were prepared and are included in each worksheet. Values shown as "<0" in this section are the result of subtracting the average seasonal WWI from the flows in Section 3. If the value was negative or zero, this identifier was used. The 80th percentile calculations are for information purposes only, and are based on the non-zero values in Section 4.

Table 4-3. Example Wet Season Infiltration Calculations for D001C

USA Wet Weather Estimated I/I
Basin: D001C
Dry Weather Monitor: D001C

ADWF					
Year	1991	1992	1994	1995	1997 est
Weekday	245.7	339.6	290.0	288.2	315.0
Weekend	265.4	349.9	290.0	289.6	320.0

Monitored Area	
Total	968.0 acres
Residual	968.0 acres
(Use estimated area)	

AVERAGE WWI	
Average I/I	33.7 gpm
Std. Dev.	30.6 gpm
Average I/I	50 gpad

Unit ADWF	Weekday		0.708	0.534	0.490	0.501	0.460	0.517	0.996	1.651	1.580	1.392	1.289	1.194	1.104	1.060	1.000	0.960	0.959	1.014	1.113	1.153	1.155	1.123	1.103	0.943	Storm Limit
Unit ADWF	Weekend		0.719	0.572	0.479	0.451	0.453	0.482	0.584	0.837	1.194	1.496	1.611	1.550	1.429	1.293	1.190	1.101	1.081	1.099	1.131	1.130	1.101	1.078	1.035	0.902	0.20 in/day
SECTION 3 - INFLOW AND INFILTRATION COMPONENT (WWI & SRI) (gpm)																											
			Time of Day																								
Date	Year	Day of Week	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	Hourly Average	WWI/SRI Indicator
05-DEC-91	1991	THU	NA	NA	NA	NA	NA	7.5	52.3	78.2	17.1	NA	NA	NA	NA	NA	NA	NA	NA	11.0	23.8	NA	15.1	NA	NA	NA		Storm
06-DEC-91	1991	FRI	NA	8.1	8.7	26.9	40.9	83.4	167.0	199.7	166.7	172.1	156.0	153.0	138.9	142.4	190.7	100.8	105.5	113.6	102.9	62.7	19.1	24.1	19.2	22.8		Storm
07-DEC-91	1991	SAT	41.7	61.9	66.4	71.0	46.5	49.1	41.2	33.2	84.2	70.6	62.3	53.3	27.0	18.0	0.5	14.5	37.1	60.6	27.6	4.3	NA	NA	NA	NA		Storm
08-DEC-91	1991	SUN	NA	10.2	5.8	8.7	2.5	NA	NA	NA	NA	NA	5.3	19.5	67.5	23.1	25.7	20.6	18.2	26.8	NA	30.2	14.5	14.1	NA	NA		Storm
09-DEC-91	1991	MON	NA	2.0	NA	NA	NA	4.2	37.1	69.8	6.5	NA	24.8	14.4	NA	13.8	NA	NA	NA	NA	NA	5.5	NA	5.2	NA	NA	7.6	1.0
10-DEC-91	1991	TUE	NA	NA	NA	NA	NA	NA	95.1	226.7	48.6	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	15.4	1.0
11-DEC-91	1991	WED	NA	NA	NA	NA	NA	NA	41.1	50.5	12.0	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.3	1.0
12-DEC-91	1991	THU	NA	NA	NA	NA	NA	NA	34.3	52.5	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3.6	1.0
13-DEC-91	1991	FRI	NA	NA	NA	NA	NA	NA	10.4	30.7	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1.7	1.0
14-DEC-91	1991	SAT	NA	NA	NA	NA	NA	NA	NA	NA	NA	29.5	48.2	10.1	0.5	NA	NA	NA	NA	27.6	8.9	NA	NA	NA	NA	NA	5.2	1.0
15-DEC-91	1991	SUN	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	15.5	14.3	15.3	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1.9	1.0
16-DEC-91	1991	MON	NA	NA	NA	NA	NA	NA	NA	12.8	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.5	1.0
17-DEC-91	1991	TUE	NA	NA	NA	NA	NA	NA	55.3	173.9	6.8	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	9.8	1.0
11-Nov-94	1994	FRI	12.7	14.6	10.8	NA	NA	NA	NA	NA	NA	2.1	52.8	72.9	48.0	39.8	39.8	43.2	26.9	30.0	18.5	6.1	NA	NA	2.1	8.6	17.9	1.0
12-Nov-94	1994	SAT	29.3	29.0	16.6	14.7	3.9	10.1	16.6	25.4	68.0	44.7	68.1	64.7	62.1	63.3	67.5	42.2	43.9	32.9	30.9	44.5	11.8	8.5	NA	NA	33.3	1.0
13-Nov-94	1994	SUN	7.1	14.1	24.7	21.9	25.9	14.6	NA	NA	NA	NA	35.7	56.8	55.2	60.3	50.8	71.2	37.0	63.1	36.0	51.1	52.7	40.2	18.3	3.8	30.9	1.0
14-Nov-94	1994	MON	NA	NA	NA	NA	NA	NA	14.6	31.8	NA	20.5	NA	NA	13.2	NA	NA	NA	NA	NA	17.7	30.0	40.4	9.8	NA	4.6	7.6	1.0
15-Nov-94	1994	TUE	NA	NA	20.7	33.8	36.2	62.2	192.6	299.9	124.2	NA	NA	NA	NA	NA	NA	NA	NA	NA	23.7	48.5	59.8	52.8	56.0	31.3	43.4	1.0
16-Nov-94	1994	WED	21.8	31.8	56.1	61.3	71.2	90.0	87.3	99.2	123.5	82.3	21.4	43.9	60.8	63.0	52.9	47.1	74.8	80.3	87.4	112.5	115.3	78.3	84.9	92.6	72.5	1.0
17-Nov-94	1994	THU	113.4	85.6	86.4	68.5	71.0	103.9	135.6	104.9	66.9	35.6	75.5	65.4	58.0	46.0	62.3	37.4	54.6	72.8	64.5	52.7	77.6	66.3	42.2	50.3	70.7	1.0
18-Nov-94	1994	FRI	45.5	48.0	44.8	25.3	36.8	64.9	64.1	38.3	32.5	19.3	23.2	33.2	23.5	7.9	19.0	35.1	43.5	36.6	16.8	29.7	9.2	NA	NA	12.1		Storm
19-Nov-94	1994	SAT	34.3	32.1	31.4	15.1	18.6	21.7	34.7	47.6	48.6	13.7	30.5	17.8	32.6	44.8	38.2	42.1	49.5	47.8	65.2	72.1	109.0	67.9	53.6	72.8		Storm
20-Nov-94	1994	SUN	68.1	61.4	54.8	38.5	30.9	19.1	NA	NA	2.8	29.2	85.9	61.6	44.7	20.4	52.1	55.0	29.5	49.2	43.5	64.2	50.1	12.1	3.4	NA		Storm
21-Nov-94	1994	MON	NA	3.0	NA	NA	NA	6.4	NA	NA	NA	NA	NA	NA	4.1	10.1	8.3	8.5	15.1	NA	12.6	15.4	19.2	22.8	16.9	NA	5.9	1.0
22-Nov-94	1994	TUE	NA	NA	4.3	2.9	1.8	9.7	131.3	255.9	102.0	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	13.4	19.1	13.2	12.9	NA	23.6	1.0
23-Nov-94	1994	WED	NA	21.2	19.0	NA	NA	NA	NA	NA	NA	33.0	7.9	NA	NA	NA	NA	0.9	0.5	NA	NA	2.6	33.9	13.6	14.3	45.4		Storm
24-Nov-94	1994	THU	62.3	71.0	60.5	27.0	30.5	21.3	NA	NA	NA	87.1	194.9	233.2	231.7	154.0	131.5	105.3	58.4	17.9	NA	NA	27.8	15.6	NA	19.5		Storm
25-Nov-94	1994	FRI	97.8	118.9	99.2	75.4	84.3	72.3	NA	NA	NA	145.3	168.9	188.1	168.8	129.5	109.5	125.7	125.8	140.0	107.1	105.5	126.9	122.5	134.9	187.9		Storm
26-Nov-94	1994	SAT	219.1	230.1	227.2	197.1	165.1	167.9	163.2	160.5	224.7	207.0	211.1	227.0	206.7	203.2	161.0	141.7	144.7	159.5	154.4	134.2	135.1	68.2	80.5	95.6		Storm
27-Nov-94	1994	SUN	105.2	115.2	114.5	87.5	68.4	93.9	81.7	37.3	37.1	36.5	43.2	96.9	88.6	120.0	172.9	179.2	184.3	170.2	153.1	134.2	121.4	149.3	115.6	116.7	109.3	1.0
28-Nov-94	1994	MON	112.8	116.7	133.4	97.6	108.6	119.6	139.7	174.4	133.6	119.8	125.2	85.1	83.4	93.8	83.1	64.8	57.3	62.0	71.5	88.2	86.2	61.3	58.1	46.8	96.8	1.0
29-Nov-94	1994	TUE	20.3	25.8	32.1	13.7	12.0	45.2	166.8	280.2	124.2	NA	NA	NA	NA	NA	NA	NA	5.4	15.6	31.4	75.5	70.1	56.7	55.6	43.8	44.8	1.0
30-Nov-94	1994	WED	21.6	20.5	16.1	8.7	18.9	26.4	74.9	112.4	107.4	80.4	99.8	132.9	166.3	208.3	270.8	390.7	469.3	377.3	336.8	293.5	280.9	248.0	232.2	210.1		Storm
01-Dec-94	1994	THU	248.2	248.6	220.6	184.4	193.9	189.4	210.4	198.8	135.2	122.1	137.7	143.9	129.6	103.9	71.7	58.1	62.0	63.6	73.0	94.8	117.8	115.5	114.3	95.5		Storm
02-Dec-94	1994	FRI	88.3	96.4	88.3	63.4	71.3	97.7	125.0	88.1	67.5	63.4	58.5	66.5	59.8	73.4	75.5	82.4	94.2	81.5	78.0	67.0	57.4	18.0	40.4	58.5	73.4	1.0
03-Dec-94	1994	SAT	95.0	76.8	67.1	64.4	53.4	50.3	53.6	59.3	79.2	54.8	73.4	92.0	96.2	92.8	68.6	88.2	91.5	113.5	74.1	47.6	41.1	34.6	27.7	45.2	68.4	1.0
04-Dec-94	1994	SUN	60.5	53.9	59.3	38.8	28.0	16.7	5.1	NA	13.9	13.5	38.8	61.2	50.0	52.5	50.7	77.8	60.8	63.5	53.5	61.1	61.7	67.2	63.6	28.9	45.0	1.0
05-Dec-94	1994	MON	21.0	26.2	21.4	8.4	22.2	39.7	56.1	8.7	17.6	20.7	17.6	16.4	30.5	21.9	11.8	16.5	22.1	26.0	28.1	29.3	36.7	24.3	22.8	15.1	23.4	1.0
06-Dec-94	1994	TUE	25.3	30.6	44.1	38.3	39.5	56.3	140.8	144.1	55.2	NA	NA	NA	NA	NA	NA	NA	8.8	26.3	52.2	52.5	76.7	NA	NA	NA		Storm
07-Dec-94	1994	WED	NA	NA	NA	NA	11.4	53.3	62.3	17.4	6.6	NA	1.0	27.1	0.6	40.8	22.1	16.9	20.8	23.5	20.3	16.0	14.8	3.3	13.2	25.0		Storm
10-Nov-95	1995	FRI	2.0	0.3	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA		Storm
11-Nov-95	1995	SAT	257.3	282.3	240.0	144.6	114.2	217.2	283.4	298.6	335.8	424.5	282.1	299.8	235.4	210.0	237.4	158.0	81.8	77.0	75.9	87.7	57.8	44.0	41.4	46.6		Storm
12-Nov-95	1995	SUN	71.1	82.5	76.4	68.5	38.4	20.6	NA	NA	NA	NA	NA	NA	6.3	11.3	NA	NA	NA	NA	NA	NA	NA	0.8	NA	7.8		Storm

Table 4-4. Example Rapid Infiltration Calculations for D001C

USA Stormwater Related I/I (SRI)
Basin: D001C

80TH Percentile SRI (gpm)	151.0
80TH Percentile SRI (gpad)	225

DAILY RAINFALL (inches)					SECTION 4 - STORM RELATED I/I (SRI) (gpm)																							
Date	Rain Gage	On Day	Previous Day	Previous 2 Days	Time of Day																							Daily Average
	RVR	0.00	0.00																									
	RVR	0.00	0.00		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	
05-Dec-91	RVR	0.58	0.16		<0	<0	<0	<0	<0	<0	18.7	44.5	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	2.6
06-Dec-91	RVR	0.98	0.58		<0	<0	<0	<0	7.2	49.7	133.3	166.0	133.1	138.4	122.3	119.3	105.2	108.7	157.1	67.1	71.9	80.0	69.2	29.1	<0	<0	<0	<0	64.9
07-Dec-91	RVR	0.24	0.98		8.0	28.3	32.7	37.4	12.8	15.4	7.6	<0	50.6	36.9	28.7	19.7	<0	<0	<0	<0	3.4	26.9	<0	<0	<0	<0	<0	<0	12.9
08-Dec-91	RVR	0.02	0.24		<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	33.8	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	1.4
09-Dec-91	RVR	0.05	0.02																										0.0
10-Dec-91	RVR	0.01	0.05																										0.0
11-Dec-91	RVR	0.04	0.01																										0.0
12-Dec-91	RVR	0.00	0.04																										0.0
13-Dec-91	RVR	0.00	0.00																										0.0
14-Dec-91	RVR	0.00	0.00																										0.0
15-Dec-91	RVR	0.00	0.00																										0.0
16-Dec-91	RVR	0.01	0.00																										0.0
17-Dec-91	RVR	0.00	0.01																										0.0
11-Nov-94	RVR	0.04	0.14																										0.0
12-Nov-94	RVR	0.08	0.04																										0.0
13-Nov-94	RVR	0.02	0.08																										0.0
14-Nov-94	RVR	0.00	0.02																										0.0
15-Nov-94	RVR	0.20	0.00																										0.0
16-Nov-94	RVR	0.11	0.20																										0.0
17-Nov-94	RVR	0.06	0.11																										0.0
18-Nov-94	RVR	0.36	0.06		11.8	14.4	11.2	<0	3.1	31.2	30.4	4.6	<0	<0	<0	<0	<0	<0	<0	1.4	9.8	2.9	<0	<0	<0	<0	<0	<0	5.0
19-Nov-94	RVR	0.80	0.36		0.7	<0	<0	<0	<0	<0	1.0	14.0	14.9	<0	<0	<0	<0	11.1	4.6	8.5	15.9	14.1	31.6	38.4	75.3	34.2	19.9	39.1	13.5
20-Nov-94	RVR	0.02	0.80		34.5	27.8	21.2	4.9	<0	<0	<0	<0	<0	<0	52.2	27.9	11.0	<0	18.5	21.3	<0	15.5	9.8	30.5	16.5	<0	<0	<0	12.1
21-Nov-94	RVR	0.01	0.02																										0.0
22-Nov-94	RVR	0.00	0.01																										0.0
23-Nov-94	RVR	0.22	0.00		<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	0.3	<0	<0	11.7	0.5
24-Nov-94	RVR	0.27	0.22		28.6	37.3	26.9	<0	<0	<0	<0	<0	<0	53.4	161.2	199.5	198.0	120.3	97.8	71.6	24.7	<0	<0	<0	<0	<0	<0	<0	42.5
25-Nov-94	RVR	0.28	0.27		64.1	85.2	65.5	41.7	50.7	38.6	<0	<0	<0	111.6	135.2	154.4	135.1	95.8	75.8	92.0	92.2	106.3	73.5	71.9	93.3	88.9	101.2	154.3	80.3
26-Nov-94	RVR	0.04	0.28		185.5	196.5	193.6	163.4	131.4	134.2	129.6	126.9	191.0	173.4	177.5	193.3	173.1	169.6	127.3	108.1	111.0	125.8	120.7	100.6	101.5	34.6	46.8	61.9	136.5
27-Nov-94	RVR	0.14	0.04																										0.0
28-Nov-94	RVR	0.01	0.14																										0.0
29-Nov-94	RVR	0.05	0.01																										0.0
30-Nov-94	RVR	1.55	0.05		<0	<0	<0	<0	<0	<0	41.3	78.8	73.8	46.7	66.1	99.2	132.6	174.6	237.1	357.0	435.6	343.6	303.1	259.9	247.3	214.4	198.5	176.4	145.3
01-Dec-94	RVR	0.09	1.55		214.5	214.9	187.0	150.7	160.2	155.8	176.8	165.1	101.5	88.5	104.0	110.2	96.0	70.2	38.0	24.4	28.3	30.0	39.3	61.2	84.2	81.8	80.6	61.8	105.2
02-Dec-94	RVR	0.07	0.09																										0.0
03-Dec-94	RVR	0.00	0.07																										0.0
04-Dec-94	RVR	0.00	0.00																										0.0
05-Dec-94	RVR	0.00	0.00																										0.0
06-Dec-94	RVR	0.27	0.00		<0	<0	10.4	4.6	5.8	22.6	107.2	110.5	21.6	<0	<0	<0	<0	<0	<0	<0	<0	<0	18.6	18.9	43.1	<0	<0	<0	15.1
07-Dec-94	RVR	0.01	0.27		<0	<0	<0	<0	<0	19.7	28.6	<0	<0	<0	<0	<0	<0	7.1	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	2.3
10-Nov-95	CHR	0.68	0.25		<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	0.0
11-Nov-95	CHR	1.88	0.68		223.6	248.6	206.4	110.9	80.5	183.6	249.8	264.9	302.1	390.8	248.4	266.2	201.7	176.4	203.7	124.4	48.1	43.3	42.3	54.0	24.2	10.3	7.7	13.0	155.2
12-Nov-95	CHR	0.18	1.88		37.4	48.8	42.7	34.8	4.7	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	<0	7.0
21-Feb-97	RVR	0.00	0.02																										0.0
22-Feb-97	RVR	0.00	0.00																										0.0
23-Feb-97	RVR	0.00	0.00																										0.0
24-Feb-97	RVR	0.00	0.00																										0.0
25-Feb-97	RVR	0.13	0.00																										0.0

For illustration purposes, the November 30-December 1, 1994 rapid infiltration event was selected from the D001C records. This event produced 1.56 inches of rainfall over 16 hours. Figure 4-4 and Table 4-5 illustrate the hydrographs and summary data for this event. Figure 4-4 shows the total, dry season sanitary and rapid infiltration hydrographs. Table 4-5 lists the data used to plot the hydrograph and shows the computations used to review the event and estimate defect parameters, including total volumes, maximum hourly rates, duration, volumes, rapid infiltration area, and ratio of rapid area to monitored area.

The rapid infiltration area, which is specific to an event, is the volume under the SRI curve divided by the volume of rain. The rapid-infiltration area is divided by the monitor area to compute the ratio. This ratio was then applied to each subbasin represented by monitor D001C. For instance, infiltration characteristics for service are No. 8 in the Durham system are represented by monitor D001C. The area of service No. 8, which is 198.65 acres, is multiplied by a ratio of 0.0082, yielding an estimated rapid infiltration area of 70,955 square feet. This value was then entered into the *RAP_AREA* field of Hydra defects database.

Figure 4-5 and Table 4-6 illustrate the analysis of a representative event for monitor D033, located downstream of the Cedar Hills rehabilitation project.

Estimates for the rapid infiltration timing (*RAP_BEG*, *RAP_MAX* and *RAP_END* hours) were also taken from the plots. In most cases, both the rapid area ratio and timing were estimated from multiple events, since no single event exactly represents the 5-year 24-hour design event response.

This procedure required an intensive review of the flow monitoring data as well as engineering judgement. It also closely related rainfall to rapid-infiltration response. Because the project scope did not include a complete calibration effort for the models, a data analysis method was needed that would provide reasonable estimates of defects database inputs.

Figure 4-4. Monitor D001C - November 30-December 1, 1994 Event

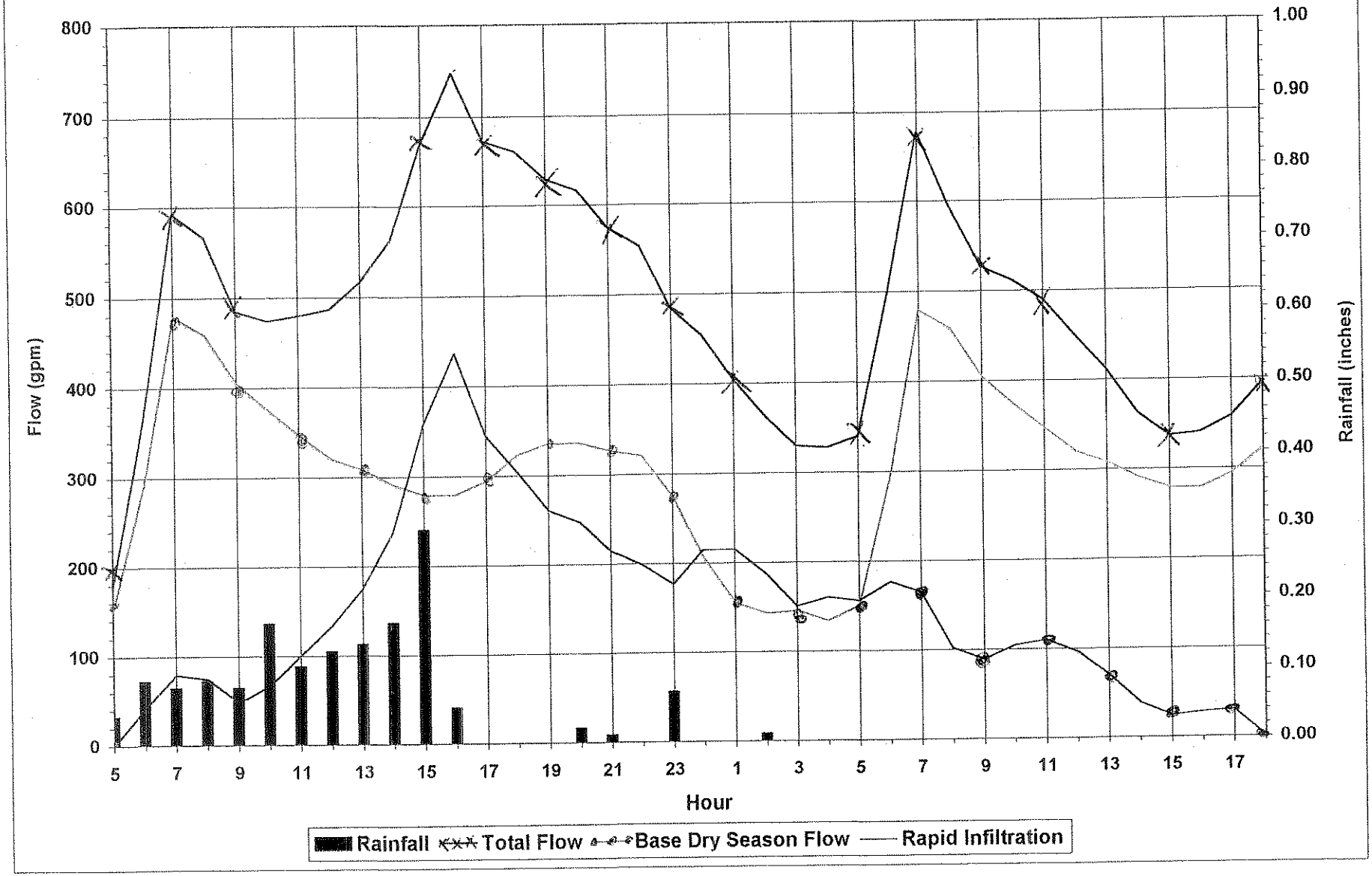


Table 4-5. Representative SRI Event Computations for D001C

Event 3 November 30-December 1, 1994				
Hour	Total	DWF	SRI	Rain
5	176.3	149.9	<0	0.04
6	363.8	288.9	41.3	0.09
7	591.2	478.7	78.8	0.08
8	565.6	458.2	73.8	0.09
9	484.0	403.7	46.7	0.08
10	473.6	373.8	66.1	0.17
11	479.0	346.2	99.2	0.11
12	486.3	320.0	132.6	0.13
13	515.8	307.5	174.6	0.14
14	560.9	290.1	237.1	0.17
15	669.1	278.4	357.0	0.30
16	747.5	278.2	435.6	0.05
17	671.4	294.1	343.6	0.00
18	659.6	322.8	303.1	0.00
19	628.1	334.5	259.9	0.00
20	615.7	334.8	247.3	0.02
21	573.7	325.6	214.4	0.01
22	552.2	320.0	198.5	0.00
23	483.6	273.5	176.4	0.07
0	453.5	205.3	214.5	0.00
1	403.5	154.9	214.9	0.00
2	362.8	142.2	187.0	0.01
3	329.6	145.2	150.7	0.00
4	327.3	133.5	160.2	0.00
5	339.3	149.9	155.8	0.00
6	499.3	288.9	176.8	0.00
7	677.5	478.7	165.1	0.00
8	593.3	458.2	101.5	0.00
9	525.8	403.7	88.5	0.00
10	511.4	373.8	104.0	0.00
11	490.1	346.2	110.2	0.00
12	449.7	320.0	96.0	0.00
13	411.4	307.5	70.2	0.00
14	361.8	290.1	38.0	0.00
15	336.5	278.4	24.4	0.00
16	340.2	278.2	28.3	0.00
17	357.7	294.1	30.0	0.00
18	395.8	322.8	0.0	0.00
Totals (cu.ft./in.)			44938	1.56
Max (gpm/gpad)			435.6	648
Rain Duration (hours)				16
Adjusted Volume (cu.ft.)			44938	
Rapid Area (sq.ft.)			345675	
Ratio of Rapid vs. Monitor Area			0.0082	

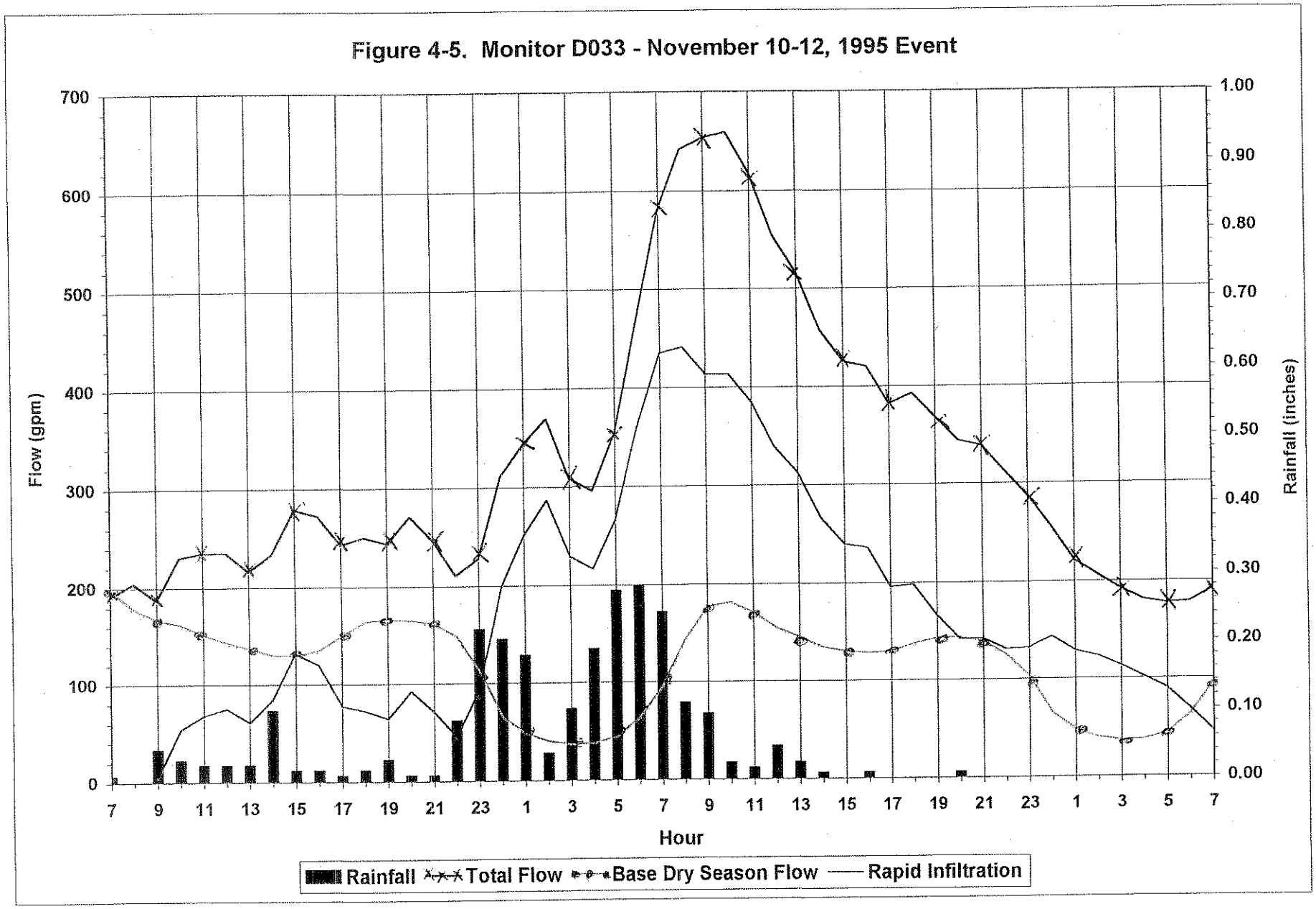


Figure 4-5. Monitor D033 - November 10-12, 1995 Event
Flow (gpm)
Rainfall (inches)
Hour
0
100
200
300
400
500
600
700
0.00
0.10
0.20
0.30
0.40
0.50
0.60
0.70
0.80
0.90
1.00
7 9 11 13 15 17 19 21 23 1 3 5 7 9 11 13 15 17 19 21 23 1 3 5 7
Rainfall
Total Flow
Base Dry Season Flow
Rapid Infiltration

Table 4-6. Representative SRI Event Computations for D033

Event 4 November 10-12, 1995				
Hour	Total	DWF	SRI	Rain
7	189.0	196.02		0.01
8	203.0	177.45		0.00
9	185.3	166.23	4.9	0.05
10	229.2	160.93	53.4	0.03
11	233.5	149.90	67.2	0.02
12	233.8	142.33	74.0	0.02
13	214.7	136.37	60.1	0.02
14	232.0	129.33	83.4	0.10
15	277.8	128.09	130.4	0.02
16	271.3	134.14	118.6	0.02
17	241.3	148.44	76.2	0.01
18	249.0	163.42	71.0	0.02
19	242.7	164.90	63.4	0.03
20	269.7	163.95	91.2	0.01
21	245.5	160.80	69.8	0.01
22	209.2	148.23	44.4	0.09
23	226.6	112.03	93.0	0.22
0	310.4	64.76	198.8	0.21
1	342.5	47.59	250.7	0.18
2	368.5	39.84	285.7	0.04
3	307.0	36.48	228.1	0.10
4	294.8	37.29	214.9	0.19
5	352.7	44.07	265.0	0.28
6	470.2	63.28	360.3	0.28
7	580.3	94.40	434.4	0.25
8	641.7	142.11	440.7	0.11
9	652.7	175.72	412.8	0.10
10	658.6	180.82	412.7	0.02
11	616.8	169.65	383.8	0.02
12	553.0	154.47	337.7	0.05
13	515.7	144.53	311.8	0.02
14	457.0	134.18	265.1	0.01
15	425.1	129.51	238.6	0.00
16	419.7	127.85	235.1	0.01
17	381.0	129.38	194.6	0.00
18	392.0	136.77	197.1	0.00
19	367.2	142.57	165.6	0.00
20	343.3	143.00	141.2	0.01
21	338.0	137.99	141.7	0.00
22	312.0	125.10	130.6	0.00
23	286.3	101.94	131.6	0.00
0	254.6	64.76	143.0	0.00
1	220.1	47.59	128.4	0.00
2	205.5	39.84	122.7	0.00
3	191.4	36.48	112.5	0.00
4	180.3	37.29	100.5	0.00
5	176.4	44.07	88.7	0.00
6	177.9	63.28	68.0	0.00
7	190.6	94.40	44.7	0.00
Totals (cu.ft./in.)			66483	2.55
Max (gpm/gpad)			440.7	3340
Rain Duration (hours)				33
Adjusted Volume (cu.ft.)			66483	
Rapid Area (sq.ft.)			312495	
Ratio of Rapid vs. Monitor Area			0.0378	

Sewer Rehabilitation Areas

As previously mentioned, flow monitoring records for sewer rehabilitation areas were divided into "before" and "after" periods. USA had previously analyzed the effectiveness of these projects for a sample set of rainfall events. The results indicated that sewer main rehabilitation would reduce WWI and SRI rates by 50 percent, and that service lateral rehabilitation would yield a reduction of 80 percent during those events. USA's reduction estimates were based largely on storms more frequent than a 5-year return period.

The available flow data for significant rainfall events (e.g. 2-3 inches of total depth) suggests that reduction rates are lower. However, due to data quality problems, USA's reduction ratios were used in estimating defects database parameters for rehabilitated service areas.

4.4.2. Summary of Hydra Defect Parameters

Based on the analysis of the flow monitoring data, estimated values were summarized in a table, which is presented in Appendix C-6. This table was linked to tables defining representative flow monitors and defect parameters for each service area, which are in Appendix C-7. The latter data were then copied into the defects database files.

For unmonitored subbasins within the Durham and Rock Creek systems, typical values were computed from the monitored basins, as shown on the Appendix C-6 table. For undeveloped areas, a total peak unit rate of 1650 gpad was used (300 gpad for WWI and 1350 gpad for peak SRI), which was adopted in part from the 1995 *Collection System Needs Analysis*.

The 1995 analysis suggested a value of 1850 gpad (500 gpad for WWI and 1350 gpad for peak SRI) for undeveloped areas. The 500-gpad rate represented an 80-percentile value. For this study, only average WWI rates were computed. In order to achieve consistency between the two analyses, the 300-gpad rate computed during the 1995 work was used. Rapid infiltration parameters were defined to approximate the 1350-gpad value.

4.4.3. Verification of Approach to Modeling Defects

The model verification process only involved a check on the rapid infiltration characterization method to ascertain whether the procedure would yield reasonable results. The models were not calibrated. Test runs were completed for selected locations and events. Figures 4-6 and 4-7 present graphical results for test runs completed for selected events from monitors D001C and F008, respectively.

In the case of monitor D001C, the accuracy of the results depend on the accuracy of defect inputs for the upstream meters D001A, D001B and D005, as well as the simulation of the Barnes Road diversion to the Rock Creek system. In addition, the modeled hydrograph peak occurs several hours after the metered peak flow. This problem occurs at many of the flow monitors, primarily because defect characteristics were based on monitors with collection areas that are generally larger than the service areas (sanitary subbasins). The average collection area of the monitors used for this analysis is approximately 920 acres, while the average service area (excluding additional buildout areas) is 100 acres. A few of the monitor basins are thousands of acres in size. Resolving these problems is the purpose of calibration.

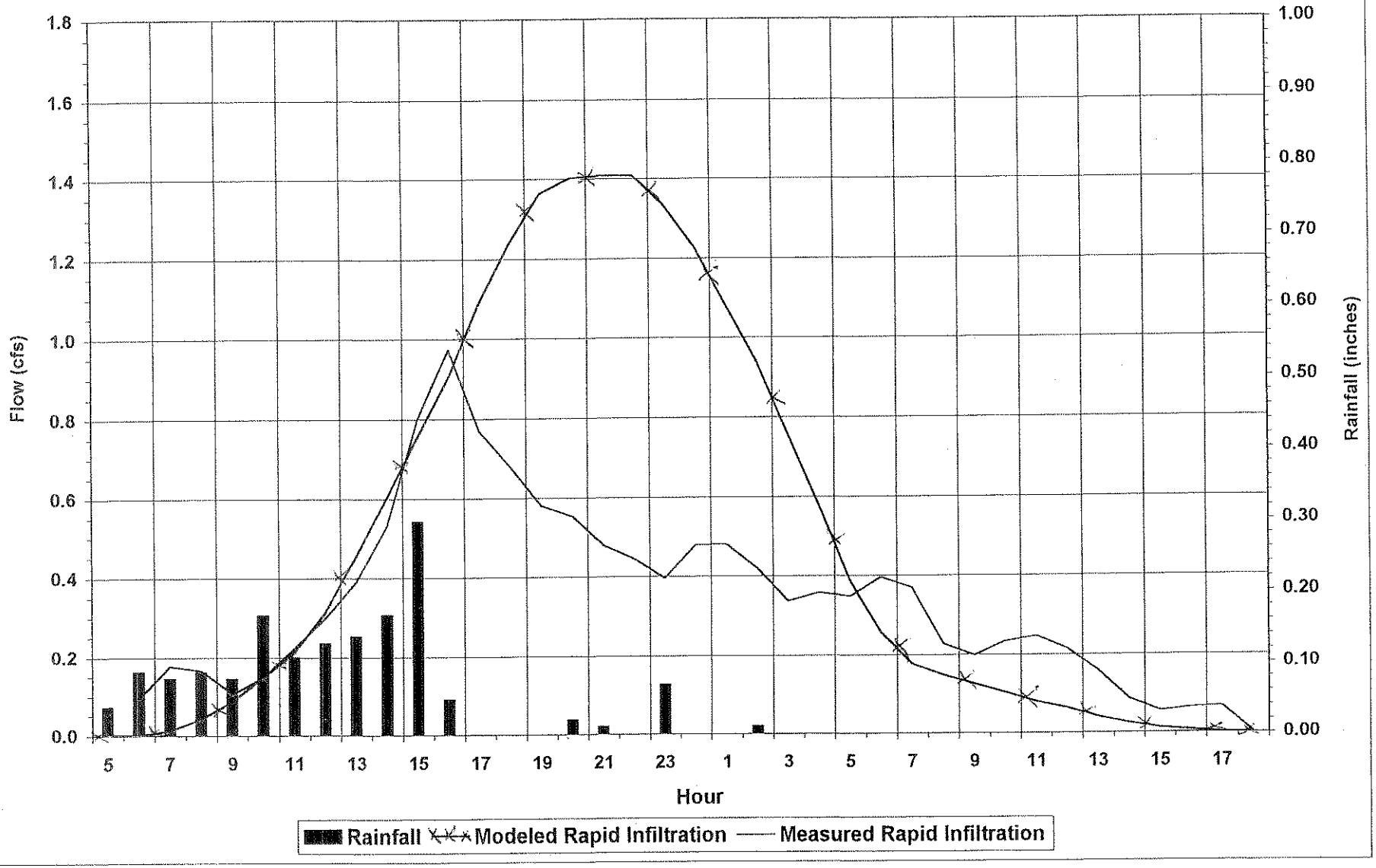
A calibration process would involve selecting representative events throughout the service area, and adjusting the rapid infiltration parameters so that a reasonable match is achieved. The Hydra databases include "tweak" fields for this purpose. For instance, model calibration would have included adjusting the *RAP* hours so that metered and modeled hydrographs would approximately match. Various rainfall/SRI events would be required, since the monitoring periods were not concurrent.

4.5. Defects Databases

The results of the flow monitoring data analysis was used to set up defects databases for each treatment plant basin model, based upon the tables in Appendix C-7. The databases vary between planning years 2000-2010 versus buildout. For instance, if a service area is currently undeveloped but will become developed at buildout then the defects databases will have no I/I contribution until buildout for that service area.

Chapter 5 describes the review of USA's I/I design characteristics based on the results of the defect characterization, and Chapter 6 presents an evaluation of rehabilitation needs.

Figure 4-6. Monitor D001C - November 30-December 1, 1994 Event
Modeled versus Metered Rapid Infiltration



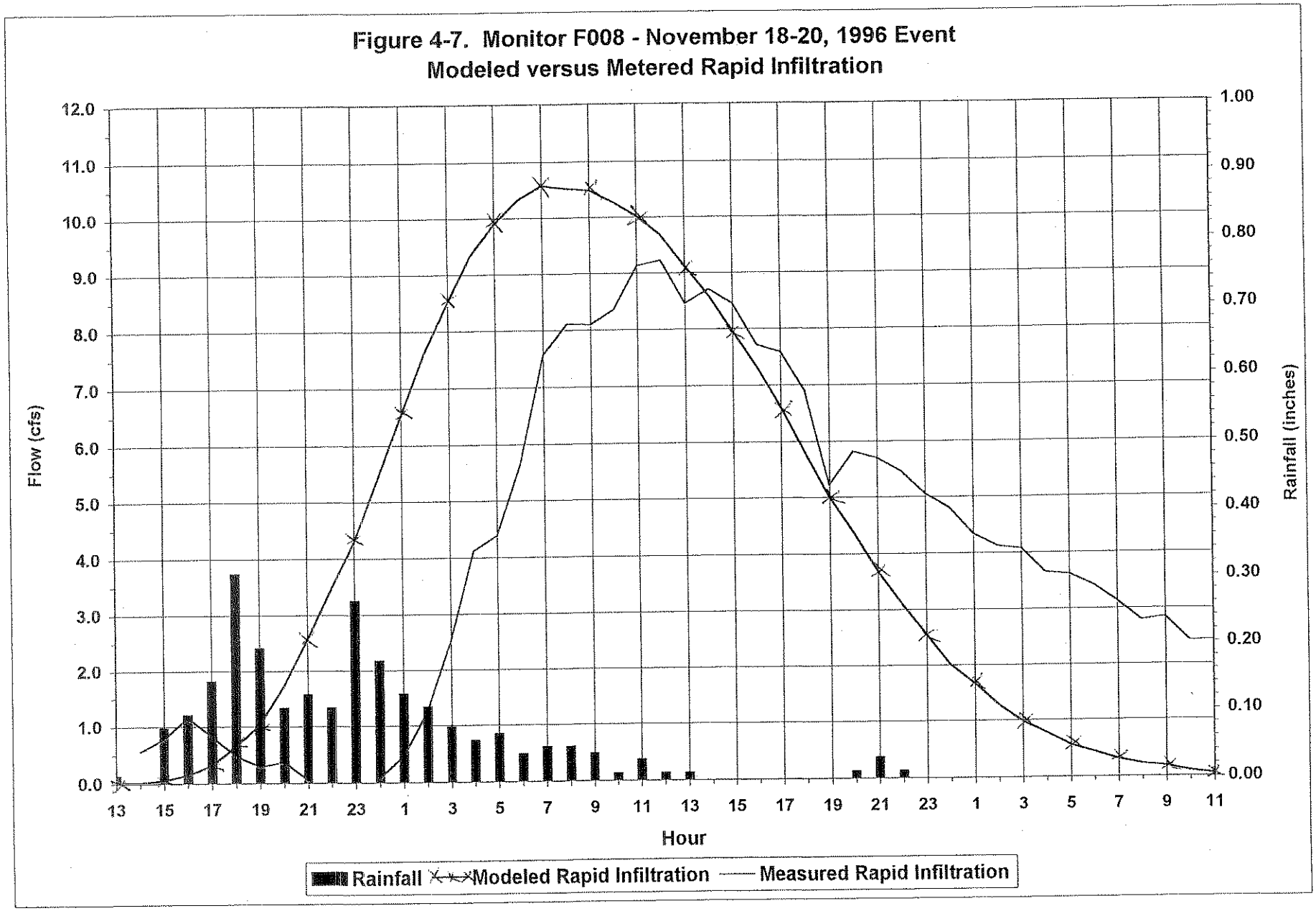


Figure 4-7. Monitor F008 - November 18-20, 1996 Event
Modeled versus Metered Rapid Infiltration
Flow (cfs)
12.0
11.0
10.0
9.0
8.0
7.0
6.0
5.0
4.0
3.0
2.0
1.0
0.0
Rainfall (inches)
1.00
0.90
0.80
0.70
0.60
0.50
0.40
0.30
0.20
0.10
0.00
13 15 17 19 21 23 1 3 5 7 9 11 13 15 17 19 21 23 1 3 5 7 9 11
Hour
Rainfall
Modeled Rapid Infiltration
Measured Rapid Infiltration

APPENDIX H

Technical Memorandum 3 – Proposed Model Extensions

WEST YOST ASSOCIATES
Consulting Engineers

TECHNICAL MEMORANDUM NO. 3

DATE:	June 8, 2007	Project No.:	517-03-06-14
TO:	Andy Braun Clean Water Services	CC:	Distribution (see Attachment)
FROM:	Jeff Pelz	Reviewed By:	Lynne Chicoine

SUBJECT: Sanitary Sewer Master Plan Update—Model Update: Small Diameter Sewer Extensions and Rehabilitation Areas

The purpose of this memorandum is to present the methodology used to identify small diameter sewers to be added to the Clean Water Services (District) sanitary sewer model, and to solicit feedback on the resulting proposed model extensions. Several member cities have indicated a need to model sewers smaller than 10-inch (the previously size limit for modeled facilities). The smaller sewers of concern are those gravity pipelines subject to flows at or exceeding their open channel flow (un-surcharged) capacity. In addition, the model update needs to reflect sewer rehabilitation projects completed since 1999. The analysis and requests are presented under the following headings:

- Justification for Adding Smaller Sewers
- Methodology
- Recommended Small Diameter Model Extensions
- Rehabilitation Project Areas
- Requested Feedback

JUSTIFICATION FOR ADDING SMALLER SEWERS

The small diameter sewers of concern to the District and member cities are those sewers which may be subject to excessive flows. One approach to identifying these sewers would be to add all pipes to the model. While possible, this approach is very time consuming relative to the benefit it provides. Further, the substantial effort would produce an unwieldy model that was significantly

more difficult to use, and that would not likely identify most problems in small diameter sewers since most small diameter sewer capacity limitations are likely to be related to structural and maintenance deficiencies.

The model is a useful tool for identifying capacity limitations associated with excessive flows relative to pipe capacity as determined by their diameter and slope. However, pipeline capacity is also affected by the physical condition of the pipeline; structural deficiencies and buildup of grease and other debris can both reduce capacity in ways that a computer model can not practically account for. Nevertheless, some small diameter sewers may be subject to excessive flows that can be identified by the model. It is those sewers at risk of experiencing flows that exceed their gravity flow capacity when the pipeline is in good condition that should be added to model for evaluation.

METHODOLOGY

The following screening process was used to identify small diameter sewers to be added to the model:

1. Calculate a preliminary average sanitary flow for each model service area. (Service areas are small polygons defined by the collection system configuration. All flow from a single service area is assigned to a single node within the model.) Service areas from the previous (2000) model are used for the purposes of this screening-level analysis.
2. For each service area, estimate an approximate peak wet weather flow as follows:
    a. Estimate the peak sanitary flow using a peaking factor of 2.5 multiplied by the average sanitary flow. The collection system model uses sanitary diurnal curves with a peak-to-average ratio in the range of 1.5 to 2.2 to simulate sanitary flow patterns in 10-inch and larger sewers. The peak-to-average flow ratio in smaller sewers will tend to be higher than in larger sewers. A factor of 2.5 is used as an approximation for screening purposes; the model will be used in later master planning steps to predict peak flows in each sewer.
    b. Estimate an approximate peak infiltration and inflow (I&I) rate using two values, 2,500 and 4,000 gallons per day per acre (gpd/acre). The value of 4,000 gpd/acre was cited as a design value in the 2000 Master Plan Update, and 2,500 gpd/acre is the threshold triggering a recommendation for further investigation. By considering flows based on both I&I rates, a range of potential service area flows can be used to assess which areas may be generating flows exceeding the capacity of small diameter sewers.
    c. Estimate the peak wet weather flow (PWWF) by adding the estimate peak sanitary flow and peak I&I values.
3. Compare the estimated PWWF to the capacity of an 8-inch sewer at a standard minimum slope of and 0.004 feet/foot, respectively, and a Manning's "n" value of 0.013 (CWS Design and Construction Standards for Sanitary Sewer and Surface Water Management, June 2007). The resulting calculated capacity is a reasonable estimate of the minimum capacity to be expected in a pipeline in fair condition. Pipelines that benefit from available

ground slope and were thus constructed at greater than the minimum allowable slope would have a higher capacity. Flatter, sub-standard pipelines would have a lower capacity. Based on the stated assumptions, an 8-inch pipeline would have a full-pipe gravity flow (un-surcharged) capacity of about 0.49 million gallons per day (mgd).

4. Inspect each service area to determine the number and size of the small diameter sewers carrying flow to a sewer already included in the model.
5. For service areas with an estimated approximate PWWF less than the capacity of the minimum sized pipe exiting the service area, no further analysis is warranted and no small diameter sewers need be added to the model.
6. Where the estimated PWWF appears likely to exceed the capacity of the small diameter sewers carrying most or all flow from a given service area, at least one small diameter sewer segment should be added to the model. This determination requires professional judgment, taking into account the collection system configuration and the relative amounts of the service area served by the individual small diameter sewers at the downstream outlet(s). For this determination, the PWWF is assumed to be proportional to area.
7. In most cases the original service area will be divided into two or more service areas for each small diameter sewer segment to be added. Either the entire original service area, or one of the revised service areas will be assigned to the upstream end of the newly added segment.
8. Additional sewers will be added later in the master planning process where growth areas would connect to existing un-modeled sewer segments.

RECOMMENDED SMALL DIAMETER MODEL EXTENSIONS

Using the methodology described above, West Yost Associates identified the small diameter sewers shown in green on Figures 1 through 5 and recommends they be added to the District model. The proposed model extensions are identified as “Small Diameter Segments of Concern” on the figures. In addition, the figures show in red the 10-inch and larger sewers that appear in the District’s GIS but are not included in the previous model. These sewers, identified as “recent construction” on the figures, will also be added to the model. Locations where the sewer diameter listed in the District’s GIS differs from the diameter listed in the previous model are highlighted in blue.

REHABILITATION PROJECT AREAS

Some sewer rehabilitation projects have been implemented since the collection system model was last updated. Completed rehabilitation projects that reduced infiltration and inflow rates should be reflected in the model. The member cities are asked to identify the location of all I&I rehabilitation projects completed after 1999. This information will be used to adjust the parameters used to simulate I&I in the updated model.

REQUESTED FEEDBACK

In response this memorandum, each member agency is asked to provide the following feedback:

1. Review comments of the following nature pertaining the relevant attached figure:
   - corrections (diameters or schematic configurations shown incorrectly on the figures); these might be the result of recent upsizing to the trunk sewer system not yet reflected in the GIS
   - deletions (pipelines for which the effort to incorporate in the model is not warranted)
   - additions (pipelines the reader is aware currently experience chronic capacity limitations that may be attributed to under sizing)
2. A mark-up of the relevant attached figure identifying rehabilitation areas or pipes for which modeled I&I rates should be reduced.
3. To facilitate the model update, WYA requests from the member agencies and the District the following data for the green, red, and blue highlighted pipes, plus any additional segments identified by the reviewer:
   - confirmation of pipeline diameters
   - confirmation of the schematic configuration of the collection system
   - pipe segment lengths, or alternatively, direction to rely on the lengths of pipe segments as shown in the District's GIS
   - invert elevation data for each segment

   It will not be possible to properly model the added or upsized sewers without data describing their physical characteristics. Ideally, data for all highlighted pipes on the figures, plus any other segments identified during the review, should be provided along with the initial feedback in response to this memorandum. Pipe data may be submitted separately at a later date if necessary to expedite the initial feedback.

A table (Attachment 2) is provided for the reader's use as an outline of the requested feedback. An editable, expandable electronic version of the table may also be requested from Corie Peterson of West Yost Associates. A printout of the applicable figure will also be needed in most cases to indicate locations associated with each comment. Legible hand-marks on large-scale excerpts of a figure are acceptable and encouraged if this is most convenient for the reader.

Please contact Jeff Pelz (530-792-3259, jpelz@westyost.com) or Corie Peterson (503-657-8813, cpeterson@westyost.com) with questions regarding the requested feedback..

Feedback items 1 and 2, plus item 3 if possible, are requested by June 22, 2007, and may be submitted to Corie.

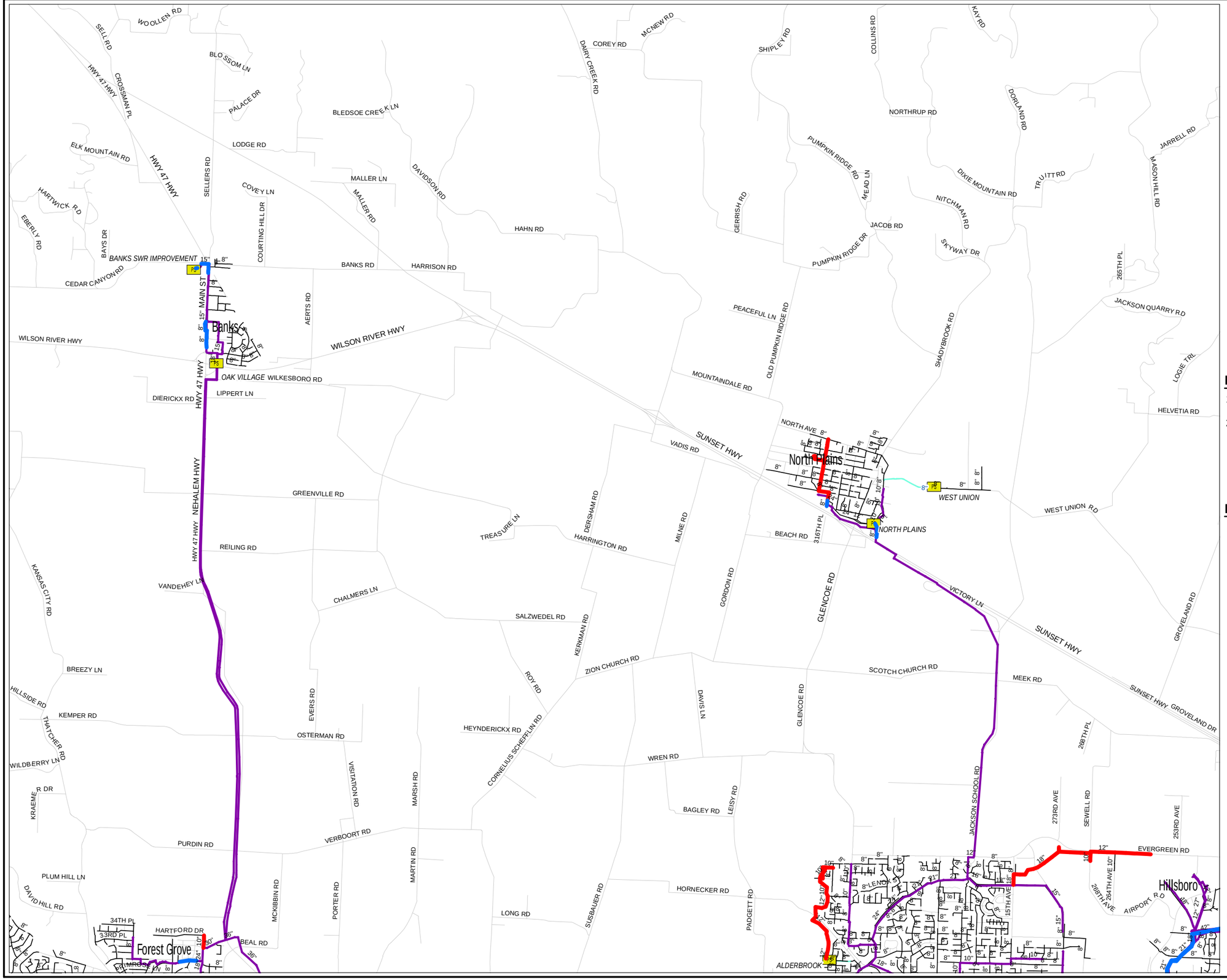
JDP:nmp

attachments

Clean Water Services
Sanitary Sewer Master Plan Update
2007 MODEL EXTENSIONS

Figure 1. Banks / North Plains

DRAFT 6/8/07



0 3,500 7,000
Feet

NOTES:

1. Base mapping, sewer diameters, and alignments based on Clean Water Services GIS.
2. Model sanitary sewers are based on 2000 model, and are subject to revision for 2007.

LEGEND:

- Small Diameter Segments of Concern
- Recent Construction (10" and larger)
- Model vs. GIS Dissimilarity
- WWTP
- Pump Station
- Model Sanitary Sewer
- Other Sanitary Sewer
- Force Main

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n/c/517/030614/gis/model/figure 1_Banks.mxd

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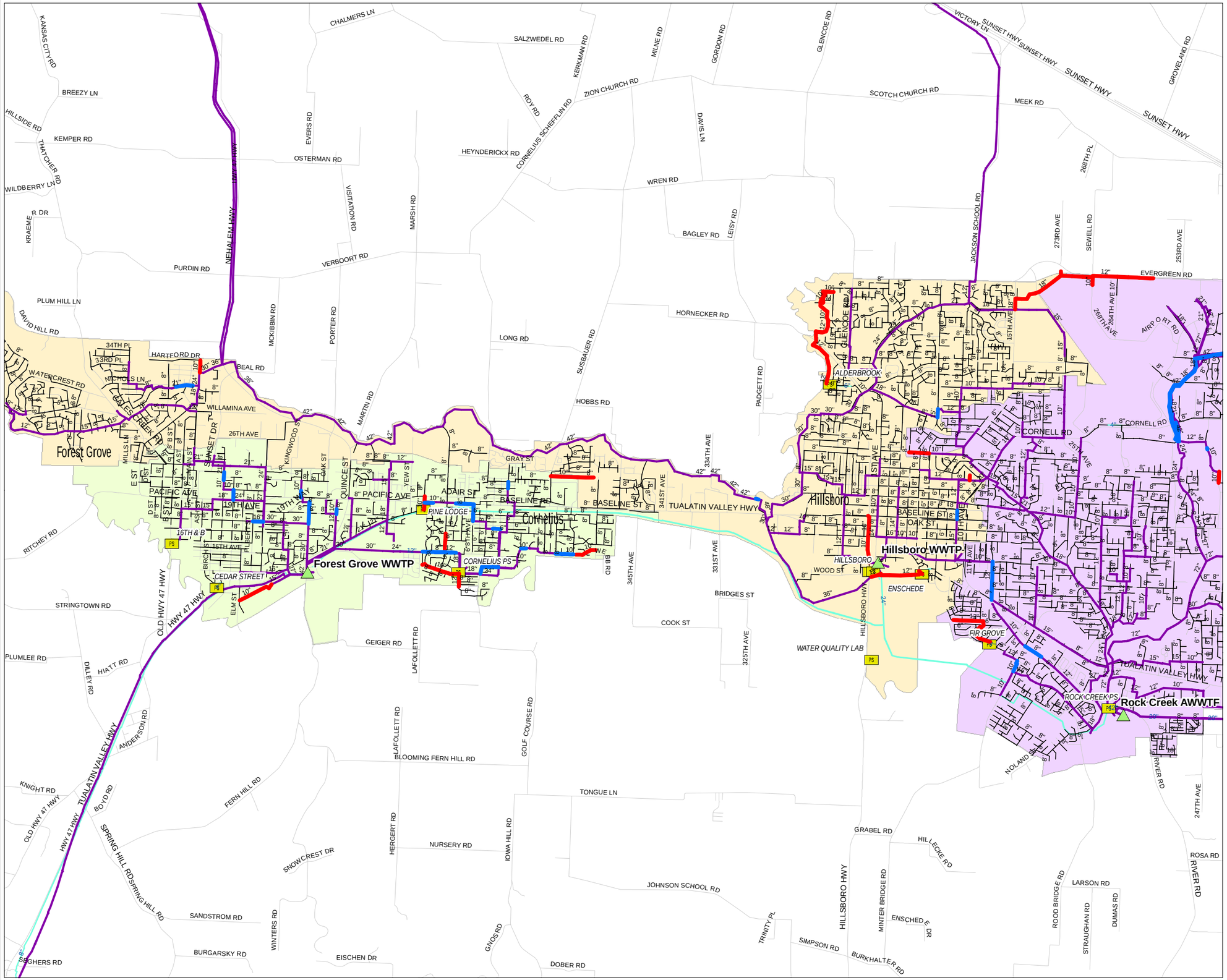
Sanitary Sewer Master Plan Update
2007 MODEL EXTENSIONS

Figure 2. Forest Grove / Cornelius / Hillsboro

DRAFT 6/8/07



NOTES:

1. Base mapping, sewer diameters, and alignments based on Clean Water Services GIS.
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LEGEND:

- Small Diameter Segments of Concern
- Recent Construction (10" and larger)
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- WWTP
- Pump Station
- Model Sanitary Sewer
- Other Sanitary Sewer
- Force Main
- Hillsboro Sanitary Basin
- Forest Grove Sanitary Basin
- Rock Creek Sanitary Basin

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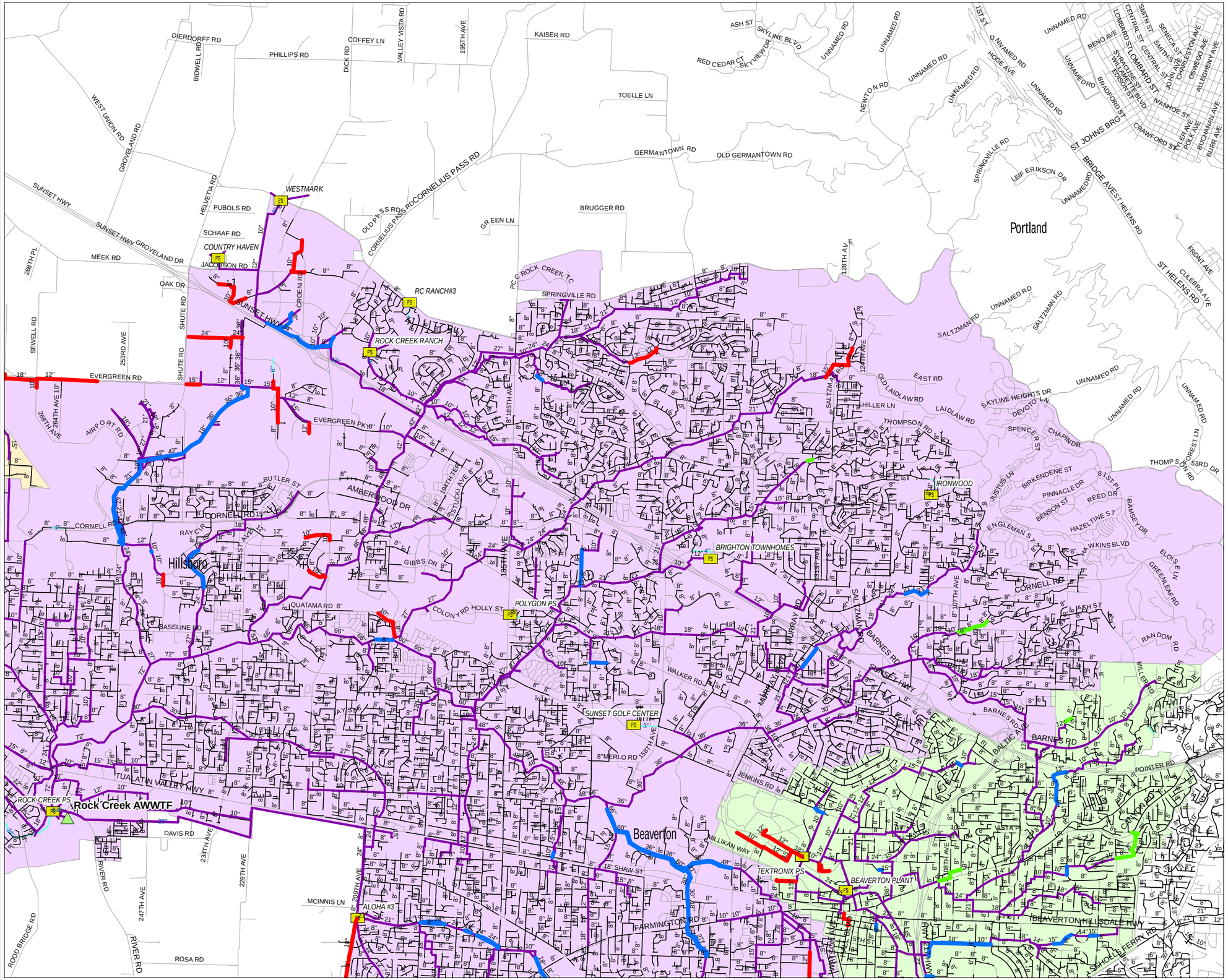
n/c/517/030614/gis/model/figure 2_ForestGrove.mxd

Clean Water Services
Sanitary Sewer Master Plan Update
2007 MODEL EXTENSIONS

Figure 3. Hillsboro / Beaverton

DRAFT 6/8/07



NOTES:

1. Base mapping, sewer diameters, and alignments based on Clean Water Services GIS.
2. Model sanitary sewers are based on 2000 model, and are subject to revision for 2007.

LEGEND:

- Small Diameter Segments of Concern
- Recent Construction (10" and larger)
- Model vs. GIS Dissimilarity
- WWTP
- Pump Station
- Model Sanitary Sewer
- Other Sanitary Sewer
- Force Main
- Hillsboro Sanitary Basin
- Rock Creek Sanitary Basin
- Durham Sanitary Basin

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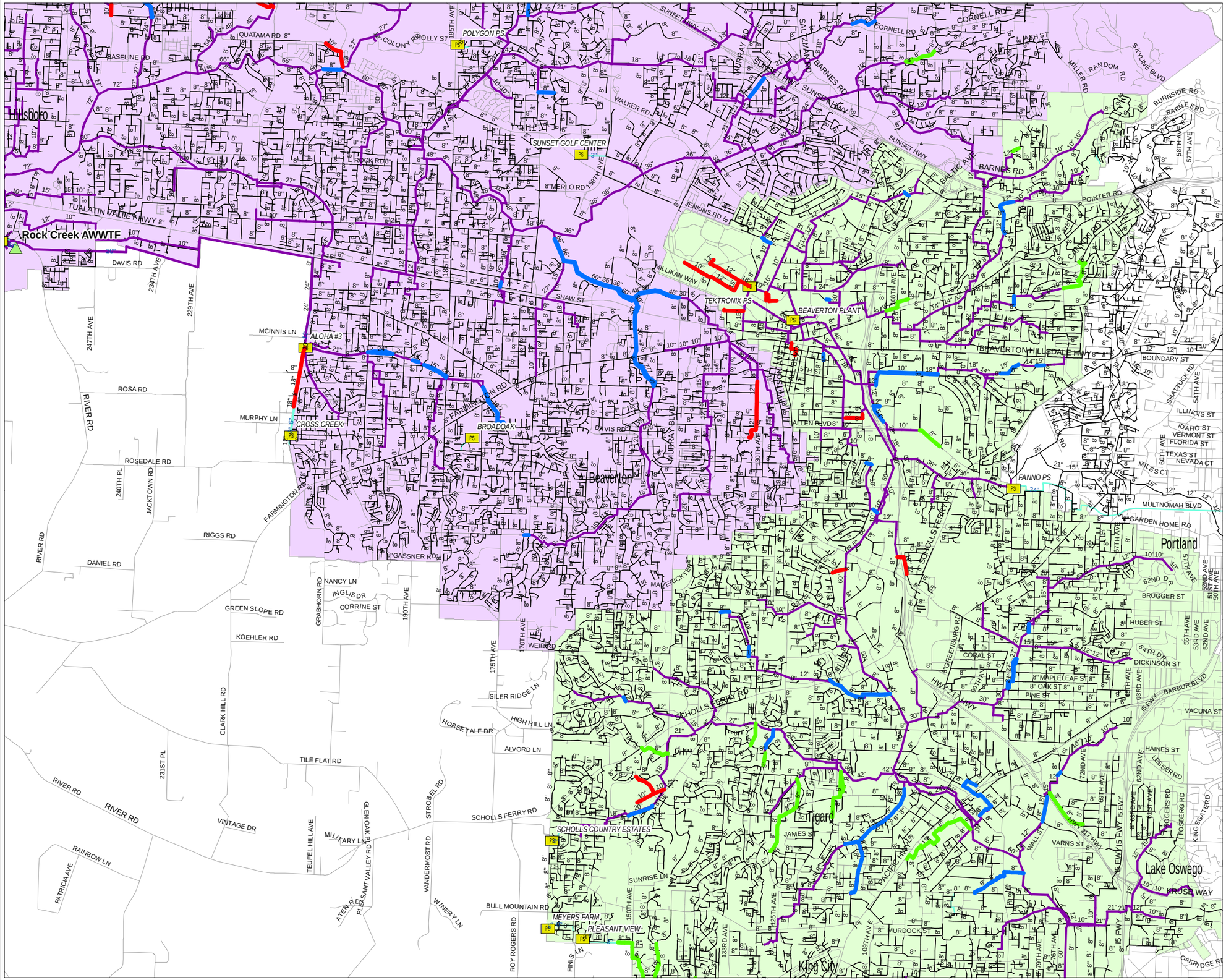
n/c/517/030614/gis/model/figure 3_Hboro.mxd

Clean Water Services
Sanitary Sewer Master Plan Update
2007 MODEL EXTENSIONS

Figure 4. Beaverton / Tigard

DRAFT 6/8/07



NOTES:

1. Base mapping, sewer diameters, and alignments based on Clean Water Services GIS.
2. Model sanitary sewers are based on 2000 model, and are subject to revision for 2007.

LEGEND:

- Small Diameter Segments of Concern
- Recent Construction (10" and larger)
- Model vs. GIS Dissimilarity
- WWTP
- Pump Station
- Model Sanitary Sewer
- Other Sanitary Sewer
- Force Main
- Rock Creek Sanitary Basin
- Durham Sanitary Basin

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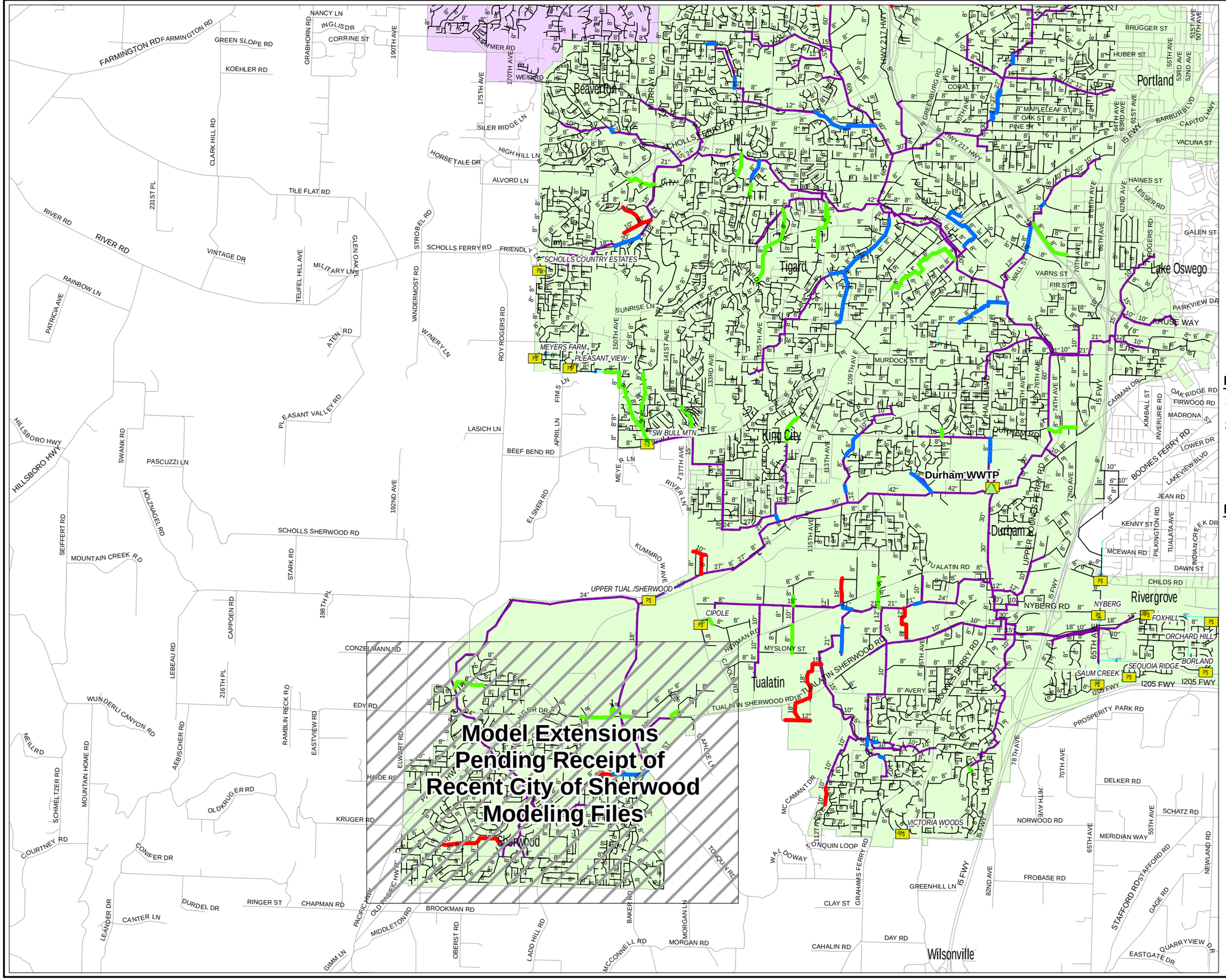
n/c/517/030614/gis/model/figure 4_Beaverton.mxd

Clean Water Services
Sanitary Sewer Master Plan Update
2007 MODEL EXTENSIONS

Figure 5. Tigard / Tualatin / Sherwood

DRAFT 6/8/07



NOTES:

1. Base mapping, sewer diameters, and alignments based on Clean Water Services GIS.
2. Model sanitary sewers are based on 2000 model, and are subject to revision for 2007.

LEGEND:

- Small Diameter Segments of Concern
- Recent Construction (10" and larger)
- Model vs. GIS Dissimilarity
- WWTP
- Pump Station
- Model Sanitary Sewer
- Other Sanitary Sewer
- Force Main
- Rock Creek Sanitary Basin
- Durham Sanitary Basin

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Consulting Engineers

n/c/517/030614/gis/model/figure 5_Tualatin.mxd

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Agency Input Request

The following table lists specific items for which Clean Water Services (District) and West Yost Associates (WYA) would like agency feedback prior to modeling of the District's sanitary sewer system. The table lists the issue, a desired completion date, and a response area for agency staff completion. If more space is required, please feel free to attach additional pages or to provide electronic files. Spreadsheet files of tabular data are preferred.

Issue	Requested Completion Date	City Response
1. Are the pipeline diameters shown on the TM No. 3 figures correct and complete?	June 22, 2007	
2. Are the pipeline schematic configurations shown on the TM No. 3 figures correct and complete?	June 22, 2007	
3. What I&I rehabilitation projects have been completed since 1999? (Please indicate locations. If convenient, use hand-marks on an enlarged excerpt of the relevant figure.)	June 22, 2007	
4. Are all proposed model pipeline extensions shown on the TM No. 3 figures warranted? (If not, please indicate deletions.)	June 22, 2007	
5. Are there additional pipelines that should be added to the model? (Please indicate locations.)	June 22, 2007	
6. Is invert elevation and pipe length data for each new modeled pipe available and if so, when will it be transmitted to WYA?	June 22, 2007	

Please return this table via fax, email or hard copy to:

Corie Peterson
West Yost Associates
1800 Blankenship Road, Suite 425
West Linn, Oregon 97062
Phone: 503-657-8813
Fax: 503-722-2342
email: cpeterson@westyost.com

Additional questions can be directed to Jeff Pelz at:

Jeff Pelz
West Yost Associates
1260 Lake Boulevard, Suite 240
Davis, California 95616
Phone: 530-756-5905
Fax: 530-756-5991
email: jpelz@westyost.com

APPENDIX I

Summary and Detailed Diversion Curve Tables

APPENDIX B-8
DIVERSION DATA WORKSHEETS

2000 MP Update Hydra Diversion Curves

Basin	Diversion Name	Diversion MH	MH G_ID	To MH	To Pipe	Pipe G_ID	Q	DID Values													Notes
DR	Barnes Rd Diversion	1522	5005	1523	01522_01523	55	SysQ	0.00	2.33	5.06	7.99	10.11	10.69	11.24	11.77	12.51	13.21	15.70	5.00		Dual MH No. 12883 abandoned
DR	Barnes Rd Diversion	1522	5005	12822	01522_12822	2117	DivQ	0.00	1.25	2.71	4.28	5.42	5.67	5.92	6.15	6.48	6.80	7.94	5.00		12282_12883 (G_ID 2117) to RC
DR	Fairfield Diversion	13862	5007	9917	13862_09917	736	SysQ	0.00	0.58	2.14	4.27	5.82	6.82	9.58	11.57	13.21	17.10	20.18	22.81	25.15	Dual MH No. 13861 abandoned
DR	Fairfield Diversion	13862	5007	9961	13862_09961	2118	DivQ	0.00	0.30	1.06	1.93	2.12	2.13	2.14	2.15	2.16	2.20	2.23	2.26	2.29	
DR	SW Lombard Diversion #2	18554	5000	18828	18554_18828	562	SysQ	0.00	5.87	14.77	24.54	46.81	67.54	77.53	82.23	90.90	98.81	112.96	125.52		Dual MH No. 18553 abandoned
DR	SW Lombard Diversion #2	18554	5000	18552	18554_18552	561	DivQ	0.00	3.20	8.96	15.35	35.18	55.01	63.97	68.09	75.66	82.54	94.81	105.67		
DR	5th St Diversion	18571	5003	20580	18571_20580	603	SysQ	0.00	0.15	0.71	3.24	6.28	7.61	10.57	12.91	14.84	18.05	20.75	23.13		Dual MH No. 20581 abandoned
DR	5th St Diversion	18571	5003	18570	18571_18570	569	DivQ	0.00	0.15	0.53	1.70	3.16	3.99	6.71	8.71	10.33	12.98	15.17	17.09		
DR	SW Lombard Diversion #1	18828	5880	18852	18828_18852		SysQ	0.00	0.39	2.30	5.73	10.02	15.29	20.77	28.78	34.05	35.42	41.25	46.30		Dual MH No. 18555 abandoned
DR	SW Lombard Diversion #1	18828	5880	20942	18828_20942	600	DivQ	0.00	0.13	0.70	1.46	2.54	3.81	5.02	6.35	7.08	7.74	9.96	11.76		NOT INCLUDED IN MODEL
DR	SW 5th St Diversion	20606	5004	13244	20606_13244	628	SysQ	0.00	1.66	3.77	6.92	7.48	7.98	8.44	8.87	9.27	9.65	10.02	10.70	11.63	Dual MH No. 20605 abandoned
DR	SW 5th St Diversion	20606	5004	20604	20606_20604	627	DivQ	0.00	0.56	1.54	3.31	3.36	3.40	3.45	3.50	3.54	3.59	3.63	3.72	3.84	
DR	Sherwood Rd Diversion	20760	5006	20761	20760_20761	1802	SysQ	0.00	0.44	1.73	3.65	5.49	5.99	6.28	6.54	6.78	7.12	7.44	8.54	9.02	Dual MH No. 20969 abandoned
DR	Sherwood Rd Diversion	20760	5006	20970	20760_20970	1857	DivQ	0.00	0.01	0.16	0.46	0.83	1.19	1.39	1.57	1.72	1.94	2.13	2.77	3.03	
DR	Tektronix Diversion	20834	5002	20833	20834_20833	651	SysQ	0.00	2.45	8.54	14.99	16.25	19.58	22.42	24.93	27.21	29.32	31.28	34.88	39.67	Dual MH No. 20957 abandoned
DR	Tektronix Diversion	20834	5002	20956	20834_20956	692	DivQ	0.00	0.51	1.74	3.11	3.32	3.84	4.31	4.72	5.11	5.46	5.80	6.41	7.24	High pipe flow split - NOT USED
DR	Tektronix PS Diversion	20911	5772	20910	20911_20910	664	SysQ	0.00	1.00	2.00	2.32	2.52	3.06	4.51	5.11	5.97	6.66	7.26	8.04	8.73	Diverted flow is 1.5 mgd
DR	Tektronix PS Diversion	20911	5772	27865	20911_27865	7603	DivQ	0.00	1.00	2.00	2.32	2.32	2.32	2.32	2.32	2.32	2.32	2.32	2.32	2.32	15" diversion pipe added to model
FG	Cornelius Diversion	12751	5328	12750	12751_12750	23	SysQ	0.00	0.17	0.81	1.84	3.10	4.48	5.60	9.46	16.50	21.13	26.54	30.99	44.53	
FG	Cornelius Diversion	12751	5328	27547	12751_27547	5924	DivQ	0.00	0.11	0.43	0.91	1.48	2.12	2.64	6.11	12.57	16.69	21.43	25.30	36.93	
FG	Hawthorn St Diversion	18846	5013	18845	18846_18845	82	SysQ	0.00	0.86	3.28	7.13	11.27	14.26	21.69	24.16	27.36	33.90	44.72	53.39	60.83	
FG	Hawthorn St Diversion	18846	5013	20393	18846_20393	89	DivQ	0.00	0.00	0.00	0.00	0.00	0.00	0.39	0.99	1.90	4.40	5.51	6.43	7.24	
FG	SE 1st Ave Diversion	20013	5012	21067	20013_21067	65	SysQ	0.00	0.89	3.26	5.94	6.45	7.48	8.37	10.61	11.56	12.45	14.04	14.78		Dual MH 21068 abandoned
FG	SE 1st Ave Diversion	20013	5012	20014	20013_20014	42	DivQ	0.00	0.47	1.62	2.89	3.13	3.75	4.29	5.60	6.15	6.66	7.57	7.99		
FG	23rd Ave Diversion	20414	5014	20420	20414_20420	235	SysQ	0.00	0.00	1.33	4.82	8.60	11.67	13.75	14.67	16.37	17.91	20.64	21.88	23.05	
FG	23rd Ave Diversion	20414	5014	20413	20414_20413	231	DivQ	0.00	0.00	0.35	1.05	1.18	1.33	1.58	1.70	1.90	2.09	2.42	2.57	2.71	
FG	SW Linden Diversion	27860	5904	27859	27860_27859	5907	SysQ	0.00	2.72	4.47	9.72	12.45	14.00	17.88	21.75	27.80	33.21	38.39	42.63		
FG	SW Linden Diversion	27860	5904	27534	27860_27534	5905	DivQ	0.00	0.00	0.00	0.00	0.00	0.00	0.18	2.30	4.14	5.98	8.00	9.38		
HL	W Main St Diversion	19808	5008	19820	19808_19820	163	SysQ	0.00	0.30	1.45	2.46	4.72	5.74	6.98	7.68	9.98	11.84	13.45			Dual MH No. 19819 abandoned
HL	W Main St Diversion	19808	5008	19807	19808_19807	167	DivQ	0.00	0.30	1.04	1.32	1.52	1.71	1.88	2.03	2.56	3.00	3.38			
HL	S 9th Ave Diversion (to RC)	19863	5024	19854	19863_19854	135	SysQ	0.00	0.44	1.49	2.79	4.16	5.17	6.01	8.02	9.62	10.33	10.99	11.62		Dual MH No. 19855 abandoned
HL	S 9th Ave Diversion (to RC)	19863	5024	19856	19863_19856	380	DivQ	0.00	0.40	1.17	1.62	2.24	2.72	3.13	4.12	4.91	5.27	5.60	5.91		19863_19856 (G_ID 308) to RC
HL	9th Ave Diversion (to RC)	20299	5011	20268	20299_20268	1946	SysQ	0.00	0.68	2.54	3.23	3.70	4.12	4.50	5.48	5.90	6.30	7.04	7.37		Dual MH No. 20267 abandoned
HL	9th Ave Diversion (to RC)	20299	5011	20300	20299_20300	49	DivQ	0.00	0.40	1.36	1.72	2.00	2.24	2.45	3.01	3.26	3.48	3.90	4.09		20299_20268 (G_ID 1946) to RC
HL	N 9th Ave Diversion (to RC)	20312	5025	20320	20312_20320	227	SysQ	0.00	0.93	3.57	5.01	5.39	5.83	6.24	6.81	7.33	8.27	9.11	9.89		Dual MH No. 20319 abandoned
HL	N 9th Ave Diversion (to RC)	20312	5025	20318	20312_20318	1986	DivQ	0.00	0.76	2.60	3.29	3.54	3.78	4.01	4.32	4.62	5.16	5.64	6.09		20317_20281 (GID 1990) to RC
RC	SW Madeline St Diversion	7925	5022	7927	07925_07927	1561	SysQ	0.00	0.38	2.13	3.52	7.20	8.87	9.79	12.25	14.28	15.20	16.07			Dual MH No. 16366 abandoned
RC	SW Madeline St Diversion	7925	5022	7922	07925_07922	1411	DivQ	0.00	0.34	1.18	1.49	1.82	2.10	2.34	2.95	3.46	3.68	3.90			
RC	Aloha PS #3 Diversion	12682	5028	12682	12682_12682	1926	SysQ	0.00	0.59	1.18	2.66	4.73	5.92	9.47	14.79	22.19	28.40	48.31	72.46	90.37	Aloha PS dual force mains to RC
RC	Aloha PS #3 Diversion	12682	5028	571	12682_00571	1930	DivQ	0.00	0.30	0.59	1.33	2.37	2.96	4.73	7.40	11.09	14.20	24.15	36.23	45.19	12682 is FM #1, 21795 is FM #2
RC	198th Ave Diversion	16250	5023	16249	16250_16249	1560	SysQ	0.00	1.07	5.17	11.19	17.45	21.04	21.69	23.58	25.32	26.95	28.48	31.32	35.15	Dual MH No. 17003 abandoned
RC	198th Ave Diversion	16250	5023	7706	16250_07706	1548	DivQ	0.00	0.32	2.27	5.40	8.86	11.23	11.43	12.21	12.95	13.65	14.32	15.56	17.26	
RC	Murray Blvd Diverson	16566	5015	1347	16566_01347	238	SysQ	0.00	0.20	0.72	1.45	1.94	2.52	3.06	3.51	3.81	4.09	4.84	5.49	6.07	Dual MH No. 1346 abandoned
RC	Murray Blvd Diverson	16566	5015	1338	16566_01338	92	DivQ	0.00	0.00	0.00	0.13	0.49	0.97	1.42	1.69	1.84	1.97	2.33	2.64	2.91	
RC	Stoddard Dr Diversion	16578	5029	7650	16578_07650	1617	SysQ	0.00	1.53	5.75	11.88	17.63	20.50	20.52	22.19	23.75	25.21	26.59	29.16	32.63	Dual MH No. 7651 abandoned
RC	Stoddard Dr Diversion	16578	5029	16243	16578_16243	1562	DivQ	0.00	0.78	2.94	6.08	9.03	10.50	10.50	11.35	12.15	12.89	13.59	14.90	16.68	
RC	185th Ave Diversion	17992	5016	17991	17992_17991	322	SysQ	0.00	1.12	2.46	4.47	6.48	8.93	14.94	18.25	21.23	26.38	29.10	33.82	37.95	Dual MH No. 5242 abandoned
RC	185th Ave Diversion	17992	5016	5482	17992_05482	277	DivQ	0.00	0.00	0.00	0.00	0.00	0.00	0.20	0.61	1.13	2.48	3.08	3.57	4.01	

2000 MP Update Hydra Diversion Curves

Basin	Diversion Name	Diversion MH	MH G_ID	To MH	To Pipe	Pipe G_ID	Q	DID Values													Notes
RC	Fairmont Dr Diversion	18260	5019	18259	18260_18259	1137	SysQ	0.00	0.17	0.63	1.21	1.70	1.84	2.10	2.33	2.53	2.82	3.07	3.93	4.30	
RC	Fairmont Dr Diversion	18260	5019	20669	18260_20669	1927	DivQ	0.00	0.07	0.26	0.47	0.60	0.67	0.79	0.90	0.99	1.12	1.23	1.61	1.77	
RC	Erickson St Diversion	18263	5020	18545	18263_18545	1166	SysQ	0.00	0.24	0.85	1.54	1.76	2.20	2.68	3.38	4.20	4.66	5.27	5.82	7.62	Incorrect in 95 model as 18236
RC	Erickson St Diversion	18263	5020	18262	18263_18262	1140	DivQ	0.00	0.00	0.00	0.00	0.06	0.25	0.52	0.82	1.31	1.46	1.67	1.85	2.45	Dual MH No. 18548 abandoned
RC	Pearl St Diversion	18344	5021	18545	18344_18545	1144	SysQ	0.00	0.52	1.80	3.60	4.91	5.71	5.96	6.04	6.20	6.43	6.65	7.47		Dual MH No. 18264 abandoned
RC	Pearl St Diversion	18344	5021	18263	18344_18263	1141	DivQ	0.00	0.25	0.91	1.67	1.81	1.84	1.89	1.91	1.94	1.98	2.03	2.20		
RC	Rock Creek PS Diversion	20083	5027	20083	20083_20083	1928	SysQ	0.00	10.00	20.00	30.00	40.00	60.00	80.00	100.00	120.00	140.00	160.00	180.00	200.00	RC PS WWTP dual force mains
RC	Rock Creek PS Diversion	20083	5027	570	20083_00570	1932	DivQ	0.00	3.38	6.76	10.14	13.51	20.27	27.03	33.78	40.54	47.30	54.05	60.81	67.57	20083 is FM #1, 20084 is FM #2
RC	Golf Course Diversion	22342	5017	17982	22342_17982	989	SysQ	0.00	0.70	2.79	5.92	10.18	12.93	17.32	21.24	23.01	36.09	44.02	52.60	66.32	Dual MH No. 5338 abandoned
RC	Golf Course Diversion	22342	5017	5339	22342_05339	988	DivQ	0.00	0.00	0.00	0.00	0.60	1.26	2.69	4.18	5.60	8.22	8.66	9.22	10.24	
RC	Willow Cr Trunk	23959	8003	23958	23959_23958	8006	SysQ	0.00	0.64	2.54	5.97	9.88	15.40	20.69	23.89	29.37	33.06	91.80	109.93		Dual MH No. 23984
RC	Willow Cr Trunk	23959	8003	6966	23959_06966	8004	DivQ	0.00	0.64	2.54	5.41	8.74	12.56	15.58	16.85	18.71	21.15	25.33	28.92		
RC	Willow Cr Trunk	23964	8151	23963	23964_23963	8156	SysQ	0.00	0.62	2.97	12.18	24.95	37.27	40.39	55.84	62.52	94.70	116.69	134.85	165.08	Dual MH No. 23966
RC	Willow Cr Trunk	23964	8151	10579	23964_10579	8154	DivQ	0.00	0.48	2.38	9.52	19.03	28.55	30.92	42.82	47.58	58.47	67.63	75.68	89.65	
RC	Willow Cr Trunk	23967	7986	23965	23967_23965	7989	SysQ	0.00	1.53	6.12	12.24	18.36	24.18	30.60	54.36	68.77	80.32	99.18	114.85	128.57	Dual MH No. 23968
RC	Willow Cr Trunk	23967	7986	10578	23967_10578	7988	DivQ	0.00	0.64	2.58	5.16	7.74	10.19	12.90	34.72	47.38	57.31	73.23	86.27	97.57	
RC	Willow Cr Trunk	23973	7978	23971	23973_23971	7979	SysQ	0.00	1.90	7.61	15.23	24.75	34.26	40.36	59.29	67.41	81.23	93.01	112.95		Dual MH No. 23972
RC	Willow Cr Trunk	23973	7978	10670	23973_10670	8158	DivQ	0.00	0.74	2.94	5.88	9.56	13.23	15.59	25.14	28.98	35.43	40.88	50.03		
RC	Willow Cr Trunk	23977	5896	23976	23977_23976	7970	SysQ	0.00	1.57	6.26	12.53	18.79	24.74	29.76	31.32	52.51	65.86	76.79	94.86	109.96	Dual MH No. 10665
RC	Willow Cr Trunk	23977	5896	10666	23977_10666	572	DivQ	0.00	0.15	0.58	1.17	1.75	2.30	2.77	2.91	14.85	20.80	25.39	32.70	38.64	
RC	Willow Cr Trunk	23983	5853	23982	23983_23982	7959	SysQ	0.00	2.44	9.69	19.71	31.84	38.28	45.57	50.26	67.68	81.39	93.07	112.85	129.64	Dual MH No. 12214
RC	Willow Cr Trunk	23983	5853	6825	23983_06825	606	DivQ	0.00	0.51	1.95	4.24	6.70	7.71	8.82	11.57	13.99	16.06	17.88	21.06	23.82	
RC	Butternut Cr Trunk	25677	8020	25676	25677_25676	8021	SysQ	0.00	0.91	3.64	7.10	9.10	12.75	15.57	17.95	23.69	29.67	38.89	44.14	46.60	Dual MH No. 28357
RC	Butternut Cr Trunk	25677	8020	8609	25677_08609	8023	DivQ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.27	7.29	7.64	
RC	185th Ave Trunk	28053	7886	28052	28053_28052	7889	SysQ	0.00	2.63	5.15	7.56	11.74	12.99	16.16	19.60	21.11	22.52	23.84	25.10		Dual MH No. 28358
RC	185th Ave Trunk	28053	7886	8065	28053_08065	7888	DivQ	0.00	0.00	0.01	0.98	2.56	2.76	3.27	3.86	4.12	4.36	4.60	4.82		

! Diversion MH 1522	Basin:	DR	Name:	Barnes Rd Diversion												
DR01522_Divn= 0.00 / 0.00		~~2.33 / 1.25~~		~~5.06 / 2.71~~	~~7.99 / 4.28~~	~~10.11 / 5.42~~	~~10.69 / 5.67~~	~~11.24 / 5.92~~	~~11.77 / 6.15~~	~~12.51 / 6.48~~	~~13.21 / 6.80~~	~~15.70 / 7.94~~	~~0.00 / 0.00~~	~~0.00 / 0.00~~	5.00/5.00	
! Diversion MH 13862	Basin:	DR	Name:	Fairfield Diversion												
DR13862_Divn= 0.00 / 0.00		0.58 / 0.30		2.14 / 1.06	4.27 / 1.93	5.82 / 2.12	6.82 / 2.13	9.58 / 2.14	11.57 / 2.15	13.21 / 2.16	17.10 / 2.20	20.18 / 2.23	22.81 / 2.26	25.15 / 2.29		
! Diversion MH 18554	Basin:	DR	Name:	SW Lombard Diversion #2												
DR18554_Divn= 0.00 / 0.00		5.87 / 3.20		14.77 / 8.96	24.54 / 15.35	46.81 / 35.18	67.54 / 55.01	77.53 / 63.97	82.23 / 68.09	90.90 / 75.66	98.81 / 82.54	112.96 / 94.81	125.52 / 105.67	0.00 / 0.00		
! Diversion MH 18571	Basin:	DR	Name:	5th St Diversion												
DR18571_Divn= 0.00 / 0.00		0.15 / 0.15		0.71 / 0.53	3.24 / 1.70	6.28 / 3.16	7.61 / 3.99	10.57 / 6.71	12.91 / 8.71	14.84 / 10.33	18.05 / 12.98	20.75 / 15.17	23.13 / 17.09	0.00 / 0.00		
! Diversion MH 18828	Basin:	DR	Name:	SW Lombard Diversion #1												
DR18828_Divn= 0.00 / 0.00		0.39 / 0.13		2.30 / 0.70	5.73 / 1.46	10.02 / 2.54	15.29 / 3.81	20.77 / 5.02	28.78 / 6.35	34.05 / 7.08	35.42 / 7.74	41.25 / 9.96	46.30 / 11.76	0.00 / 0.00		
! Diversion MH 20606	Basin:	DR	Name:	SW 5th St Diversion												
DR20606_Divn= 0.00 / 0.00		1.66 / 0.56		3.77 / 1.54	6.92 / 3.31	7.48 / 3.36	7.98 / 3.40	8.44 / 3.45	8.87 / 3.50	9.27 / 3.54	9.65 / 3.59	10.02 / 3.63	10.70 / 3.72	11.63 / 3.84		
! Diversion MH 20760	Basin:	DR	Name:	Sherwood Rd Diversion												
DR20760_Divn= 0.00 / 0.00		0.44 / 0.01		1.73 / 0.16	3.65 / 0.46	5.49 / 0.83	5.99 / 1.19	6.28 / 1.39	6.54 / 1.57	6.78 / 1.72	7.12 / 1.94	7.44 / 2.13	8.54 / 2.77	9.02 / 3.03		
! Diversion MH 20834	Basin:	DR	Name:	Tektronix Diversion												
DR20834_Divn= 0.00 / 0.00		2.45 / 0.51		8.54 / 1.74	14.99 / 3.11	16.25 / 3.32	19.58 / 3.84	22.42 / 4.31	24.93 / 4.72	27.21 / 5.11	29.32 / 5.46	31.28 / 5.80	34.88 / 6.41	39.67 / 7.24		
! Diversion MH 20911	Basin:	DR	Name:	Tektronix PS Diversion												
DR20911_Divn= 0.00 / 0.00		1.00 / 1.00		2.00 / 2.00	2.32 / 2.32	2.52 / 2.32	3.06 / 2.32	4.51 / 2.32	5.11 / 2.32	5.97 / 2.32	6.66 / 2.32	7.26 / 2.32	8.04 / 2.32	8.73 / 2.32		
! Diversion MH 12751	Basin:	FG	Name:	Cornelius Diversion												
FG12751_Divn= 0.00 / 0.00		0.17 / 0.11		0.81 / 0.43	1.84 / 0.91	3.10 / 1.48	4.48 / 2.12	5.60 / 2.64	9.46 / 6.11	16.50 / 12.57	21.13 / 16.69	26.54 / 21.43	30.99 / 25.30	44.53 / 36.93		
! Diversion MH 18846	Basin:	FG	Name:	Hawthorn St Diversion												
FG18846_Divn= 0.00 / 0.00		0.86 / 0.00		3.28 / 0.00	7.13 / 0.00	11.27 / 0.00	14.26 / 0.00	21.69 / 0.39	24.16 / 0.99	27.36 / 1.90	33.90 / 4.40	44.72 / 5.51	53.39 / 6.43	60.83 / 7.24		
! Diversion MH 20013	Basin:	FG	Name:	SE 1st Ave Diversion												
FG20013_Divn= 0.00 / 0.00		0.89 / 0.47		3.26 / 1.62	5.94 / 2.89	6.45 / 3.13	7.48 / 3.75	8.37 / 4.29	10.61 / 5.60	11.56 / 6.15	12.45 / 6.66	14.04 / 7.57	14.78 / 7.99	0.00 / 0.00		
! Diversion MH 20414	Basin:	FG	Name:	23rd Ave Diversion												
FG20414_Divn= 0.00 / 0.00		0.00 / 0.00		1.33 / 0.35	4.82 / 1.05	8.60 / 1.18	11.67 / 1.33	13.75 / 1.58	14.67 / 1.70	16.37 / 1.90	17.91 / 2.09	20.64 / 2.42	21.88 / 2.57	23.05 / 2.71		
! Diversion MH 27860	Basin:	FG	Name:	SW Linden Diversion												
FG27860_Divn= 0.00 / 0.00		2.72 / 0.00		4.47 / 0.00	9.72 / 0.00	12.45 / 0.00	14.00 / 0.00	17.88 / 0.18	21.75 / 2.30	27.80 / 4.14	33.21 / 5.98	38.39 / 8.00	42.63 / 9.38	0.00 / 0.00		
! Diversion MH 19808	Basin:	HL	Name:	W Main St Diversion												
HL19808_Divn= 0.00 / 0.00		0.30 / 0.30		1.45 / 1.04	2.46 / 1.32	4.72 / 1.52	5.74 / 1.71	6.98 / 1.88	7.68 / 2.03	9.98 / 2.56	11.84 / 3.00	13.45 / 3.38	0.00 / 0.00	0.00 / 0.00		
! Diversion MH 19863	Basin:	HL	Name:	S 9th Ave Diversion (to RC)												
HL19863_Divn= 0.00 / 0.00		0.44 / 0.40		1.49 / 1.17	2.79 / 1.62	4.16 / 2.24	5.17 / 2.72	6.01 / 3.13	8.02 / 4.12	9.62 / 4.91	10.33 / 5.27	10.99 / 5.60	11.62 / 5.91	0.00 / 0.00		
! Diversion MH 20299	Basin:	HL	Name:	9th Ave Diversion (to RC)												
HL20299_Divn= 0.00 / 0.00		0.68 / 0.40		2.54 / 1.36	3.23 / 1.72	3.70 / 2.00	4.12 / 2.24	4.50 / 2.45	5.48 / 3.01	5.90 / 3.26	6.30 / 3.48	7.04 / 3.90	7.37 / 4.09	0.00 / 0.00		
! Diversion MH 20312	Basin:	HL	Name:	N 9th Ave Diversion (to RC)												
HL20312_Divn= 0.00 / 0.00		0.93 / 0.76		3.57 / 2.60	5.01 / 3.29	5.39 / 3.54	5.83 / 3.78	6.24 / 4.01	6.81 / 4.32	7.33 / 4.62	8.27 / 5.16	9.11 / 5.64	9.89 / 6.09	0.00 / 0.00		
! Diversion MH 7925	Basin:	RC	Name:	SW Madeline St Diversion												
RC07925_Divn= 0.00 / 0.00		0.38 / 0.34		2.13 / 1.18	3.52 / 1.49	7.20 / 1.82	8.87 / 2.10	9.79 / 2.34	12.25 / 2.95	14.28 / 3.46	15.20 / 3.68	16.07 / 3.90	0.00 / 0.00	0.00 / 0.00		
! Diversion MH 12682	Basin:	RC	Name:	Aloha PS #3 Diversion												
RC12682_Divn= 0.00 / 0.00		0.59 / 0.30		1.18 / 0.59	2.66 / 1.33	4.73 / 2.37	5.92 / 2.96	9.47 / 4.73	14.79 / 7.40	22.19 / 11.09	28.40 / 14.20	48.31 / 24.15	72.46 / 36.23	90.37 / 45.19		
! Diversion MH 16250	Basin:	RC	Name:	198th Ave Diversion												
RC16250_Divn= 0.00 / 0.00		1.07 / 0.32		5.17 / 2.27	11.19 / 5.40	17.45 / 8.86	21.04 / 11.23	21.69 / 11.43	23.58 / 12.21	25.32 / 12.95	26.95 / 13.65	28.48 / 14.32	31.32 / 15.56	35.15 / 17.26		
! Diversion MH 16566	Basin:	RC	Name:	Murray Blvd Diverson												
RC16566_Divn= 0.00 / 0.00		0.20 / 0.00		0.72 / 0.00	1.45 / 0.13	1.94 / 0.49	2.52 / 0.97	3.06 / 1.42	3.51 / 1.69	3.81 / 1.84	4.09 / 1.97	4.84 / 2.33	5.49 / 2.64	6.07 / 2.91		
! Diversion MH 16578	Basin:	RC	Name:	Stoddard Dr Diversion												
RC16578_Divn= 0.00 / 0.00		1.53 / 0.78		5.75 / 2.94	11.88 / 6.08	17.63 / 9.03	20.50 / 10.50	20.52 / 10.50	22.19 / 11.35	23.75 / 12.15	25.21 / 12.89	26.59 / 13.59	29.16 / 14.90	32.63 / 16.68		
! Diversion MH 17992	Basin:	RC	Name:	185th Ave Diversion												
RC17992_Divn= 0.00 / 0.00		1.12 / 0.00		2.46 / 0.00	4.47 / 0.00	6.48 / 0.00	8.93 / 0.00	14.94 / 0.20	18.25 / 0.61	21.23 / 1.13	26.38 / 2.48	29.10 / 3.08	33.82 / 3.57	37.95 / 4.01		
! Diversion MH 18260	Basin:	RC	Name:	Fairmont Dr Diversion												
RC18260_Divn= 0.00 / 0.00		0.17 / 0.07		0.63 / 0.26	1.21 / 0.47	1.70 / 0.60	1.84 / 0.67	2.10 / 0.79	2.33 / 0.90	2.53 / 0.99	2.82 / 1.12	3.07 / 1.23	3.93 / 1.61	4.30 / 1.77		
! Diversion MH 18263	Basin:	RC	Name:	Erickson St Diversion												
RC18263_Divn= 0.00 / 0.00		0.24 / 0.00		0.85 / 0.00	1.54 / 0.00	1.76 / 0.06	2.20 / 0.25	2.68 / 0.52	3.38 / 0.82	4.20 / 1.31	4.66 / 1.46	5.27 / 1.67	5.82 / 1.85	7.62 / 2.45		
! Diversion MH 18344	Basin:	RC	Name:	Pearl St Diversion												
RC18344_Divn= 0.00 / 0.00		0.52 / 0.25		1.80 / 0.91	3.60 / 1.67	4.91 / 1.81	5.71 / 1.84	5.96 / 1.89	6.04 / 1.91	6.20 / 1.94	6.43 / 1.98	6.65 / 2.03	7.47 / 2.20	0.00 / 0.00		

! Diversion MH 20083 Basin: RC Name: Rock Creek PS Diversion

RC20083_Divn=	0.00 / 0.00	10.00 / 3.38	20.00 / 6.76	30.00 / 10.14	40.00 / 13.51	60.00 / 20.27	80.00 / 27.03	100.00 / 33.78	120.00 / 40.54	140.00 / 47.30	160.00 / 54.05	180.00 / 60.81	200.00 / 67.57

! Diversion MH 22342 Basin: RC Name: Golf Course Diversion

RC22342_Divn=	0.00 / 0.00	0.70 / 0.00	2.79 / 0.00	5.92 / 0.00	10.18 / 0.60	12.93 / 1.26	17.32 / 2.69	21.24 / 4.18	23.01 / 5.60	36.09 / 8.22	44.02 / 8.66	52.60 / 9.22	66.32 / 10.24

! Diversion MH 23959 Basin: RC Name: Willow Cr Trunk

RC23959_Divn=	0.00 / 0.00	0.64 / 0.64	2.54 / 2.54	5.97 / 5.41	9.88 / 8.74	15.40 / 12.56	20.69 / 15.58	23.89 / 16.85	29.37 / 18.71	33.06 / 21.15	91.80 / 25.33	109.93 / 28.92	0.00 / 0.00

! Diversion MH 23964 Basin: RC Name: Willow Cr Trunk

RC23964_Divn=	0.00 / 0.00	0.62 / 0.48	2.97 / 2.38	12.18 / 9.52	24.95 / 19.03	37.27 / 28.55	40.39 / 30.92	55.84 / 42.82	62.52 / 47.58	94.70 / 58.47	116.69 / 67.63	134.85 / 75.68	165.08 / 89.65

! Diversion MH 23967 Basin: RC Name: Willow Cr Trunk

RC23967_Divn=	0.00 / 0.00	1.53 / 0.64	6.12 / 2.58	12.24 / 5.16	18.36 / 7.74	24.18 / 10.19	30.60 / 12.90	54.36 / 34.72	68.77 / 47.38	80.32 / 57.31	99.18 / 73.23	114.85 / 86.27	128.57 / 97.57

! Diversion MH 23973 Basin: RC Name: Willow Cr Trunk

RC23973_Divn=	0.00 / 0.00	1.90 / 0.74	7.61 / 2.94	15.23 / 5.88	24.75 / 9.56	34.26 / 13.23	40.36 / 15.59	59.29 / 25.14	67.41 / 28.98	81.23 / 35.43	93.01 / 40.88	112.95 / 50.03	0.00 / 0.00

! Diversion MH 23977 Basin: RC Name: Willow Cr Trunk

RC23977_Divn=	0.00 / 0.00	1.57 / 0.15	6.26 / 0.58	12.53 / 1.17	18.79 / 1.75	24.74 / 2.30	29.76 / 2.77	31.32 / 2.91	52.51 / 14.85	65.86 / 20.80	76.79 / 25.39	94.86 / 32.70	109.96 / 38.64

! Diversion MH 23983 Basin: RC Name: Willow Cr Trunk

RC23983_Divn=	0.00 / 0.00	2.44 / 0.51	9.69 / 1.95	19.71 / 4.24	31.84 / 6.70	38.28 / 7.71	45.57 / 8.62	50.26 / 11.57	67.68 / 13.99	81.39 / 16.06	93.07 / 17.88	112.85 / 21.06	129.64 / 23.82

! Diversion MH 25677 Basin: RC Name: Butternut Cr Trunk

RC25677_Divn=	0.00 / 0.00	0.91 / 0.00	3.64 / 0.00	7.10 / 0.00	9.10 / 0.00	12.75 / 0.00	15.57 / 0.00	17.95 / 0.00	23.69 / 0.00	29.67 / 0.00	36.89 / 2.27	44.14 / 7.29	46.60 / 7.64

! Diversion MH 28053 Basin: RC Name: 185th Ave Trunk

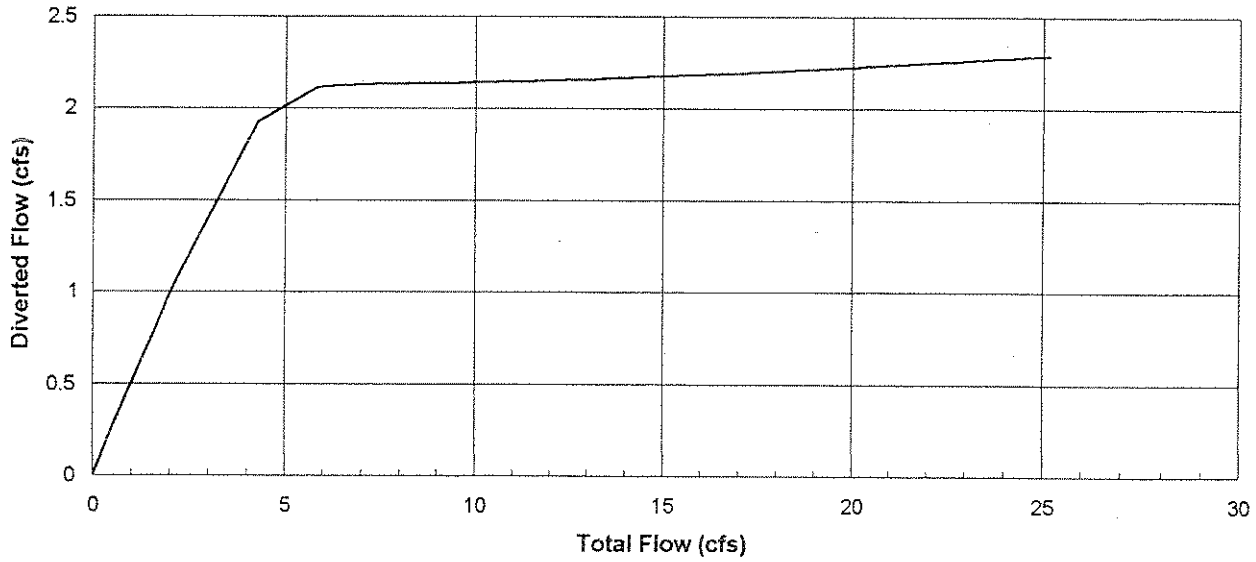
RC28053_Divn=	0.00 / 0.00	2.63 / 0.00	5.15 / 0.01	7.56 / 0.98	11.74 / 2.56	12.99 / 2.76	16.16 / 3.27	19.60 / 3.86	21.11 / 4.12	22.52 / 4.36	23.84 / 4.60	25.10 / 4.82	0.00 / 0.00

FLOW SPLIT AT MANHOLE 13862 (DR)

Fairfield Diversion

MH 9961 Diverted			MH 9917 Main				
Dia =	8	inches	Dia =	12	inches		
Area =	0.3491	sq ft	Area =	0.7854	sq ft		
Head =	30.41	feet	Head =	0.22	feet		
Length =	860	feet	Length =	11	feet		
Qfull =	2.12	cfs	Qfull =	4.69	cfs	Manning =	0.014
do =	0.0	inches	do =	0.0	inches		

Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.25	0.14	0.30	0.17	0.06	0.28	0.58	0.30
4	0.50	0.50	1.06	0.33	0.23	1.08	2.14	1.06
6	0.75	0.91	1.93	0.50	0.50	2.35	4.27	1.93
8	1.00	1.00	2.12	0.67	0.79	3.71	5.82	2.12
12	1.50	1.01	2.13	1.00	1.00	4.69	6.82	2.13
16	2.00	1.01	2.14	1.33	1.59	7.44	9.58	2.14
20	2.50	1.02	2.15	1.67	2.01	9.42	11.57	2.15
24	3.00	1.02	2.16	2.00	2.35	11.05	13.21	2.16
36	4.50	1.04	2.20	3.00	3.18	14.90	17.10	2.20
48	6.00	1.05	2.23	4.00	3.83	17.95	20.18	2.23
60	7.50	1.07	2.26	5.00	4.38	20.55	22.81	2.26
72	9.00	1.08	2.29	6.00	4.87	22.85	25.15	2.29

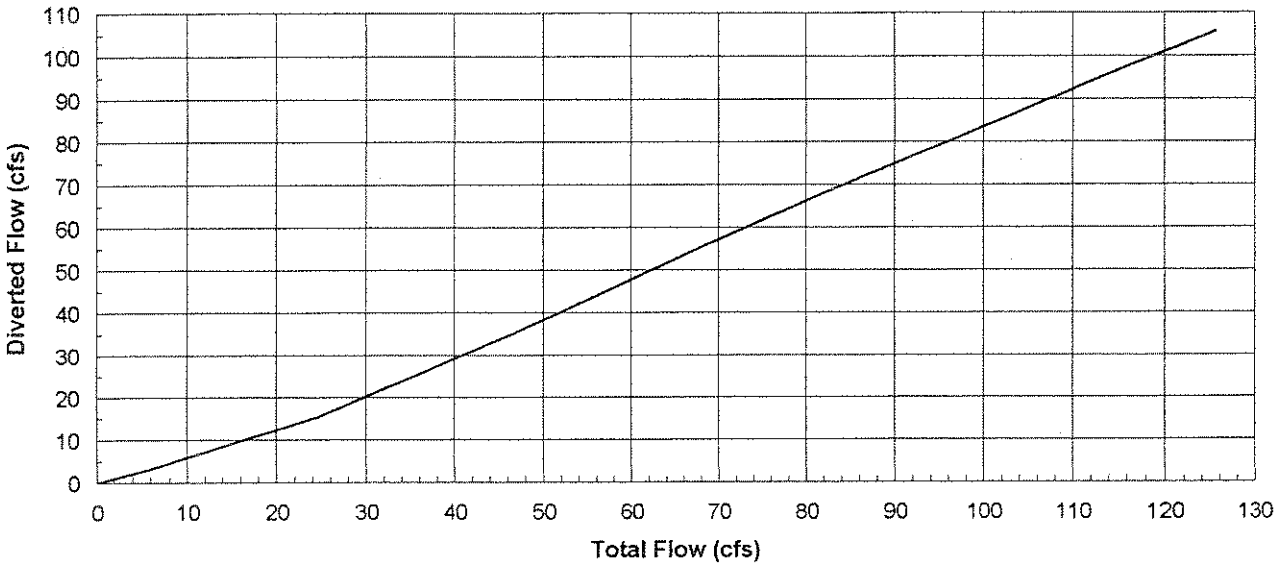


FLOW SPLIT AT MANHOLE 18554 (DR)

SW Lombard Diversion #2

MH 18552 Diverted			MH 18828 Main				
Dia =	21	inches	Dia =	12	inches		
Area =	2.4053	sq ft	Area =	0.7854	sq ft		
Head =	1.88	feet	Head =	2.09	feet		
Length =	10	feet	Length =	17	feet		
Qfull =	63.97	cfs	Qfull =	11.63	cfs	Manning =	0.014
do =	0.8	inches	do =	0.0	inches		

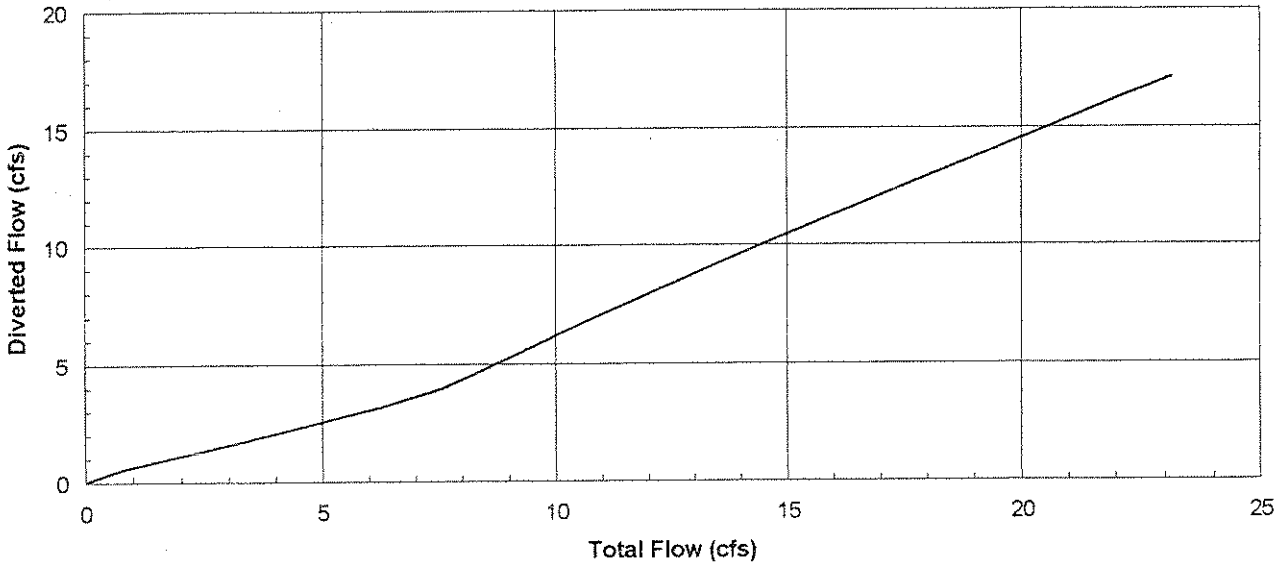
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.15	0.05	3.20	0.33	0.23	2.68	5.87	3.20
6	0.25	0.14	8.96	0.50	0.50	5.82	14.77	8.96
8	0.34	0.24	15.35	0.67	0.79	9.19	24.54	15.35
12	0.53	0.55	35.18	1.00	1.00	11.63	46.81	35.18
16	0.72	0.86	55.01	1.33	1.08	12.52	67.54	55.01
21	0.96	1.00	63.97	1.75	1.17	13.56	77.53	63.97
24	1.10	1.06	68.09	2.00	1.22	14.14	82.23	68.09
30	1.39	1.18	75.66	2.50	1.31	15.24	90.90	75.66
36	1.67	1.29	82.54	3.00	1.40	16.27	98.81	82.54
48	2.25	1.48	94.81	4.00	1.56	18.15	112.96	94.81
60	2.82	1.65	105.67	5.00	1.71	19.85	125.52	105.67



FLOW SPLIT AT MANHOLE 18571 (DR)

5th Street Diversion

	MH 18570 Diverted			MH 20580 Main				
	Dia =	18	inches	Dia =	12	inches		
	Area =	1.7671	sq ft	Area =	0.7854	sq ft		
	Head =	0.23	feet	Head =	1.75	feet		
	Length =	155	feet	Length =	203	feet		
	Qfull =	3.77	cfs	Qfull =	3.08	cfs	Manning =	0.014
	do =	3.5	inches	do =	6.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6	0.14	0.04	0.15	0.00	0.00	0.00	0.15	0.15
8	0.25	0.14	0.53	0.17	0.06	0.18	0.71	0.53
12	0.47	0.45	1.70	0.50	0.50	1.54	3.24	1.70
16	0.70	0.84	3.16	0.83	1.01	3.11	6.28	3.16
20	0.92	1.06	3.99	1.17	1.18	3.62	7.61	3.99
24	1.14	1.78	6.71	1.50	1.25	3.86	10.57	6.71
30	1.47	2.31	8.71	2.00	1.36	4.20	12.91	8.71
36	1.81	2.74	10.33	2.50	1.46	4.51	14.84	10.33
48	2.47	3.45	12.98	3.50	1.65	5.07	18.05	12.98
60	3.14	4.03	15.17	4.50	1.81	5.58	20.75	15.17
72	3.81	4.53	17.09	5.50	1.96	6.05	23.13	17.09



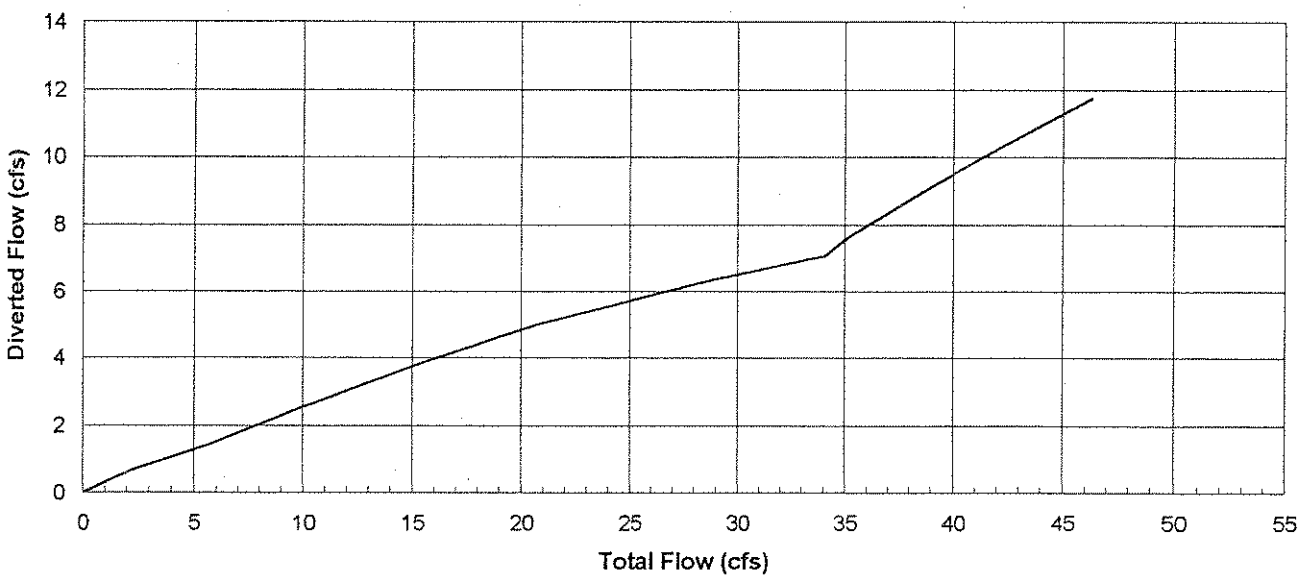
DR18571.wk4

Date 07/14/01

FLOW SPLIT AT MANHOLE 18828 (DR)

SW Lombard Diversion #1 - NOT USED IN MODEL - DATA NOT CHECKED

	MH 20942 Diverted			MH 18552 Main (to 18551)				
	Dia =	18	inches	Dia =	21	inches		
	Area =	1.7671	sq ft	Area =	2.4053	sq ft		
	Head =	1.03	feet	Head =	3.34	feet		
	Length =	244	feet	Length =	102	feet	Estimated	
	Qfull =	6.35	cfs	Qfull =	26.70	cfs	Manning =	0.014
	do =	0.00	inches	do =	0.39	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.11	0.02	0.13	0.08	0.01	0.27	0.39	0.13
4	0.22	0.11	0.70	0.17	0.06	1.60	2.30	0.70
6	0.33	0.23	1.46	0.27	0.16	4.27	5.73	1.46
8	0.44	0.40	2.54	0.36	0.28	7.47	10.02	2.54
10	0.56	0.60	3.81	0.46	0.43	11.48	15.29	3.81
12	0.67	0.79	5.02	0.55	0.59	15.75	20.77	5.02
15	0.83	1.00	6.35	0.70	0.84	22.42	28.78	6.35
21	1.17	1.11	7.08	0.98	1.01	26.96	34.05	7.08
24	1.33	1.22	7.74	1.12	1.04	27.68	35.42	7.74
36	2.00	1.57	9.96	1.70	1.17	31.30	41.25	9.96
48	2.67	1.85	11.76	2.27	1.29	34.54	46.30	11.76



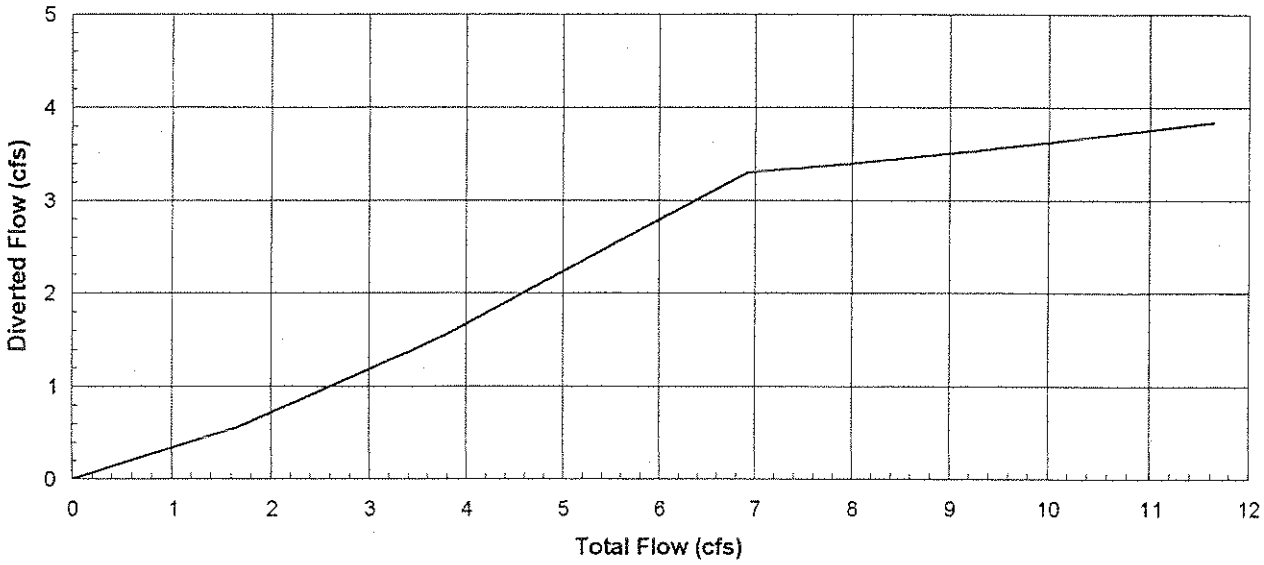
DR18828.wk4

Date 07/14/01

FLOW SPLIT AT MANHOLE 20606 (DR)

SW 5th Street Diversion

	MH 20604 Diverted			MH 13244 Main				
	Dia =	10	inches	Dia =	10	inches		
	Area =	0.5454	sq.ft	Area =	0.5454	sq.ft		
	Head =	11.27	feet	Head =	0.93	feet		
	Length =	435	feet	Length =	35	feet		
	Qfull =	3.28	cfs	Qfull =	3.33	cfs	Manning =	0.014
	do =	1.2	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.28	0.17	0.56	0.40	0.33	1.10	1.66	0.56
6	0.48	0.47	1.54	0.60	0.67	2.23	3.77	1.54
12	1.08	1.01	3.31	1.20	1.09	3.61	6.92	3.31
16	1.48	1.02	3.36	1.60	1.24	4.12	7.48	3.36
20	1.88	1.04	3.40	2.00	1.38	4.58	7.98	3.40
24	2.28	1.05	3.45	2.40	1.50	4.99	8.44	3.45
28	2.68	1.06	3.50	2.80	1.62	5.38	8.87	3.50
32	3.08	1.08	3.54	3.20	1.72	5.73	9.27	3.54
36	3.48	1.09	3.59	3.60	1.82	6.07	9.65	3.59
40	3.88	1.11	3.63	4.00	1.92	6.39	10.02	3.63
48	4.68	1.13	3.72	4.80	2.10	6.98	10.70	3.72
60	5.88	1.17	3.84	6.00	2.34	7.78	11.63	3.84



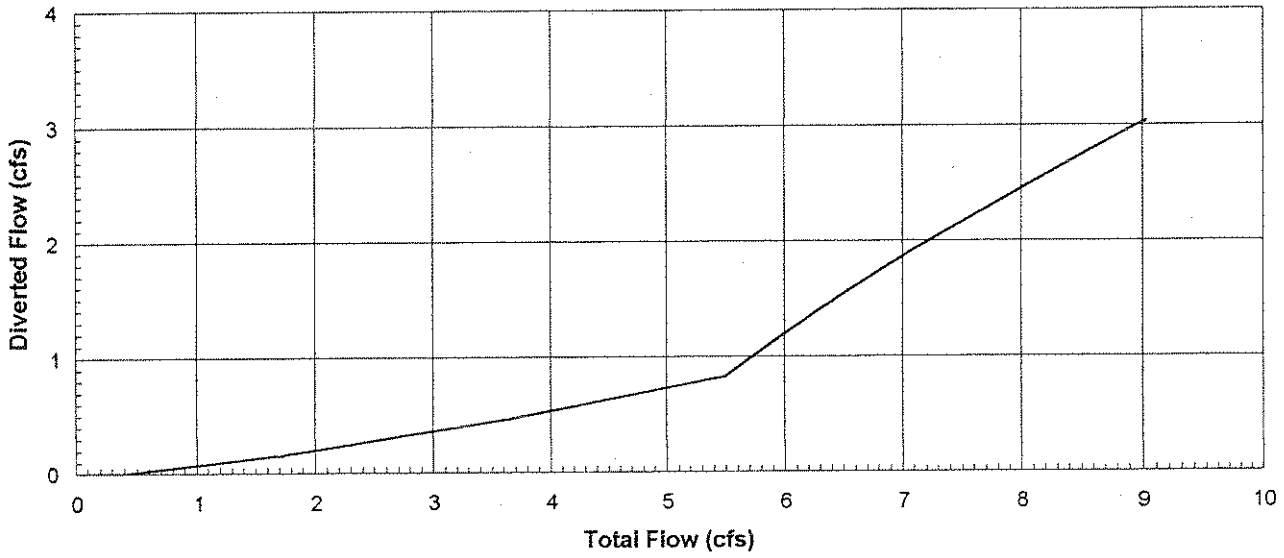
FLOW SPLIT AT MANHOLE 20760 (DR)

Sherwood Road Diversion

MH 20970 Diverted			MH 20761 Main		
Dia =	10	inches	Dia =	10	inches
Area =	0.5454	sq ft	Area =	0.5454	sq ft
Head =	0.74	feet	Head =	8.80	feet
Length =	267	feet	Length =	162	feet
Qfull =	1.07	cfs	Qfull =	4.75	cfs
do =	1.4	inches	do =	0.0	inches

Manning = 0.014

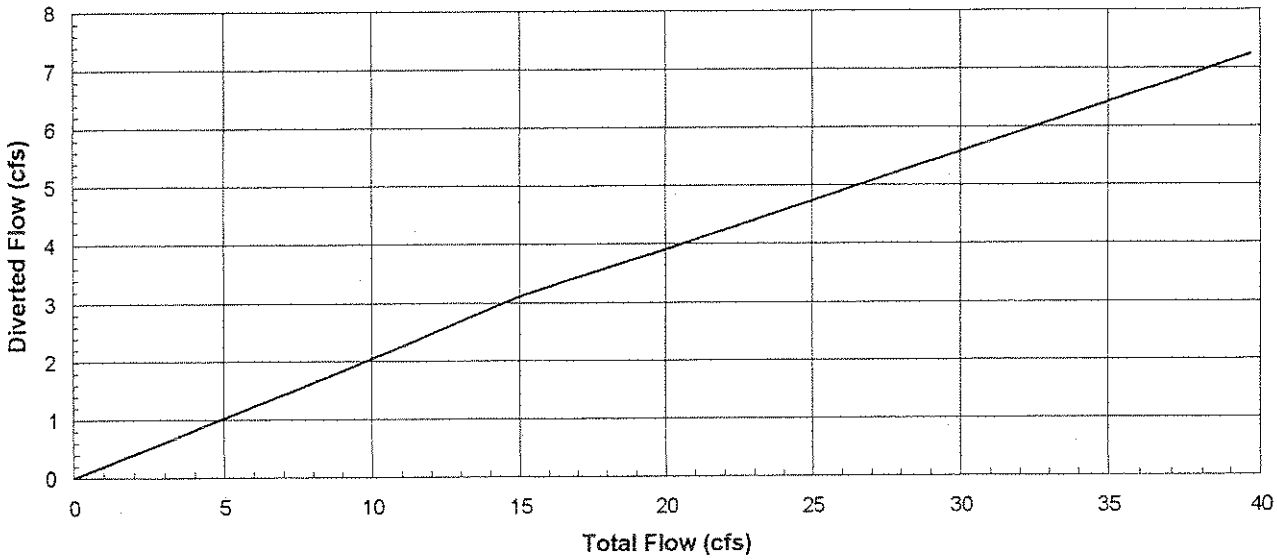
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.06	0.01	0.01	0.20	0.09	0.43	0.44	0.01
4	0.26	0.15	0.16	0.40	0.33	1.57	1.73	0.16
6	0.46	0.43	0.46	0.60	0.67	3.19	3.65	0.46
8	0.66	0.77	0.83	0.80	0.98	4.66	5.49	0.83
12	1.06	1.11	1.19	1.20	1.01	4.80	5.99	1.19
16	1.46	1.29	1.39	1.60	1.03	4.89	6.28	1.39
20	1.86	1.46	1.57	2.00	1.05	4.97	6.54	1.57
24	2.26	1.61	1.72	2.40	1.06	5.06	6.78	1.72
30	2.86	1.80	1.94	3.00	1.09	5.19	7.12	1.94
36	3.46	1.98	2.13	3.60	1.12	5.31	7.44	2.13
60	5.86	2.58	2.77	6.00	1.21	5.77	8.54	2.77
72	7.06	2.83	3.03	7.20	1.26	5.99	9.02	3.03



FLOW SPLIT AT MANHOLE 20834 Tektronix (DR)

Tektronix Diversion - high manhole flow split - NOT USED IN MODEL

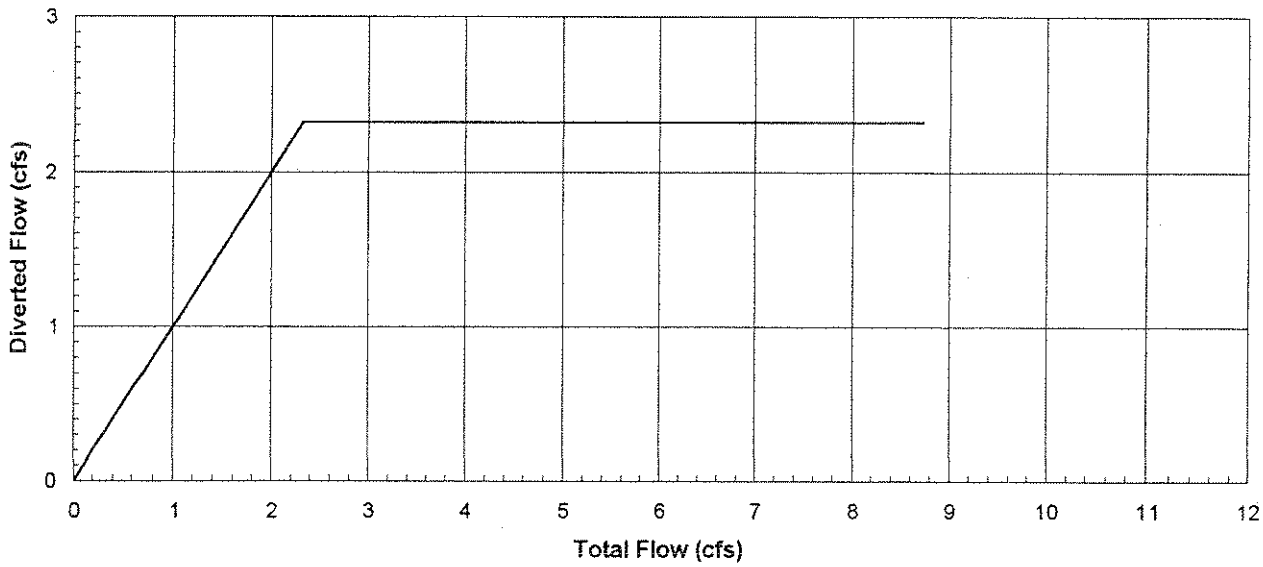
	MH 20956 Diverted			MH 20833 Main				
	Dia =	15	inches	Dia =	15	inches		
	Area =	1.2272	sq.ft	Area =	1.2272	sq.ft		
	Head =	0.89	feet	Head =	0.61	feet		
	Length =	320	feet	Length =	15	feet		
	Qfull =	3.17	cfs	Qfull =	12.13	cfs	Manning =	0.014
	do =	0.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.27	0.16	0.51	0.27	0.16	1.94	2.45	0.51
8	0.53	0.55	1.74	0.53	0.56	6.79	8.54	1.74
12	0.80	0.98	3.11	0.80	0.98	11.89	14.99	3.11
16	1.07	1.05	3.32	1.07	1.07	12.93	16.25	3.32
20	1.33	1.21	3.84	1.33	1.30	15.74	19.58	3.84
24	1.60	1.36	4.31	1.60	1.49	18.11	22.42	4.31
28	1.87	1.49	4.72	1.87	1.67	20.21	24.93	4.72
32	2.13	1.61	5.11	2.13	1.82	22.11	27.21	5.11
36	2.40	1.72	5.46	2.40	1.97	23.86	29.32	5.46
40	2.67	1.83	5.80	2.67	2.10	25.49	31.28	5.80
48	3.20	2.02	6.41	3.20	2.35	28.47	34.88	6.41
60	4.00	2.28	7.24	4.00	2.67	32.43	39.67	7.24



FLOW SPLIT AT MANHOLE 20911 (DR)

Tektronix PS Diversion - first 1.5 mgd diverted from system to PS

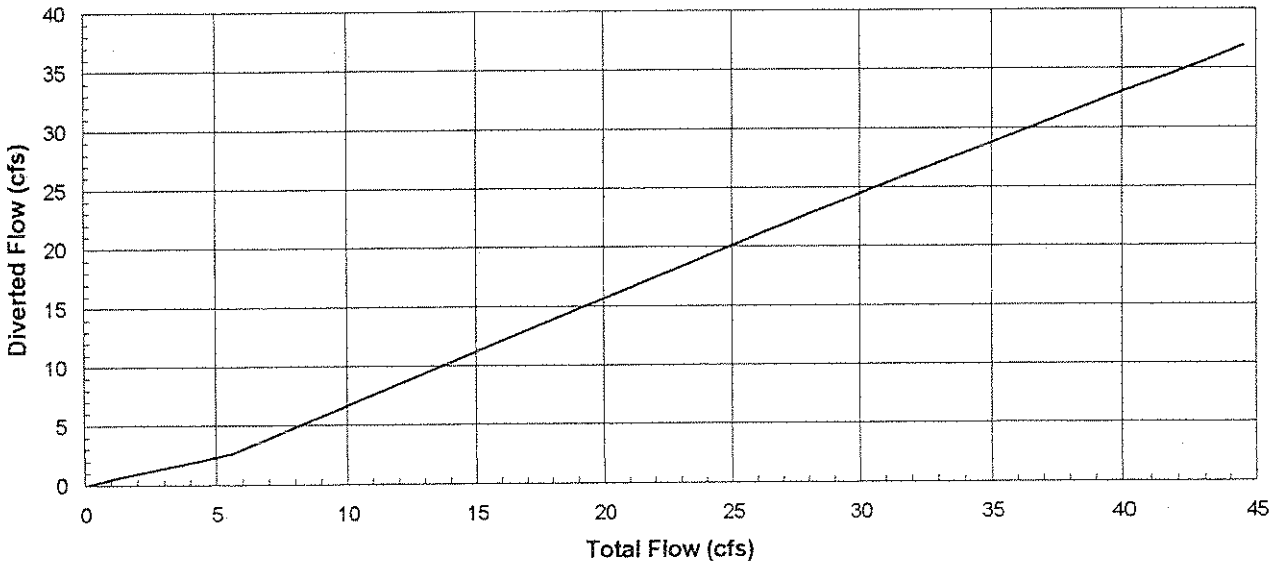
	MH 27685 Diverted (to PS)			MH 20910 Main				
	Dia =	15	inches	Dia =	10	inches		
	Area =	1.2272	sq.ft	Area =	0.5454	sq.ft		
	Head =	6.00	feet	Head =	0.30	feet		
	Length =	197	feet	Length =	25	feet		
	Qfull =	10.50	cfs	Qfull =	2.23	cfs	Manning =	0.014
	do =	0.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00		0.00	0.00	0.00	0.00	0.00	0.00
							1.00	1.00
							2.00	2.00
							2.32	2.32
2	0.13		2.32	0.20	0.09	0.20	2.52	2.32
4	0.27		2.32	0.40	0.33	0.74	3.06	2.32
8	0.53		2.32	0.80	0.98	2.19	4.51	2.32
12	0.80		2.32	1.20	1.25	2.79	5.11	2.32
16	1.07		2.32	1.60	1.63	3.65	5.97	2.32
20	1.33		2.32	2.00	1.94	4.34	6.66	2.32
24	1.60		2.32	2.40	2.21	4.94	7.26	2.32
30	2.00		2.32	3.00	2.56	5.72	8.04	2.32
36	2.40		2.32	3.60	2.87	6.41	8.73	2.32



FLOW SPLIT AT MANHOLE 12751 (FG)

Cornelius Diversion

MH 27547 (to 27546) Diverted			MH 12750 Main				
Dia =	15	inches	Dia =	15	inches		
Area =	1.2272	sq.ft	Area =	1.2272	sq.ft		
Head =	0.02	feet	Head =	0.80	feet		
Length =	10	feet	Length =	285	feet		
Qfull =	2.69	cfs	Qfull =	3.19	cfs	Manning =	0.014
do =	0.0	inches	do =	0.4	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.13	0.04	0.11	0.11	0.02	0.06	0.17	0.11
4	0.27	0.16	0.43	0.24	0.12	0.38	0.81	0.43
6	0.40	0.34	0.91	0.37	0.29	0.92	1.84	0.91
8	0.53	0.55	1.48	0.51	0.51	1.63	3.10	1.48
10	0.67	0.79	2.12	0.64	0.74	2.36	4.48	2.12
12	0.80	0.98	2.64	0.77	0.93	2.96	5.60	2.64
16	1.07	2.27	6.11	1.04	1.05	3.35	9.46	6.11
20	1.33	4.67	12.57	1.31	1.23	3.93	16.50	12.57
24	1.60	6.20	16.69	1.57	1.39	4.44	21.13	16.69
30	2.00	7.97	21.43	1.97	1.60	5.10	26.54	21.43
36	2.40	9.41	25.30	2.37	1.79	5.69	30.99	25.30
60	4.00	13.73	36.93	3.97	2.38	7.60	44.53	36.93



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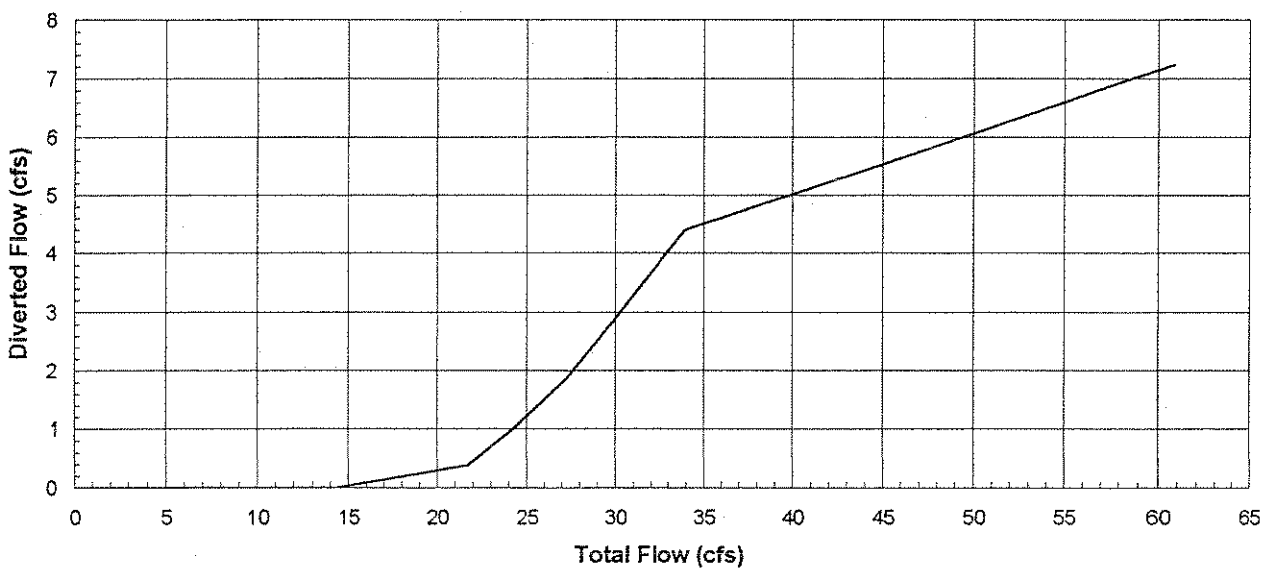
Date 07/14/01

FLOW SPLIT AT MANHOLE 18846 (FG)

Hawthorn Street Diversion

	MH 20393 Diverted			MH 18845 (to 12708) Main				
	Dia =	14	inches	Dia =	24	inches		
	Area =	1.0690	sq.ft	Area =	3.1416	sq.ft		
	Head =	0.68	feet	Head =	0.61	feet		
	Length =	455	feet	Length =	133	feet		
	Qfull =	1.93	cfs	Qfull =	14.26	cfs	Manning =	0.014
	do =	28.8	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.00	0.00	0.00	0.17	0.06	0.86	0.86	0.00
8	0.00	0.00	0.00	0.33	0.23	3.28	3.28	0.00
12	0.00	0.00	0.00	0.50	0.50	7.13	7.13	0.00
16	0.00	0.00	0.00	0.67	0.79	11.27	11.27	0.00
24	0.00	0.00	0.00	1.00	1.00	14.26	14.26	0.00
33	0.30	0.20	0.39	1.38	1.49	21.30	21.69	0.39
36	0.51	0.51	0.99	1.50	1.62	23.17	24.16	0.99
40	0.80	0.98	1.90	1.67	1.78	25.46	27.36	1.90
48	1.37	2.27	4.40	2.00	2.07	29.51	33.90	4.40
72	3.09	2.85	5.51	3.00	2.75	39.21	44.72	5.51
96	4.80	3.32	6.43	4.00	3.29	46.96	53.39	6.43
120	6.51	3.74	7.24	5.00	3.76	53.59	60.83	7.24

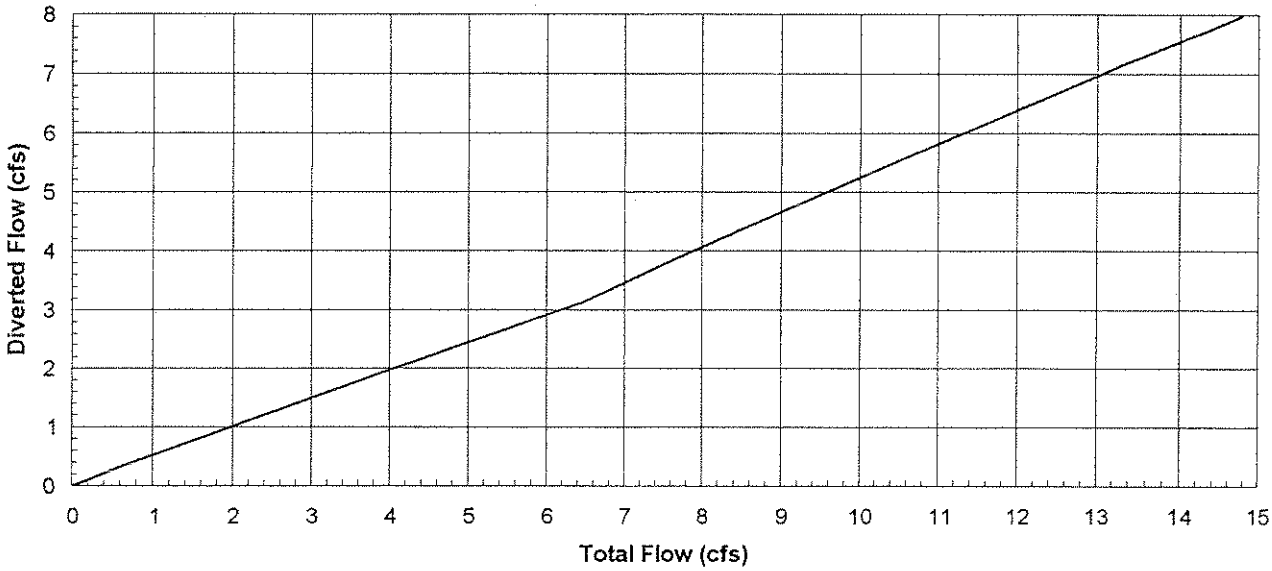


FLOW SPLIT AT MANHOLE 20013 (FG)

SE 1st Avenue Diversion

	MH 20014 Diverted			MH 21067 Main				
Dia =	15	inches	Dia =	15	inches			
Area =	1.2272	sq ft	Area =	1.2272	sq ft			
Head =	0.67	feet	Head =	1.23	feet			
Length =	279	feet	Length =	430	feet			
Qfull =	2.95	cfs	Qfull =	3.22	cfs	Manning =	0.014	
do =	0.0	inches	do =	0.4	inches			

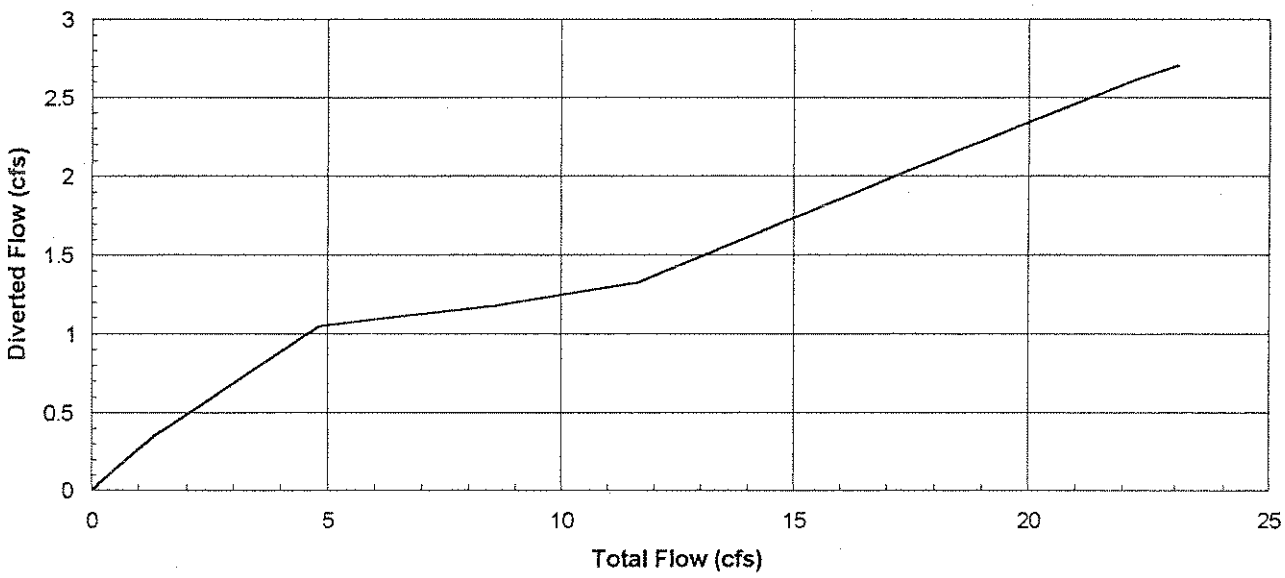
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.27	0.16	0.47	0.24	0.13	0.42	0.89	0.47
8	0.53	0.55	1.62	0.51	0.51	1.64	3.26	1.62
12	0.80	0.98	2.89	0.78	0.95	3.06	5.94	2.89
16	1.07	1.06	3.13	1.04	1.03	3.32	6.45	3.13
20	1.33	1.27	3.75	1.31	1.16	3.72	7.48	3.75
24	1.60	1.46	4.29	1.58	1.27	4.08	8.37	4.29
36	2.40	1.90	5.60	2.38	1.56	5.01	10.61	5.60
42	2.80	2.09	6.15	2.78	1.68	5.41	11.56	6.15
48	3.20	2.26	6.66	3.18	1.80	5.79	12.45	6.66
60	4.00	2.57	7.57	3.98	2.01	6.47	14.04	7.57
66	4.40	2.71	7.99	4.38	2.11	6.79	14.78	7.99



FLOW SPLIT AT MANHOLE 20414 (FG)

23rd Avenue Diversion

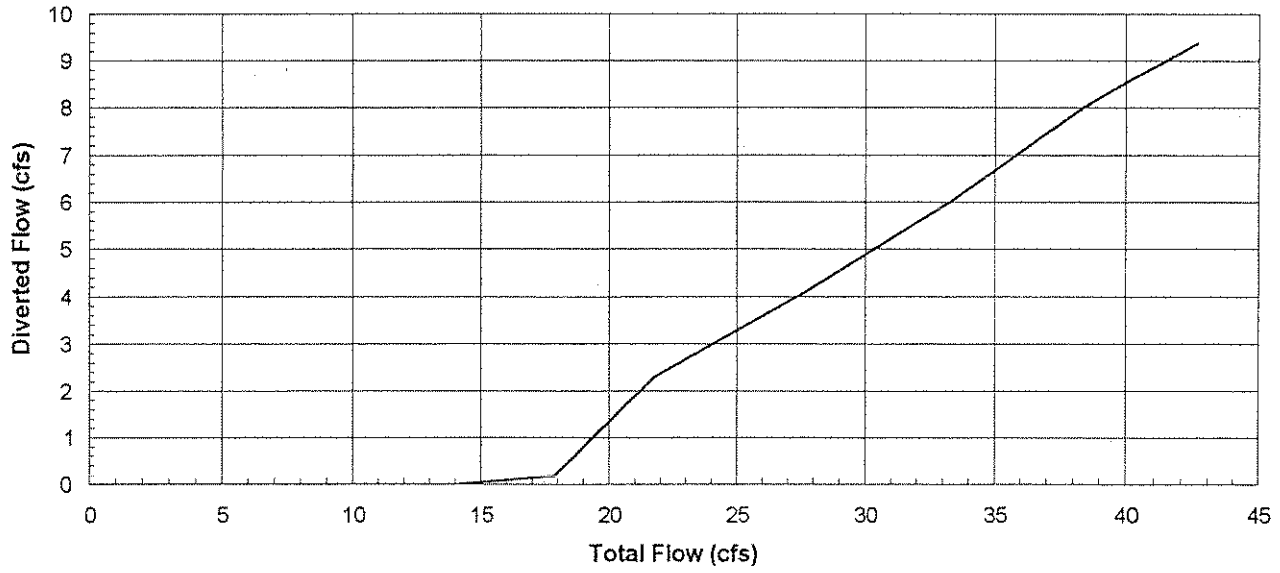
	MH 20413 Diverted			MH 20420 Main				
	Dia =	10	inches	Dia =	21	inches		
	Area =	0.5454	sq ft	Area =	2.4053	sq ft		
	Head =	0.77	feet	Head =	1.81	feet		
	Length =	280	feet	Length =	266	feet		
	Qfull =	1.07	cfs	Qfull =	12.16	cfs	Manning =	0.014
	do =	0.0	inches	do =	0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.40	0.33	0.35	0.19	0.08	0.97	1.33	0.35
8	0.80	0.98	1.05	0.38	0.31	3.77	4.82	1.05
12	1.20	1.10	1.18	0.57	0.61	7.42	8.60	1.18
15	1.50	1.24	1.33	0.71	0.85	10.34	11.67	1.33
21	2.10	1.48	1.58	1.00	1.00	12.16	13.75	1.58
24	2.40	1.59	1.70	1.14	1.07	12.98	14.67	1.70
30	3.00	1.78	1.90	1.43	1.19	14.47	16.37	1.90
36	3.60	1.95	2.09	1.71	1.30	15.82	17.91	2.09
48	4.80	2.26	2.42	2.29	1.50	18.22	20.64	2.42
54	5.40	2.40	2.57	2.57	1.59	19.31	21.88	2.57
60	6.00	2.53	2.71	2.86	1.67	20.34	23.05	2.71



FLOW SPLIT AT MANHOLE 27860 (FG)

SW Linden Diversion

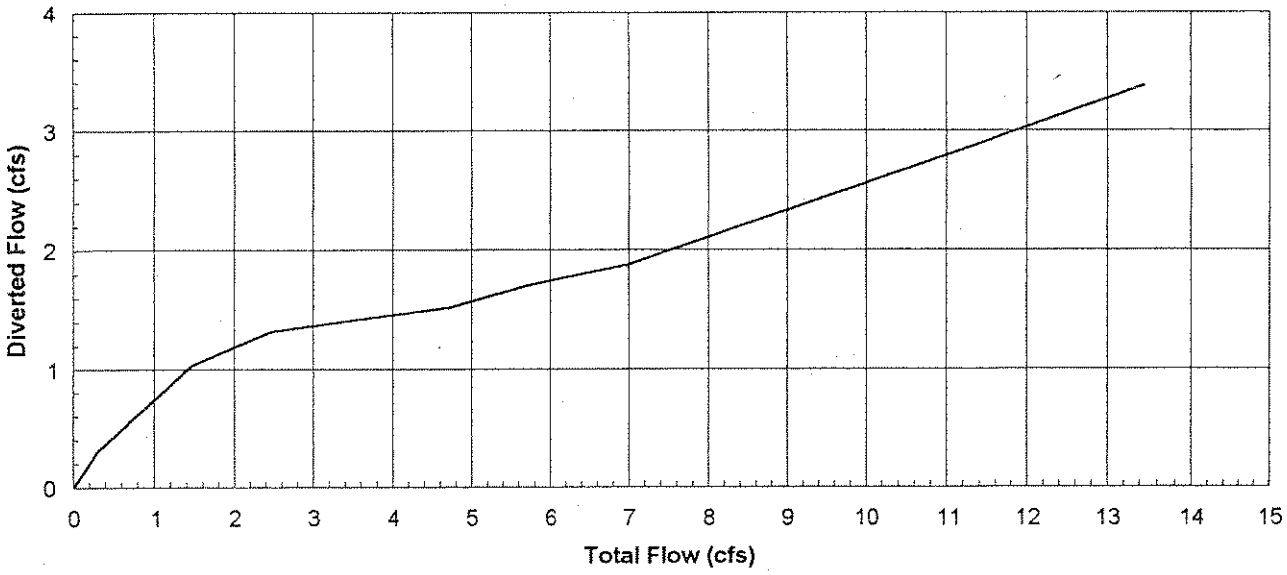
	MH 27534 Diverted			MH 27859 Main				
	Dia =	24	inches	Dia =	24	inches		
	Area =	3.1416	sq.ft	Area =	3.1416	sq.ft		
	Head =	0.04	feet	Head =	0.52	feet		
	Length =	21	feet	Length =	61	feet		
	Qfull =	9.19	cfs	Qfull =	19.45	cfs	Manning =	0.014
	do =	15.8	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6	0.00	0.00	0.00	0.25	0.14	2.72	2.72	0.00
8	0.00	0.00	0.00	0.33	0.23	4.47	4.47	0.00
12	0.00	0.00	0.00	0.50	0.50	9.72	9.72	0.00
14	0.00	0.00	0.00	0.58	0.64	12.45	12.45	0.00
15	0.00	0.00	0.00	0.63	0.72	14.00	14.00	0.00
18	0.09	0.02	0.18	0.75	0.91	17.70	17.88	0.18
24	0.34	0.25	2.30	1.00	1.00	19.45	21.75	2.30
27	0.47	0.45	4.14	1.13	1.22	23.66	27.80	4.14
30	0.59	0.65	5.98	1.25	1.40	27.24	33.21	5.98
33	0.72	0.87	8.00	1.38	1.56	30.39	38.39	8.00
36	0.84	1.02	9.38	1.50	1.71	33.25	42.63	9.38



FLOW SPLIT AT MANHOLE 19808 (HL)

W Main Street Diversion

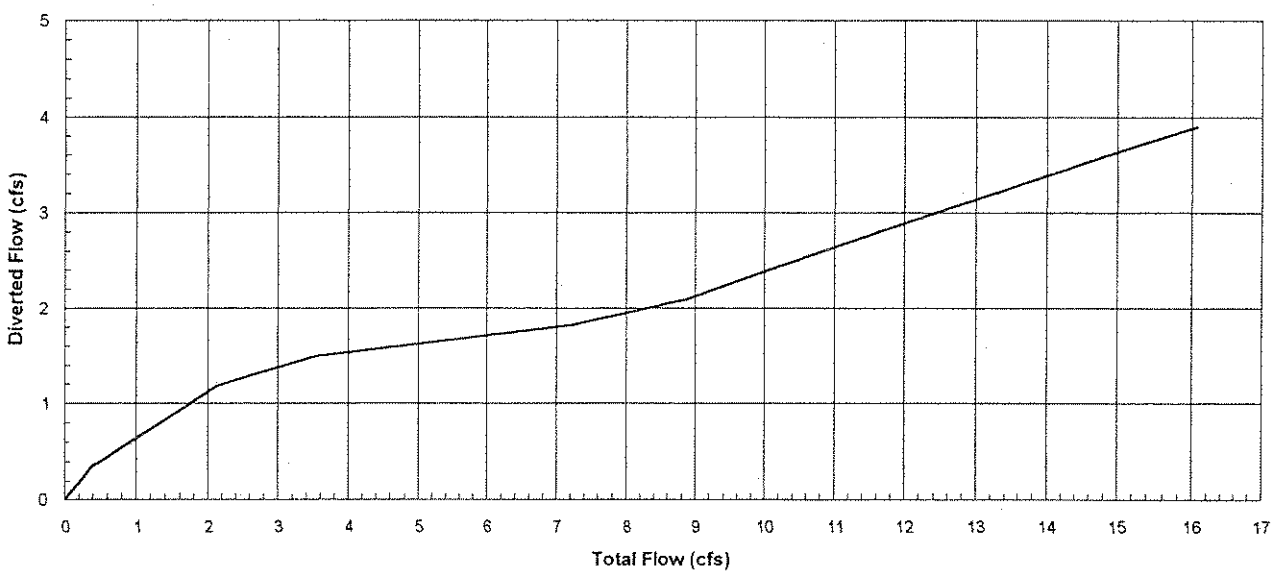
	MH 19807 Diverted			MH 19820 Main				
	Dia =	12	inches	Dia =	15	inches		
	Area =	0.7854	sq ft	Area =	1.2272	sq ft		
	Head =	0.71	feet	Head =	0.62	feet		
	Length =	455	feet	Length =	156	feet		
	Qfull =	1.31	cfs	Qfull =	3.80	cfs	Manning =	0.014
	do =	0.0	inches	do =	4.4	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.33	0.23	0.30	0.00	0.00	0.00	0.30	0.30
8	0.67	0.79	1.04	0.24	0.11	0.42	1.45	1.04
10	0.83	1.01	1.32	0.37	0.30	1.14	2.46	1.32
15	1.25	1.16	1.52	0.70	0.84	3.20	4.72	1.52
18	1.50	1.31	1.71	0.90	1.06	4.03	5.74	1.71
21	1.75	1.43	1.88	1.10	1.34	5.11	6.98	1.88
24	2.00	1.55	2.03	1.30	1.48	5.64	7.68	2.03
36	3.00	1.95	2.56	2.10	1.95	7.42	9.98	2.56
48	4.00	2.29	3.00	2.90	2.33	8.85	11.84	3.00
60	5.00	2.58	3.38	3.70	2.65	10.07	13.45	3.38



FLOW SPLIT AT MANHOLE 7925 (RC)

SW Madeline Street Diversion

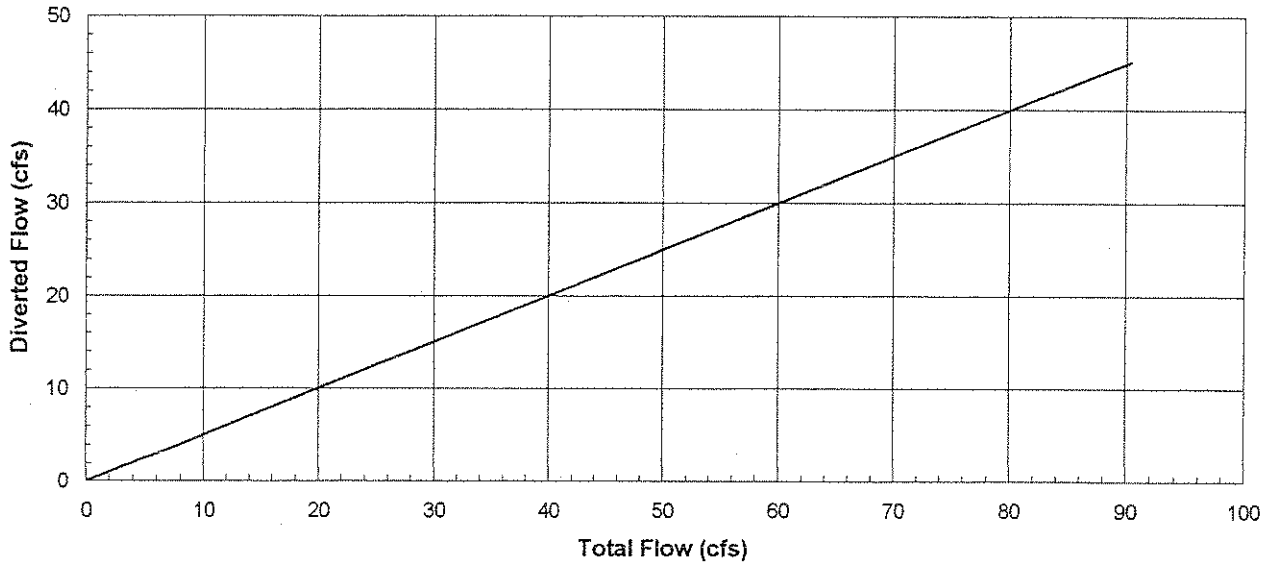
	MH 7922 Diverted			MH 7927 Main				
	Dia =	12	inches	Dia =	18	inches		
	Area =	0.7854	sq ft	Area =	1.7671	sq ft		
	Head =	0.69	feet	Head =	1.30	feet		
	Length =	340	feet	Length =	310	feet		
	Qfull =	1.49	cfs	Qfull =	6.33	cfs	Manning =	0.014
	do =	0.0	inches	do =	3.2	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.33	0.23	0.34	0.04	0.01	0.03	0.38	0.34
8	0.67	0.79	1.18	0.26	0.15	0.95	2.13	1.18
12	1.00	1.00	1.49	0.49	0.32	2.03	3.52	1.49
16	1.33	1.22	1.82	0.71	0.85	5.38	7.20	1.82
20	1.67	1.40	2.10	0.93	1.07	6.78	8.87	2.10
24	2.00	1.57	2.34	1.15	1.18	7.45	9.79	2.34
36	3.00	1.97	2.95	1.82	1.47	9.30	12.25	2.95
48	4.00	2.31	3.46	2.49	1.71	10.83	14.28	3.46
54	4.50	2.46	3.68	2.82	1.82	11.52	15.20	3.68
60	5.00	2.61	3.90	3.15	1.92	12.17	16.07	3.90



FLOW SPLIT AT MANHOLE 12682 (Aloha PS) (RC)

Aloha PS #3 Diversion - Pipes A and B are equivalent

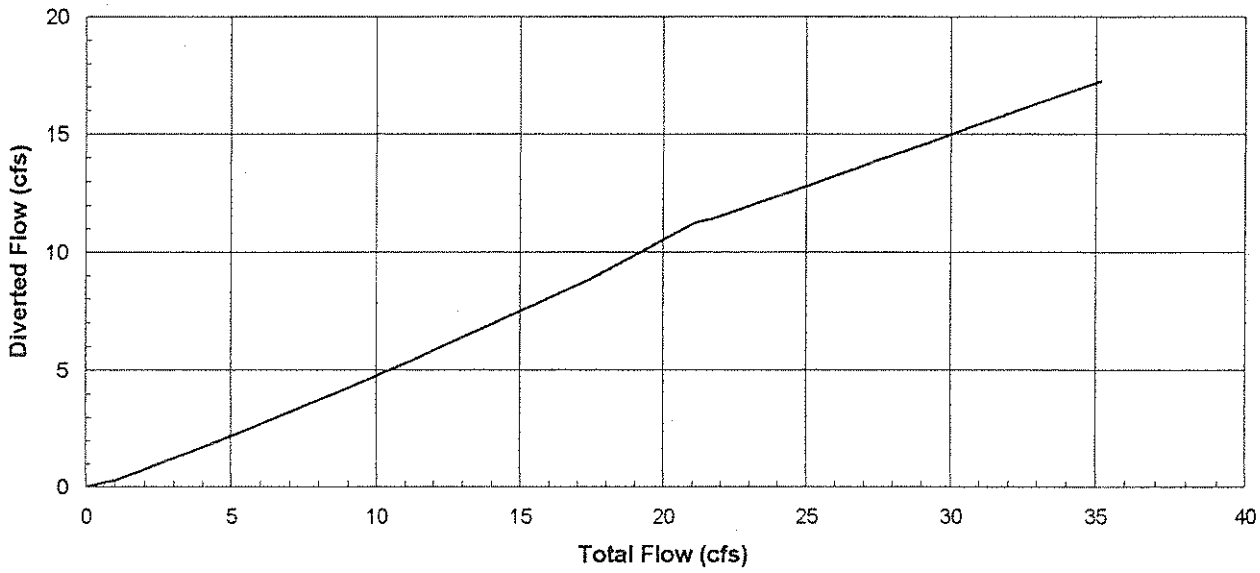
	Pipe A (to PS 21795 - FM #1)			Pipe B (to PS 12682 - FM #2)				
Assume	Dia =	30	inches	Dia =	30	inches		
	Area =	4.9087	sq ft	Area =	4.9087	sq ft		
Assume	Head =	0.30	feet	Head =	0.30	feet		
Assume	Length =	200	feet	Length =	200	feet		
	Qfull =	14.79	cfs	Qfull =	14.79	cfs	Manning =	0.014
Assume	do =	0.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.07	0.02	0.30	0.07	0.02	0.30	0.59	0.30
4	0.13	0.04	0.59	0.13	0.04	0.59	1.18	0.59
6	0.20	0.09	1.33	0.20	0.09	1.33	2.66	1.33
8	0.27	0.16	2.37	0.27	0.16	2.37	4.73	2.37
10	0.33	0.20	2.96	0.33	0.20	2.96	5.92	2.96
12	0.40	0.32	4.73	0.40	0.32	4.73	9.47	4.73
16	0.53	0.50	7.40	0.53	0.50	7.40	14.79	7.40
20	0.67	0.75	11.09	0.67	0.75	11.09	22.19	11.09
24	0.80	0.96	14.20	0.80	0.96	14.20	28.40	14.20
36	1.20	1.63	24.15	1.20	1.63	24.15	48.31	24.15
48	1.60	2.45	36.23	1.60	2.45	36.23	72.46	36.23
60	2.00	3.06	45.19	2.00	3.06	45.19	90.37	45.19



FLOW SPLIT AT MANHOLE 16250 (RC)

198th Avenue Diversion

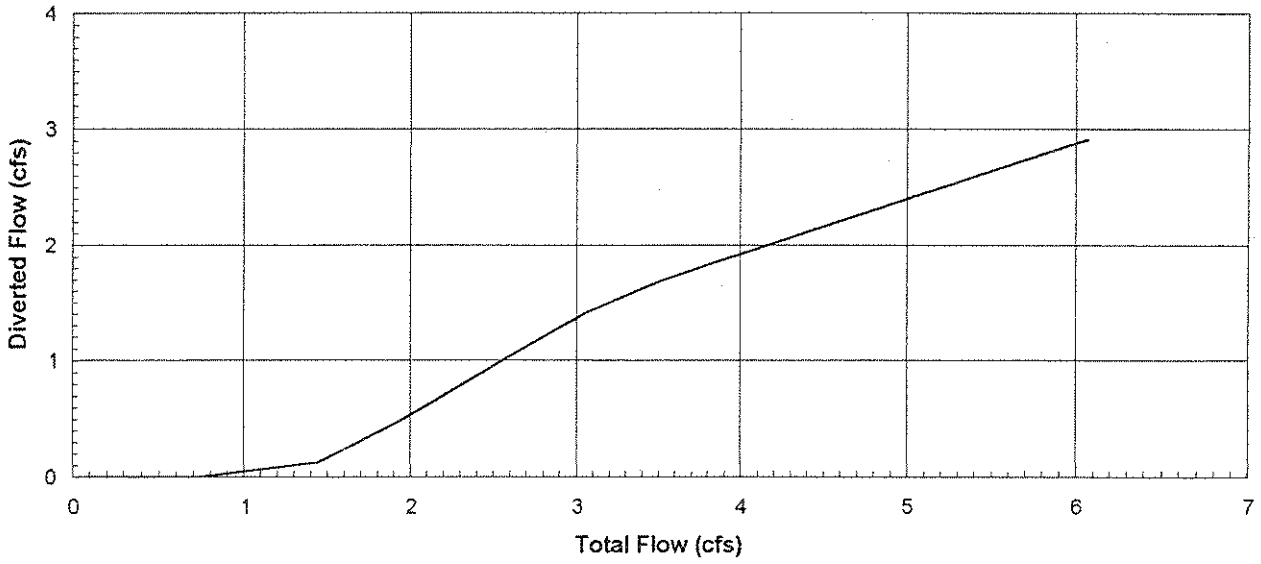
	MH 7706 Diverted			MH 16249 Main				
	Dia =	21	inches	Dia =	21	inches		
	Area =	2.4053	sq.ft	Area =	2.4053	sq.ft		
	Head =	2.09	feet	Head =	1.22	feet		
	Length =	390	feet	Length =	304	feet		
	Qfull =	10.80	cfs	Qfull =	9.35	cfs	Manning =	0.014
	do =	1.4	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.12	0.03	0.32	0.19	0.08	0.75	1.07	0.32
8	0.31	0.21	2.27	0.38	0.31	2.90	5.17	2.27
12	0.50	0.50	5.40	0.57	0.62	5.79	11.19	5.40
16	0.69	0.82	8.86	0.76	0.92	8.60	17.45	8.86
20	0.88	1.04	11.23	0.95	1.05	9.81	21.04	11.23
24	1.07	1.06	11.43	1.14	1.10	10.26	21.69	11.43
28	1.26	1.13	12.21	1.33	1.22	11.36	23.58	12.21
32	1.46	1.20	12.95	1.52	1.32	12.37	25.32	12.95
36	1.65	1.26	13.65	1.71	1.42	13.30	26.95	13.65
40	1.84	1.33	14.32	1.90	1.52	14.17	28.48	14.32
48	2.22	1.44	15.56	2.29	1.69	15.76	31.32	15.56
60	2.79	1.60	17.26	2.86	1.91	17.89	35.15	17.26



FLOW SPLIT AT MANHOLE 16566 (RC)

Murray Boulevard Diversion

	MH 1338 Diverted			MH 1347 Main				
	Dia =	10	inches	Dia =	8	inches		
	Area =	0.5454	sq.ft	Area =	0.3491	sq.ft		
	Head =	1.36	feet	Head =	1.16	feet		
	Length =	271	feet	Length =	70	feet		
	Qfull =	1.45	cfs	Qfull =	1.45	cfs	Manning =	0.014
	do =	4.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.25	0.14	0.20	0.20	0.00
4	0.00	0.00	0.00	0.50	0.50	0.72	0.72	0.00
6	0.20	0.09	0.13	0.75	0.91	1.32	1.45	0.13
8	0.40	0.34	0.49	1.00	1.00	1.45	1.94	0.49
10	0.60	0.67	0.97	1.25	1.07	1.55	2.52	0.97
12	0.80	0.98	1.42	1.50	1.13	1.64	3.06	1.42
16	1.20	1.17	1.69	2.00	1.25	1.82	3.51	1.69
20	1.60	1.27	1.84	2.50	1.36	1.98	3.81	1.84
24	2.00	1.36	1.97	3.00	1.47	2.12	4.09	1.97
36	3.20	1.61	2.33	4.50	1.74	2.51	4.84	2.33
48	4.40	1.82	2.64	6.00	1.97	2.85	5.49	2.64
60	5.60	2.02	2.91	7.50	2.18	3.15	6.07	2.91

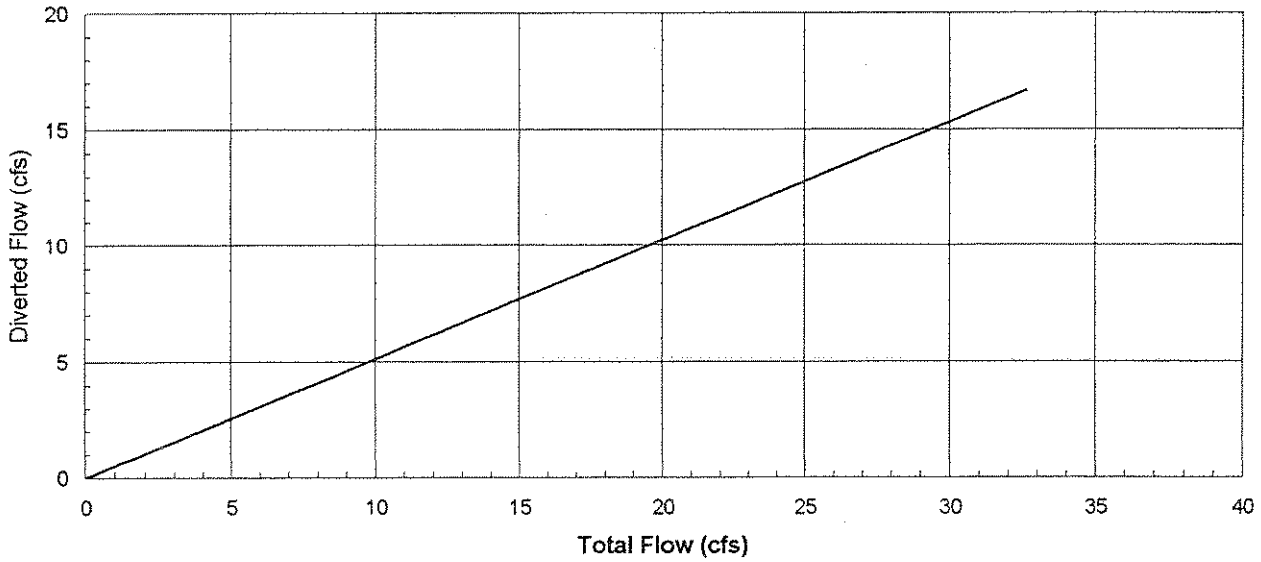


FLOW SPLIT AT MANHOLE 16578 (RC)

Stoddard Drive Diversion

MH 16243 (thru to MH 16242)			MH 7650				
Dia =	21	inches	Dia =	21	inches		
Area =	2.4053	sq ft	Area =	2.4053	sq ft		
Head =	1.72	feet	Head =	1.70	feet		
Length =	389	feet	Length =	423	feet		
Qfull =	9.81	cfs	Qfull =	9.35	cfs	Manning =	0.014
do =	0.0	inches	do =	0.0	inches		

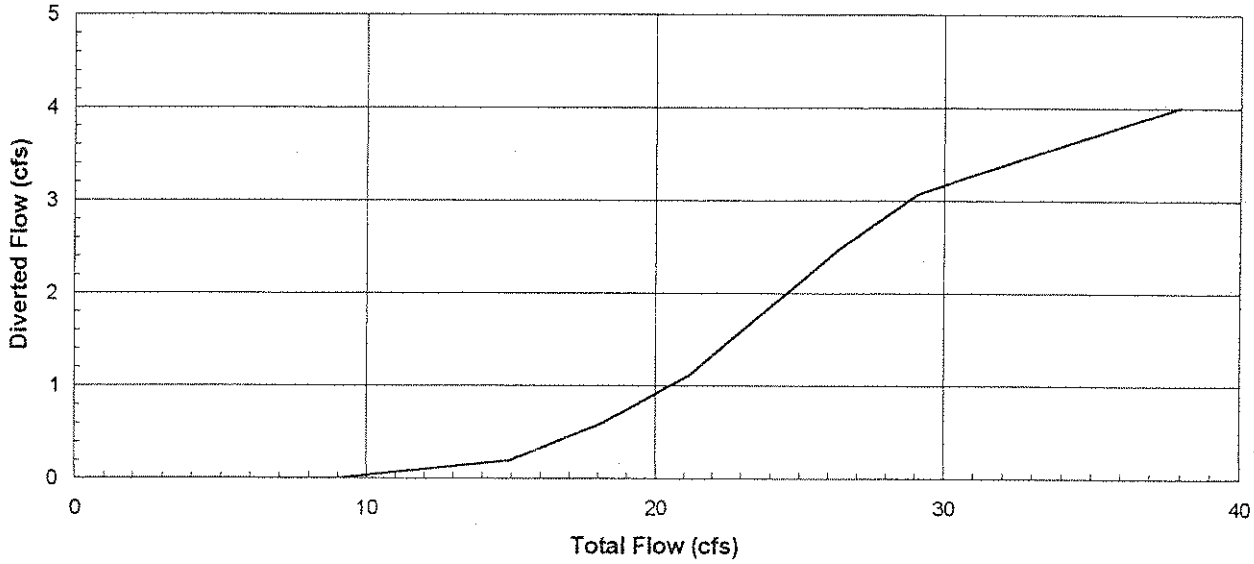
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.19	0.08	0.78	0.19	0.08	0.75	1.53	0.78
8	0.38	0.30	2.94	0.38	0.30	2.81	5.75	2.94
12	0.57	0.62	6.08	0.57	0.62	5.80	11.88	6.08
16	0.76	0.92	9.03	0.76	0.92	8.60	17.63	9.03
20	0.95	1.07	10.50	0.95	1.07	10.01	20.50	10.50
24	1.14	1.07	10.50	1.14	1.07	10.02	20.52	10.50
28	1.33	1.16	11.35	1.33	1.16	10.84	22.19	11.35
32	1.52	1.24	12.15	1.52	1.24	11.60	23.75	12.15
36	1.71	1.31	12.89	1.71	1.32	12.32	25.21	12.89
40	1.90	1.39	13.59	1.90	1.39	13.00	26.59	13.59
48	2.29	1.52	14.90	2.29	1.52	14.26	29.16	14.90
60	2.86	1.70	16.68	2.86	1.71	15.96	32.63	16.68



FLOW SPLIT AT MANHOLE 17992 (RC)

185th Avenue Diversion

	MH 5482 Diverted			MH 17991 Main				
	Dia =	10	inches	Dia =	27	inches		
	Area =	0.5454	sq.ft	Area =	3.9761	sq.ft		
	Head =	0.70	feet	Head =	2.10	feet		
	Length =	126	feet	Length =	350	feet		
	Qfull =	1.52	cfs	Qfull =	22.34	cfs	Manning =	0.014
	do =	13.6	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.00	0.00	0.00	0.15	0.05	1.12	1.12	0.00
6	0.00	0.00	0.00	0.22	0.11	2.46	2.46	0.00
8	0.00	0.00	0.00	0.30	0.20	4.47	4.47	0.00
10	0.00	0.00	0.00	0.37	0.29	6.48	6.48	0.00
12	0.00	0.00	0.00	0.44	0.40	8.93	8.93	0.00
16	0.24	0.13	0.20	0.59	0.66	14.74	14.94	0.20
18	0.44	0.40	0.61	0.67	0.79	17.65	18.25	0.61
20	0.64	0.74	1.13	0.74	0.90	20.10	21.23	1.13
24	1.04	1.63	2.48	0.89	1.07	23.90	26.38	2.48
36	2.24	2.02	3.08	1.33	1.16	26.02	29.10	3.08
48	3.44	2.35	3.57	1.78	1.35	30.24	33.82	3.57
60	4.64	2.64	4.01	2.22	1.52	33.94	37.95	4.01

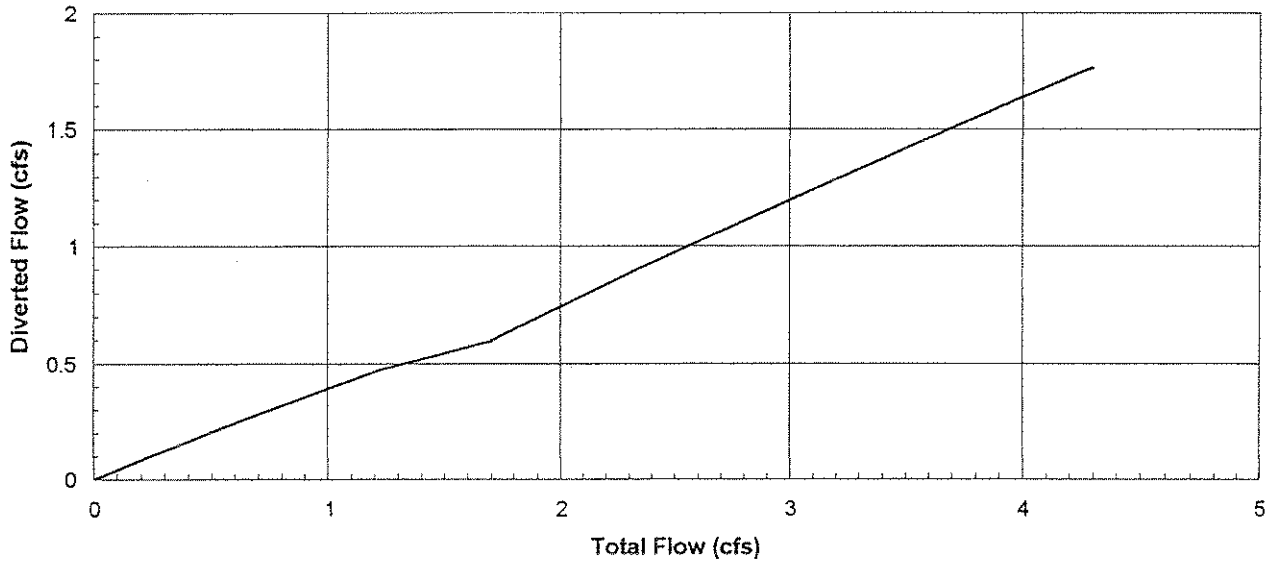


FLOW SPLIT AT MANHOLE 18260 (RC)

Fairmont Drive Diversion

MH 20669 Diverted			MH 18259 Main				
Dia =	8	inches	Dia =	10	inches		
Area =	0.3491	sq.ft	Area =	0.5454	sq.ft		
Head =	0.50	feet	Head =	1.20	feet		
Length =	237	feet	Length =	413	feet		
Qfull =	0.52	cfs	Qfull =	1.10	cfs	Manning =	0.014
do =	0.0	inches	do =	0.0	inches		

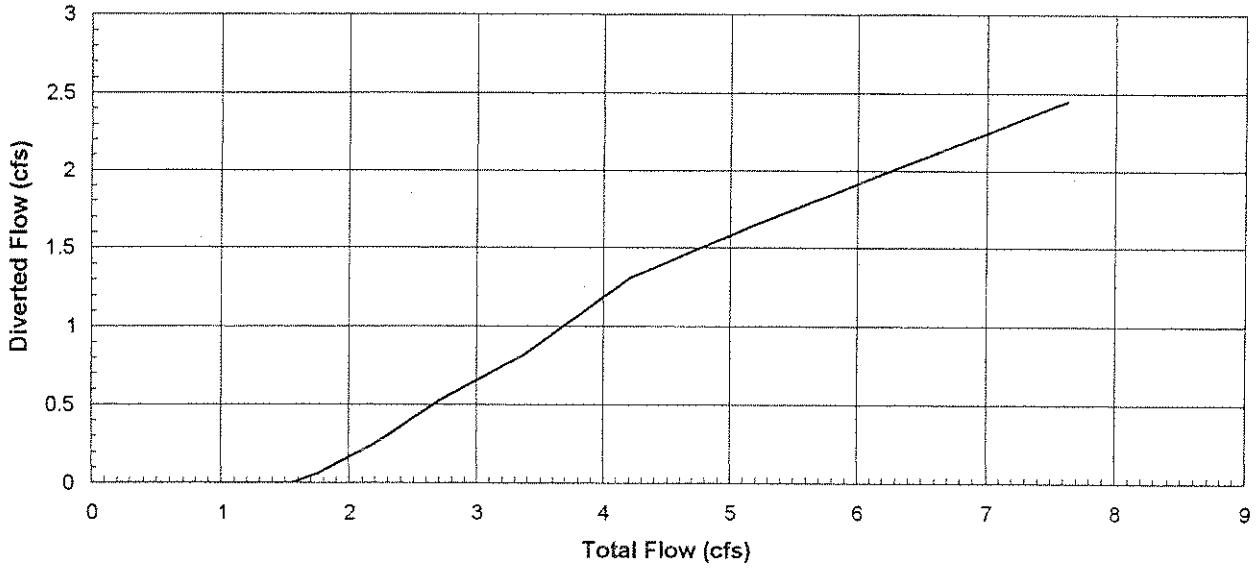
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.25	0.14	0.07	0.20	0.09	0.10	0.17	0.07
4	0.50	0.50	0.26	0.40	0.34	0.37	0.63	0.26
6	0.75	0.91	0.47	0.60	0.67	0.74	1.21	0.47
10	1.25	1.15	0.60	1.00	1.00	1.10	1.70	0.60
12	1.50	1.29	0.67	1.20	1.07	1.17	1.84	0.67
16	2.00	1.53	0.79	1.60	1.19	1.31	2.10	0.79
20	2.50	1.73	0.90	2.00	1.30	1.43	2.33	0.90
24	3.00	1.91	0.99	2.40	1.41	1.54	2.53	0.99
30	3.75	2.16	1.12	3.00	1.55	1.70	2.82	1.12
36	4.50	2.38	1.23	3.60	1.68	1.84	3.07	1.23
60	7.50	3.11	1.61	6.00	2.12	2.32	3.93	1.61
72	9.00	3.42	1.77	7.20	2.31	2.53	4.30	1.77



FLOW SPLIT AT MANHOLE 18263 (RC)

Erickson Street Diversion

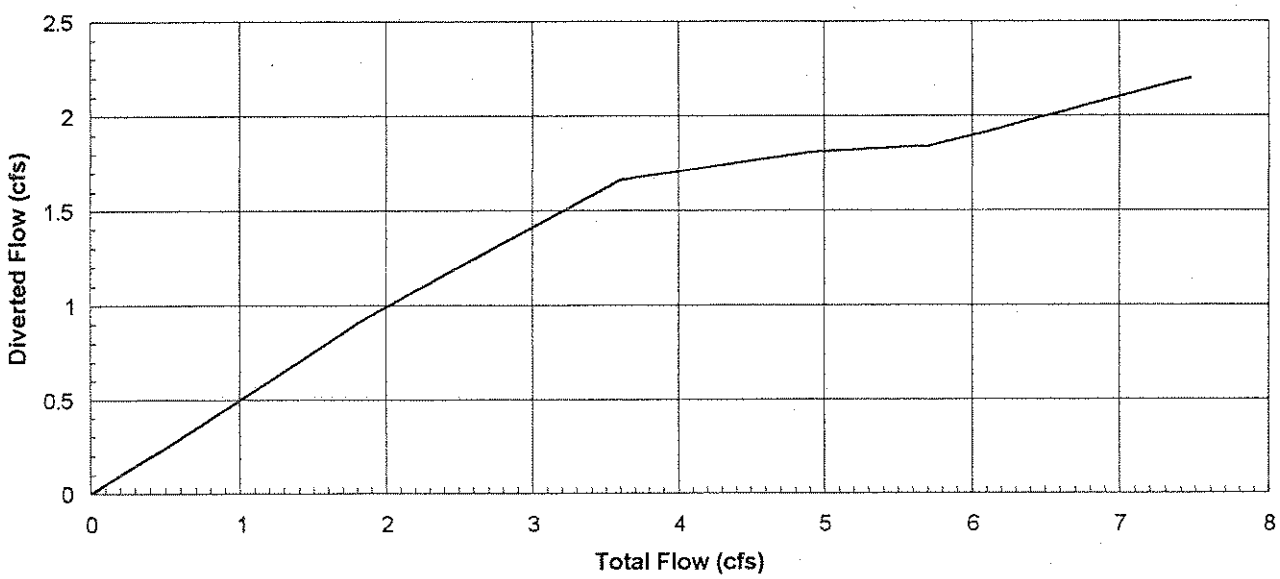
	MH 18262 Diverted			MH 18342 Main				
	Dia =	10	inches	Dia =	8	inches		
	Area =	0.5454	sq.ft	Area =	0.3491	sq.ft		
	Head =	0.49	feet	Head =	0.52	feet		
	Length =	322	feet	Length =	23	feet		
	Qfull =	0.80	cfs	Qfull =	1.69	cfs	Manning =	0.014
	do =	6.12	inches	do =	0.00	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.25	0.14	0.24	0.24	0.00
4	0.00	0.00	0.00	0.50	0.50	0.85	0.85	0.00
6	0.00	0.00	0.00	0.75	0.91	1.54	1.54	0.00
8	0.19	0.08	0.06	1.00	1.00	1.69	1.76	0.06
10	0.39	0.32	0.25	1.25	1.15	1.94	2.20	0.25
12	0.59	0.65	0.52	1.50	1.28	2.17	2.68	0.52
16	0.99	1.03	0.82	2.00	1.51	2.56	3.38	0.82
20	1.39	1.64	1.31	2.50	1.71	2.89	4.20	1.31
24	1.79	1.84	1.46	3.00	1.89	3.19	4.66	1.46
30	2.39	2.10	1.67	3.75	2.13	3.60	5.27	1.67
36	2.99	2.33	1.85	4.50	2.34	3.96	5.82	1.85
60	5.39	3.08	2.45	7.50	3.06	5.17	7.62	2.45



FLOW SPLIT AT MANHOLE 18344 (RC)

Pearl Street Diversion

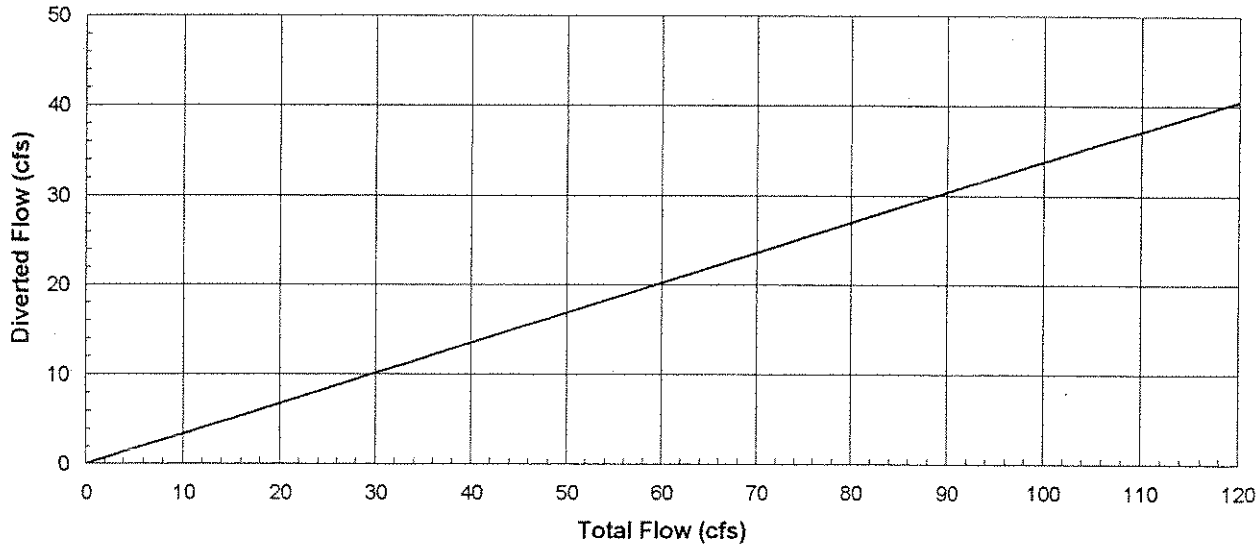
	MH 18263 Diverted			MH 18545 Main (thru to 18343)				
	Dia =	8	inches	Dia =	12	inches		
	Area =	0.3491	sq ft	Area =	0.7854	sq ft		
	Head =	9.11	feet	Head =	4.70	feet		
	Length =	352	feet	Length =	345	feet		
	Qfull =	1.81	cfs	Qfull =	3.87	cfs	Manning =	0.014
	do =	0.00	inches	do =	0.00	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.25	0.14	0.25	0.17	0.07	0.27	0.52	0.25
4	0.50	0.50	0.91	0.33	0.23	0.89	1.80	0.91
6	0.75	0.92	1.67	0.50	0.50	1.94	3.60	1.67
8	1.00	1.00	1.81	0.67	0.80	3.10	4.91	1.81
12	1.50	1.02	1.84	1.00	1.00	3.87	5.71	1.84
18	2.25	1.04	1.89	1.50	1.05	4.07	5.96	1.89
20	2.50	1.05	1.91	1.67	1.07	4.14	6.04	1.91
24	3.00	1.07	1.94	2.00	1.10	4.26	6.20	1.94
30	3.75	1.10	1.98	2.50	1.15	4.45	6.43	1.98
36	4.50	1.12	2.03	3.00	1.19	4.62	6.65	2.03
60	7.50	1.21	2.20	5.00	1.36	5.27	7.47	2.20



FLOW SPLIT AT MANHOLE 20083 (RC PS)

Rock Creek PS Diversion

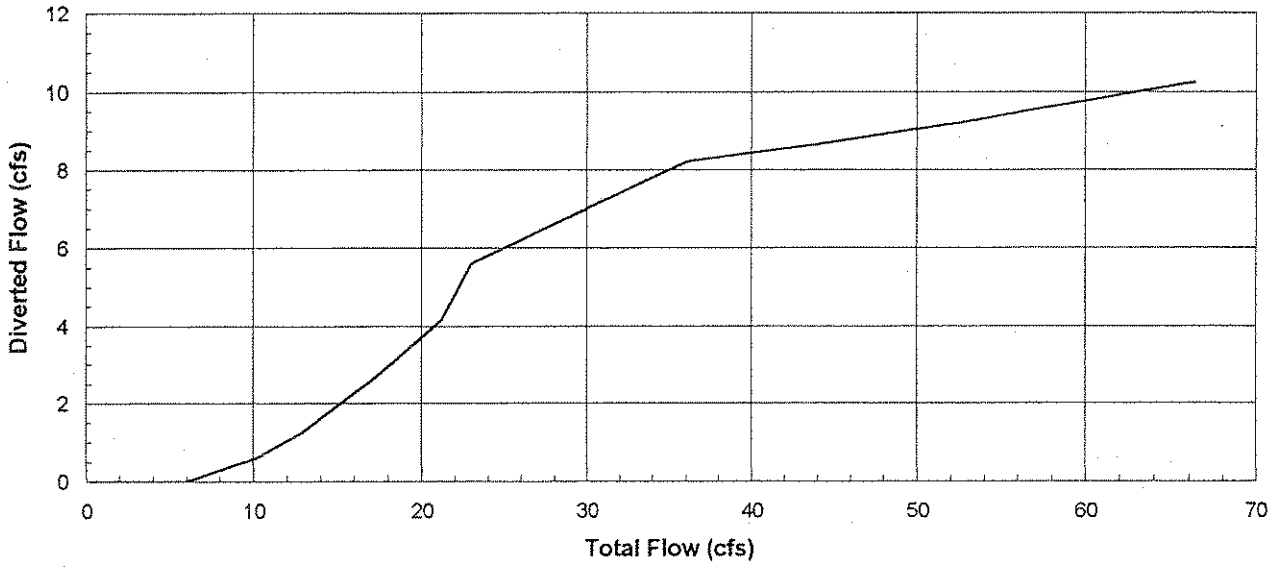
	Pipe A Diverted			Pipe B Main				
	Dia =	42	inches	Dia =	54	inches		
	Area =	9.6211	sq.ft.	Area =	15.9043	sq.ft.		
	Head =		feet	Head =		feet		
	Length =		feet	Length =		feet		
	Qfull =		cfs	Qfull =		cfs	Manning =	0.014
	do =	0.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
			0.00			0.00	0.00	0.00
			3.38			6.62	10.00	3.38
			6.76			13.25	20.00	6.76
			10.14			19.87	30.00	10.14
			13.51			26.49	40.00	13.51
			20.27			39.74	60.00	20.27
			27.03			52.98	80.00	27.03
			33.78			66.23	100.00	33.78
			40.54			79.47	120.00	40.54
			47.30			92.72	140.00	47.30
			54.05			105.96	160.00	54.05
			60.81			119.21	180.00	60.81
			67.57			132.45	200.00	67.57



FLOW SPLIT AT MANHOLE 22342 (RC)

Golf Course Diversion

	MH 5339 Diverted			MH 17982 Main				
	Dia =	18	inches	Dia =	30	inches		
	Area =	1.7671	sq.ft.	Area =	4.9087	sq.ft.		
	Head =	1.01	feet	Head =	0.16	feet		
	Length =	320	feet	Length =	77	feet		
	Qfull =	5.49	cfs	Qfull =	17.41	cfs	Manning =	0.014
	do =	12.1	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.00	0.00	0.00	0.13	0.04	0.70	0.70	0.00
8	0.00	0.00	0.00	0.27	0.16	2.79	2.79	0.00
12	0.00	0.00	0.00	0.40	0.34	5.92	5.92	0.00
16	0.22	0.11	0.60	0.53	0.55	9.57	10.18	0.60
18	0.33	0.23	1.26	0.60	0.67	11.66	12.93	1.26
21	0.49	0.49	2.69	0.70	0.84	14.62	17.32	2.69
24	0.66	0.76	4.18	0.80	0.98	17.06	21.24	4.18
30	0.99	1.02	5.60	1.00	1.00	17.41	23.01	5.60
33	1.16	1.50	8.22	1.10	1.60	27.87	36.09	8.22
36	1.33	1.58	8.66	1.20	2.03	35.36	44.02	8.66
40	1.55	1.68	9.22	1.33	2.49	43.38	52.60	9.22
48	1.99	1.86	10.24	1.60	3.22	56.07	66.32	10.24

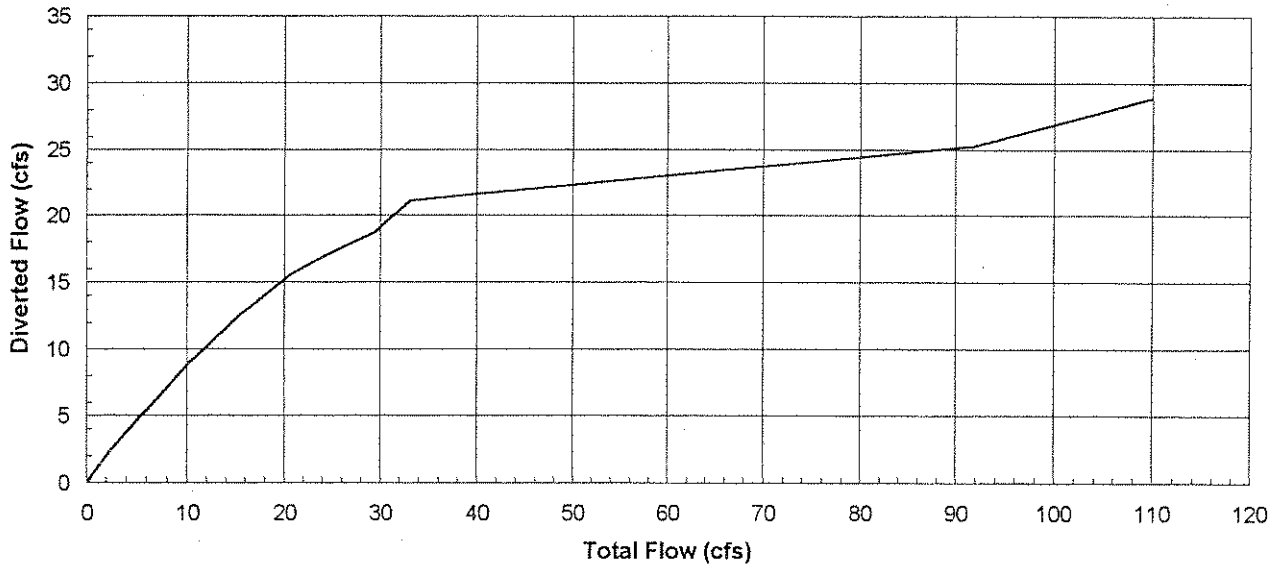


FLOW SPLIT AT MANHOLE 23959 (RC)

Willow Creek Trunk

MH 6966 Diverted			MH 23958 Main				
Dia =	30	inches	Dia =	30	inches		
Area =	4.9087	sq.ft	Area =	4.9087	sq.ft		
Head =	0.65	feet	Head =	0.03	feet		
Length =	375	feet	Length =	34	feet		
Qfull =	15.90	cfs	Qfull =	11.34	cfs	Manning =	0.014
do =	0.0	inches	do =	9.8	inches		

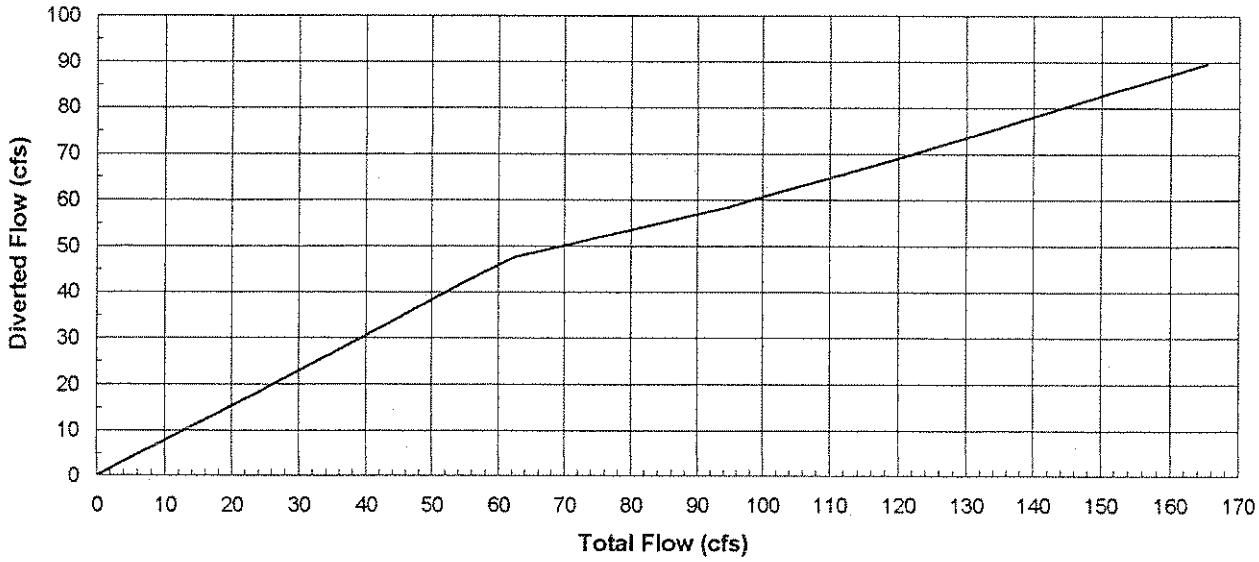
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.13	0.04	0.64	0.00	0.00	0.00	0.64	0.64
8	0.27	0.16	2.54	0.00	0.00	0.00	2.54	2.54
12	0.40	0.34	5.41	0.07	0.05	0.57	5.97	5.41
16	0.53	0.55	8.74	0.21	0.10	1.13	9.88	8.74
20	0.67	0.79	12.56	0.34	0.25	2.84	15.40	12.56
24	0.80	0.98	15.58	0.47	0.45	5.10	20.69	15.58
27	0.90	1.06	16.85	0.57	0.62	7.03	23.89	16.85
33	1.10	1.18	18.71	0.77	0.94	10.66	29.37	18.71
36	1.20	1.33	21.15	0.87	1.05	11.91	33.06	21.15
42	1.40	1.59	25.33	1.07	5.86	66.47	91.80	25.33
48	1.60	1.82	28.92	1.27	7.14	81.01	109.93	28.92



FLOW SPLIT AT MANHOLE 23964 (RC)

Willow Creek Trunk

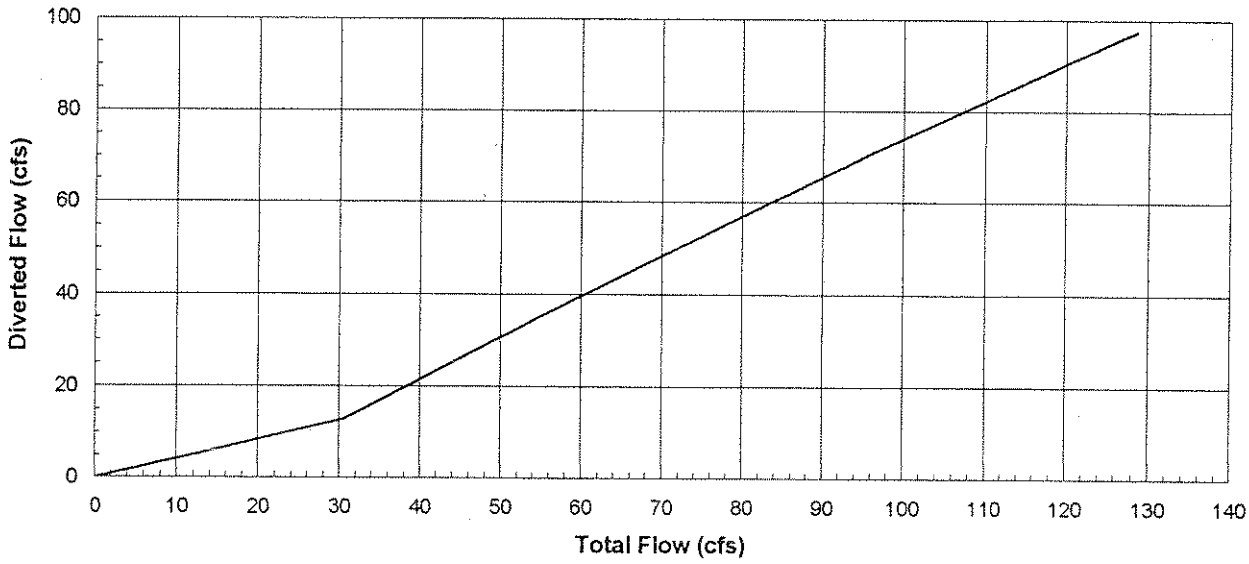
	MH 10579 Diverted			MH 23963 Main				
	Dia =	27	inches	Dia =	27	inches		
	Area =	3.9761	sq.ft	Area =	3.9761	sq.ft		
	Head =	0.49	feet	Head =	0.05	feet		
	Length =	18	feet	Length =	19	feet		
	Qfull =	47.58	cfs	Qfull =	14.79	cfs	Manning =	0.014
	do =	0.0	inches	do =	0.2	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.07	0.01	0.48	0.07	0.01	0.15	0.62	0.48
4	0.15	0.05	2.38	0.14	0.04	0.59	2.97	2.38
8	0.30	0.20	9.52	0.29	0.18	2.66	12.18	9.52
12	0.44	0.40	19.03	0.44	0.40	5.92	24.95	19.03
15	0.56	0.60	28.55	0.55	0.59	8.73	37.27	28.55
16	0.59	0.65	30.92	0.58	0.64	9.47	40.39	30.92
20	0.74	0.90	42.82	0.73	0.88	13.02	55.84	42.82
27	1.00	1.00	47.58	0.99	1.01	14.94	62.52	47.58
30	1.11	1.23	58.47	1.10	2.45	36.23	94.70	58.47
33	1.22	1.42	67.63	1.21	3.32	49.06	116.69	67.63
36	1.33	1.59	75.68	1.32	4.00	59.17	134.85	75.68
42	1.56	1.88	89.65	1.55	5.10	75.43	165.08	89.65



FLOW SPLIT AT MANHOLE 23967 (RC)

Willow Creek Trunk

	MH 10578 Diverted			MH 23965 Main				
	Dia =	27	inches	Dia =	27	inches		
	Area =	3.9761	sq.ft	Area =	3.9761	sq.ft		
	Head =	0.04	feet	Head =	1.09	feet		
	Length =	20	feet	Length =	289	feet		
	Qfull =	12.90	cfs	Qfull =	17.71	cfs	Manning =	0.014
	do =	0.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.15	0.05	0.64	0.15	0.05	0.89	1.53	0.64
8	0.30	0.20	2.58	0.30	0.20	3.54	6.12	2.58
12	0.44	0.40	5.16	0.44	0.40	7.08	12.24	5.16
15	0.56	0.60	7.74	0.56	0.60	10.63	18.36	7.74
18	0.67	0.79	10.19	0.67	0.79	13.99	24.18	10.19
27	1.00	1.00	12.90	1.00	1.00	17.71	30.60	12.90
30	1.11	2.69	34.72	1.11	1.11	19.64	54.36	34.72
33	1.22	3.67	47.38	1.22	1.21	21.39	68.77	47.38
36	1.33	4.44	57.31	1.33	1.30	23.01	80.32	57.31
42	1.56	5.68	73.23	1.56	1.47	25.95	99.18	73.23
48	1.78	6.69	86.27	1.78	1.61	28.59	114.85	86.27
54	2.00	7.57	97.57	2.00	1.75	31.00	128.57	97.57



RC23967.wk4

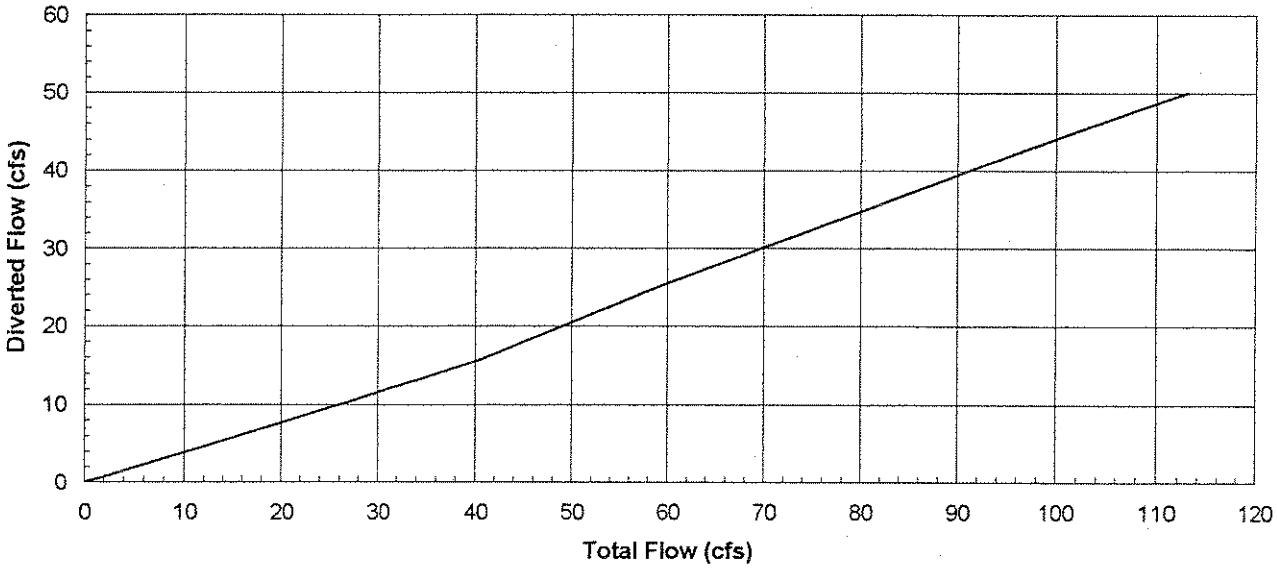
Date 07/14/01

FLOW SPLIT AT MANHOLE 23973 (RC)

Willow Creek Trunk

MH 10670 Diverted			MH 23971 Main			
Dia =	27	inches	Dia =	27	inches	
Area =	3.9761	sq.ft.	Area =	3.9761	sq.ft.	
Head =	0.26	feet	Head =	0.44	feet	
Length =	100	feet	Length =	67	feet	
Qfull =	14.70	cfs	Qfull =	23.37	cfs	Manning = 0.014
do =	0.0	inches	do =	0.0	inches	

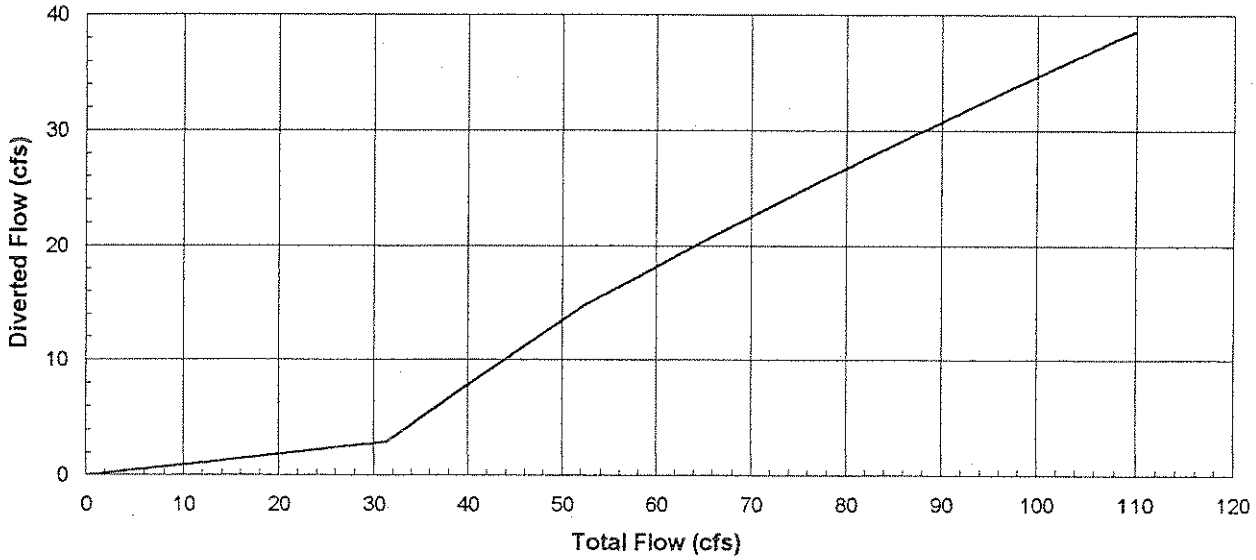
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.15	0.05	0.74	0.15	0.05	1.17	1.90	0.74
8	0.30	0.20	2.94	0.30	0.20	4.67	7.61	2.94
12	0.44	0.40	5.88	0.44	0.40	9.35	15.23	5.88
16	0.59	0.65	9.56	0.59	0.65	15.19	24.75	9.56
20	0.74	0.90	13.23	0.74	0.90	21.03	34.26	13.23
24	0.89	1.06	15.59	0.89	1.06	24.77	40.36	15.59
33	1.22	1.71	25.14	1.22	1.46	34.16	59.29	25.14
36	1.33	1.97	28.98	1.33	1.64	38.43	67.41	28.98
42	1.56	2.41	35.43	1.56	1.96	45.80	81.23	35.43
48	1.78	2.78	40.88	1.78	2.23	52.13	93.01	40.88
60	2.22	3.40	50.03	2.22	2.69	62.92	112.95	50.03



FLOW SPLIT AT MANHOLE 23977 (RC)

Willow Creek Trunk

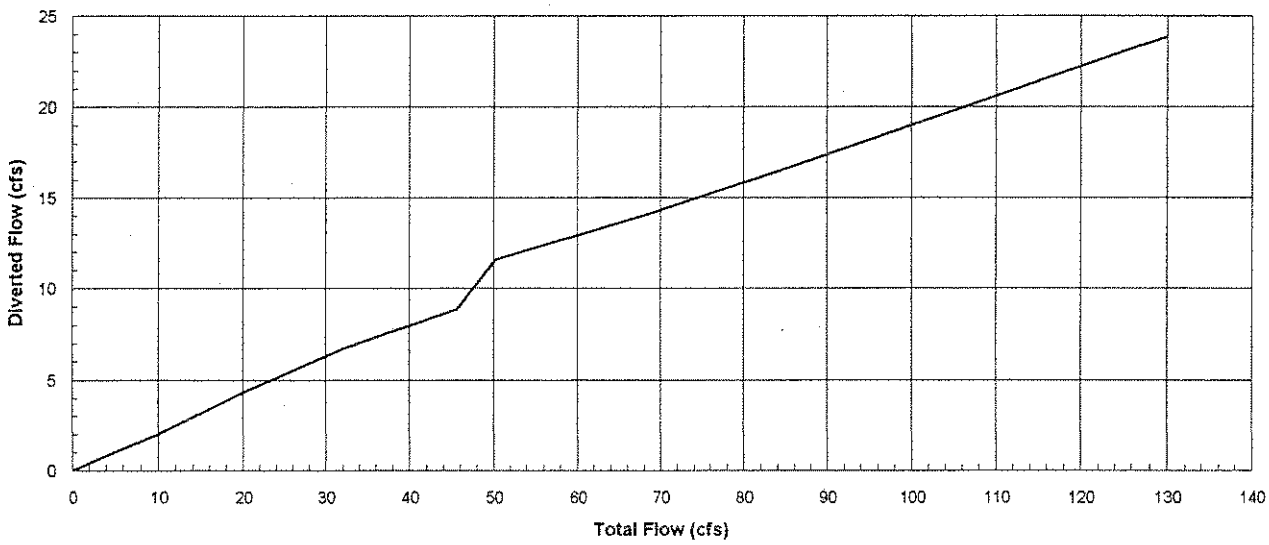
	MH 10666 Diverted			MH 23976 Main				
	Dia =	27	inches	Dia =	27	inches		
	Area =	3.9761	sq.ft	Area =	3.9761	sq.ft		
	Head =	0.01	feet	Head =	0.33	feet		
	Length =	98	feet	Length =	34	feet		
	Qfull =	2.91	cfs	Qfull =	28.41	cfs	Manning =	0.014
	do =	0.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.15	0.05	0.15	0.15	0.05	1.42	1.57	0.15
8	0.30	0.20	0.58	0.30	0.20	5.68	6.26	0.58
12	0.44	0.40	1.17	0.44	0.40	11.36	12.53	1.17
15	0.56	0.60	1.75	0.56	0.60	17.04	18.79	1.75
18	0.67	0.79	2.30	0.67	0.79	22.44	24.74	2.30
21	0.78	0.95	2.77	0.78	0.95	26.99	29.76	2.77
27	1.00	1.00	2.91	1.00	1.00	28.41	31.32	2.91
30	1.11	5.10	14.85	1.11	1.33	37.66	52.51	14.85
33	1.22	7.14	20.80	1.22	1.59	45.05	65.86	20.80
36	1.33	8.72	25.39	1.33	1.81	51.39	76.79	25.39
42	1.56	11.22	32.70	1.56	2.19	62.16	94.86	32.70
48	1.78	13.27	38.64	1.78	2.51	71.32	109.96	38.64



FLOW SPLIT AT MANHOLE 23983 (RC)

Willow Creek Trunk

	MH 6825 Diverted			MH 23982 Main				
	Dia =	24	inches	Dia =	27	inches		
	Area =	3.1416	sq ft	Area =	3.9761	sq ft		
	Head =	0.29	feet	Head =	0.27	feet		
	Length =	179	feet	Length =	15	feet		
	Qfull =	8.48	cfs	Qfull =	38.69	cfs	Manning =	0.014
	do =	0.0	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.17	0.06	0.51	0.15	0.05	1.93	2.44	0.51
8	0.33	0.23	1.95	0.30	0.20	7.74	9.69	1.95
12	0.50	0.50	4.24	0.44	0.40	15.47	19.71	4.24
16	0.67	0.79	6.70	0.59	0.65	25.15	31.84	6.70
18	0.75	0.91	7.71	0.67	0.79	30.56	38.28	7.71
21	0.88	1.04	8.82	0.78	0.95	36.75	45.57	8.82
27	1.13	1.36	11.57	1.00	1.00	38.69	50.26	11.57
30	1.25	1.65	13.99	1.11	1.39	53.69	67.68	13.99
33	1.38	1.89	16.06	1.22	1.69	65.33	81.39	16.06
36	1.50	2.11	17.88	1.33	1.94	75.19	93.07	17.88
42	1.75	2.48	21.06	1.56	2.37	91.79	112.85	21.06
48	2.00	2.81	23.82	1.78	2.74	105.82	129.64	23.82

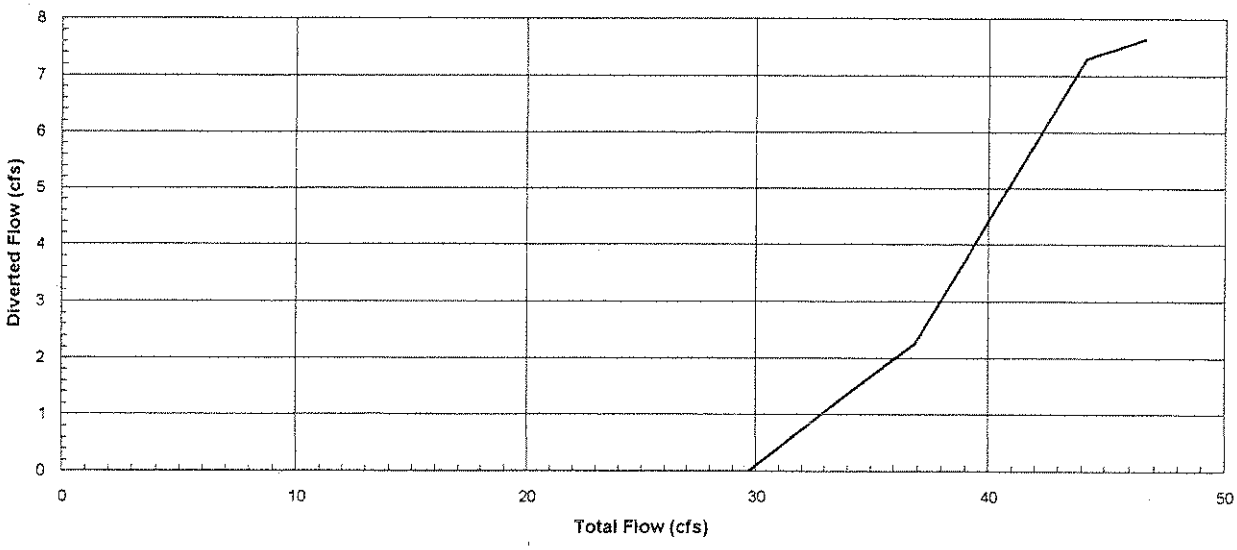


FLOW SPLIT AT MANHOLE 25677 (RC)

Butternut Creek Trunk

MH 8609 Diverted			MH 25676 Main				
Dia =	10	inches	Dia =	18	inches		
Area =	0.5454	sq.ft	Area =	1.7671	sq.ft		
Head =	0.44	feet	Head =	0.26	feet		
Length =	40	feet	Length =	30	feet		
Qfull =	2.14	cfs	Qfull =	9.10	cfs	Manning =	0.014
do =	51.0	inches	do =	0.0	inches		

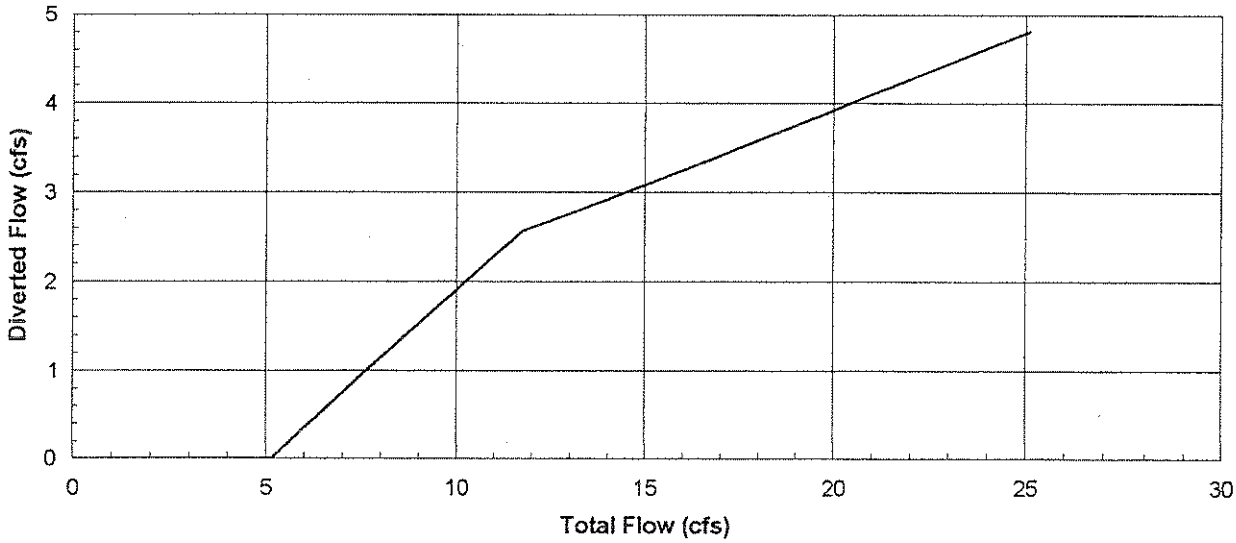
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
4	0.00	0.00	0.00	0.22	0.10	0.91	0.91	0.00
8	0.00	0.00	0.00	0.44	0.40	3.64	3.64	0.00
12	0.00	0.00	0.00	0.67	0.78	7.10	7.10	0.00
18	0.00	0.00	0.00	1.00	1.00	9.10	9.10	0.00
21	0.00	0.00	0.00	1.17	1.08	12.75	12.75	0.00
24	0.00	0.00	0.00	1.33	1.71	15.57	15.57	0.00
27	0.00	0.00	0.00	1.50	1.97	17.95	17.95	0.00
36	0.00	0.00	0.00	2.00	2.60	23.69	23.69	0.00
48	0.00	0.00	0.00	2.67	3.26	29.67	29.67	0.00
60	0.90	1.06	2.27	3.33	3.80	34.62	36.89	2.27
66	1.50	3.41	7.29	3.67	4.05	36.85	44.14	7.29
72	2.10	3.57	7.64	4.00	4.28	38.96	46.60	7.64



FLOW SPLIT AT MANHOLE 28053 (RC)

185th Avenue Trunk

	MH 8065 Diverted			MH 28052 Main				
	Dia =	10	inches	Dia =	18	inches		
	Area =	0.5454	sq ft	Area =	1.7671	sq ft		
	Head =	0.41	feet	Head =	0.53	feet		
	Length =	100	feet	Length =	117	feet		
	Qfull =	1.31	cfs	Qfull =	6.58	cfs	Manning =	0.014
	do =	11.5	inches	do =	0.0	inches		
Depth inches	d/D	q/Q	Q(d) cfs	d/D	q/Q	Q(d) cfs	QTot cfs	QDiv cfs
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8	0.00	0.00	0.00	0.44	0.40	2.63	2.63	0.00
12	0.05	0.01	0.01	0.67	0.78	5.13	5.15	0.01
18	0.65	0.75	0.98	1.00	1.00	6.58	7.56	0.98
24	1.25	1.96	2.56	1.33	1.39	9.18	11.74	2.56
27	1.55	2.11	2.76	1.50	1.55	10.23	12.99	2.76
36	2.45	2.51	3.27	2.00	1.96	12.88	16.16	3.27
48	3.65	2.95	3.86	2.67	2.39	15.74	19.60	3.86
54	4.25	3.15	4.12	3.00	2.58	16.99	21.11	4.12
60	4.85	3.34	4.36	3.33	2.76	18.15	22.52	4.36
66	5.45	3.52	4.60	3.67	2.92	19.24	23.84	4.60
72	6.05	3.69	4.82	4.00	3.08	20.28	25.10	4.82



APPENDIX J

Modeling “Project.des” Criteria Files

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Project.Des for Durham Basin

!  DESIGN FILE FOR CLEAN WATER SERVICES MASTER PLAN MODEL (07/2008)
!  SYSTEM FACTORS AND DESIGN CRITERIA
!  MODIFIED FROM USA 1999 MASTER PLAN UPDATE (01/2001)

!  DESIGN PIPE DATA
!  (Mininum velocity changed to 2.0 fps from 1995 value)
[DPI]
Default=0.013  8  8  7  2.3  0.0010  0.8  120 0

!  DESIGN PIPE PRESSURE DATA
[PRE]
Default=100  0  5 0 0

!  EXISTING PIPE DATA
[EPI]
Default=0.013 2 0.9 0 0 0

!  MANHOLE DEFAULT DATA
[MAN]
Default=2  4  4  0

!  DIURNAL CURVES
!  Unit Diurnal Curves for Weekdays/Weekends
!  by Basin Type & Confidence Level
!  Originally generated March 3, 1995

[DIU]

Default=1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00

!  Basin Type 1 - Weekday Diurnal Hydrograph - Median
DIU_1WDMed=0.51 0.28 0.21 0.21 0.24 0.41 1.25 2.20 1.97 1.57 1.37 1.20 1.02 0.93
0.82 0.80 0.84 0.98 1.19 1.34 1.36 1.33 1.20 0.87

!  Basin Type 2 - Weekday Diurnal Hydrograph - Median
DIU_2WDMed=0.58 0.39 0.31 0.29 0.31 0.52 1.21 1.77 1.60 1.40 1.31 1.19 1.08 1.02
0.95 0.91 0.95 1.06 1.21 1.28 1.28 1.24 1.14 0.88

!  Basin Type 3 - Weekday Diurnal Hydrograph - Median
DIU_3WDMed=0.59 0.40 0.32 0.29 0.29 0.43 0.98 1.63 1.60 1.44 1.37 1.27 1.15 1.06
0.99 0.94 0.96 1.05 1.19 1.27 1.28 1.25 1.15 0.89

!  Basin Type 4 - Weekday Diurnal Hydrograph - Median
DIU_4WDMed=0.55 0.41 0.35 0.31 0.32 0.39 0.70 1.15 1.30 1.43 1.53 1.44 1.36 1.30
1.26 1.16 1.12 1.13 1.16 1.16 1.18 1.10 1.01 0.79

!  Basin Type 1 - Weekend Diurnal Hydrograph - Median
DIU_1WEMed=0.59 0.38 0.26 0.22 0.22 0.25 0.37 0.72 1.29 1.78 1.94 1.80 1.56 1.35
1.19 1.14 1.12 1.14 1.20 1.26 1.24 1.20 1.07 0.85

!  Basin Type 2 - Weekend Diurnal Hydrograph - Median
DIU_2WEMed=0.65 0.47 0.37 0.32 0.31 0.34 0.48 0.81 1.31 1.65 1.73 1.62 1.44 1.29
1.17 1.10 1.09 1.12 1.17 1.21 1.23 1.17 1.05 0.86

!  Basin Type 3 - Weekend Diurnal Hydrograph - Median
DIU_3WEMed=0.69 0.52 0.42 0.37 0.35 0.37 0.47 0.73 1.15 1.53 1.66 1.59 1.44 1.29
1.18 1.13 1.10 1.13 1.16 1.19 1.22 1.18 1.09 0.91

!  Basin Type 4 - Weekend Diurnal Hydrograph - Median
DIU_4WEMed=0.73 0.58 0.48 0.41 0.41 0.42 0.50 0.70 1.02 1.45 1.57 1.57 1.44 1.35
1.21 1.17 1.10 1.10 1.13 1.14 1.12 1.08 1.01 0.83
```

```
!   DIVERSION DETAILS

[DIV]

!  Diversion  1522 Basin  DR  Name:  Barnes Rd Diversion
!Previous model  DR01522_Divn= 0.00/0.00   2.33/1.25    5.06/2.71    7.99/4.28
10.11/5.42   10.69/5.67   11.24/5.92   11.77/6.15   12.51/6.48   13.21/6.80
15.70/7.94
DR01522_Divn= 0.00/0.00   2.33/0    5.06/0    7.99/0   10.11/0   10.69/0   11.24/0
11.77/0   12.51/0   13.21/0   15.70/0

!  Diversion 13862 Basin  DR  Name:  Fairfield Diversion
DR13862_Divn= 0.00/0.00   0.58/0.30    2.14/1.06    4.27/1.93    5.82/2.12
6.82/2.13    9.58/2.14   11.57/2.15   13.21/2.16   17.10/2.20   20.18/2.23
22.81/2.26   25.15/2.29

!  Diversion 18554 Basin  DR  Name:  SW Lombard Diversion #2
DR18554_Divn= 0.00/0.00   5.87/3.20   14.77/8.96   24.54/15.35  46.81/35.18
67.54/55.01  77.53/63.97  82.23/68.09  90.90/75.66  98.81/82.54 112.96/94.81
125.52/105.67

!  Diversion 18571 Basin  DR  Name:  5th St Diversion
DR18571_Divn= 0.00/0.00   0.15/0.15    0.71/0.53    3.24/1.70    6.28/3.16
7.61/3.99   10.57/6.71   12.91/8.71   14.84/10.33  18.05/12.98  20.75/15.17
23.13/17.09

!  Diversion 18828 Basin  DR  Name:  SW Lombard Diversion #1
DR18828_Divn= 0.00/0.00   0.39/0.13    2.30/0.70    5.73/1.46   10.02/2.54
15.29/3.81   20.77/5.02   28.78/6.35   34.05/7.08   35.42/7.74   41.25/9.96
46.30/11.76

!  Diversion 20606 Basin  DR  Name:  SW 5th St Diversion
DR20606_Divn= 0.00/0.00   1.66/0.00    3.77/0.00    6.92/0.00    7.48/0.00
7.98/0.00    8.44/0.00    8.87/0.00    9.27/0.00    9.65/0.00   10.02/0.00
10.70/0.00   11.63/0.00
REM_DR20606_Divn=0.00/0.00   1.66/0.56    3.77/1.54    6.92/3.31    7.48/3.36
7.98/3.40    8.44/3.45    8.87/3.50    9.27/3.54    9.65/3.59   10.02/3.63
10.70/3.72   11.63/3.84

!  Diversion 20760 Basin  DR  Name:  Sherwood Rd Diversion
DR20760_Divn= 0.00/0.00   0.44/0.01    1.73/0.16    3.65/0.46    5.49/0.83
5.99/1.19    6.28/1.39    6.54/1.57    6.78/1.72    7.12/1.94    7.44/2.13
8.54/2.77    9.02/3.03

!  Diversion 20834 Basin  DR  Name:  Tektronix Diversion
DR20834_Divn= 0.00/0.00   2.45/0.51    8.54/1.74   14.99/3.11   16.25/3.32
19.58/3.84   22.42/4.31   24.93/4.72   27.21/5.11   29.32/5.46   31.28/5.80
34.88/6.41   39.67/7.24

!  CWS Diversion 20834 Tektronix Diversion, Basin  DR, Name: Hocken Diversion
DR_Div_Hock= 0.00 0.00    0.69 0.14    2.82 0.58    6.12 1.25    10.11 2.07    14.23
2.91    17.74 3.63    18.15 3.71    42.88 7.76    44.32 8.01    49.67 8.92    54.50
9.75

DR_DIV_BERK=0.000 0.000 0.500 0.130 1.000 0.250 2.000 0.500 3.000 0.750 4.000 1.000
5.000 1.000 20.000 1.000

!  CWS Diversion 20911 Basin  DR  Name:  Tektronix PS Diversion from City of
Beaverton
DR_Div_Tek=0.000 0.000 7.200 0.000 7.900 1.300 10.000 3.000

!  Diversion 20911 Basin  DR  Name:  Tektronix PS Diversion
DR20911_Divn= 0.00/0.00   1.00/1.00    2.00/2.00    2.32/2.32    2.52/2.32
3.06/2.32    4.51/2.32    5.11/2.32    5.97/2.32    6.66/2.32    7.26/2.32
8.04/2.32    8.73/2.32

!  CWS Diversion 18571 5th St Diversion Basin  DR  Name:  Alger Diversion
DR_Div_Alger=0.000 0.000 0.340 0.000 1.340 0.000 3.060 0.260 5.350 0.950 8.360 2.670
18.120 7.070
```

```
!  CWS Diversion 20834 Tektronix Diversion, Basin  DR, Name: Hocken Diversion
DR_Div_Hock= 0.00 0.00    0.69 0.14    2.82 0.58    6.12 1.25    10.11 2.07    14.23
2.91    17.74 3.63    18.15 3.71    42.88 7.76    44.32 8.01    49.67 8.92    54.50
9.75


DEFAULT=0.000 0.000 20.000 0.000 40.000 0.000 60.000 0.000 80.000 0.000 100.000
0.000


!  PUMPING STATIONS
!  Pumping Station Configurations

!  Command paragraphs named according to USA pumping station number
!  Pumping station numbers used as manhole numbers in the model

[PUM]

!  Upper Tualatin/Sherwood (DR)
11664_PumpDR=1   1554   0   5.79   1   1554   0   5.79

!  Beaverton PS (DR)
12681_PumpDR=2   28.3   0   1.3   2   28.3   0   1.3

!  SW Bull Mtn. (DR)
15068_PumpDR=1   665.2   0   4.01   1   712.7   0   4.01

!  Cipole (DR)
17795_PumpDR=1   296.6   0   1.29   1   346.8   0   1.29

!  Tektronix (DR)
!  (total station rating of 3250 gpm)
27865_PumpDR=2  1830.0  771.0  5.0  2  2096.0  771.0  2.2


PUM_DEFAULT=2 0.0000 0.0000 100.0000 0 0.0000 0.0000 0.0000 0 0.0000 0.0000 0.0000
```

```
Project.Des for Forest Grove Basin

!  DESIGN FILE FOR CLEAN WATER SERVICES MASTER PLAN MODEL (07/2008)
!  SYSTEM FACTORS AND DESIGN CRITERIA
!  MODIFIED FROM USA 1999 MASTER PLAN UPDATE (01/2001)


!  DESIGN PIPE DATA
!  (Mininum velocity changed to 2.0 fps from 1995 value)
[DPI]
Default=0.013  8  8  7  2.3  0.0010  0.8  120 0

!  DESIGN PIPE PRESSURE DATA
[PRE]
Default=100  0  5 0 0

!  EXISTING PIPE DATA
[EPI]
NuPipe=0.013 2 0.8 0 0 0
Default=0.013 2 0.9 0 0 0

!  MANHOLE DEFAULT DATA
[MAN]
Default=2  4  4  0

!  DIURNAL CURVES
!  Unit Diurnal Curves for Weekdays/Weekends
!  by Basin Type & Confidence Level
!  Originally generated March 3, 1995

[DIU]

!  Basin Type 1 - Weekday Diurnal Hydrograph - Median
DIU_1WDMed=0.51 0.28 0.21 0.21 0.24 0.41 1.25 2.20 1.97 1.57 1.37 1.20 1.02 0.93
0.82 0.80 0.84 0.98 1.19 1.34 1.36 1.33 1.20 0.87

!  Basin Type 2 - Weekday Diurnal Hydrograph - Median
DIU_2WDMed=0.58 0.39 0.31 0.29 0.31 0.52 1.21 1.77 1.60 1.40 1.31 1.19 1.08 1.02
0.95 0.91 0.95 1.06 1.21 1.28 1.28 1.24 1.14 0.88

!  Basin Type 3 - Weekday Diurnal Hydrograph - Median
DIU_3WDMed=0.59 0.40 0.32 0.29 0.29 0.43 0.98 1.63 1.60 1.44 1.37 1.27 1.15 1.06
0.99 0.94 0.96 1.05 1.19 1.27 1.28 1.25 1.15 0.89

!  Basin Type 4 - Weekday Diurnal Hydrograph - Median
DIU_4WDMed=0.55 0.41 0.35 0.31 0.32 0.39 0.70 1.15 1.30 1.43 1.53 1.44 1.36 1.30
1.26 1.16 1.12 1.13 1.16 1.16 1.18 1.10 1.01 0.79

!  Basin Type 1 - Weekend Diurnal Hydrograph - Median
DIU_1WEMed=0.59 0.38 0.26 0.22 0.22 0.25 0.37 0.72 1.29 1.78 1.94 1.80 1.56 1.35
1.19 1.14 1.12 1.14 1.20 1.26 1.24 1.20 1.07 0.85

!  Basin Type 2 - Weekend Diurnal Hydrograph - Median
DIU_2WEMed=0.65 0.47 0.37 0.32 0.31 0.34 0.48 0.81 1.31 1.65 1.73 1.62 1.44 1.29
1.17 1.10 1.09 1.12 1.17 1.21 1.23 1.17 1.05 0.86

!  Basin Type 3 - Weekend Diurnal Hydrograph - Median
DIU_3WEMed=0.69 0.52 0.42 0.37 0.35 0.37 0.47 0.73 1.15 1.53 1.66 1.59 1.44 1.29
1.18 1.13 1.10 1.13 1.16 1.19 1.22 1.18 1.09 0.91

!  Basin Type 4 - Weekend Diurnal Hydrograph - Median
DIU_4WEMed=0.73 0.58 0.48 0.41 0.41 0.42 0.50 0.70 1.02 1.45 1.57 1.57 1.44 1.35
1.21 1.17 1.10 1.10 1.13 1.14 1.12 1.08 1.01 0.83

!  Flat diurnal for checking average rates of flow
DIU_UNITY=1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

!   DIVERSION DETAILS

[DIV]
```

```
!  Diversion  1522 Basin  DR  Name:  Barnes Rd Diversion
DR01522_Divn= 0.00/0.00   2.33/1.25    5.06/2.71    7.99/4.28   10.11/5.42
10.69/5.67   11.24/5.92   11.77/6.15   12.51/6.48   13.21/6.80   15.70/7.94

!  Diversion 13862 Basin  DR  Name:  Fairfield Diversion
DR13862_Divn= 0.00/0.00   0.58/0.30    2.14/1.06    4.27/1.93    5.82/2.12
6.82/2.13    9.58/2.14   11.57/2.15   13.21/2.16   17.10/2.20   20.18/2.23
22.81/2.26   25.15/2.29

!  Diversion 18554 Basin  DR  Name:  SW Lombard Diversion #2
DR18554_Divn= 0.00/0.00   5.87/3.20   14.77/8.96   24.54/15.35  46.81/35.18
67.54/55.01  77.53/63.97  82.23/68.09  90.90/75.66  98.81/82.54 112.96/94.81
125.52/105.67

!  Diversion 18571 Basin  DR  Name:  5th St Diversion
DR18571_Divn= 0.00/0.00   0.15/0.15    0.71/0.53    3.24/1.70    6.28/3.16
7.61/3.99   10.57/6.71   12.91/8.71   14.84/10.33  18.05/12.98  20.75/15.17
23.13/17.09

!  Diversion 18828 Basin  DR  Name:  SW Lombard Diversion #1
DR18828_Divn= 0.00/0.00   0.39/0.13    2.30/0.70    5.73/1.46   10.02/2.54
15.29/3.81   20.77/5.02   28.78/6.35   34.05/7.08   35.42/7.74   41.25/9.96
46.30/11.76

!  Diversion 20606 Basin  DR  Name:  SW 5th St Diversion
DR20606_Divn= 0.00/0.00   1.66/0.56    3.77/1.54    6.92/3.31    7.48/3.36
7.98/3.40    8.44/3.45    8.87/3.50    9.27/3.54    9.65/3.59   10.02/3.63
10.70/3.72   11.63/3.84

!  Diversion 20760 Basin  DR  Name:  Sherwood Rd Diversion
DR20760_Divn= 0.00/0.00   0.44/0.01    1.73/0.16    3.65/0.46    5.49/0.83
5.99/1.19    6.28/1.39    6.54/1.57    6.78/1.72    7.12/1.94    7.44/2.13
8.54/2.77    9.02/3.03

!  Diversion 20834 Basin  DR  Name:  Tektronix Diversion
DR20834_Divn= 0.00/0.00   2.45/0.51    8.54/1.74   14.99/3.11   16.25/3.32
19.58/3.84   22.42/4.31   24.93/4.72   27.21/5.11   29.32/5.46   31.28/5.80
34.88/6.41   39.67/7.24

!  Diversion 20911 Basin  DR  Name:  Tektronix PS Diversion
DR20911_Divn= 0.00/0.00   1.00/1.00    2.00/2.00    2.32/2.32    2.52/2.32
3.06/2.32    4.51/2.32    5.11/2.32    5.97/2.32    6.66/2.32    7.26/2.32
8.04/2.32    8.73/2.32

!  Diversion 12751 Basin  FG  Name:  Cornelius Diversion
FG12751_Divn= 0.00/0.00   0.17/0.11    0.81/0.43    1.84/0.91    3.10/1.48
4.48/2.12    5.60/2.64    9.46/6.11   16.50/12.57  21.13/16.69  26.54/21.43
30.99/25.30  44.53/36.93

!  Diversion 18846 Basin  FG  Name:  Hawthorn St Diversion
FG18846_Divn= 0.00/0.00   0.86/0.00    3.28/0.00    7.13/0.00   11.27/0.00
14.26/0.00   21.69/0.39   24.16/0.99   27.36/1.90   33.90/4.40   44.72/5.51
53.39/6.43   60.83/7.24


!  Diversion 20013 Basin  FG  Name:  SE 1st Ave Diversion
FG20013_Divn= 0.00/0.00   0.89/0.47    3.26/1.62    5.94/2.89    6.45/3.13
7.48/3.75    8.37/4.29   10.61/5.60   11.56/6.15   12.45/6.66   14.04/7.57
14.78/7.99

!  Diversion 20414 Basin  FG  Name:  23rd Ave Diversion
FG20414_Divn= 0.00/0.00   0.00/0.00    1.33/0.35    4.82/1.05    8.60/1.18
11.67/1.33   13.75/1.58   14.67/1.70   16.37/1.90   17.91/2.09   20.64/2.42
21.88/2.57   23.05/2.71

!  Diversion 27860 Basin  FG  Name:  SW Linden Diversion
FG27860_Divn= 0.00/0.00   2.72/0.00    4.47/0.00    9.72/0.00   12.45/0.00
14.00/0.00   17.88/0.18   21.75/2.30   27.80/4.14   33.21/5.98   38.39/8.00
42.63/9.38
```

```
!  Diversion 19808 Basin  HL  Name:  W Main St Diversion
HL19808_Divn= 0.00/0.00   0.30/0.30    1.45/1.04    2.46/1.32    4.72/1.52
5.74/1.71    6.98/1.88    7.68/2.03    9.98/2.56   11.84/3.00   13.45/3.38

!  Diversion 19863 Basin  HL  Name:  S 9th Ave Diversion (to RC)
HL19863_Divn= 0.00/0.00   0.44/0.40    1.49/1.17    2.79/1.62    4.16/2.24
5.17/2.72    6.01/3.13    8.02/4.12    9.62/4.91   10.33/5.27   10.99/5.60
11.62/5.91

!  Diversion 20299 Basin  HL  Name:  9th Ave Diversion (to RC)
HL20299_Divn= 0.00/0.00   0.68/0.40    2.54/1.36    3.23/1.72    3.70/2.00
4.12/2.24    4.50/2.45    5.48/3.01    5.90/3.26    6.30/3.48    7.04/3.90
7.37/4.09

!  Diversion 20312 Basin  HL  Name:  N 9th Ave Diversion (to RC)
HL20312_Divn= 0.00/0.00   0.93/0.76    3.57/2.60    5.01/3.29    5.39/3.54
5.83/3.78    6.24/4.01    6.81/4.32    7.33/4.62    8.27/5.16    9.11/5.64
9.89/6.09

!  Diversion  7925 Basin  RC  Name:  SW Madeline St Diversion
RC07925_Divn= 0.00/0.00   0.38/0.34    2.13/1.18    3.52/1.49    7.20/1.82
8.87/2.10    9.79/2.34   12.25/2.95   14.28/3.46   15.20/3.68   16.07/3.90

!  Diversion 12682 Basin  RC  Name:  Aloha PS #3 Diversion
RC12682_Divn= 0.00/0.00   0.59/0.30    1.18/0.59    2.66/1.33    4.73/2.37
5.92/2.96    9.47/4.73   14.79/7.40   22.19/11.09  28.40/14.20  48.31/24.15
72.46/36.23  90.37/45.19

!  Diversion 16250 Basin  RC  Name:  198th Ave Diversion
RC16250_Divn= 0.00/0.00   1.07/0.32    5.17/2.27   11.19/5.40   17.45/8.86
21.04/11.23  21.69/11.43  23.58/12.21  25.32/12.95  26.95/13.65  28.48/14.32
31.32/15.56  35.15/17.26

!  Diversion 16566 Basin  RC  Name:  Murray Blvd Diverson
RC16566_Divn= 0.00/0.00   0.20/0.00    0.72/0.00    1.45/0.13    1.94/0.49
2.52/0.97    3.06/1.42    3.51/1.69    3.81/1.84    4.09/1.97    4.84/2.33
5.49/2.64    6.07/2.91

!  Diversion 16578 Basin  RC  Name:  Stoddard Dr Diversion
RC16578_Divn= 0.00/0.00   1.53/0.78    5.75/2.94   11.88/6.08   17.63/9.03
20.50/10.50  20.52/10.50  22.19/11.35  23.75/12.15  25.21/12.89  26.59/13.59
29.16/14.90  32.63/16.68

!  Diversion 17992 Basin  RC  Name:  185th Ave Diversion
RC17992_Divn= 0.00/0.00   1.12/0.00    2.46/0.00    4.47/0.00    6.48/0.00
8.93/0.00   14.94/0.20   18.25/0.61   21.23/1.13   26.38/2.48   29.10/3.08
33.82/3.57   37.95/4.01

!  Diversion 18260 Basin  RC  Name:  Fairmont Dr Diversion
RC18260_Divn= 0.00/0.00   0.17/0.07    0.63/0.26    1.21/0.47    1.70/0.60
1.84/0.67    2.10/0.79    2.33/0.90    2.53/0.99    2.82/1.12    3.07/1.23
3.93/1.61    4.30/1.77

!  Diversion 18263 Basin  RC  Name:  Erickson St Diversion
RC18263_Divn= 0.00/0.00   0.24/0.00    0.85/0.00    1.54/0.00    1.76/0.06
2.20/0.25    2.68/0.52    3.38/0.82    4.20/1.31    4.66/1.46    5.27/1.67
5.82/1.85    7.62/2.45

!  Diversion 18344 Basin  RC  Name:  Pearl St Diversion
RC18344_Divn= 0.00/0.00   0.52/0.25    1.80/0.91    3.60/1.67    4.91/1.81
5.71/1.84    5.96/1.89    6.04/1.91    6.20/1.94    6.43/1.98    6.65/2.03
7.47/2.20

!  Diversion 20083 Basin  RC  Name:  Rock Creek PS Diversion
RC20083_Divn= 0.00/0.00  10.00/3.38   20.00/6.76   30.00/10.14  40.00/13.51
60.00/20.27  80.00/27.03 100.00/33.78 120.00/40.54 140.00/47.30 160.00/54.05
180.00/60.81 200.00/67.57
```

```
!  Diversion 22342 Basin  RC  Name:  Golf Course Diversion
RC22342_Divn= 0.00/0.00   0.70/0.00    2.79/0.00    5.92/0.00   10.18/0.60
12.93/1.26   17.32/2.69   21.24/4.18   23.01/5.60   36.09/8.22   44.02/8.66
52.60/9.22   66.32/10.24

!  Diversion 23959 Basin  RC  Name:  Willow Cr Trunk
RC23959_Divn= 0.00/0.00   0.64/0.64    2.54/2.54    5.97/5.41    9.88/8.74
15.40/12.56  20.69/15.58  23.89/16.85  29.37/18.71  33.06/21.15  91.80/25.33
109.93/28.92

!  Diversion 23964 Basin  RC  Name:  Willow Cr Trunk
RC23964_Divn= 0.00/0.00   0.62/0.48    2.97/2.38   12.18/9.52   24.95/19.03
37.27/28.55  40.39/30.92  55.84/42.82  62.52/47.58  94.70/58.47 116.69/67.63
134.85/75.68 165.08/89.65

!  Diversion 23967 Basin  RC  Name:  Willow Cr Trunk
RC23967_Divn= 0.00/0.00   1.53/0.64    6.12/2.58   12.24/5.16   18.36/7.74
24.18/10.19  30.60/12.90  54.36/34.72  68.77/47.38  80.32/57.31  99.18/73.23
114.85/86.27 128.57/97.57

!  Diversion 23973 Basin  RC  Name:  Willow Cr Trunk
RC23973_Divn= 0.00/0.00   1.90/0.74    7.61/2.94   15.23/5.88   24.75/9.56
34.26/13.23  40.36/15.59  59.29/25.14  67.41/28.98  81.23/35.43  93.01/40.88
112.95/50.03

!  Diversion 23977 Basin  RC  Name:  Willow Cr Trunk
RC23977_Divn= 0.00/0.00   1.57/0.15    6.26/0.58   12.53/1.17   18.79/1.75
24.74/2.30   29.76/2.77   31.32/2.91   52.51/14.85  65.86/20.80  76.79/25.39
94.86/32.70 109.96/38.64

!  Diversion 23983 Basin  RC  Name:  Willow Cr Trunk
RC23983_Divn= 0.00/0.00   2.44/0.51    9.69/1.95   19.71/4.24   31.84/6.70
38.28/7.71   45.57/8.82   50.26/11.57  67.68/13.99  81.39/16.06  93.07/17.88
112.85/21.06 129.64/23.82

!  Diversion 25677 Basin  RC  Name:  Butternut Cr Trunk
RC25677_Divn= 0.00/0.00   0.91/0.00    3.64/0.00    7.10/0.00    9.10/0.00
12.75/0.00   15.57/0.00   17.95/0.00   23.69/0.00   29.67/0.00   36.89/2.27
44.14/7.29   46.60/7.64

!  Diversion 28053 Basin  RC  Name:  185th Ave Trunk
RC28053_Divn= 0.00/0.00   2.63/0.00    5.15/0.01    7.56/0.98   11.74/2.56
12.99/2.76   16.16/3.27   19.60/3.86   21.11/4.12   22.52/4.36   23.84/4.60
25.10/4.82


!  PUMPING STATIONS
!  Pumping Station Configurations

!  Command paragraphs named according to USA pumping station number
!  Pumping station numbers used as manhole numbers in the model

[PUM]

!  Upper Tualatin/Sherwood (DR)
11664_PumpDR=1   1554   0   5.79   1   1554   0   5.79

!  Hillsboro WWTP (HL)
12039_PumpHL=2   210.6   0   8.13   2   280.8   70.2   8.13   2   351   140.4   8.13

!  Beaverton PS (DR)
12681_PumpDR=2   28.3   0   1.3   2   28.3   0   1.3

!  Aloha #3 (RC)
12682_PumpRC=2   125   0   2.23   2   250   125   8.91   2   500   250   12.25

!  RC Highlands #6 (RC)
12686_PumpRC=1   20   0   0.9   1   40   0   0.9
```

```
!  Cornelius  (FG)
12743_PumpFG=1   251.3   0   6.24   1   251.3   0   5.59

!  North Plains (HL)
!  (existing configuration is 2 pumps operating at 700 gpm each)
!  (start/stop volumes caluculated from station design drawings)
!  (wet well sized to handle 2 x 1000 gpm pumps)
13599_PumpHL=1   45   19   1.56   1   121   19   1.56

!  Bendemeer #1 (RC)
13778_PumpRC=1   471.2   0   5.55   1   549.8   314.2   5.55

!  Bendemeer #2 (RC)
13782_PumpRC=1   392.7   0   4.34   1   471.2   0   4.34

!  Bendemeer #3 (RC)
13795_PumpRC=1   65.1   0   0.85   1   93.4   0    0.85

!  SW Bull Mtn. (DR)
15068_PumpDR=1   665.2   0   4.01   1   712.7   0   4.01

!  Country Haven (RC)
16251_PumpRC=1   97.6   0   0.71   1   117.2   0   0.71

!  Gaston       (FG)
17599_PumpFG=1   161.4   0   1.56   1   188.3   0   1.56

!  Cipole (DR)
17795_PumpDR=1   296.6   0   1.29   1   346.8   0   1.29

!  Hillsboro # 49 (HL)
19864_PumpHL=1   20   0   1.35   1   40   0   1.35

!  Rock Creek WWTP (RC)
20083_PumpRC=2   1500   1000   34   2   2500   1000   34   2   3000   1000   68

!  Rock Creek WWTP (RC)
20084_PumpRC=2   750   500   17.3   2   1250   500   17.3   2   1500   500   34.7

!  Aloha #3 (RC)
21795_PumpRC=2   125   0   2.23   2   250   125   8.91   2   500   250   12.25

!  Banks #1 (HL)
! (original pumping station)
! (station operating limit of 1.06 mgd)
22037_PumpHL=2   50.0   0   1.64

!  Banks #2 (HL)
26891_PumpHL=1   622.0   0   1.1    1   735.0     0.0   1.6

!  Tektronix (DR)
!  (total station rating of 3250 gpm)
27865_PumpDR=2  1830.0  771.0  5.0  2  2096.0  771.0  2.2



PUM_DEFAULT=2 0.0000 0.0000 100.0000 0 0.0000 0.0000 0.0000 0 0.0000 0.0000 0.0000
```

```
Project.Des for Hillsboro Basin

!  DESIGN FILE FOR CLEAN WATER SERVICES MASTER PLAN MODEL (07/2008)
!  SYSTEM FACTORS AND DESIGN CRITERIA
!  MODIFIED FROM USA 2000 MASTER PLAN MODEL (01/2001)

!  Modified for Re-calibration of Hillsboro East - 04/2006 - Revised and deleted
diversion curves from HL to RC
!  Modified for Hillsboro East Interceptor Calibration - 10/02/03 - Added DIU Curves

!  Shifted curves for April 21-24, 1996 Storm Event Test Run
!  Moved last 3 hours to beginning of diurnal curve to simulate hour 21 start time

!  DESIGN PIPE DATA
!  (Mininum velocity changed to 2.0 fps from 1995 value)
[DPI]
Default=0.013  8  8  7  2.3  0.0010  0.8  120 0

!  DESIGN PIPE PRESSURE DATA
[PRE]
Default=100  0  5 0 0

!  EXISTING PIPE DATA
[EPI]
Default=0.013 2 0.9 0 0 0
Special=0.015 2 0.9 0 0 0

!  MANHOLE DEFAULT DATA
[MAN]
Default=2  4  4  0

!  DIURNAL CURVES
!  Unit Diurnal Curves for Weekdays/Weekends
!  by Basin Type & Confidence Level
!  Originally generated March 3, 1995

[DIU]

!  Basin Type 1 - Weekday Diurnal Hydrograph - Median
DIU_1WDMed=0.51 0.28 0.21 0.21 0.24 0.41 1.25 2.20 1.97 1.57 1.37 1.20 1.02 0.93
0.82 0.80 0.84 0.98 1.19 1.34 1.36 1.33 1.20 0.87

!  Basin Type 2 - Weekday Diurnal Hydrograph - Median
DIU_2WDMed=0.58 0.39 0.31 0.29 0.31 0.52 1.21 1.77 1.60 1.40 1.31 1.19 1.08 1.02
0.95 0.91 0.95 1.06 1.21 1.28 1.28 1.24 1.14 0.88

!  Basin Type 3 - Weekday Diurnal Hydrograph - Median
DIU_3WDMed=0.59 0.40 0.32 0.29 0.29 0.43 0.98 1.63 1.60 1.44 1.37 1.27 1.15 1.06
0.99 0.94 0.96 1.05 1.19 1.27 1.28 1.25 1.15 0.89

!  Basin Type 4 - Weekday Diurnal Hydrograph - Median
DIU_4WDMed=0.55 0.41 0.35 0.31 0.32 0.39 0.70 1.15 1.30 1.43 1.53 1.44 1.36 1.30
1.26 1.16 1.12 1.13 1.16 1.16 1.18 1.10 1.01 0.79

!  Additional Curves

!  Monitor R037A Diurnal Curve - Weekday - Mostly Commercial
DIU_R037A=0.684 0.593 0.558 0.534 0.545 0.651 0.975 1.203 1.228 1.260 1.248 1.202
1.205 1.137 1.110 1.138 1.198 1.232 1.186 1.115 1.075 1.077 1.000 0.844

! Monitor R036A Diurnal Curve - Weekday  - Almost Completely Residential
DIU_R036A=0.676 0.375 0.231 0.192 0.242 0.399 1.018 1.802 1.865 1.486 1.259 1.208
1.020 0.965 0.861 0.887 0.922 1.042 1.233 1.342 1.363 1.328 1.276 1.009

! Monitor H001 Old - Weekday - Mixture
DIU_H001=0.674 0.533 0.492 0.451 0.462 0.561 0.905 1.203 1.277 1.235 1.308 1.261
1.128 1.235 1.312 1.285 1.074 1.074 1.221 1.198 1.214 1.109 0.961 0.822

! Monitor H004 Old - Weekday - Mixture
DIU_H004=0.731 0.618 0.550 0.491 0.512 0.619 0.809 1.057 1.200 1.280 1.326 1.323
```

```
1.329 1.312 1.304 1.257 1.138 1.090 1.158 1.160 1.080 1.003 0.909 0.752

! Monitor 12325 New - Weekday - Mixture
DIU_12325=0.555 0.407 0.330 0.273 0.279 0.319 0.462 0.753 1.102 1.411 1.537 1.625
1.591 1.506 1.343 1.258 1.375 1.262 1.334 1.318 1.182 1.070 0.966 0.753

! Monitor 68368 New - Weekday - Mixture
DIU_68368=0.668 0.581 0.526 0.506 0.556 0.653 0.810 1.003 1.195 1.327 1.400 1.379
1.251 1.302 1.199 1.102 1.086 1.171 1.250 1.195 1.157 1.033 0.887 0.766

! Monitor H008 New - Weekday - Mixture
DIU_H008=0.947 0.689 0.610 0.642 0.607 0.654 0.930 0.910 1.156 1.157 1.220 1.193
1.222 1.093 1.021 1.138 1.092 1.075 1.155 1.098 1.084 1.112 1.120 1.074

!   DIVERSION DETAILS

[DIV]

DiversionOff= 0.00/0.00 100.00/0.00

!  Diversion 19808 Basin  HL  Name:  W Main St Diversion
!  Flow Split
!  HL19808_Divn= 0.00/0.00   0.30/0.30    1.45/1.04    2.46/1.32    4.72/1.52
5.74/1.71    6.98/1.88    7.68/2.03    9.98/2.56   11.84/3.00   13.45/3.38
!  REVISED DIVERSION CURVE
HL19808_Divn= 0.00/0.00   0.01/0.01 0.05/0.024 0.10/0.039 0.20/0.068 0.50/0.12
1.00/0.20 1.50/0.26 2.00/0.32 2.50/0.40 3.00/0.50 4.00/0.84
DEFAULT=0.000 0.000 20.000 0.000 40.000 0.000 60.000 0.000 80.000 0.000 100.000
0.000
COUNCILCRDIV=0.000 0.000 10.500 10.500 20.000 10.500 30.000 10.500 40.000 10.500
50.000 10.500 60.000 10.500 70.000 10.500
NO_DIV=0.000 0.000 10.000 0.000 20.000 0.000 30.000 0.000 40.000 0.000 50.000 0.000

!  PUMPING STATIONS
!  Pumping Station Configurations

!  Command paragraphs named according to USA pumping station number
!  Pumping station numbers used as manhole numbers in the model

[PUM]

!  Hillsboro WWTP (HL)
12039_PumpHL=2   210.6   0   8.13   2   280.8   70.2   8.13   2   351   140.4   8.13

!  North Plains (HL)
!  (existing configuration is 2 pumps operating at 700 gpm each)
!  (start/stop volumes caluculated from station design drawings)
!  (wet well sized to handle 2 x 1000 gpm pumps)
!13599_PumpHL=1   45   19   1.56   1   121   19   1.56
!13599_PumpHL=2   45   19   2.49
! Revise total station capacity using 60% of second pump
13599_PumpHL=2   45   19   1.56   2   121   19   0.94

!  Banks #1 (HL)
! (original pumping station)
! (station operating limit of 1.06 mgd)
22037_PumpHL=2   50.0   0   1.64

!  Banks #2 (HL)
!26891_PumpHL=1   622.0   0   1.1    1   735.0     0.0   1.6
! Revised total station capacity using 60% of second pump
26891_PumpHL=2   622.0   0   2.06

PUM_DEFAULT=2 0.0000 0.0000 100.0000 0 0.0000 0.0000 0.0000 0 0.0000 0.0000 0.0000

26215_PumpHL=2 379.4000 157.0000 1.2930 2 536.4000 157.0000 1.2930 0 0.0000 0.0000
0.0000
```

```
Project.Des for Rock Creek Basin

!  DESIGN FILE FOR CLEAN WATER SERVICES MASTER PLAN MODEL (07/2008)
!  SYSTEM FACTORS AND DESIGN CRITERIA
!  MODIFIED FROM USA 2000 MASTER PLAN UPDATE (01/2001)

!  Modified for Re-calibration of Hillsboro East - 04/2006 - Revised and deleted
diversion curves from HL to RC
!  Modified for Hillsboro East Interceptor Calibration - 10/02/03 - Added DIU Curves

!  DESIGN PIPE DATA
!  (Mininum velocity changed to 2.0 fps from 1995 value)
[DPI]
Default=0.013  8  8  7  2.3  0.0010  0.8  120 0

!  DESIGN PIPE PRESSURE DATA
[PRE]
Default=100  0  5 0 0

!  EXISTING PIPE DATA
[EPI]
Default=0.013 2 0.9 0 0 0

!  MANHOLE DEFAULT DATA
[MAN]
Default=2  4  4  0

!  DIURNAL CURVES
!  Unit Diurnal Curves for Weekdays/Weekends
!  by Basin Type & Confidence Level
!  Originally generated March 3, 1995

[DIU]

!  Basin Type 1 - Weekday Diurnal Hydrograph - Median
DIU_1WDMed=0.51 0.28 0.21 0.21 0.24 0.41 1.25 2.20 1.97 1.57 1.37 1.20 1.02 0.93
0.82 0.80 0.84 0.98 1.19 1.34 1.36 1.33 1.20 0.87

!  Basin Type 2 - Weekday Diurnal Hydrograph - Median
DIU_2WDMed=0.58 0.39 0.31 0.29 0.31 0.52 1.21 1.77 1.60 1.40 1.31 1.19 1.08 1.02
0.95 0.91 0.95 1.06 1.21 1.28 1.28 1.24 1.14 0.88

!  Basin Type 3 - Weekday Diurnal Hydrograph - Median
DIU_3WDMed=0.59 0.40 0.32 0.29 0.29 0.43 0.98 1.63 1.60 1.44 1.37 1.27 1.15 1.06
0.99 0.94 0.96 1.05 1.19 1.27 1.28 1.25 1.15 0.89

!  Basin Type 4 - Weekday Diurnal Hydrograph - Median
DIU_4WDMed=0.55 0.41 0.35 0.31 0.32 0.39 0.70 1.15 1.30 1.43 1.53 1.44 1.36 1.30
1.26 1.16 1.12 1.13 1.16 1.16 1.18 1.10 1.01 0.79

!  Additional Curves

!  Monitor R037A Diurnal Curve - Weekday - Mostly Commercial
DIU_R037A=0.684 0.593 0.558 0.534 0.545 0.651 0.975 1.203 1.228 1.260 1.248 1.202
1.205 1.137 1.110 1.138 1.198 1.232 1.186 1.115 1.075 1.077 1.000 0.844

! Monitor R036A Diurnal Curve - Weekday  - Almost Completely Residential
DIU_R036A=0.338 0.150 0.035 0.010 0.073 0.598 2.036 2.703 2.238 1.337 1.133 1.088
0.714 0.579 0.517 0.532 0.645 0.937 1.480 1.611 1.636 1.461 1.149 0.707

! Monitor R036B Diurnal Curve - Weekday  - Mixed Use
DIU_R036B=0.594 0.431 0.351 0.313 0.395 0.753 1.559 1.620 1.481 1.326 1.218 1.118
1.057 0.991 0.958 0.982 1.136 1.404 1.524 1.488 1.355 1.217 1.009 0.724

! Monitor R037C Diurnal Curve - Weekday  - Mixed Use
DIU_R037C=0.483 0.234 0.089 0.042 0.128 0.685 1.518 2.212 1.813 1.297 1.072 0.929
0.834 0.771 0.723 0.717 0.770 0.923 1.141 1.280 1.294 1.223 1.027 0.757

! Monitor H001 Old - Weekday - Mixture
DIU_H001=0.674 0.533 0.492 0.451 0.462 0.561 0.905 1.203 1.277 1.235 1.308 1.261
```

```
1.128 1.235 1.312 1.285 1.074 1.074 1.221 1.198 1.214 1.109 0.961 0.822

! Monitor H004 Old - Weekday - Mixture
DIU_H004=0.731 0.618 0.550 0.491 0.512 0.619 0.809 1.057 1.200 1.280 1.326 1.323
1.329 1.312 1.304 1.257 1.138 1.090 1.158 1.160 1.080 1.003 0.909 0.752

! Monitor 12325 New - Weekday - Mixture
DIU_12325=0.555 0.407 0.330 0.273 0.279 0.319 0.462 0.753 1.102 1.411 1.537 1.625
1.591 1.506 1.343 1.258 1.375 1.262 1.334 1.318 1.182 1.070 0.966 0.753

! Monitor 68368 New - Weekday - Mixture
DIU_68368=0.668 0.581 0.526 0.506 0.556 0.653 0.810 1.003 1.195 1.327 1.400 1.379
1.251 1.302 1.199 1.102 1.086 1.171 1.250 1.195 1.157 1.033 0.887 0.766

! Monitor H008 New - Weekday - Mixture
DIU_H008=0.947 0.689 0.610 0.642 0.607 0.654 0.930 0.910 1.156 1.157 1.220 1.193
1.222 1.093 1.021 1.138 1.092 1.075 1.155 1.098 1.084 1.112 1.120 1.074

!   DIVERSION DETAILS

[DIV]

!  Diversion  7925 Basin  RC  Name:  SW Madeline St Diversion
RC07925_Divn= 0.00/0.00   0.38/0.34    2.13/1.18    3.52/1.49    7.20/1.82
8.87/2.10    9.79/2.34   12.25/2.95   14.28/3.46   15.20/3.68   16.07/3.90

!  Diversion 12682 Basin  RC  Name:  Aloha PS #3 Diversion Future
RC12682_Divn= 0.00/0.00   9.47/9.47   22.19/22.19  28.40/28.40  48.31/48.31
72.46/72.46  90.37/90.37

!  Diversion 12682 Basin  RC  Name:  Aloha PS #3 Diversion Existing
RC12682DivEx= 0.00/0.00   0.59/0.30    1.18/0.59    2.66/1.33    4.73/2.37
5.92/2.96    9.47/4.73   14.79/7.40   22.19/11.09  28.40/14.20  48.31/24.15
72.46/36.23  90.37/45.19


!  Diversion 16250 Basin  RC  Name:  198th Ave Diversion
RC16250_Divn= 0.00/0.00   1.07/0.32    5.17/2.27   11.19/5.40   17.45/8.86
21.04/11.23  21.69/11.43  23.58/12.21  25.32/12.95  26.95/13.65  28.48/14.32
31.32/15.56  35.15/17.26

!  Diversion 16566 Basin  RC  Name:  Murray Blvd Diverson
RC16566_Divn= 0.00/0.00   0.20/0.00    0.72/0.00    1.45/0.13    1.94/0.49
2.52/0.97    3.06/1.42    3.51/1.69    3.81/1.84    4.09/1.97    4.84/2.33
5.49/2.64    6.07/2.91

!  Diversion 16578 Basin  RC  Name:  Stoddard Dr Diversion
RC16578_Divn= 0.00/0.00   1.53/0.78    5.75/2.94   11.88/6.08   17.63/9.03
20.50/10.50  20.52/10.50  22.19/11.35  23.75/12.15  25.21/12.89  26.59/13.59
29.16/14.90  32.63/16.68

!  Diversion 17992 Basin  RC  Name:  185th Ave Diversion
RC17992_Divn= 0.00/0.00   1.12/0.00    2.46/0.00    4.47/0.00    6.48/0.00
8.93/0.00   14.94/0.20   18.25/0.61   21.23/1.13   26.38/2.48   29.10/3.08
33.82/3.57   37.95/4.01

!  Diversion 18260 Basin  RC  Name:  Fairmont Dr Diversion
RC18260_Divn= 0.00/0.00   0.17/0.07    0.63/0.26    1.21/0.47    1.70/0.60
1.84/0.67    2.10/0.79    2.33/0.90    2.53/0.99    2.82/1.12    3.07/1.23
3.93/1.61    4.30/1.77

!  Diversion 18263 Basin  RC  Name:  Erickson St Diversion
RC18263_Divn= 0.00/0.00   0.24/0.00    0.85/0.00    1.54/0.00    1.76/0.06
2.20/0.25    2.68/0.52    3.38/0.82    4.20/1.31    4.66/1.46    5.27/1.67
5.82/1.85    7.62/2.45

!  Diversion 18344 Basin  RC  Name:  Pearl St Diversion
RC18344_Divn= 0.00/0.00   0.52/0.25    1.80/0.91    3.60/1.67    4.91/1.81
5.71/1.84    5.96/1.89    6.04/1.91    6.20/1.94    6.43/1.98    6.65/2.03
7.47/2.20
```

```
!  Diversion 20083 Basin  RC  Name:  Rock Creek PS Diversion
RC20083_Divn= 0.00/0.00  10.00/3.38   20.00/6.76   30.00/10.14  40.00/13.51
60.00/20.27  80.00/27.03 100.00/33.78 120.00/40.54 140.00/47.30 160.00/54.05
180.00/60.81 200.00/67.57

!  Diversion 22342 Basin  RC  Name:  Golf Course Diversion
RC22342_Divn= 0.00/0.00   0.70/0.00    2.79/0.00    5.92/0.00   10.18/0.60
12.93/1.26   17.32/2.69   21.24/4.18   23.01/5.60   36.09/8.22   44.02/8.66
52.60/9.22   66.32/10.24

!  Diversion 23959 Basin  RC  Name:  Willow Cr Trunk
RC23959_Divn= 0.00/0.00   0.64/0.64    2.54/2.54    5.97/5.41    9.88/8.74
15.40/12.56  20.69/15.58  23.89/16.85  29.37/18.71  33.06/21.15  91.80/25.33
109.93/28.92

!  Diversion 23964 Basin  RC  Name:  Willow Cr Trunk
RC23964_Divn= 0.00/0.00   0.62/0.48    2.97/2.38   12.18/9.52   24.95/19.03
37.27/28.55  40.39/30.92  55.84/42.82  62.52/47.58  94.70/58.47 116.69/67.63
134.85/75.68 165.08/89.65

!  Diversion 23967 Basin  RC  Name:  Willow Cr Trunk
RC23967_Divn= 0.00/0.00   1.53/0.64    6.12/2.58   12.24/5.16   18.36/7.74
24.18/10.19  30.60/12.90  54.36/34.72  68.77/47.38  80.32/57.31  99.18/73.23
114.85/86.27 128.57/97.57

!  Diversion 23973 Basin  RC  Name:  Willow Cr Trunk
RC23973_Divn= 0.00/0.00   1.90/0.74    7.61/2.94   15.23/5.88   24.75/9.56
34.26/13.23  40.36/15.59  59.29/25.14  67.41/28.98  81.23/35.43  93.01/40.88
112.95/50.03

!  Diversion 23977 Basin  RC  Name:  Willow Cr Trunk
RC23977_Divn= 0.00/0.00   1.57/0.15    6.26/0.58   12.53/1.17   18.79/1.75
24.74/2.30   29.76/2.77   31.32/2.91   52.51/14.85  65.86/20.80  76.79/25.39
94.86/32.70 109.96/38.64

!  Diversion 23983 Basin  RC  Name:  Willow Cr Trunk
RC23983_Divn= 0.00/0.00   2.44/0.51    9.69/1.95   19.71/4.24   31.84/6.70
38.28/7.71   45.57/8.82   50.26/11.57  67.68/13.99  81.39/16.06  93.07/17.88
112.85/21.06 129.64/23.82

!  Diversion 25677 Basin  RC  Name:  Butternut Cr Trunk
RC25677_Divn= 0.00/0.00   0.91/0.00    3.64/0.00    7.10/0.00    9.10/0.00
12.75/0.00   15.57/0.00   17.95/0.00   23.69/0.00   29.67/0.00   36.89/2.27
44.14/7.29   46.60/7.64

!  Diversion 28053 Basin  RC  Name:  185th Ave Trunk
RC28053_Divn= 0.00/0.00   2.63/0.00    5.15/0.01    7.56/0.98   11.74/2.56
12.99/2.76   16.16/3.27   19.60/3.86   21.11/4.12   22.52/4.36   23.84/4.60
25.10/4.82
DIV_19640=0.000 0.000 10.000 0.000 20.000 0.000 30.000 0.000 40.000 0.000
RC00571_DIVN=0.000 0.000 10.000 0.000 30.000 0.000 30.000 0.000 40.000 0.000
RC55970_DIVN=0.000 0.000 10.000 0.000 20.000 0.000 30.000 0.000 40.000 0.000


!  PUMPING STATIONS
!  Pumping Station Configurations

!  Command paragraphs named according to USA pumping station number
!  Pumping station numbers used as manhole numbers in the model

[PUM]

!  Aloha #3 (RC)
12682_PumpRC=2   125   0   2.23   2   250   125   8.91   2   500   250   12.25

!  RC Highlands #6 (RC)
12686_PumpRC=1   20   0   0.9   1   40   0   0.9

!  Bendemeer #1 (RC)
```

```
13778_PumpRC=1   471.2   0   5.55   1   549.8   314.2   5.55

!  Bendemeer #2 (RC)
13782_PumpRC=1   392.7   0   4.34   1   471.2   0   4.34

!  Bendemeer #3 (RC)
13795_PumpRC=1   65.1   0   0.85   1   93.4   0    0.85

!  Country Haven (RC)
16251_PumpRC=1   97.6   0   0.71   1   117.2   0   0.71

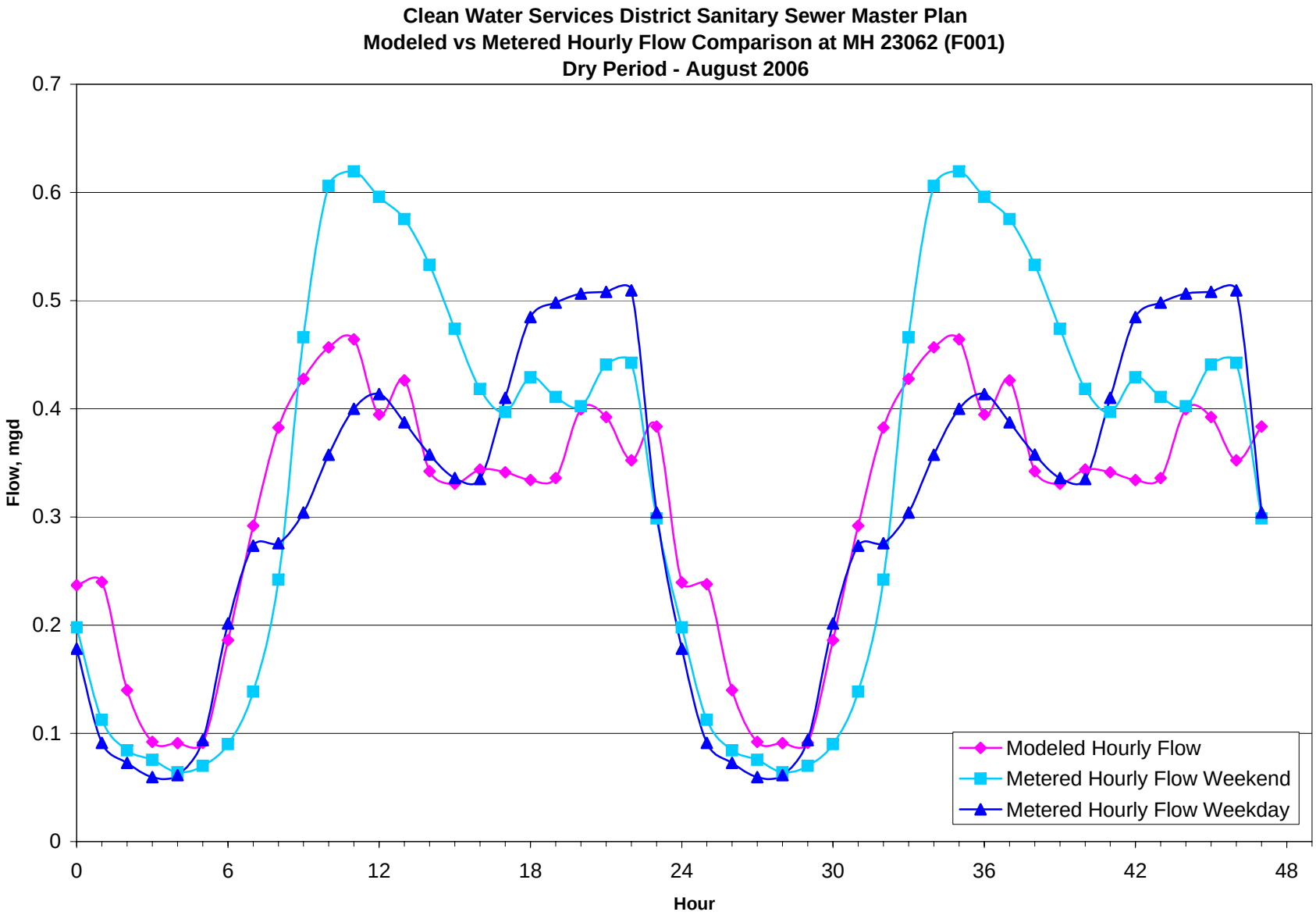
!  Rock Creek WWTP (RC)
20083_PumpRC=2   1500   1000   34   2   2500   1000   34   2   3000   1000   68

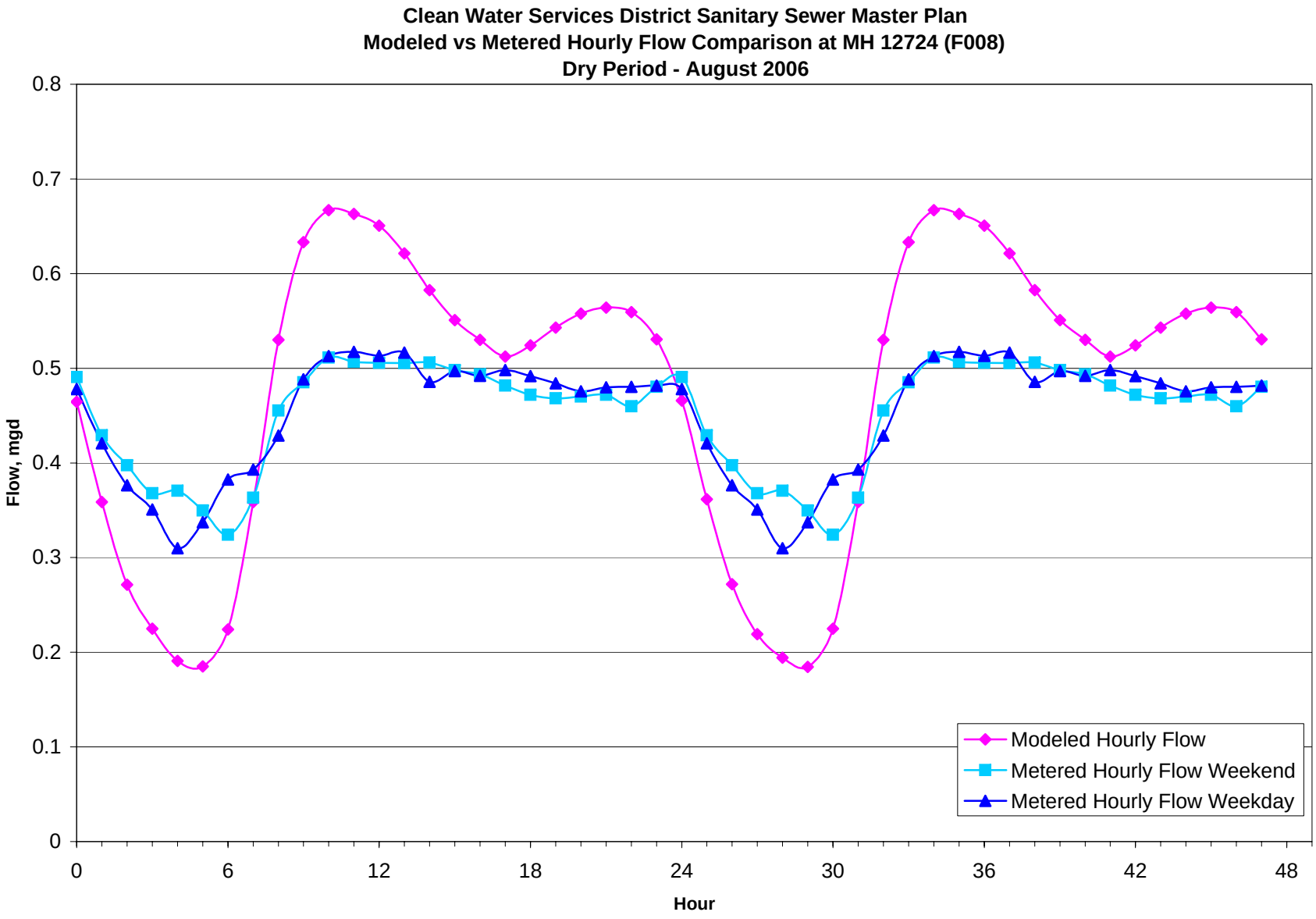
!  Rock Creek WWTP (RC)
20084_PumpRC=2   750   500   17.3   2   1250   500   17.3   2   1500   500   34.7

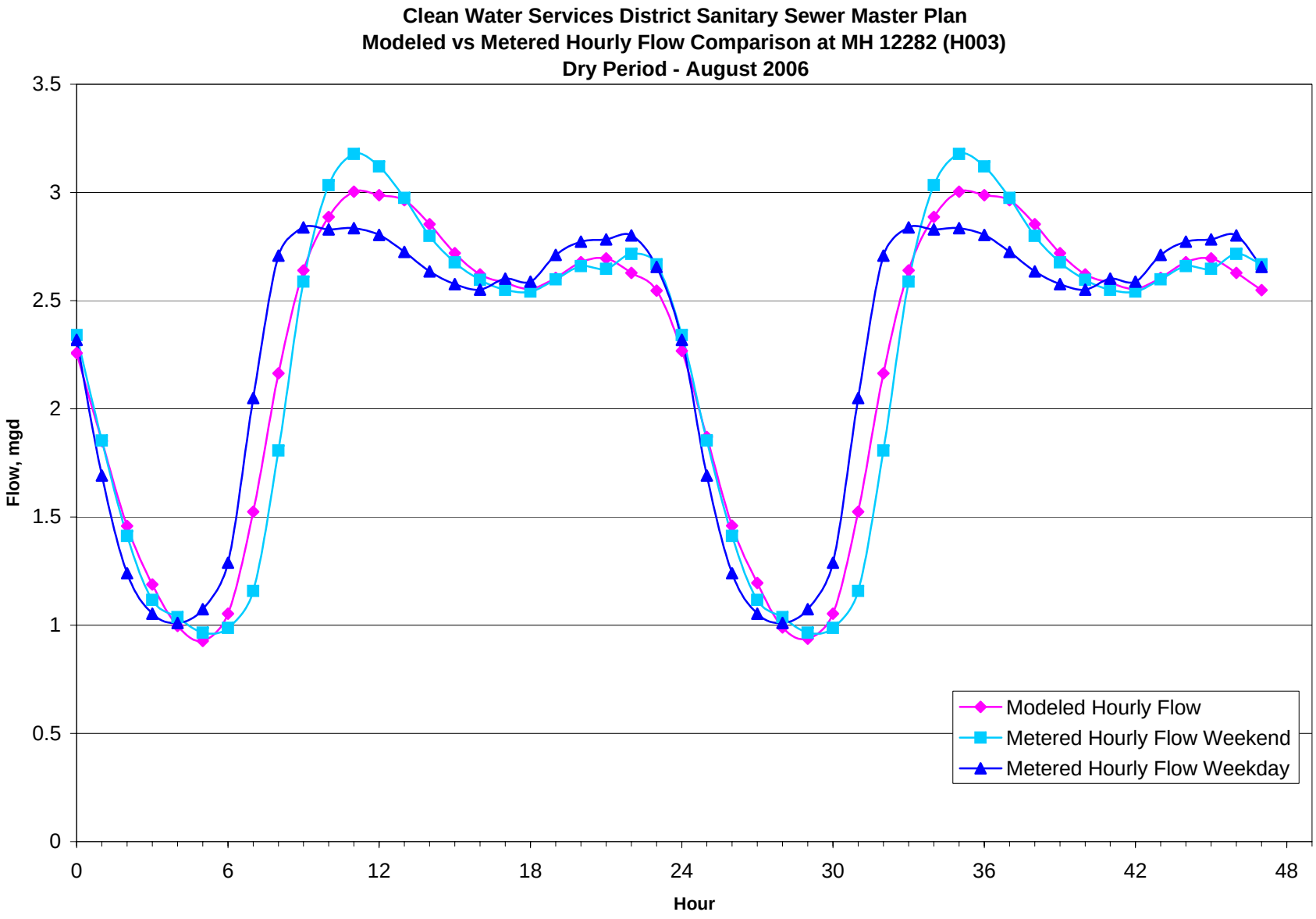
!  Aloha #3 (RC)
21795_PumpRC=2   125   0   2.23   2   250   125   8.91   2   500   250   12.25
PUM_DEFAULT=2 0.0000 0.0000 100.0000 0 0.0000 0.0000 0.0000 0 0.0000 0.0000 0.0000
```

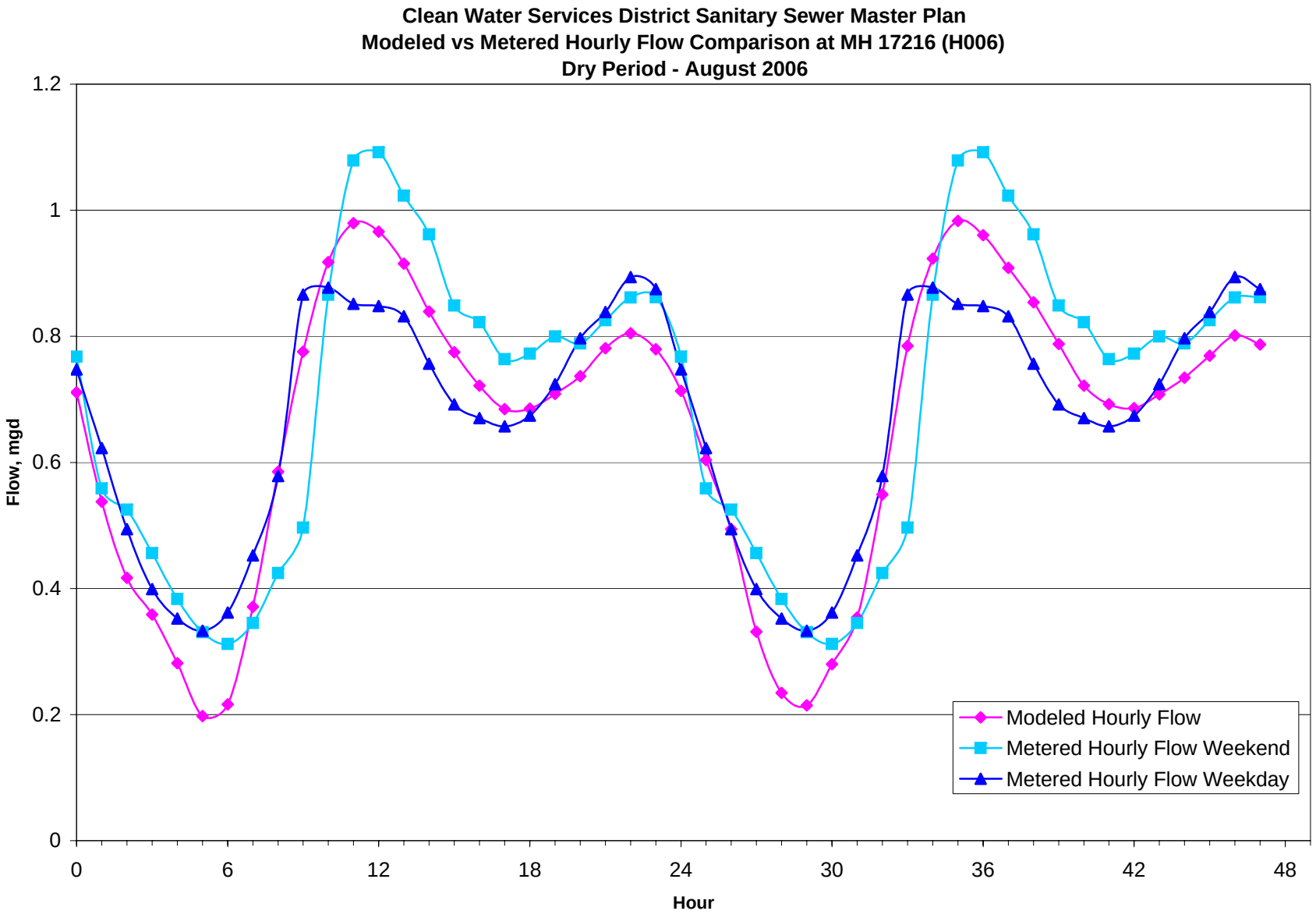
APPENDIX K

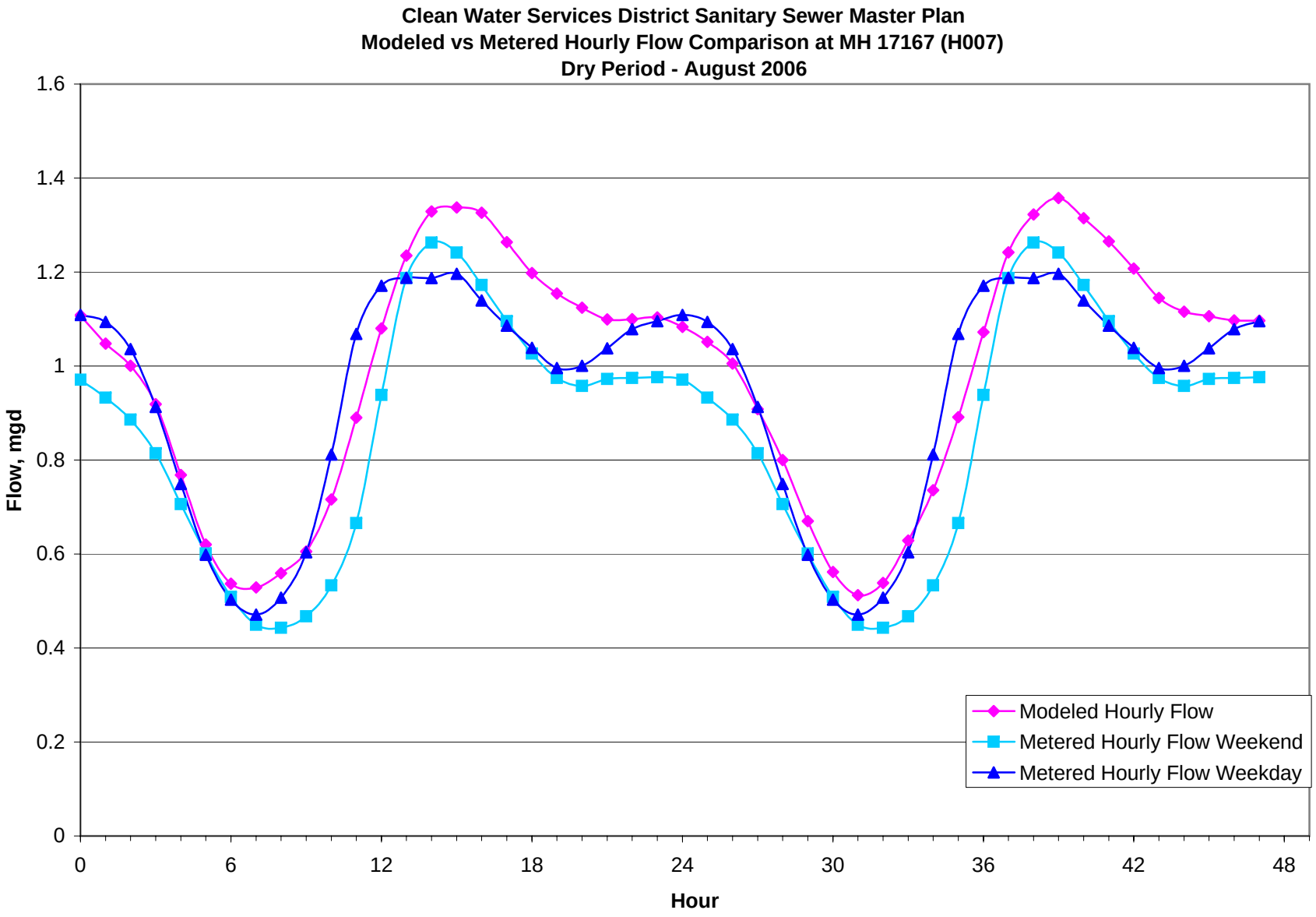
Dry Weather Flow Calibration Results

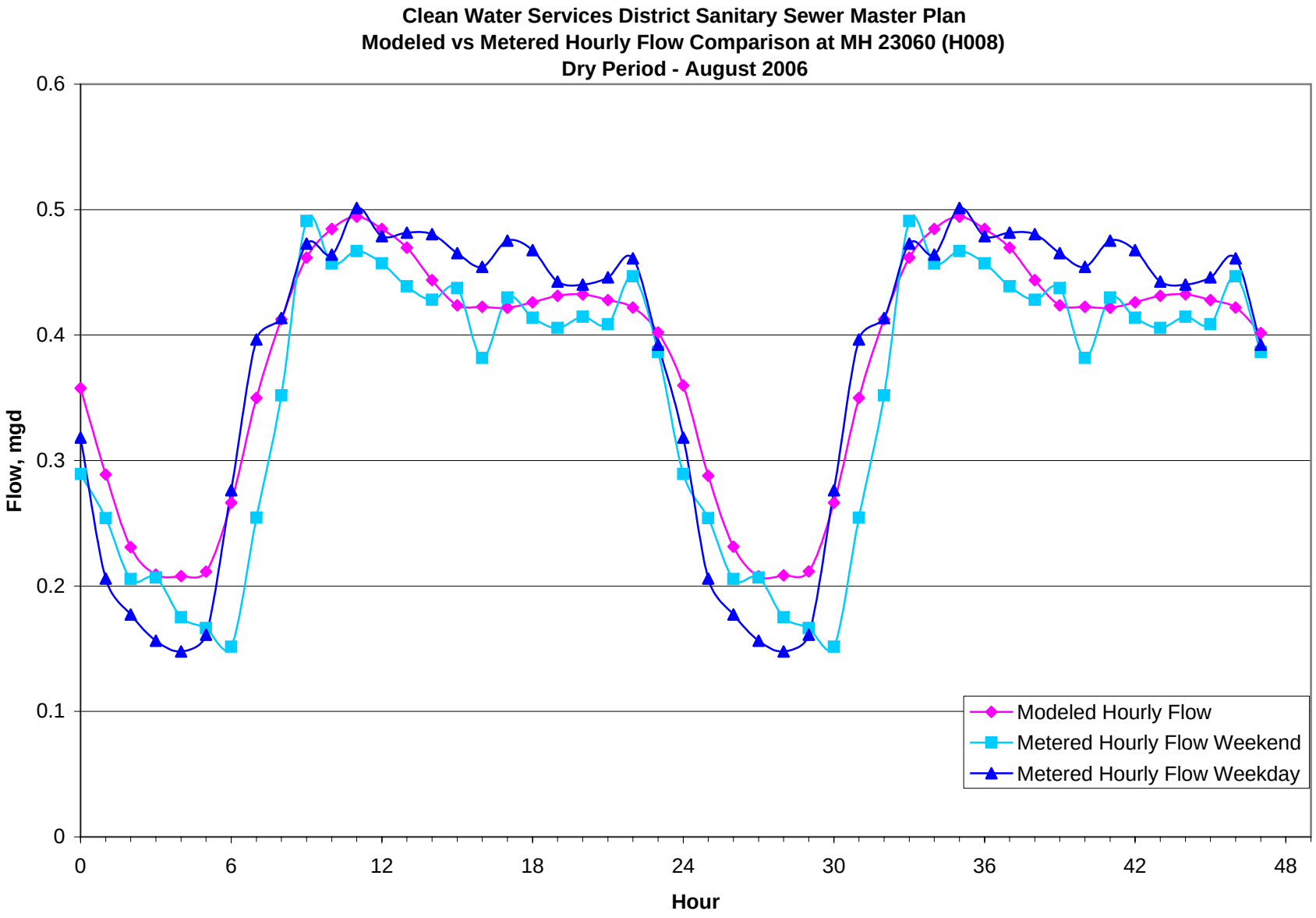

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 23062 (F001)
Dry Period - August 2006
Flow, mgd
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

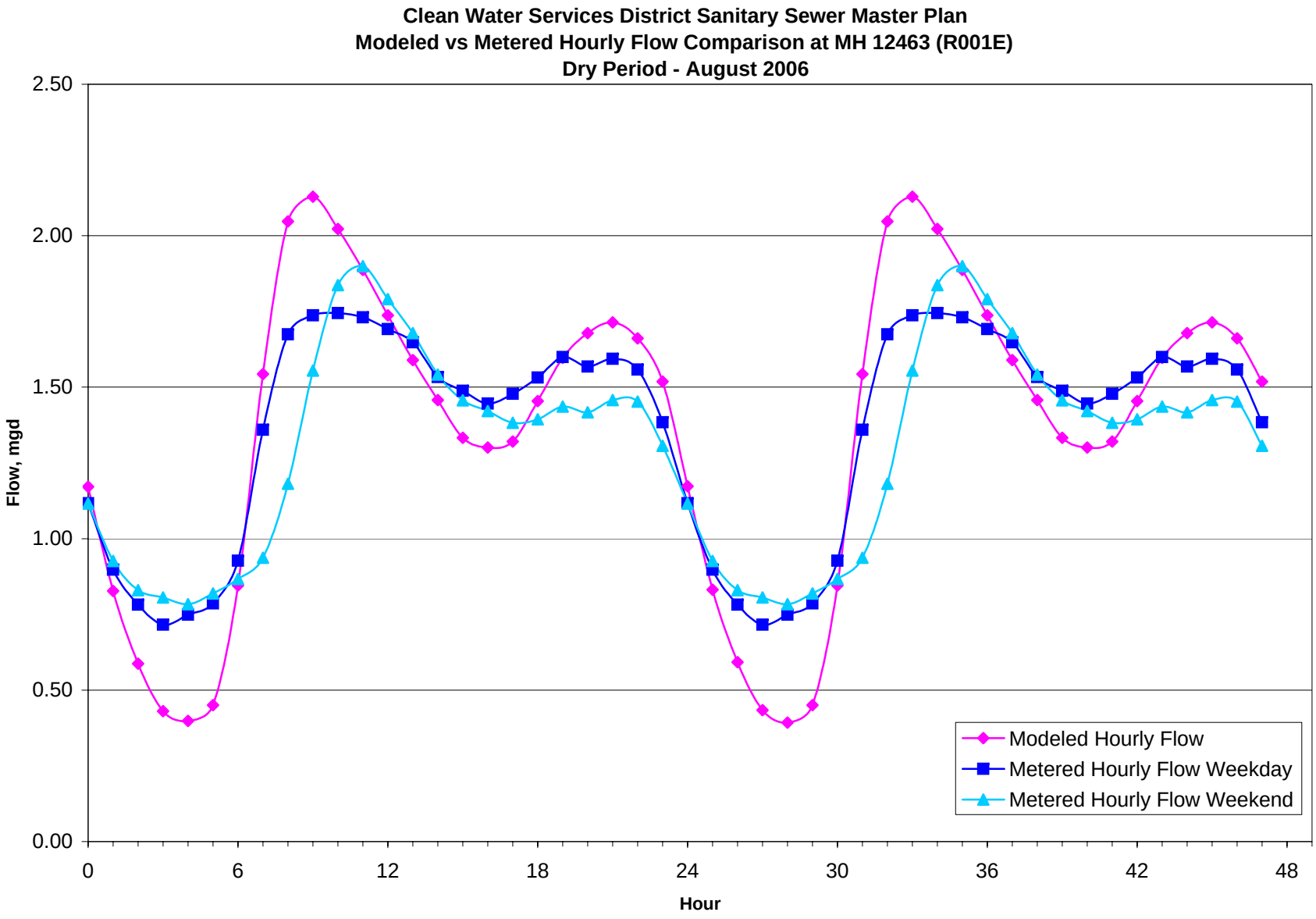

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12724 (F008)
Dry Period - August 2006
Flow, mgd
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

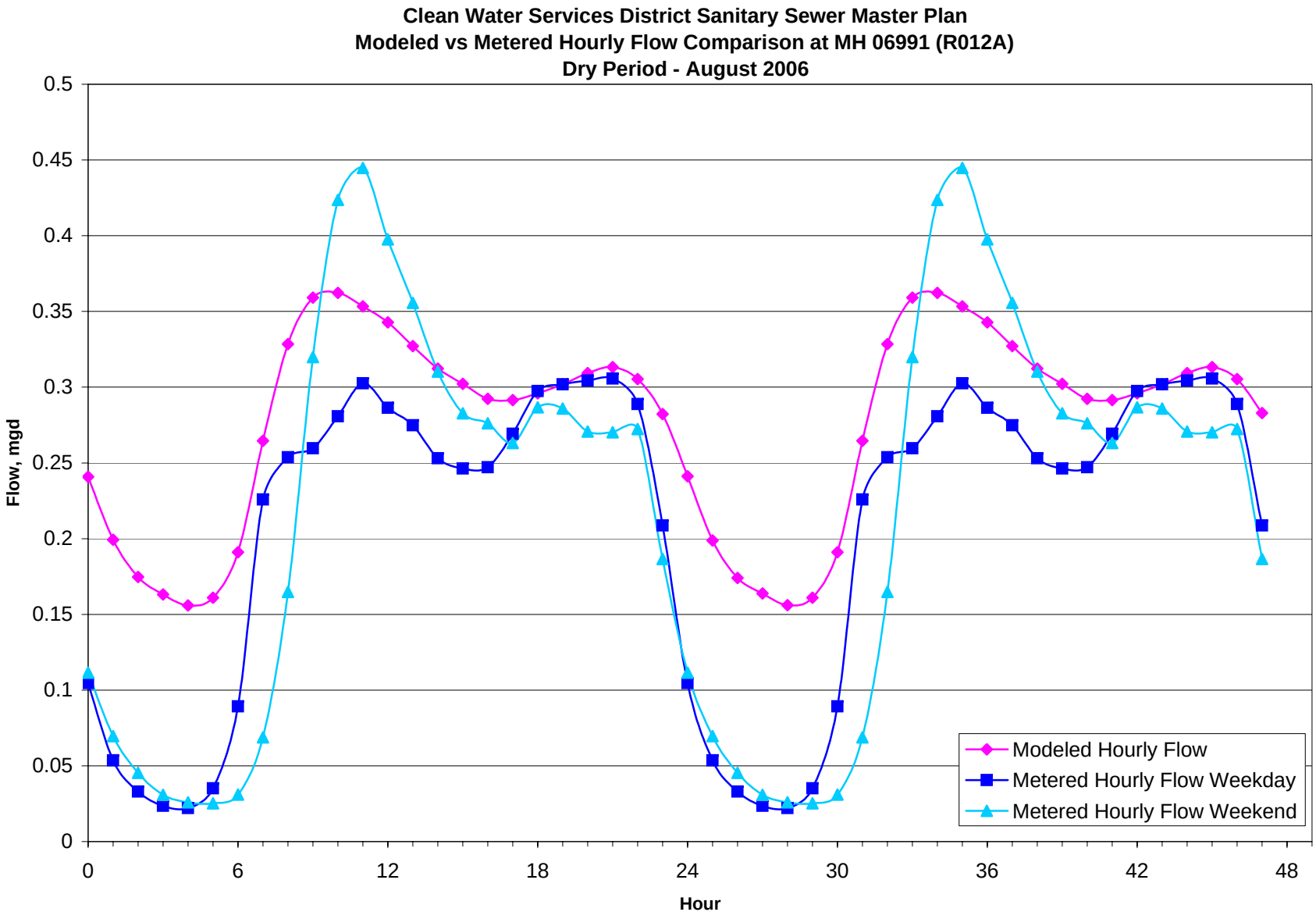

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12282 (H003)
Dry Period - August 2006
Flow, mgd
Hour
3.5
3
2.5
2
1.5
1
0.5
0
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

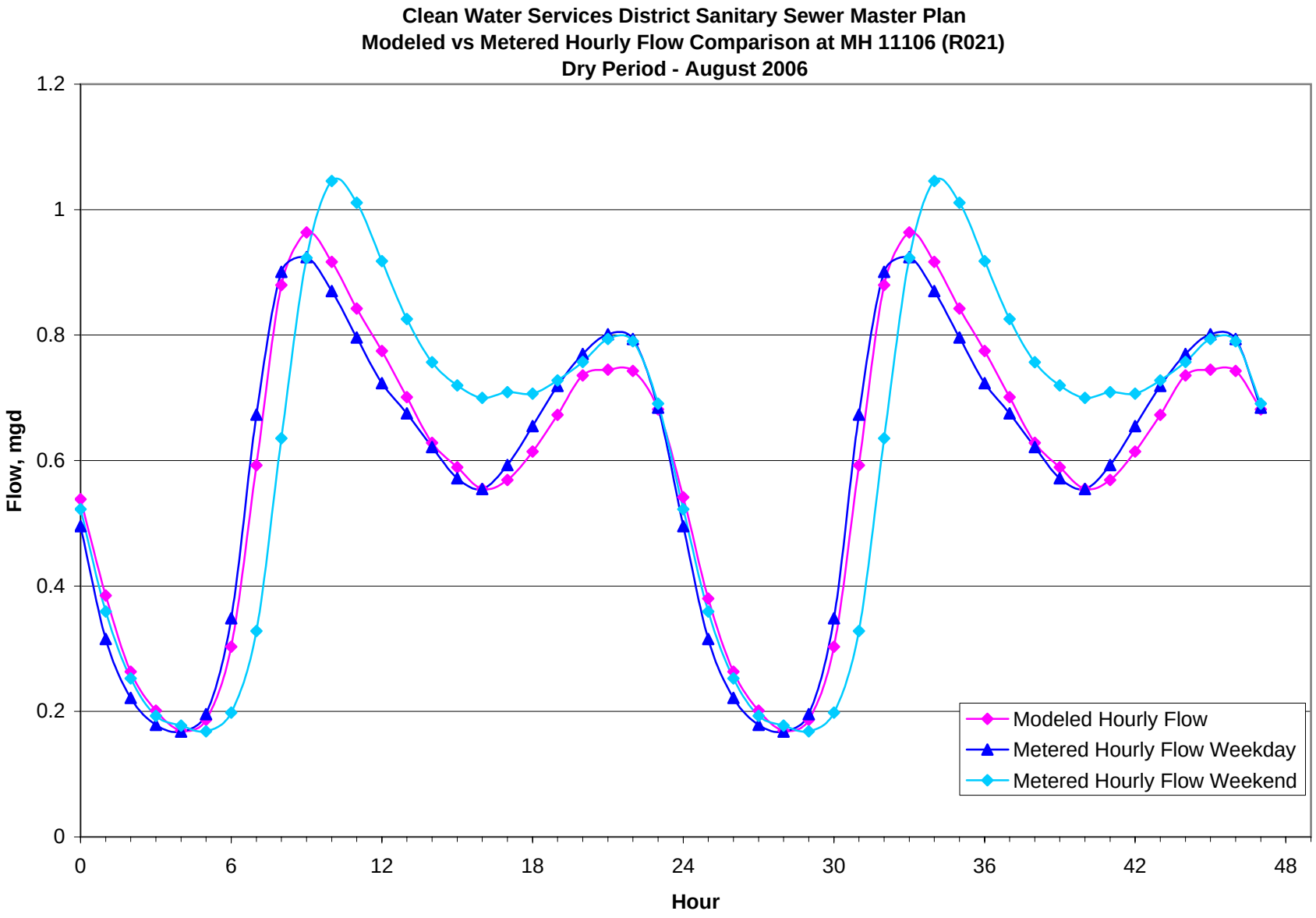

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 17216 (H006)
Dry Period - August 2006
Flow, mgd
Hour
1.2
1
0.8
0.6
0.4
0.2
0
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

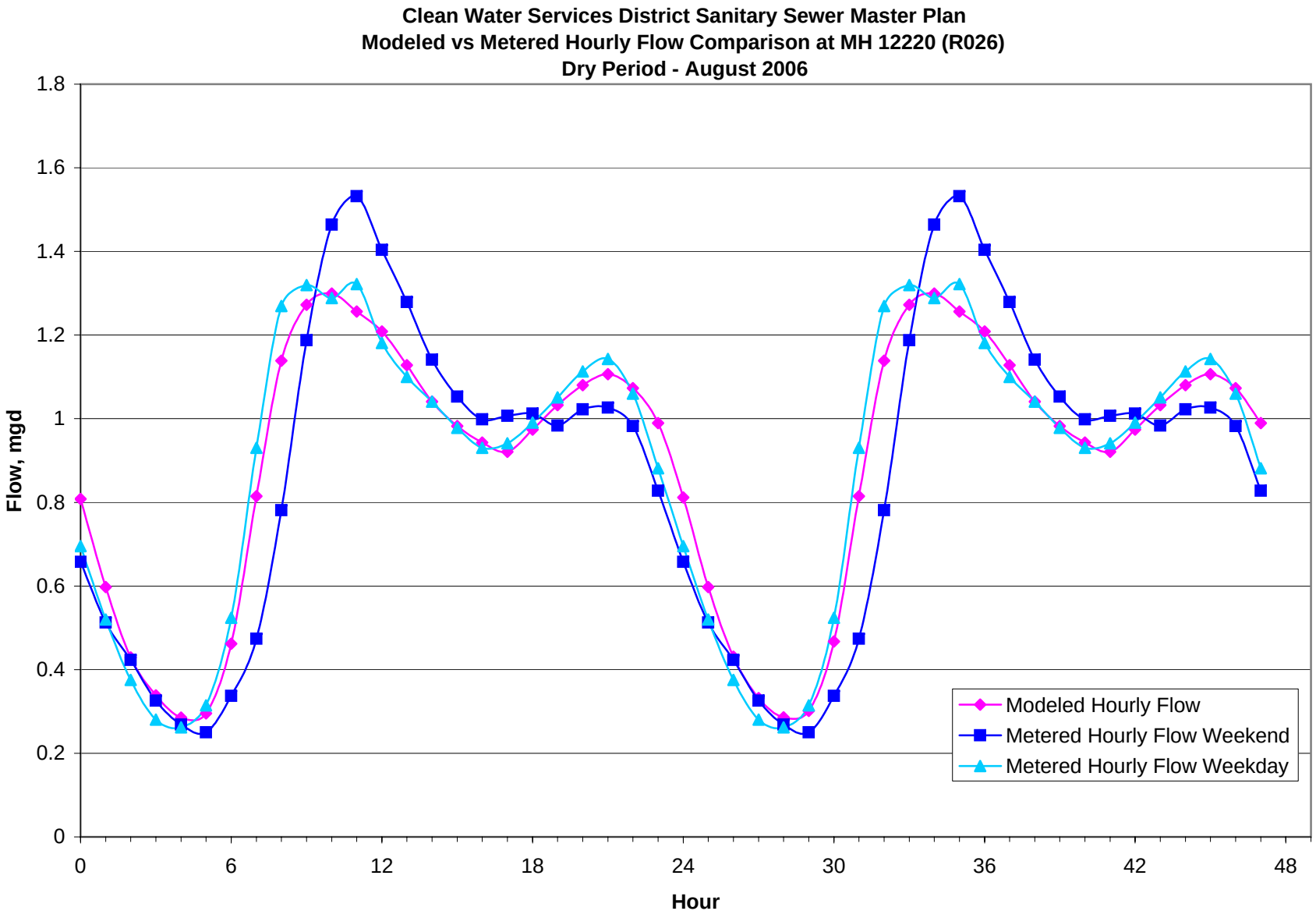

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 17167 (H007)
Dry Period - August 2006
Flow, mgd
Hour
0
0.2
0.4
0.6
0.8
1
1.2
1.4
1.6
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

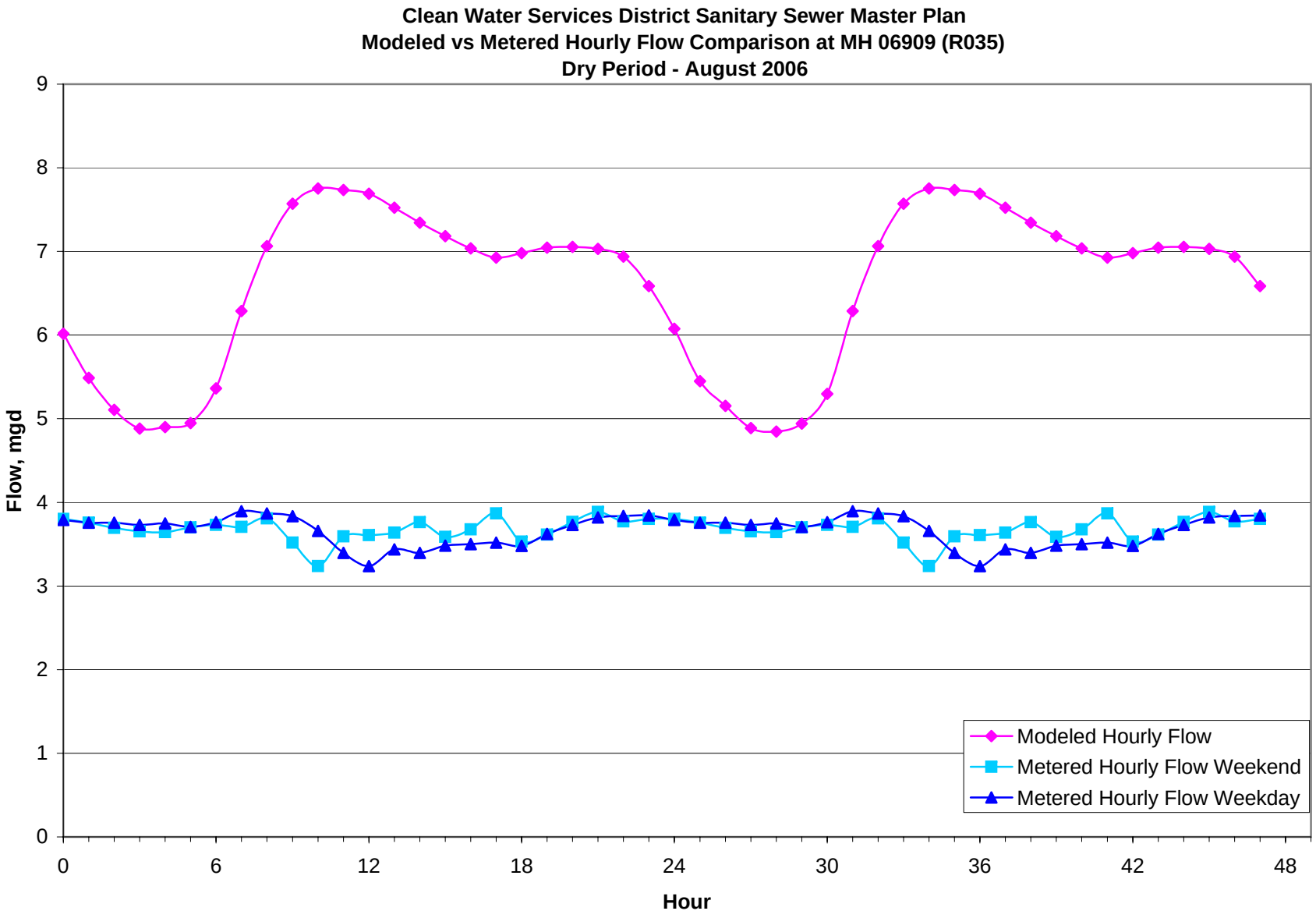

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 23060 (H008)
Dry Period - August 2006
Flow, mgd
0.6
0.5
0.4
0.3
0.2
0.1
0
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

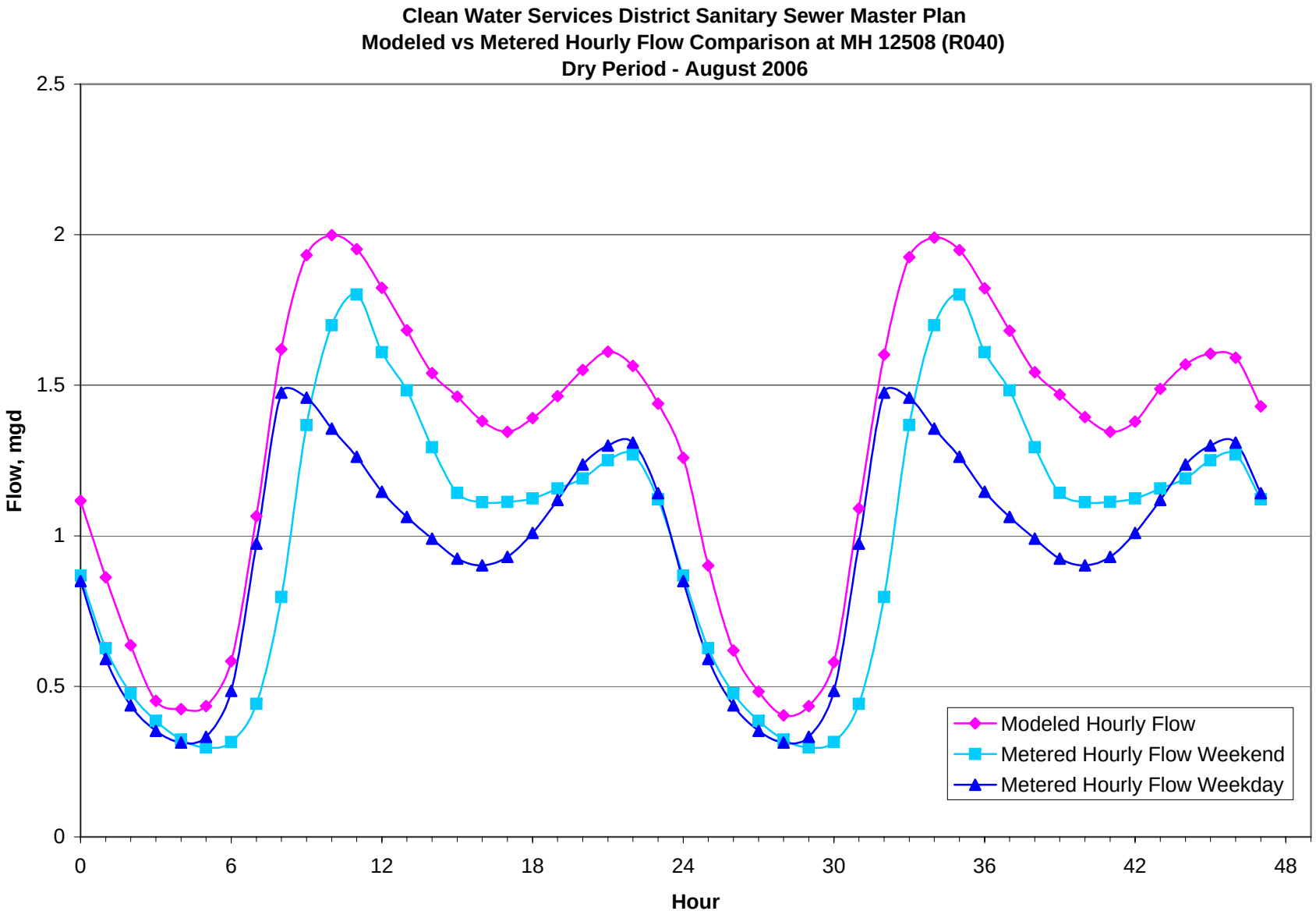

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12463 (R001E)
Dry Period - August 2006
Flow, mgd
2.50
2.00
1.50
1.00
0.50
0.00
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow Weekday
Metered Hourly Flow Weekend

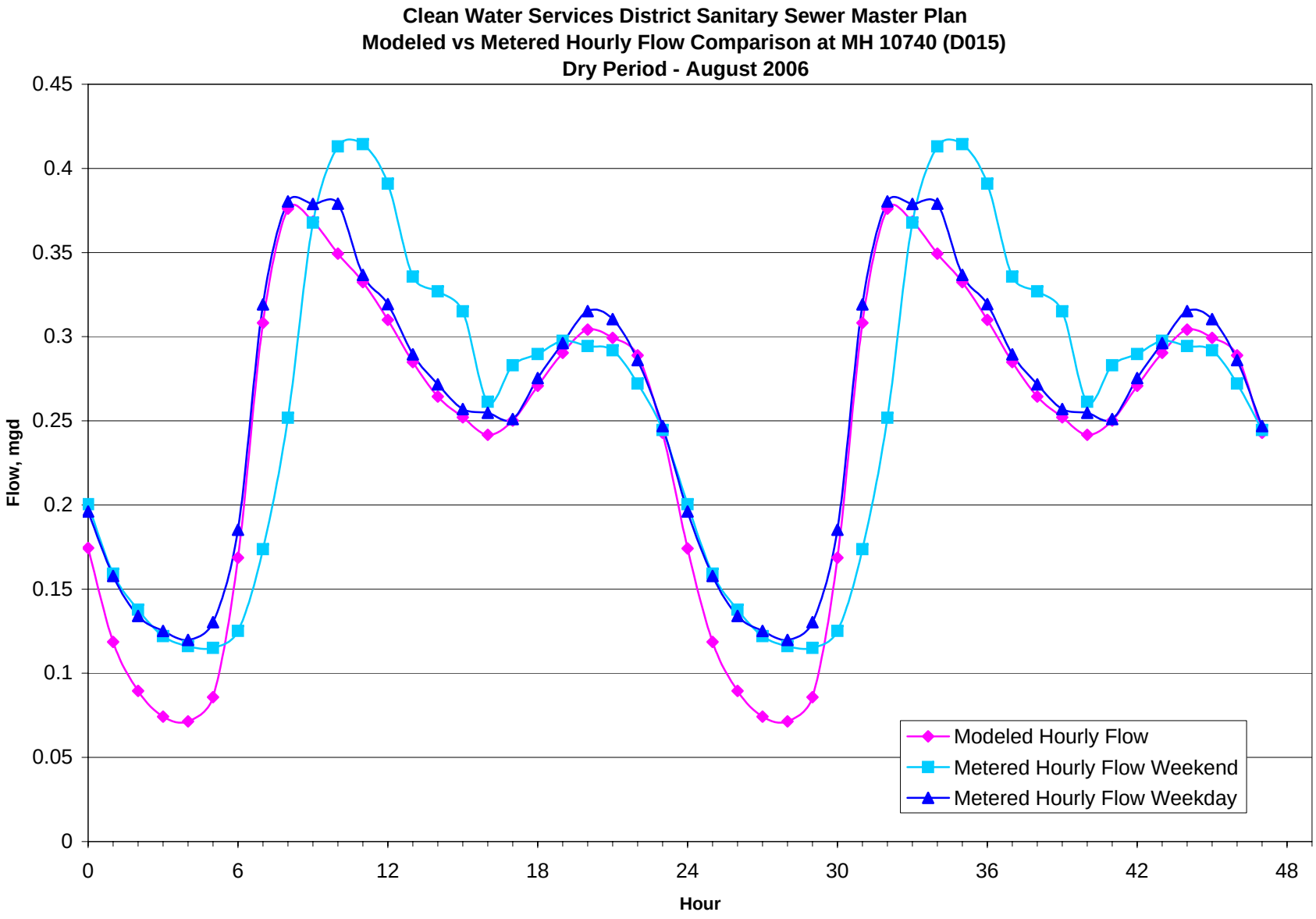

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 06991 (R012A)
Dry Period - August 2006
Flow, mgd
0.5
0.45
0.4
0.35
0.3
0.25
0.2
0.15
0.1
0.05
0
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow Weekday
Metered Hourly Flow Weekend

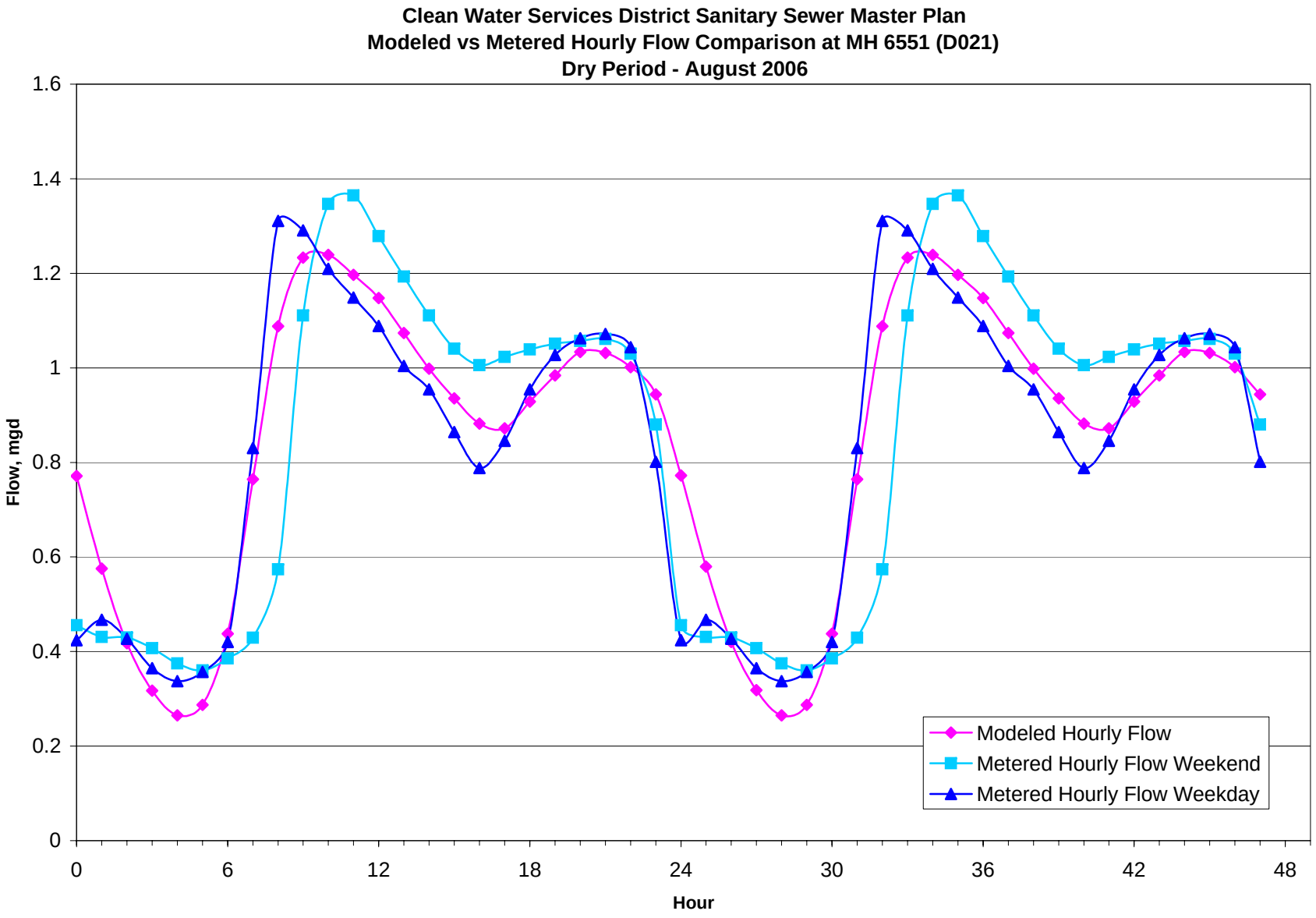

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 11106 (R021)
Dry Period - August 2006
Flow, mgd
Hour
1.2
1
0.8
0.6
0.4
0.2
0
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekday
Metered Hourly Flow Weekend

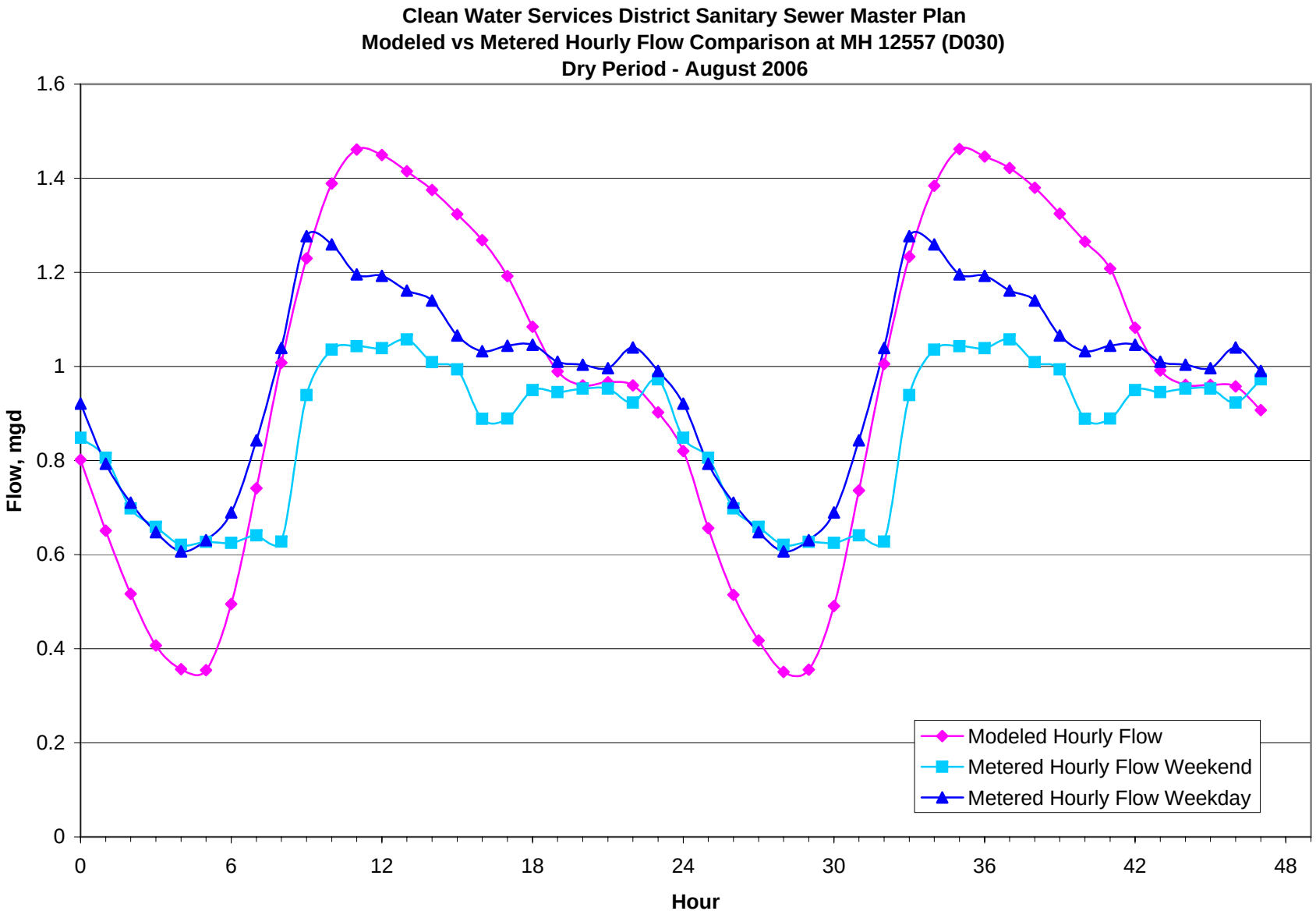

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12220 (R026)
Dry Period - August 2006
Flow, mgd
Hour
0
0.2
0.4
0.6
0.8
1
1.2
1.4
1.6
1.8
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

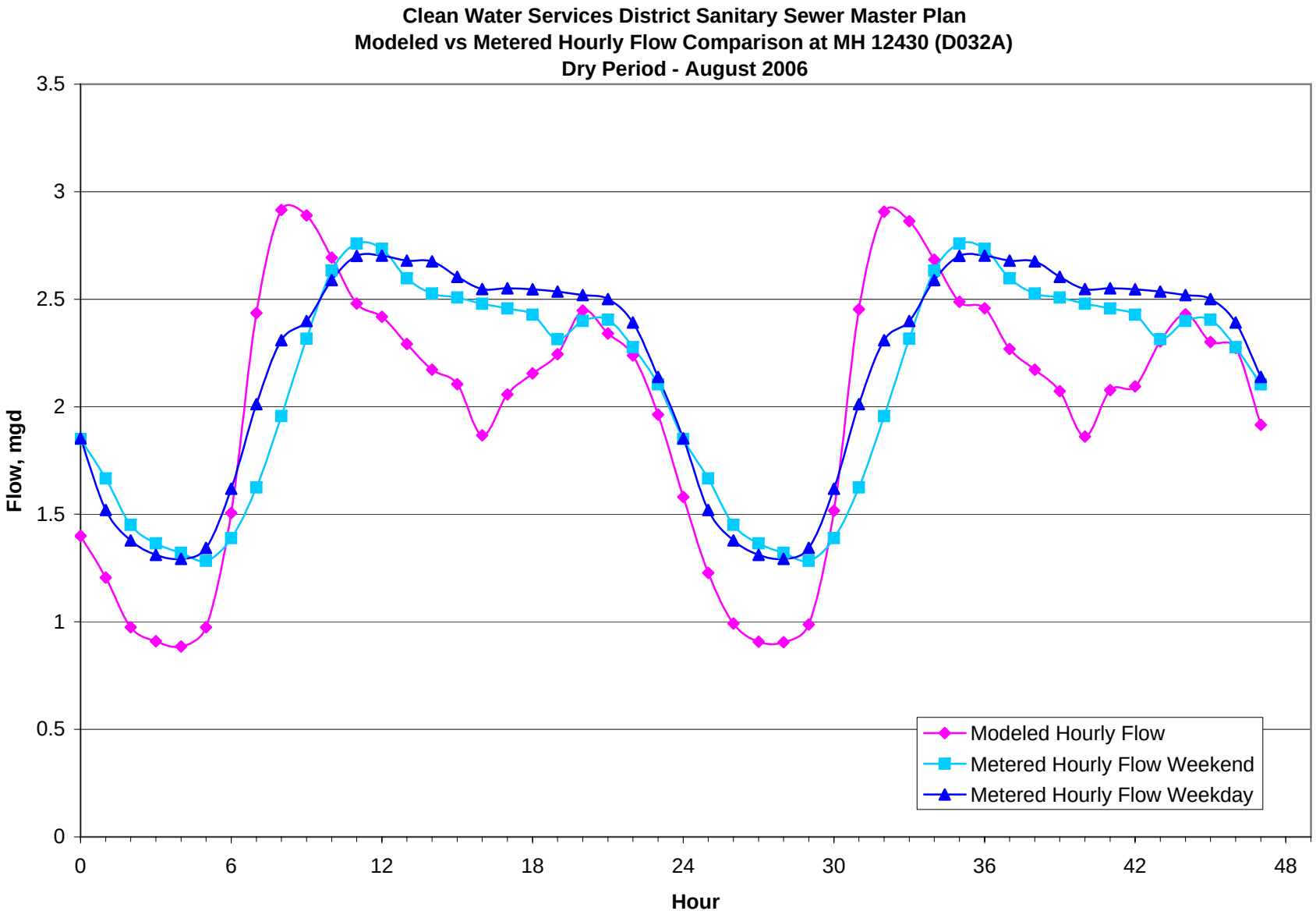

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 06909 (R035)
Dry Period - August 2006
Flow, mgd
Hour
0
1
2
3
4
5
6
7
8
9
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

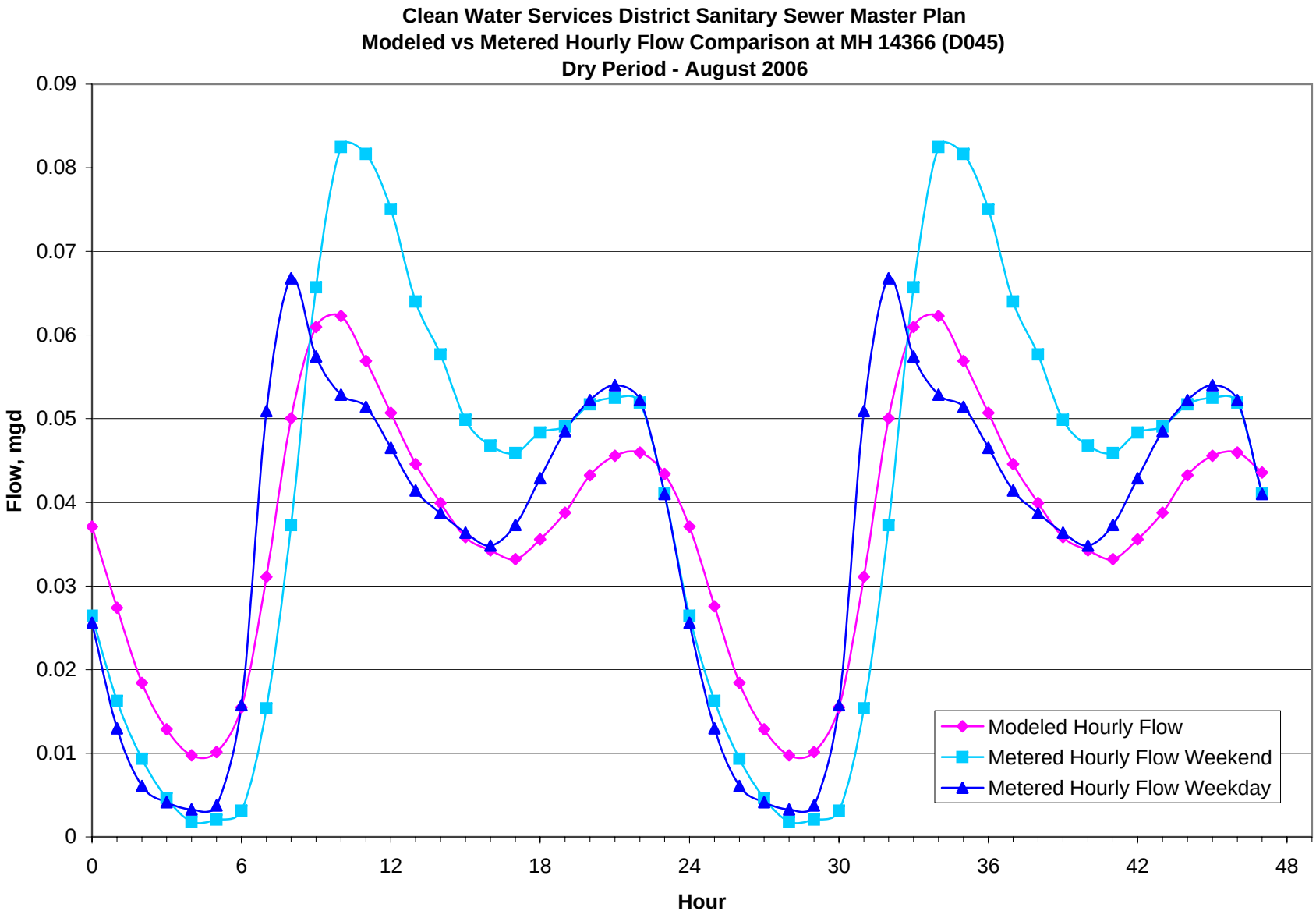

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12508 (R040)
Dry Period - August 2006
Flow, mgd
Hour
2.5
2
1.5
1
0.5
0
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

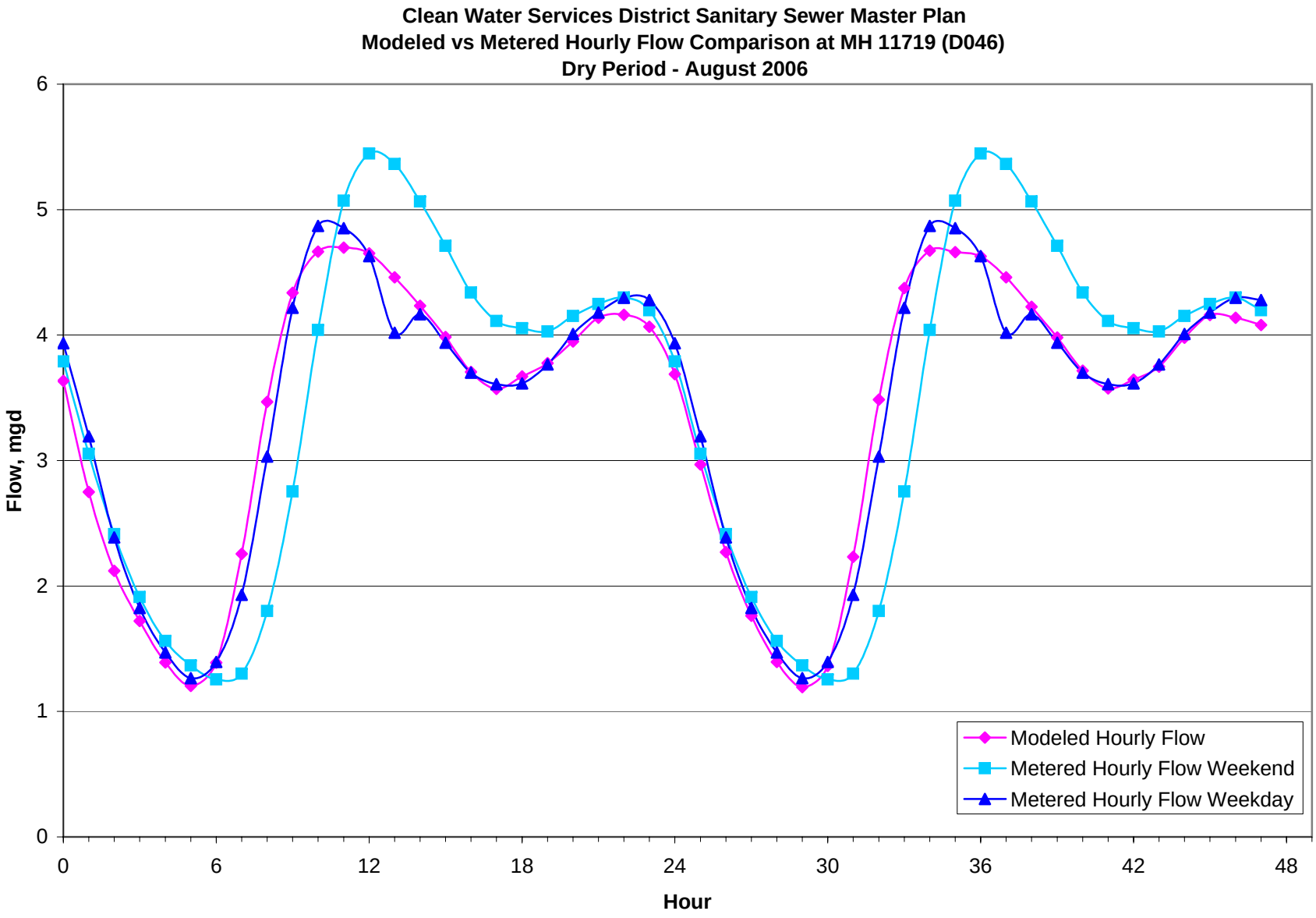

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 10740 (D015)
Dry Period - August 2006
Flow, mgd
0.45
0.4
0.35
0.3
0.25
0.2
0.15
0.1
0.05
0
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

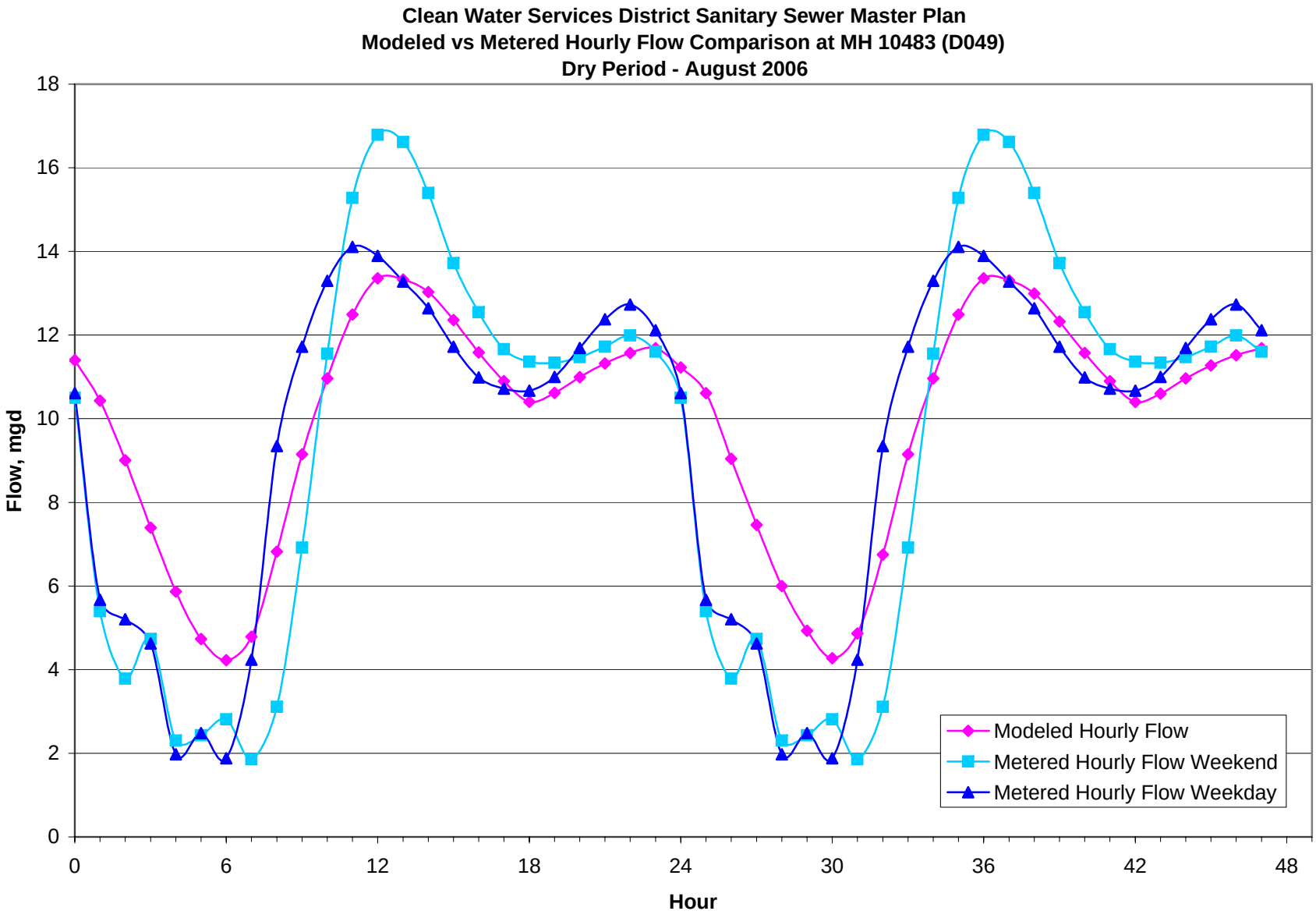

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 6551 (D021)
Dry Period - August 2006
Flow, mgd
Hour
1.6
1.4
1.2
1
0.8
0.6
0.4
0.2
0
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

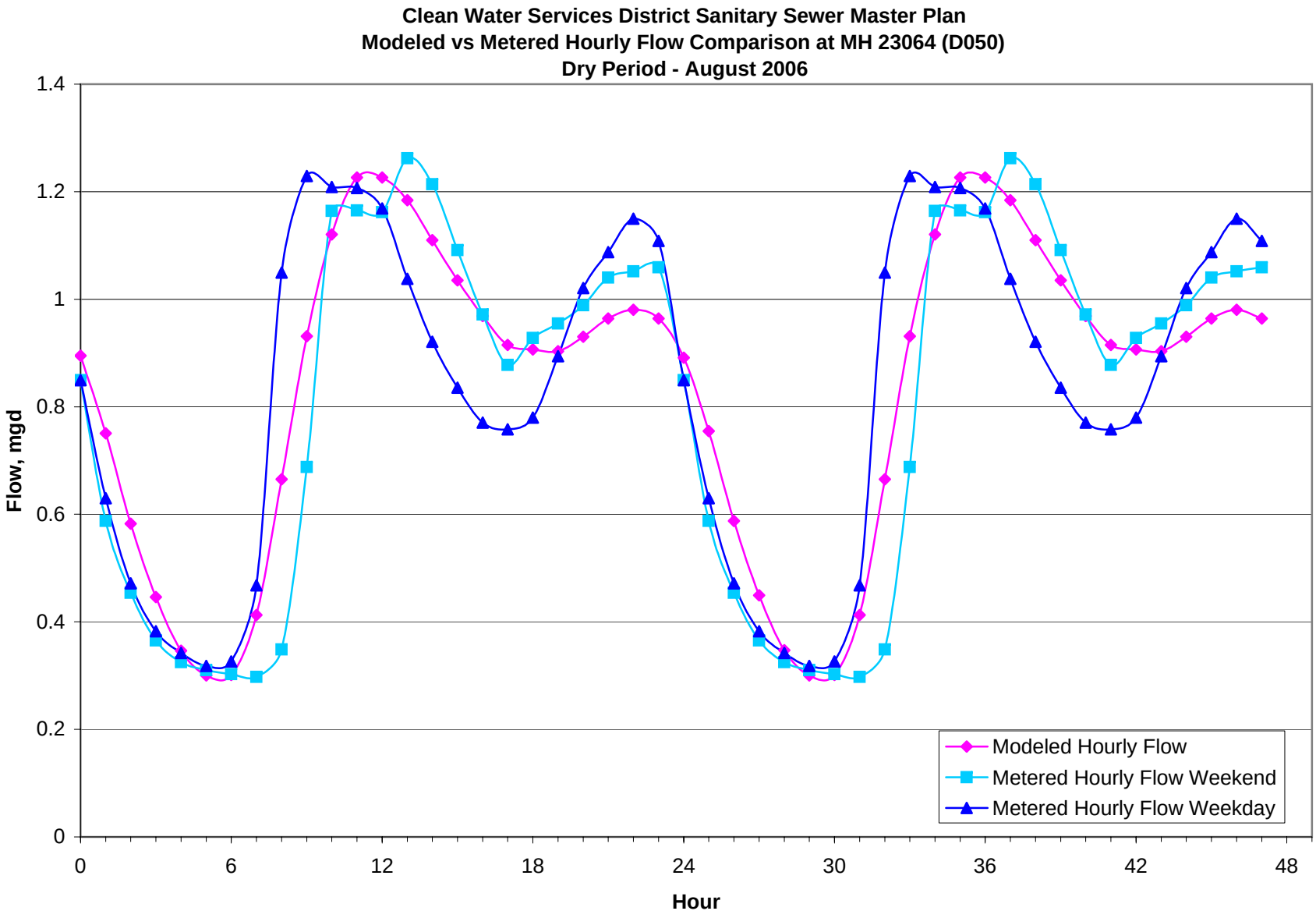

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12557 (D030)
Dry Period - August 2006
Flow, mgd
Hour
0
0.2
0.4
0.6
0.8
1
1.2
1.4
1.6
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday


Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12430 (D032A)
Dry Period - August 2006
Flow, mgd
Hour
3.5
3
2.5
2
1.5
1
0.5
0
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday


Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 14366 (D045)
Dry Period - August 2006
Flow, mgd
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

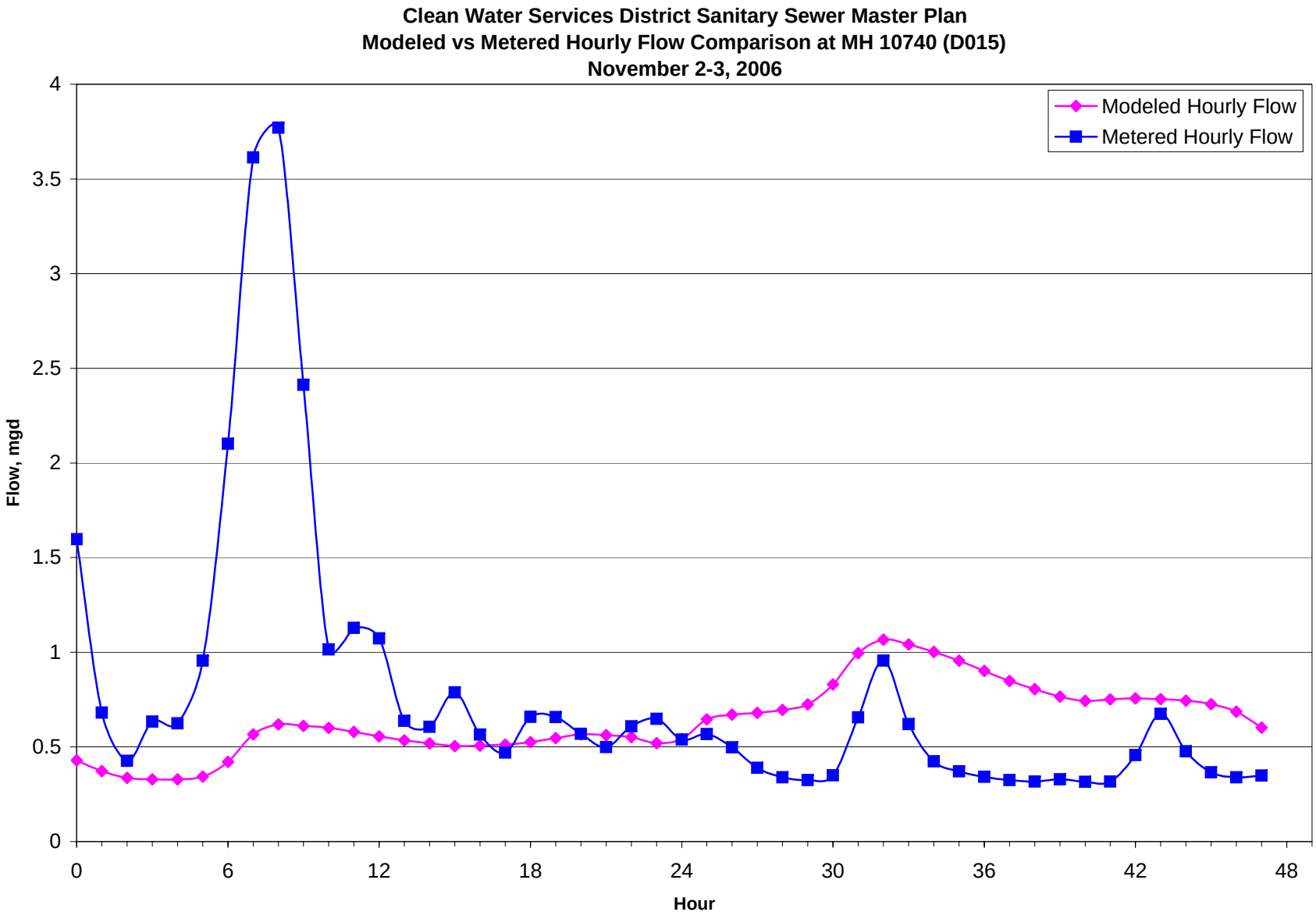

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 11719 (D046)
Dry Period - August 2006
Flow, mgd
Hour
0
1
2
3
4
5
6
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

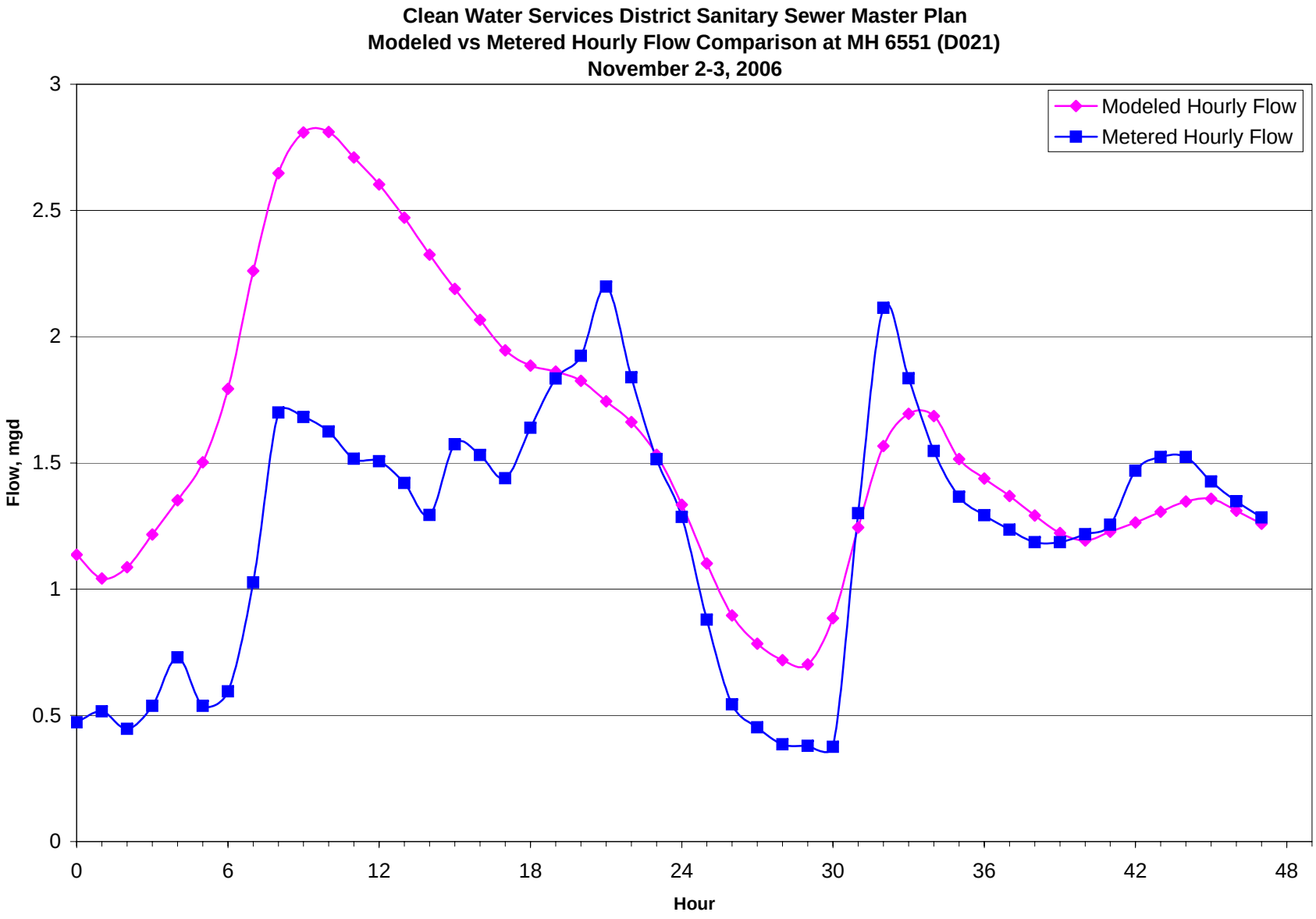

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 10483 (D049)
Dry Period - August 2006
Flow, mgd
Hour
0
2
4
6
8
10
12
14
16
18
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

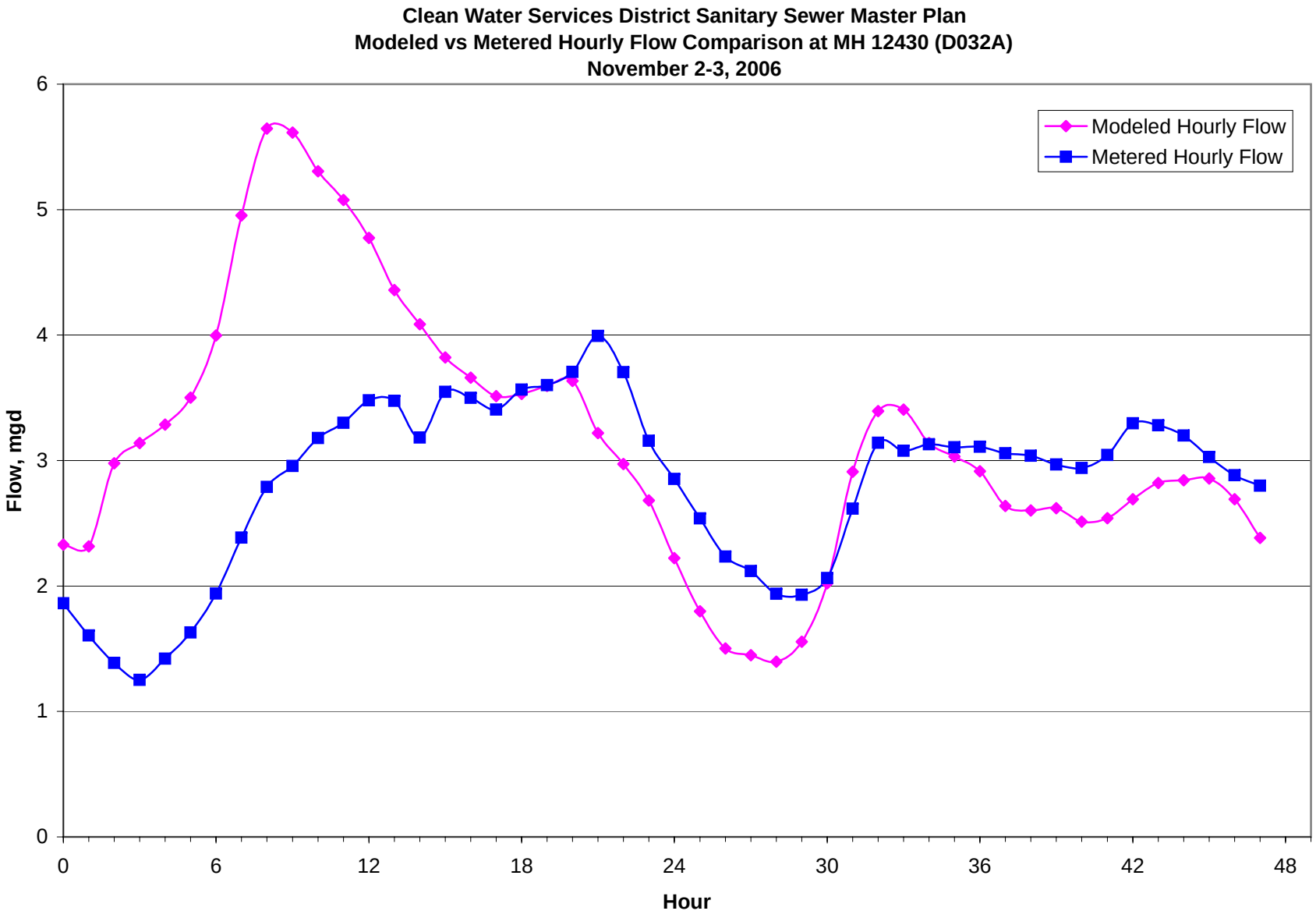

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 23064 (D050)
Dry Period - August 2006
Flow, mgd
Hour
0
0.2
0.4
0.6
0.8
1
1.2
1.4
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow Weekend
Metered Hourly Flow Weekday

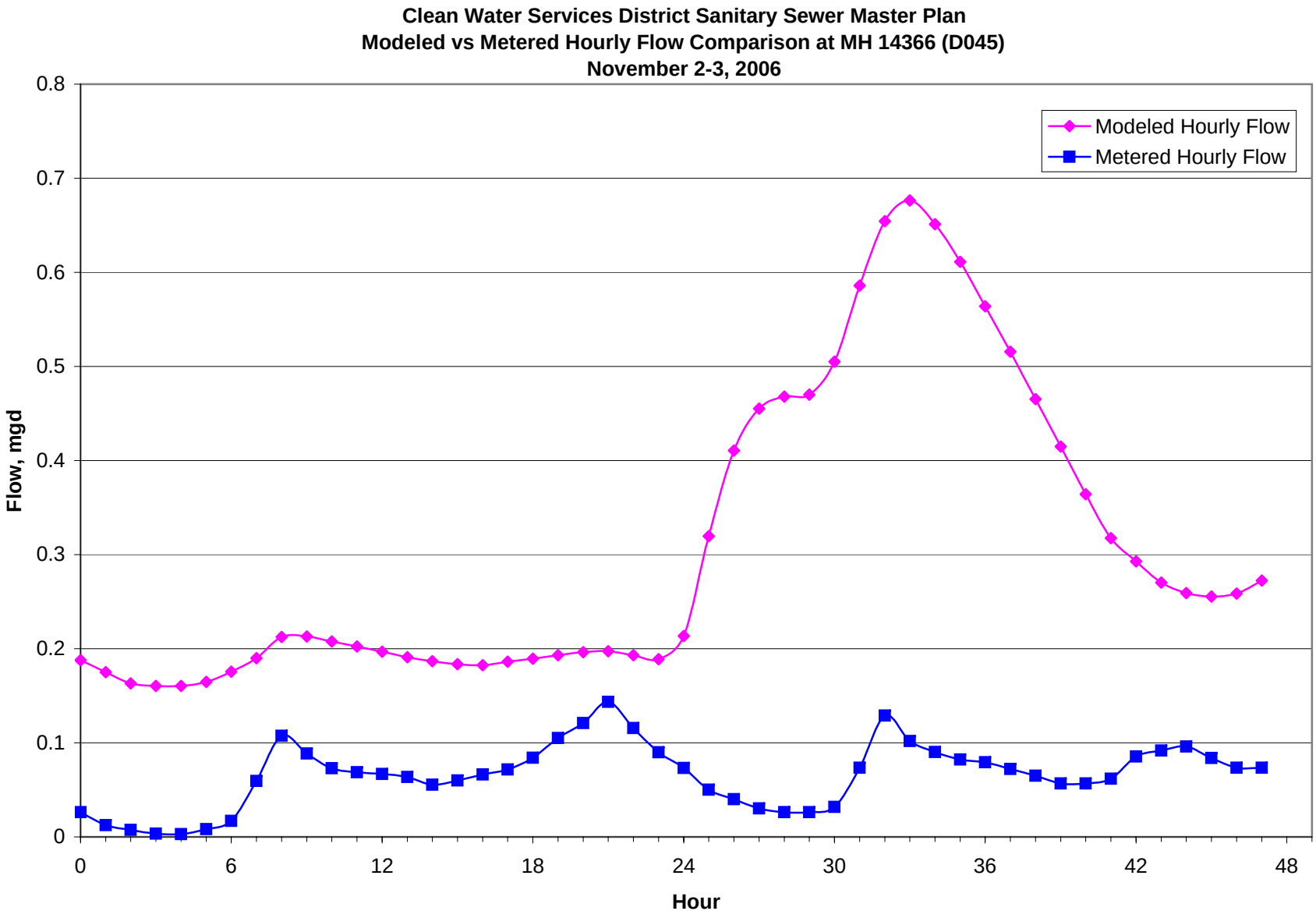
APPENDIX L

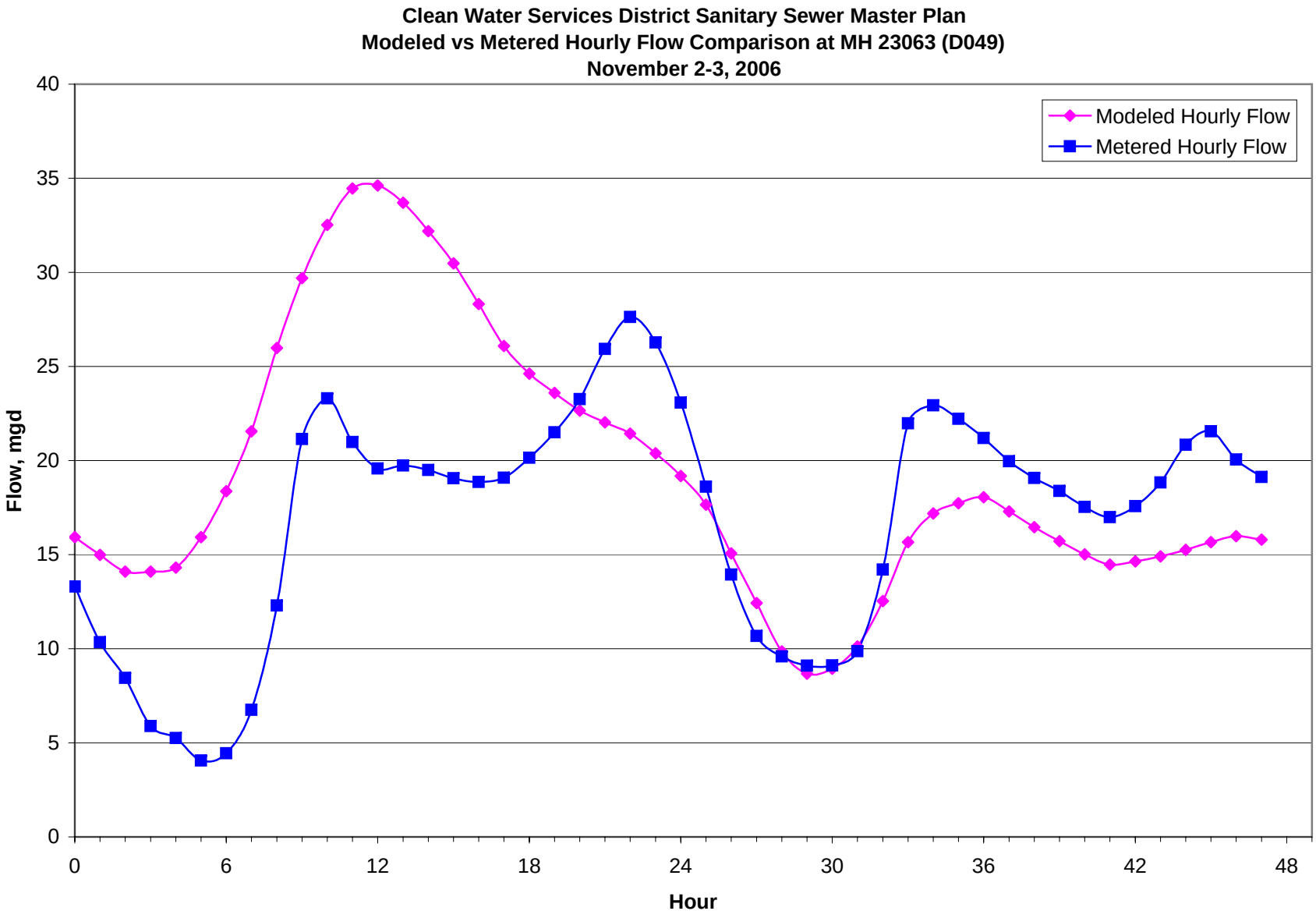
Wet Weather Flow Comparison Plots

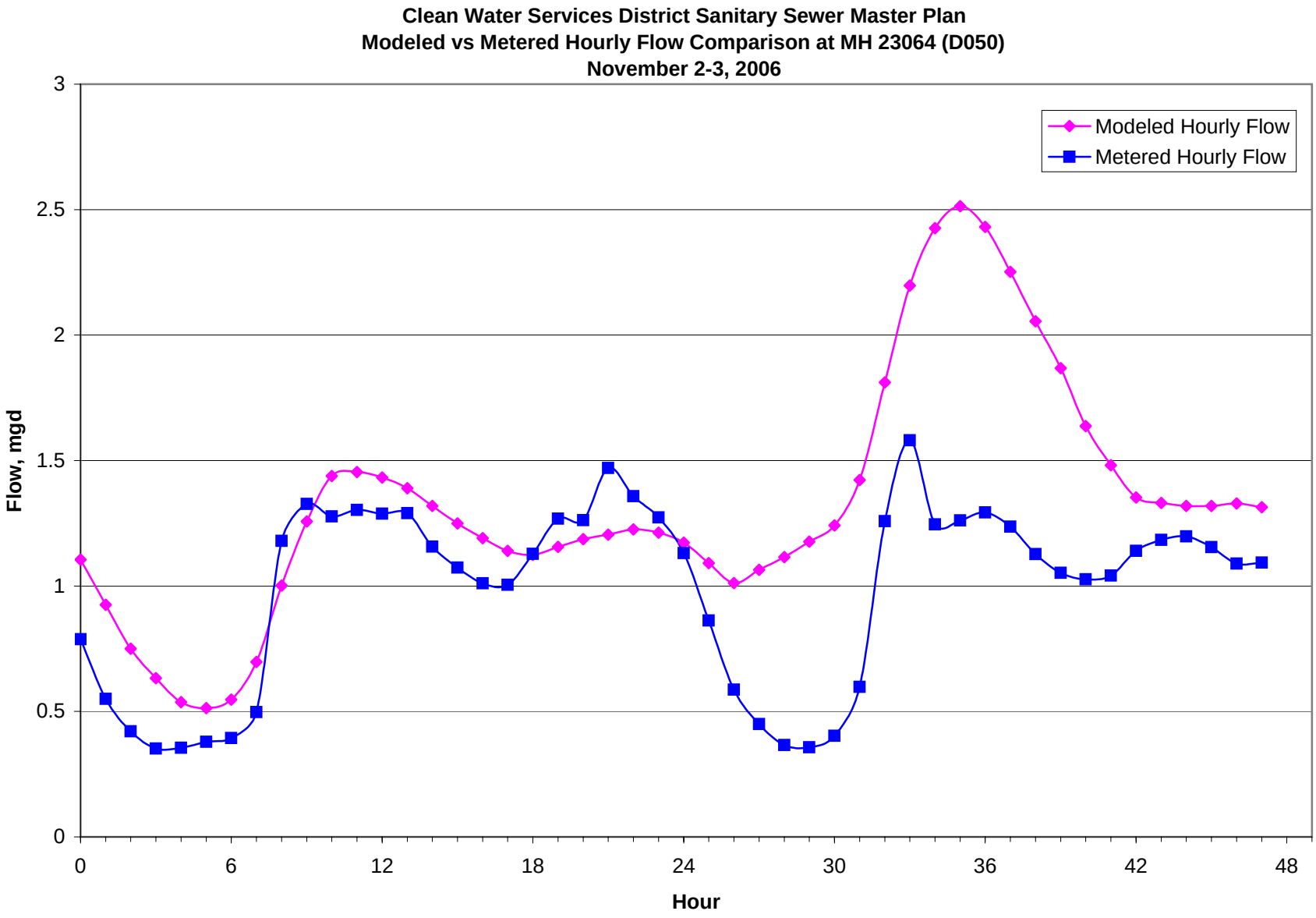

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 10740 (D015)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
0.5
1
1.5
2
2.5
3
3.5
4
0
6
12
18
24
30
36
42
48

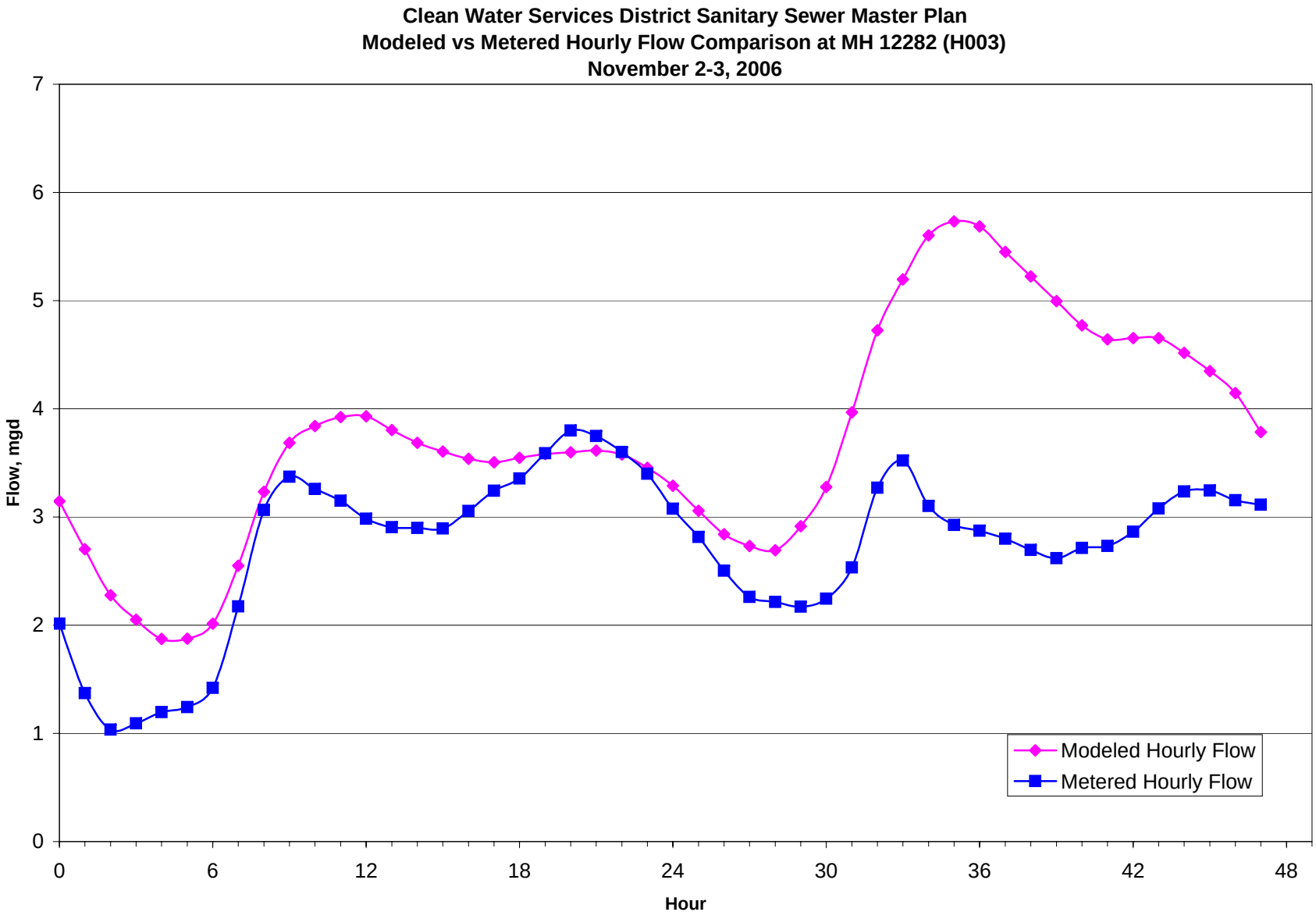

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 6551 (D021)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
0.5
1
1.5
2
2.5
3
0
6
12
18
24
30
36
42
48

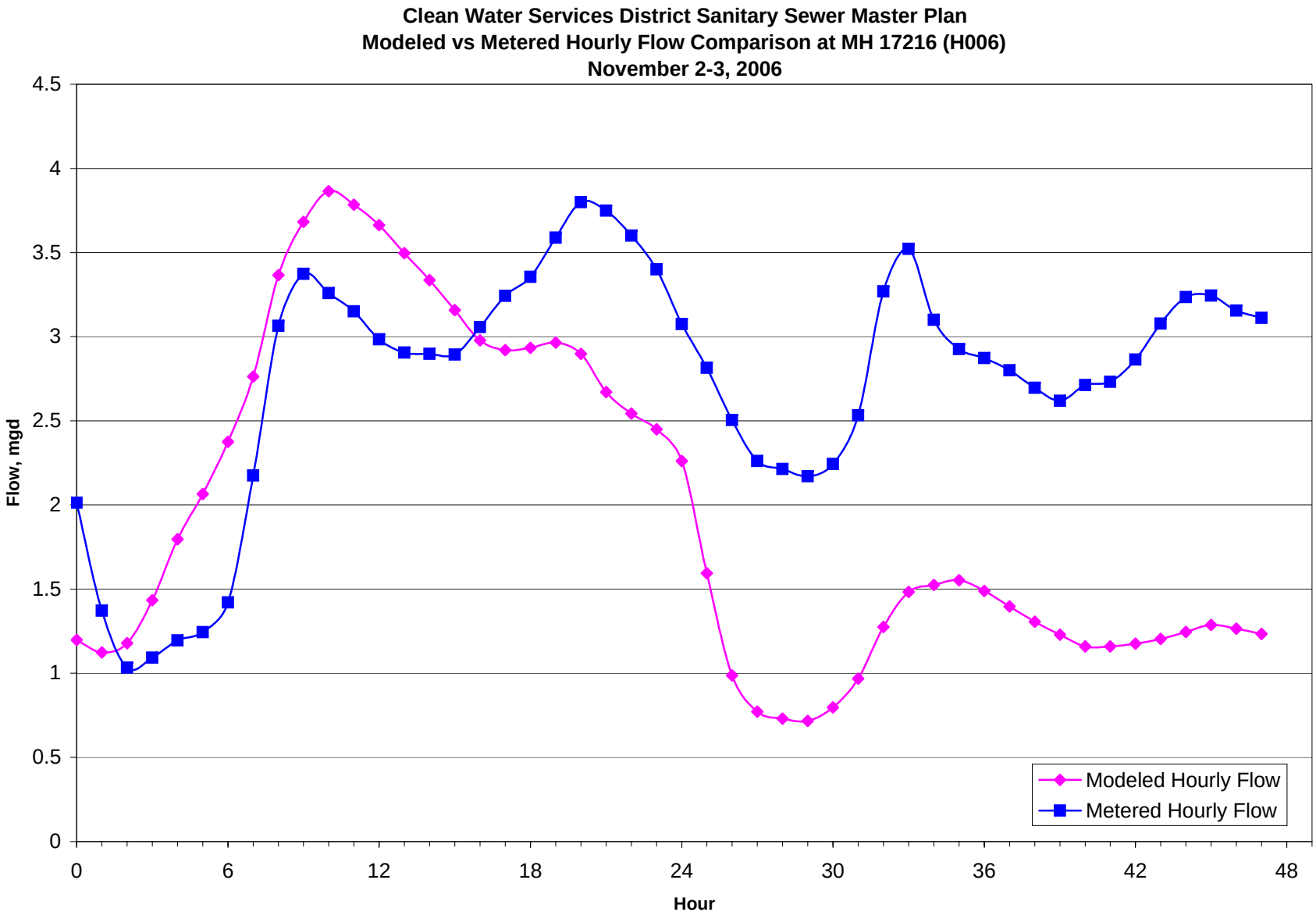

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12430 (D032A)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
1
2
3
4
5
6
0
6
12
18
24
30
36
42
48

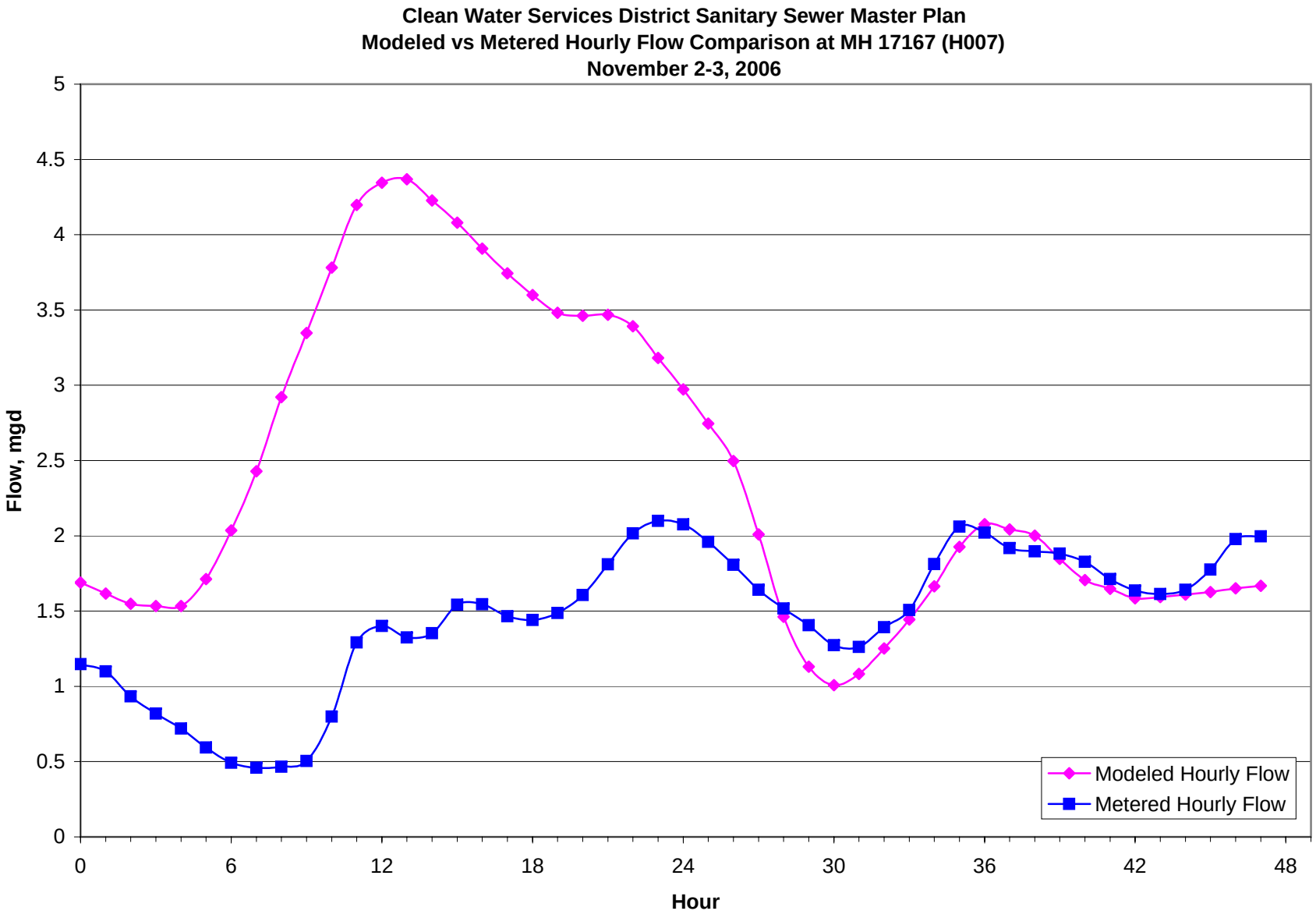

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 14366 (D045)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
0
6
12
18
24
30
36
42
48
Hour

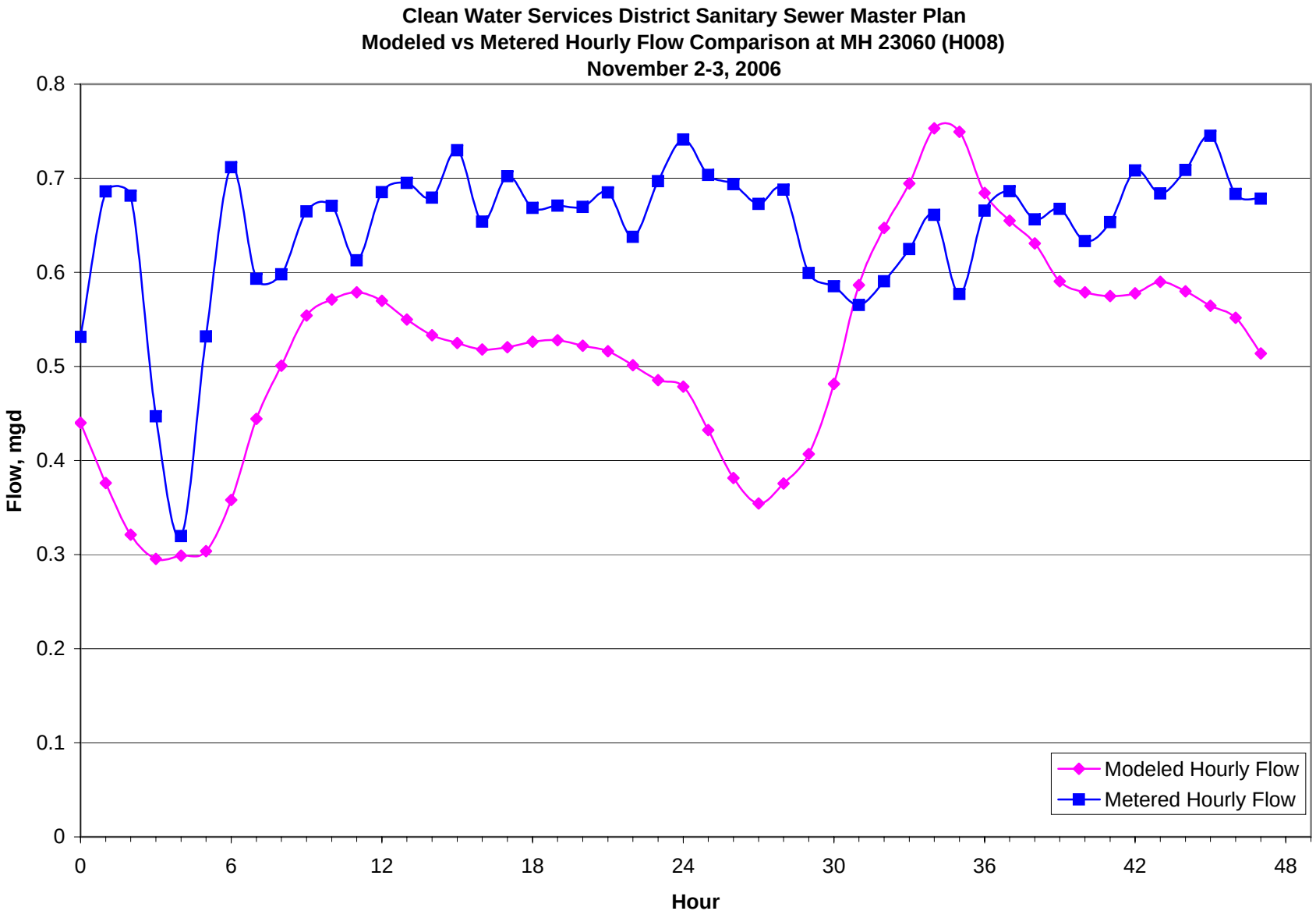

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 23063 (D049)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
5
10
15
20
25
30
35
40
0
6
12
18
24
30
36
42
48

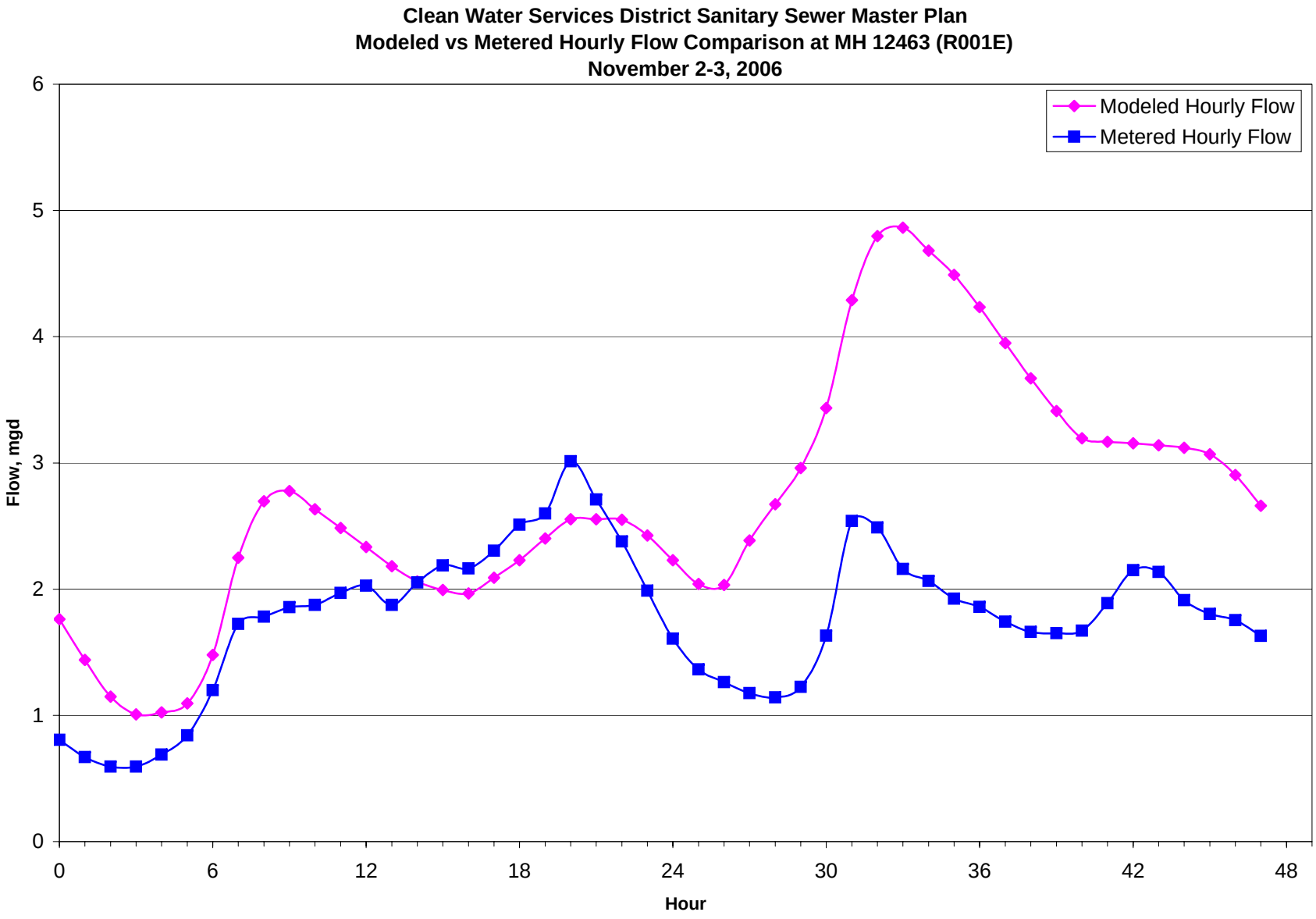

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 23064 (D050)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
0.5
1
1.5
2
2.5
3
0
6
12
18
24
30
36
42
48

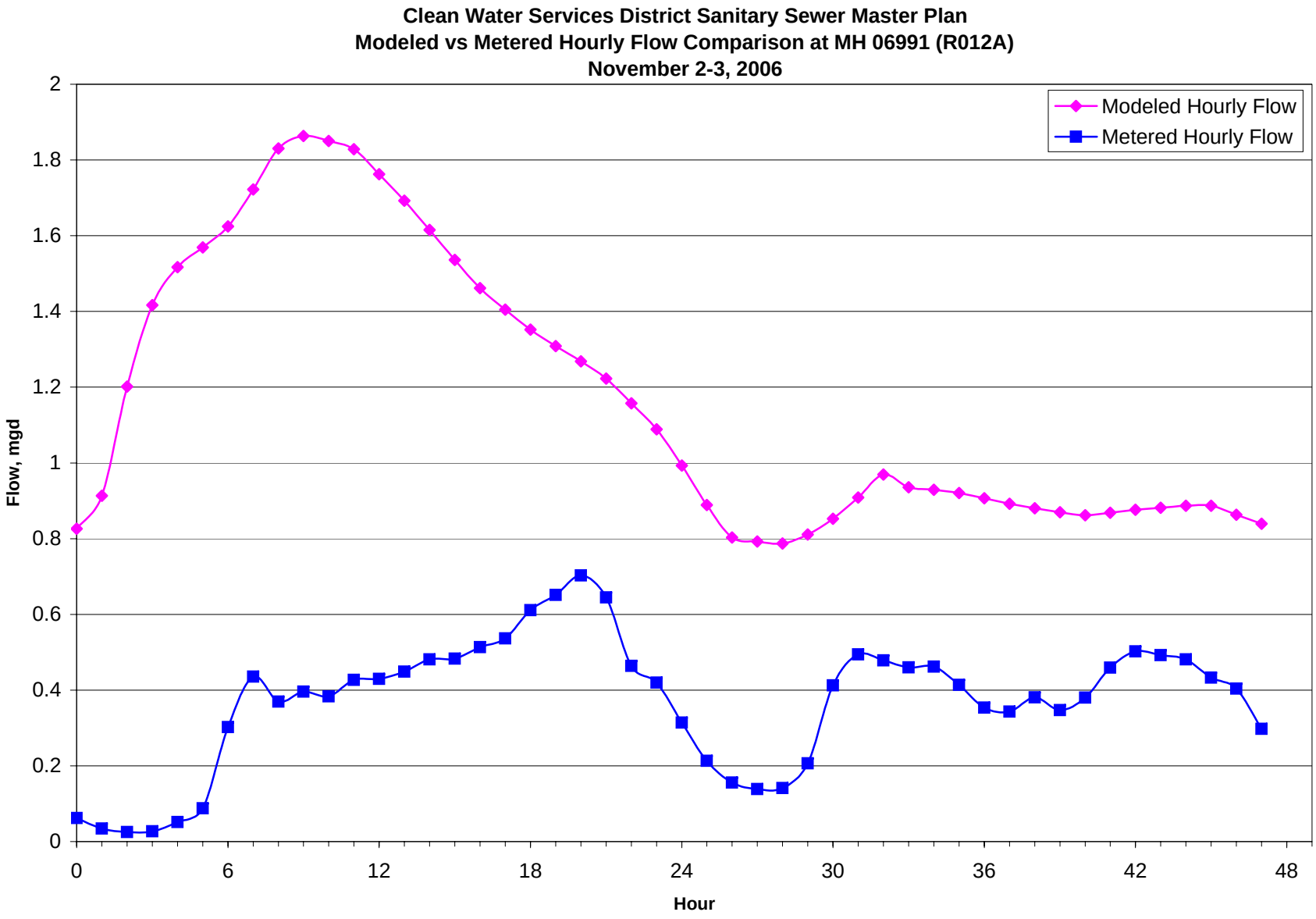

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12282 (H003)
November 2-3, 2006
Flow, mgd
Hour
0
1
2
3
4
5
6
7
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow

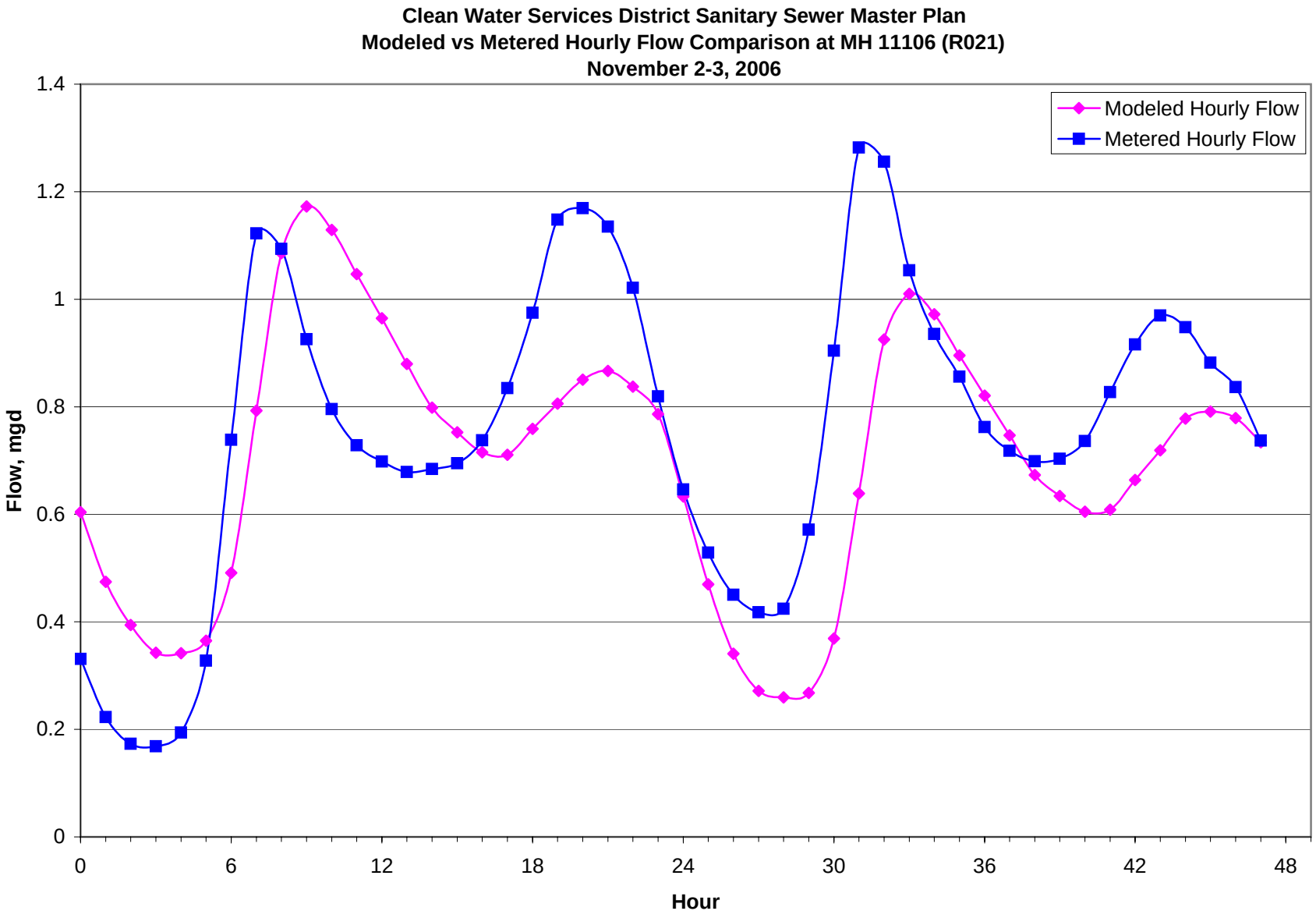

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 17216 (H006)
November 2-3, 2006
Flow, mgd
Hour
0
0.5
1
1.5
2
2.5
3
3.5
4
4.5
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow

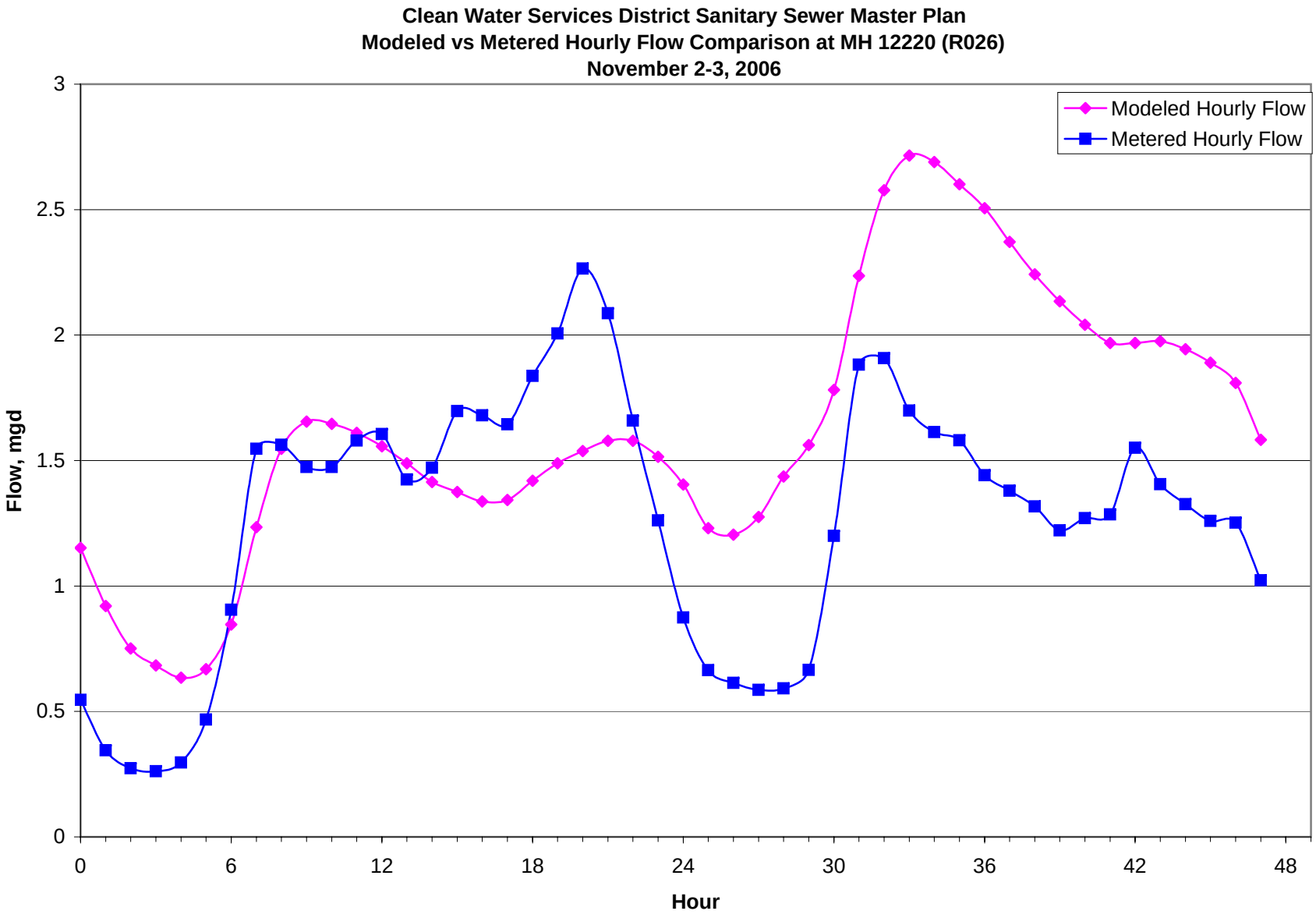

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 17167 (H007)
November 2-3, 2006
Flow, mgd
Hour
0
0.5
1
1.5
2
2.5
3
3.5
4
4.5
5
0
6
12
18
24
30
36
42
48
Modeled Hourly Flow
Metered Hourly Flow

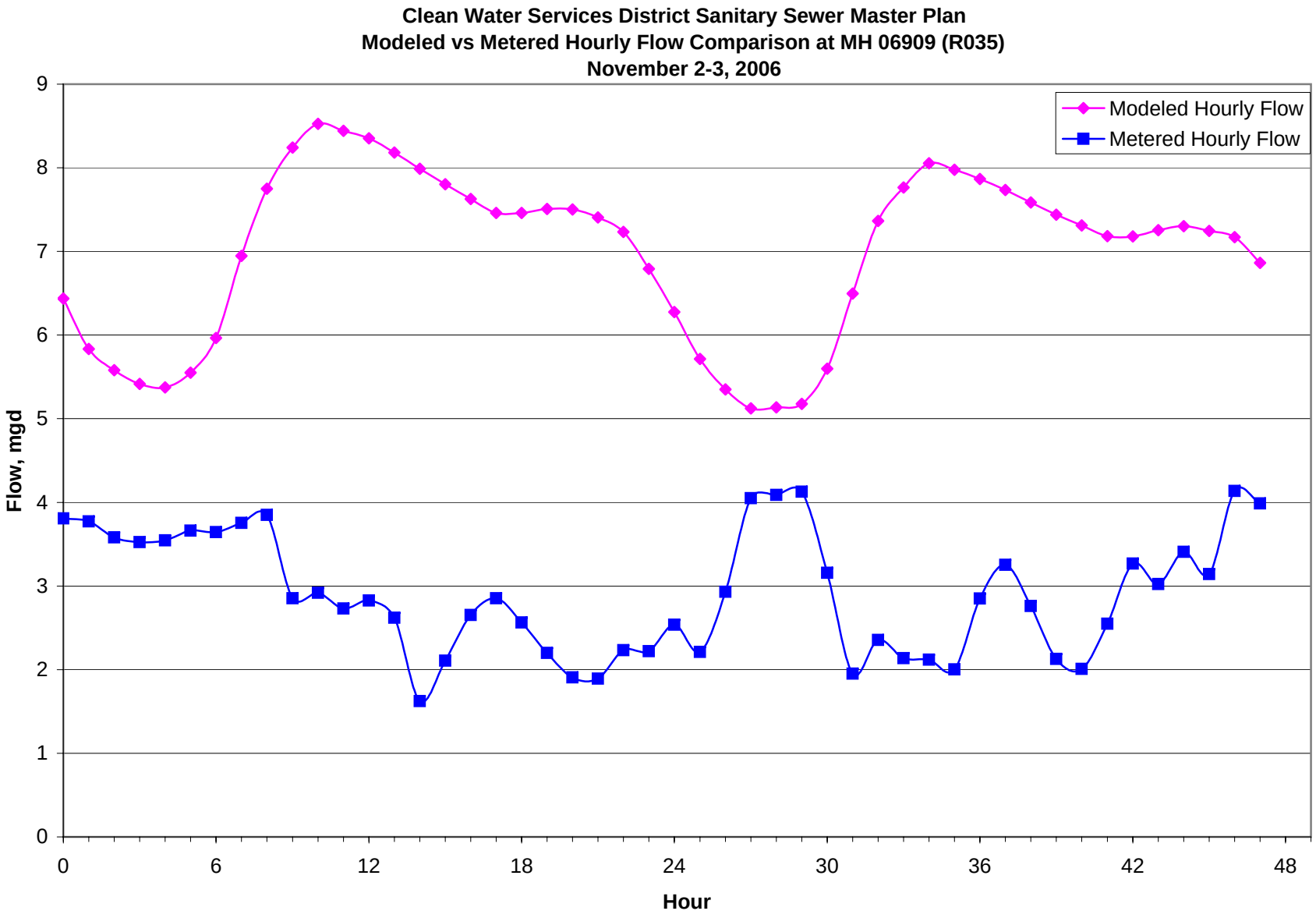

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 23060 (H008)
November 2-3, 2006
Flow, mgd
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
0
6
12
18
24
30
36
42
48
Hour
Modeled Hourly Flow
Metered Hourly Flow

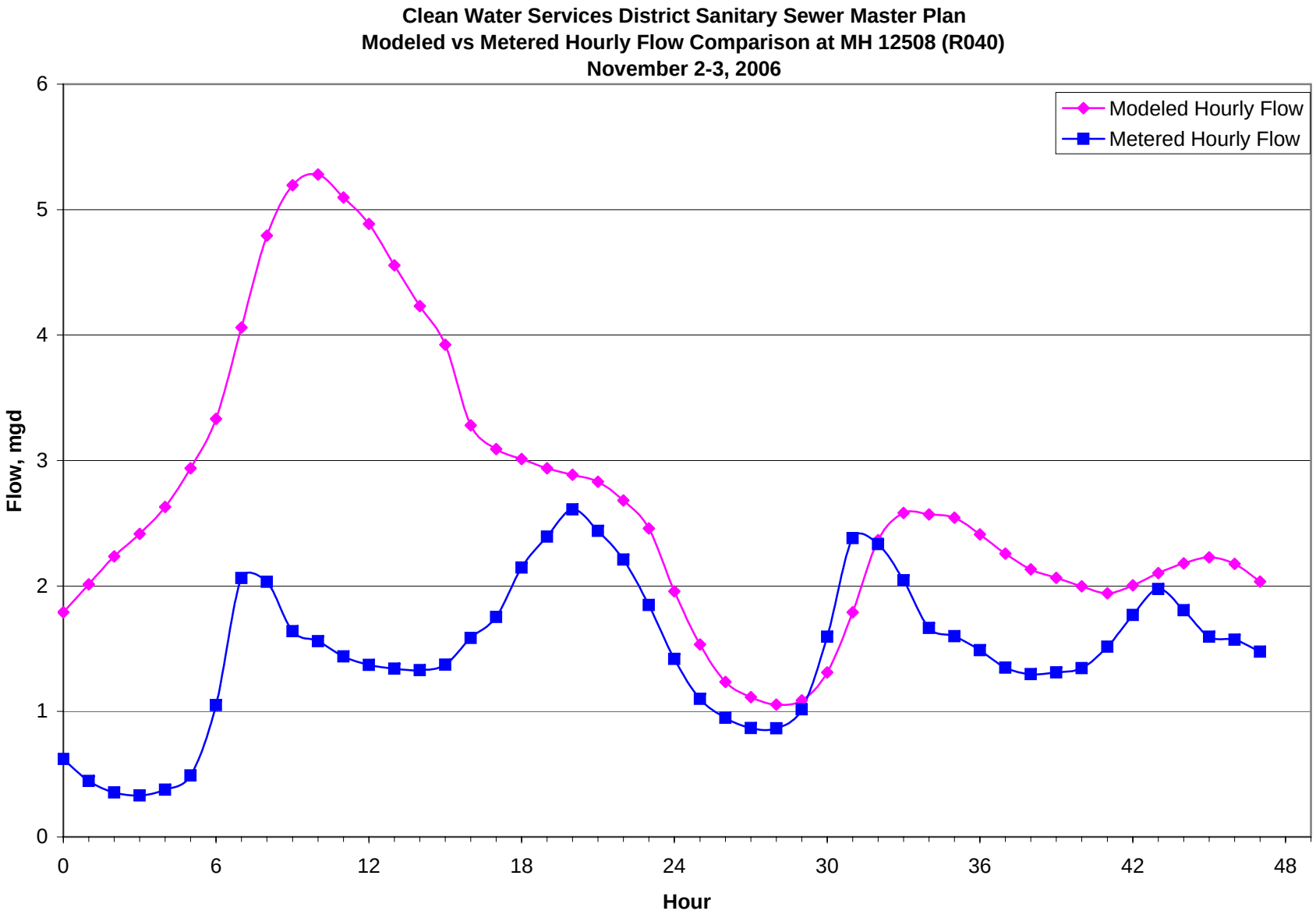

Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12463 (R001E)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
1
2
3
4
5
6
0
6
12
18
24
30
36
42
48


Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 06991 (R012A)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
0.2
0.4
0.6
0.8
1
1.2
1.4
1.6
1.8
2
0
6
12
18
24
30
36
42
48


Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 11106 (R021)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
0.2
0.4
0.6
0.8
1
1.2
1.4
0
6
12
18
24
30
36
42
48


Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12220 (R026)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
0.5
1
1.5
2
2.5
3
0
6
12
18
24
30
36
42
48


Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 06909 (R035)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
1
2
3
4
5
6
7
8
9
0
6
12
18
24
30
36
42
48


Clean Water Services District Sanitary Sewer Master Plan
Modeled vs Metered Hourly Flow Comparison at MH 12508 (R040)
November 2-3, 2006
Modeled Hourly Flow
Metered Hourly Flow
Flow, mgd
Hour
0
1
2
3
4
5
6
0
6
12
18
24
30
36
42
48

APPENDIX M

HGL Ranking Procedure - Supplemental Documentation

APPENDIX D-4
EXCERPT FROM
1995 *COLLECTION SYSTEM NEEDS ANALYSIS*
HYDRAULIC GRADE LINE STATUS

HYDRAULIC GRADE LINE STATUS DESCRIPTION
Excerpt from Section 6 of the *1995 Collection System Needs Analysis Report*
Prepared by HDR Engineering, Inc.

Hydraulic Grade Line Status --

The assessment of system improvement needs was based on a hydraulic grade line (HGL) analysis. The HGL is the projected elevation of the water surface at a specific location in the collection system. The HGL is generated by the computer model based on the design flow conditions and the hydraulic conveyance capacity of the downstream collection system. To assess the capacity of a sewer line segment, the HGL was compared to the elevations of the pipeline features such as pipe invert, the top of pipe, the ground surface at the manhole lid, etc. To identify the severity of the capacity limitation, a classification was developed called the "HGL status." This series of eight classifications (defined in Table 6-4) ranges from "OK" (HGL is below the crown of the pipe) to "LS" (manhole overflow), with intermediate levels indicating various degrees of manhole surcharging. The hydraulic conditions described in Table 6-4 are illustrated in Figure 6-2.

The HGL classification method offers several useful features:

- Assignment of a non-quantitative parameter that can be used to identify related hydraulic conditions in the collection system.
- Rating of surcharge conditions according to their property damage and health risk levels.
- Identification of collection system improvement needs according to a selected improvement HGL status threshold.
- Assessment of the consequences of not improving a sewer line that is scheduled for upgrading.

HGL Status Parameters --

Definition of key terms used in Table 6-4 is presented below:

- **Shallow HGL**. The HGL is within 3.0 feet of the ground surface.
- **Intermediate HGL.** The HGL is between 3.0 and 10.0 feet of the ground surface.

- **Deep HGL**. The HGL is greater than 10.0 feet below the ground surface.
- **Significant HGL Increase**. This means that slope of the hydraulic grade line across the pipe segment is at least five percent steeper than the slope of the pipe. This condition indicates that the pipe is creating a conveyance limitation.

Threshold HGL Status --

During the collection system analysis, HGL profiles were generated for each sewer line.

Sys_name	Improvement Project	HGL Status					Cost ($)	
		1995	2000	2005	2010	Bout	Replace	Parallel
12773_12224	South Willow Creek Int	IS	IS	IS	IS	HS	127,784	108,802

A line was identified as conveyance-limited if the HGL status equaled or exceeded the specified "threshold HGL status." In this analysis, an HGL status of "IS" or greater served as the threshold value; however, as described below, the cause of the conveyance limitation must have been attributable to the pipeline segment itself, not a downstream condition.

The year in which the improvement is first needed is indicated by two asterisks at both sides of the HGL status acronym (see *IS* is above example). The HGL status reports (included in the Appendices) list the HGL profiles for all lines that have identified conveyance limitations.

Special Considerations --

In using the HGL classification approach, there are conditions, which may cause confusion and warrant further clarification.

The first condition occurs when a pipe segment is listed as having a high HGL status, perhaps even daylighting, but is not listed as an improvement project. When this occurs, the hydraulic problem is caused by a downstream restriction, not be a capacity limitation in the pipe segment itself (see Figure 6-3). Upsizing the pipe segment will not alleviate the problem. The downstream restriction may be an undersized pipe or it may be a controlling water level at a pump station. The latter situation occurs in the Durham system where the water level in the Durham Pump Station wetwell (needed for cavitation control) causes water to back up into the interceptors, causing high HGL status despite the fact that the pipelines are not capacity limited.

A similar condition may exist for a pipe segment that is identified as needing upsizing. If a downstream restriction also exists for this pipe segment, upsizing the pipe segment may not

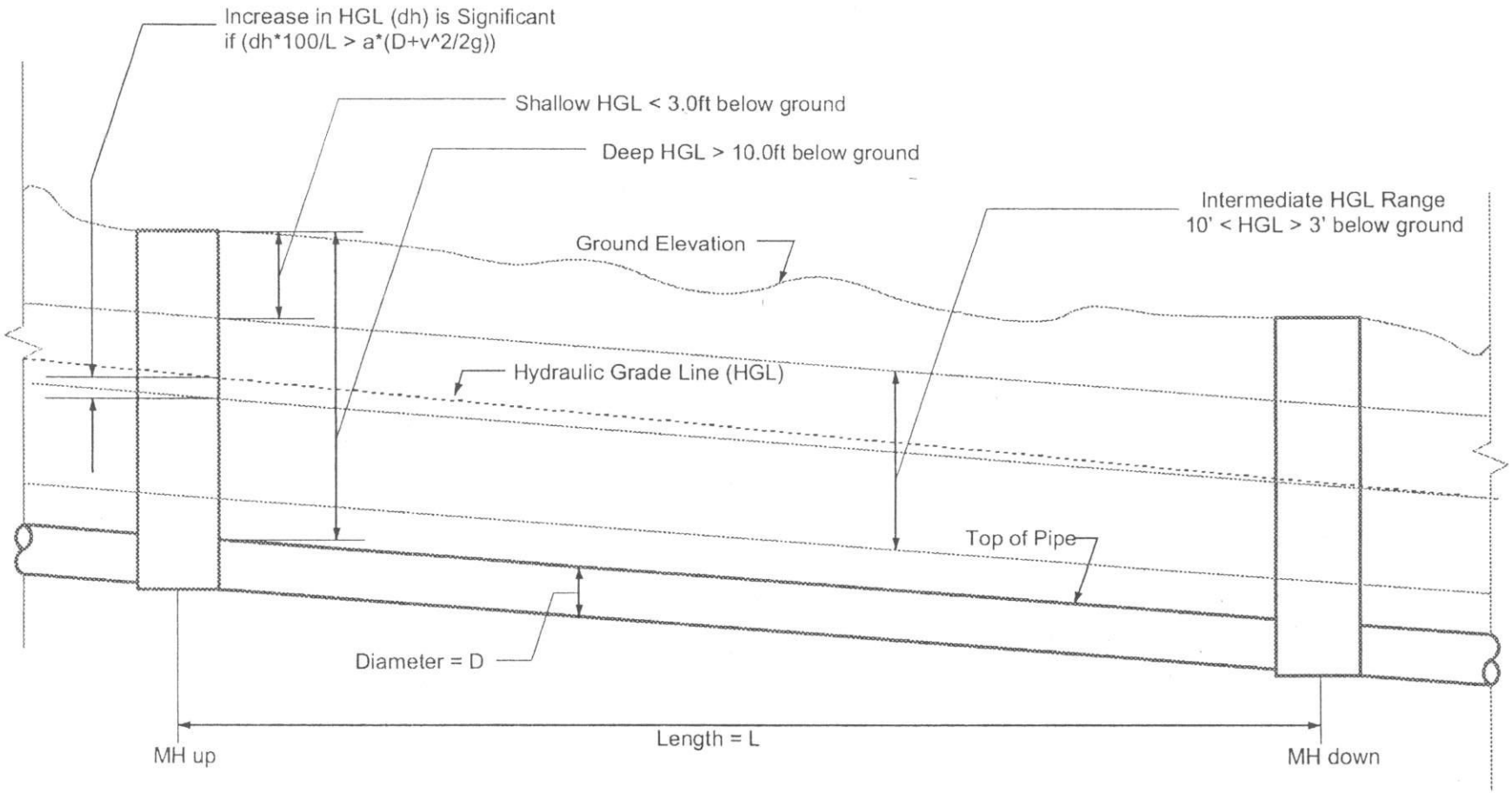
totally relieve the hydraulic problem unless the downstream restriction is also removed. Consequently, the users of the analysis results must look at the entire system when setting priorities for capacity improvements.

A third condition occurs when most of a pipeline is identified as needing upsizing, but one or two segments in the middle are not. Typically, in this situation, the individual pipe segment(s) not scheduled for improvement have higher slopes or other hydraulic features that result in adequate conveyance capacity for the projected flow (see Figure 6-4). In these cases, it is likely that the utility would replace or parallel the entire pipeline stretch, including the segments that are not identified as capacity limited; however, the costs shown in this report address only the capacity-limited segments.

Table 6-4. Hydraulic Grade Line Status Categories

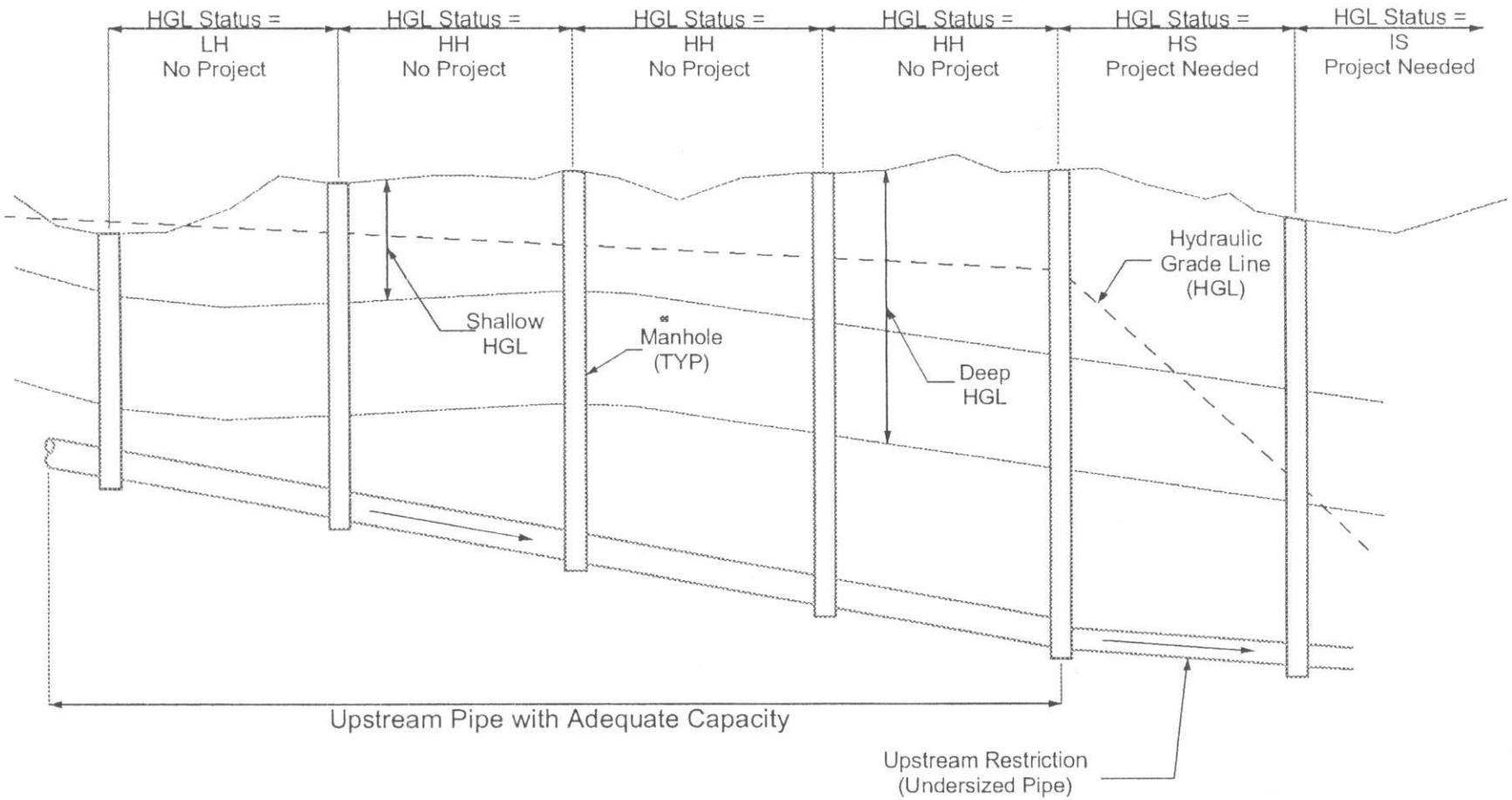
HGL Status	Description	Risk Level	Recommended Action
LS [1]	Daylight wit significant HGL increase.	High property damage and health risk.	Improve all cases
LH [2]	Daylight, i.e., the HGL is above ground elevation.	High property damage and health risk.	Improve all cases
HS [1]	High HGL with significant HGL increase.	High property damage and medium health risk.	Improve all cases
HH [2]	High HGL, i.e., the HGL is within the shallow HGL range.	High property damage and medium health risk.	Improve all cases
IS [1]	Intermediate HGL with a significant HGL increase.	Low property damage and health risk.	Improve if there are basements in service area.
IH [3]	Intermediate HGL, i.e., the HGL is between a deep HGL and a shallow HGL.	Low property damage and health risk.	None. Improvements Will not reduce HGL.
DS [1]	Deep HGL with significant increase.	Negligible	None.
DH	Deep HGL, i.e., the HGL is deeper than the specified deep HGL depth.	Negligible	None.
OK	The HGL is below the top of the pipe elevation.	Negligible	None.

Notes:
1) A significant increase in HGL over the pipe indicates a significant exceedence of the pipe's conveyance capacity.
2) Improvement of these cases will only be considered if the line's conveyance capacity has been exceeded. If the HGL condition exists due to a downstream conveyance restriction, then the upsizing of this line will not improve the HGL status.
3) Improvements of a line with IH HGL status will not improve the HGL significantly. Typically, this HGL status is associated with lines with low velocities, or lines with insignificant conveyance capacity exceedence.

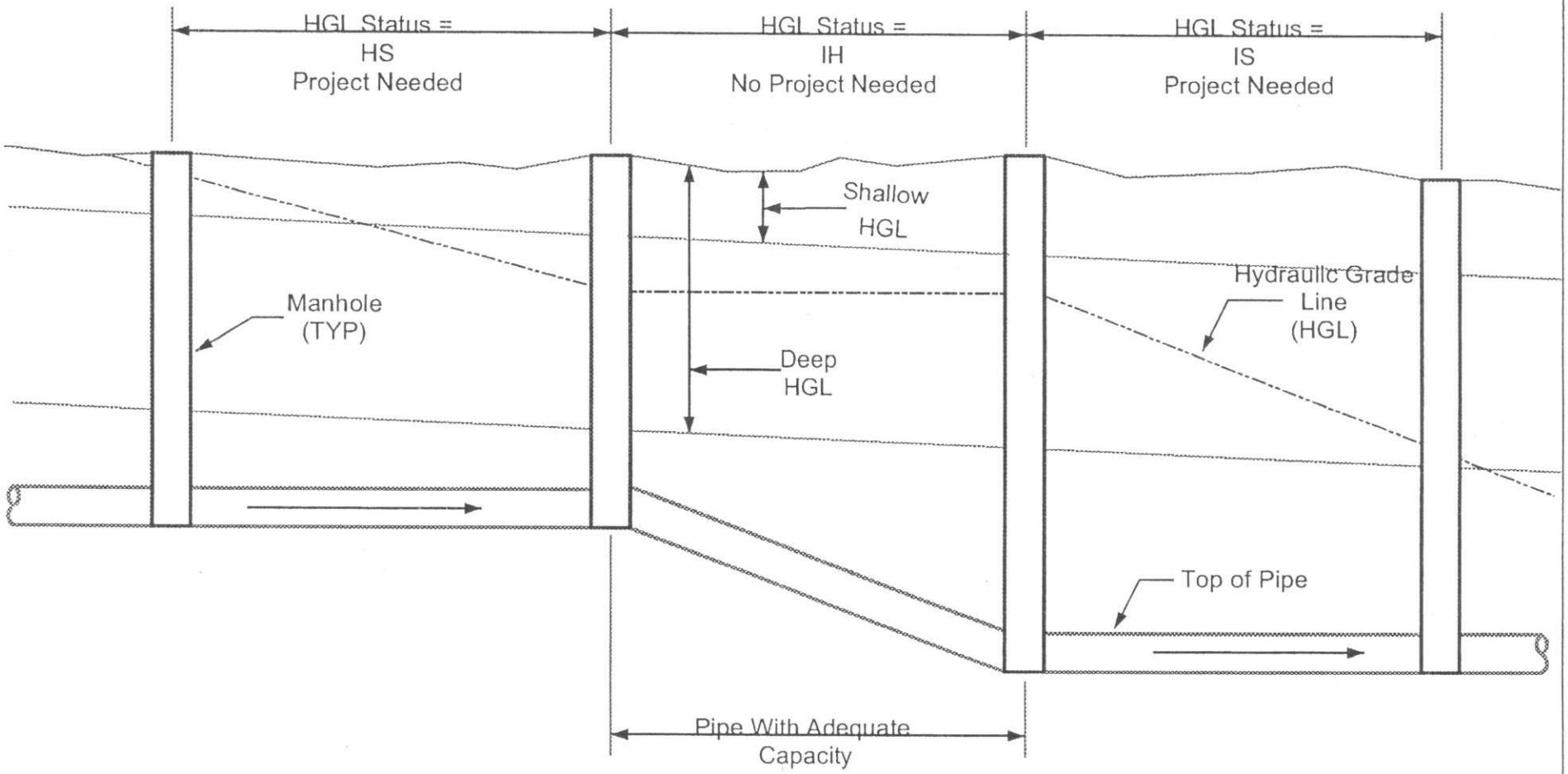


SCHEMATIC ILLUSTRATION OF THE HYDRAULIC GRADE LINE CATEGORIES

Appendix D-4
Figure 6-2



IMPACT OF DOWNSTREAM RESTRICTION ON HYDRAULIC GRADE LINE OF UPSTREAM PIPE WITH ADEQUATE CAPACITY



EXAMPLE CONDITION WHERE MOST OF PIPELINE NEEDS UPSIZING EXCEPT FOR INDIVIDUAL SEGMENT

APPENDIX N

Summary of Base Gravity Sewer Capital Improvement Project Costs

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
D-010	2015	7944	13338_13337	DLAT044	8	374	0.00440	0.52	0.53	-	-	-	0.92	0.94	0.94	12	18.9	205	76,516	99,471	124,339	1.53	66%	82,249	-
D-010	2015	7946	-	DLAT044	8	99	0.00550	0.58	0.53	0.05	90	-	0.92	0.94	0.94	12	21.0	554	54,895	71,364	89,205	1.71	66%	58,989	-
D-010	2015	1760	13333_13332	Edy Rd Trunk	10	47	0.00550	1.06	0.53	0.53	1,007	409	1.09	1.45	1.45	15	19.8	235	11,022	14,328	17,910	3.09	66%	11,802	-
D-010	2015	1759	13332_13331	Edy Rd Trunk	10	246	0.00360	0.85	0.53	0.32	611	409	1.09	1.45	1.45	15	21.0	574	141,216	183,581	229,476	2.50	66%	151,679	-
D-010	2015	1758	13331_13330	Edy Rd Trunk	10	306	0.00270	0.74	0.53	0.21	409	409	1.09	1.45	1.45	15	23.9	642	196,509	255,462	319,327	2.17	66%	209,828	-
D-010	2015	2061	13330_13329	Edy Rd Trunk	10	376	0.00290	0.76	0.53	0.23	441	409	1.09	1.45	1.45	15	25.5	1,354	509,105	661,836	827,296	2.25	66%	547,385	-
D-010	2015	2058	13329_13328	Edy Rd Trunk	10	314	0.00330	0.81	0.53	0.28	542	409	1.09	1.45	1.45	15	22.1	1,202	377,575	490,847	613,559	2.40	66%	405,560	-
D-010	2015	2057	13328_13327	Edy Rd Trunk	10	310	0.00390	0.89	0.53	0.36	686	409	1.09	1.45	1.45	15	13.7	386	119,528	155,387	194,233	2.61	66%	128,127	-
D-010	2015	2056	13327_13326	Edy Rd Trunk	10	300	0.08240	4.07	0.53	3.54	6,796	409	1.09	1.45	1.45	15	8.7	318	95,334	123,934	154,918	11.98	66%	102,235	-
D-010	2015	2055	13326_13310	Edy Rd Trunk	10	247	0.01490	1.73	0.53	1.21	2,312	409	1.09	1.45	1.45	15	9.3	326	80,524	104,681	130,851	5.09	66%	86,295	-
D-010 Total						**2,619**													**1,662,224**	**2,160,891**	**2,701,114**		**66%**	**1,784,147**	
D-020	Buildout	2039	80905_13303	Onion Flat Trunk	18	242	0.00330	3.91	1.70	2.21	4,242	1,757	2.62	4.12	17.14	33	13.8	650	157,403	204,623	255,779	19.63	80%	204,794	Regional
D-020	Buildout	2038	13303_13302	Onion Flat Trunk	18	476	0.00320	3.84	1.70	2.15	4,113	1,757	2.62	4.12	17.13	33	7.3	534	254,393	330,711	413,388	19.33	80%	331,145	Regional
D-020	Buildout	2037	13302_13301	Onion Flat Trunk	18	470	0.00340	3.96	1.70	2.26	4,331	1,757	2.62	4.12	17.11	33	4.3	482	226,449	294,384	367,980	19.92	80%	294,881	Regional
D-020	Buildout	2036	13301_13300	Onion Flat Trunk	18	452	0.00290	3.65	1.70	1.95	3,743	1,757	2.62	4.12	17.09	33	2.3	272	123,082	160,006	200,008	18.40	80%	160,337	Regional
D-020	Buildout	2035	13300_13299	Onion Flat Trunk	18	432	0.00300	3.75	1.70	2.05	3,933	1,757	2.62	4.12	17.07	33	3.1	368	158,988	206,684	258,355	18.71	80%	206,626	Regional
D-020	Buildout	2034	13299_13298	Onion Flat Trunk	18	431	0.00330	3.92	1.69	2.23	4,268	1,757	2.62	4.11	17.06	33	5.0	493	212,435	276,165	345,206	19.63	80%	276,270	Regional
D-020	Buildout	2033	13298_13297	Onion Flat Trunk	18	522	0.00350	4.03	1.69	2.34	4,481	1,757	2.62	4.11	17.04	33	5.6	504	263,165	342,114	427,642	20.21	80%	342,410	Regional
D-020	Buildout	2032	13297_13296	Onion Flat Trunk	18	520	0.00230	3.24	1.69	1.55	2,971	1,757	2.61	4.11	17.01	33	5.6	504	262,203	340,863	426,079	16.38	80%	341,799	Regional
D-020	Buildout	2031	13296_13295	Onion Flat Trunk	18	515	0.00300	3.71	1.69	2.02	3,870	1,757	2.61	4.10	16.98	33	7.0	528	272,153	353,798	442,248	18.71	80%	354,599	Regional
D-020	Buildout	2030	13295_13294	Onion Flat Trunk	18	520	0.00300	3.75	1.69	2.06	3,953	1,757	2.61	4.10	16.94	33	8.0	547	284,599	369,979	462,474	18.71	80%	369,778	Regional
D-020	Buildout	2029	13294_13293	Onion Flat Trunk	18	335	0.00300	3.74	1.69	2.05	3,929	1,757	2.61	4.10	16.89	33	10.8	896	300,122	390,158	487,697	18.71	80%	390,334	Regional
D-020 Total						**4,915**													**2,514,990**	**3,269,487**	**4,086,858**		**80%**	**3,272,971**	
D-021	Buildout	2028	13293_11663	Onion Flat Trunk	18	130	0.00150	2.60	1.68	0.92	1,757	1,757	2.85	4.41	17.22	33	13.9	326	42,423	55,150	68,937	13.23	80%	55,384	Regional
D-021	Buildout	2027	11663_11664	Upper Tualatin Int	24	531	0.00150	5.69	4.17	1.51	2,901	-	6.41	9.83	67.20	66	23.9	1,205	639,788	831,724	1,039,655	84.02	93%	969,278	Regional
D-021	Buildout	8865	-	Lateral Starting at Entity 8724	24	15	0.53330	107.01	4.17	102.84	197,160	197,160	6.75	10.17	67.55	66	36.8	1,570	23,546	30,610	38,262	1,584	93%	35,678	Regional
D-021 Total						**676**													**705,757**	**917,484**	**1,146,855**		**92%**	**1,060,340**	
D-050	Existing	911	10184_10185	Hall Blvd. Lateral	10	370	0.00600	1.10	1.20	-	-	-	1.27	1.30	1.30	12	9.4	145	53,622	69,709	87,136	1.78	38%	33,397	-
D-050	Existing	912	10185_10186	Hall Blvd. Lateral	10	390	0.00590	1.09	1.20	-	-	-	1.27	1.30	1.30	12	9.1	143	55,881	72,646	90,807	1.77	38%	34,696	-
D-050	Existing	913	10186_10190	Hall Blvd. Lateral	8	332	0.02680	1.28	1.20	0.08	151	-	1.27	1.30	1.30	12	9.3	144	47,814	62,158	77,697	3.77	66%	51,268	-
D-050	Existing	914	10190_10191	Hall Blvd. Lateral	8	329	0.03330	1.43	1.20	0.23	435	-	1.27	1.30	1.30	12	9.6	146	48,185	62,640	78,300	4.20	66%	51,648	-
D-050	Existing	915	10191_10181	Hall Blvd. Lateral	8	135	0.05830	1.89	1.20	0.69	1,319	-	1.27	1.30	1.30	12	10.0	149	20,149	26,193	32,741	5.56	66%	21,605	-
D-050	Existing	909	10181_10182	Hall Blvd. Lateral	8	216	0.02800	1.31	1.20	0.11	206	-	1.27	1.30	1.30	12	10.0	149	32,238	41,909	52,386	3.85	66%	34,583	-
D-050	Existing	910	10182_10177	Hall Blvd. Lateral	8	285	0.01620	1.00	1.20	-	-	-	1.27	1.30	1.30	12	10.0	149	42,536	55,296	69,121	2.93	66%	45,586	-
D-050	Existing	907	10177_10178	Hall Blvd. Lateral	8	279	0.01200	0.86	1.20	-	-	-	1.27	1.30	1.30	12	10.0	149	41,640	54,132	67,665	2.52	66%	44,641	-
D-050	Existing	908	10178_14284	Hall Blvd. Lateral	8	282	0.00800	0.70	1.20	-	-	-	1.27	1.30	1.30	12	10.0	149	42,088	54,714	68,393	2.06	66%	45,171	-
D-050	Existing	917	14284_06636	Hall Blvd. Lateral	8	88	0.02400	1.21	1.20	0.01	21	-	1.27	1.30	1.30	12	10.0	149	13,109	17,042	21,303	3.57	66%	14,062	-
D-050 Total						**2,706**													**397,261**	**516,440**	**645,550**		**58%**	**376,658**	
D-080	2015	7451	27768_27767	Bluff/Cipole Sewer	10	356	0.00370	0.86	0.28	0.58	1,117	1,016	1.12	7.13	12.92	30	14.5	617	219,701	285,611	357,013	16.12	95%	337,939	Regional
D-080	2015	7453	27767_27766	Bluff/Cipole Sewer	10	361	0.00320	0.81	0.28	0.53	1,016	1,016	1.12	7.13	12.91	30	19.0	694	250,390	325,506	406,883	14.99	95%	384,946	Regional
D-080	2015	7455	27766_27765	Bluff/Cipole Sewer	10	299	0.00340	0.83	0.28	0.55	1,064	1,016	1.12	7.13	12.89	30	17.0	659	197,117	256,253	320,316	15.45	95%	303,052	Regional
D-080	2015	7457	27765_27764	Bluff/Cipole Sewer	10	136	0.02910	2.42	0.28	2.14	4,111	1,016	1.12	7.12	12.88	30	15.7	637	86,638	112,629	140,786	45.20	95%	133,243	Regional
D-080	2015	7459	27764_27763	Bluff/Cipole Sewer	10	60	0.00630	1.13	0.28	0.85	1,632	1,016	1.12	7.12	12.86	30	17.1	662	39,724	51,642	64,552	21.03	95%	61,086	Regional
D-080	2015	7461	27763_27762	Bluff/Cipole Sewer	10	160	0.00560	1.06	0.28	0.79	1,508	1,016	1.12	7.12	12.84	30	15.5	635	101,612	132,096	165,120	19.83	95%	156,255	Regional
D-080	2015	7463	27762_27761	Bluff/Cipole Sewer	10	145	0.00510	1.01	0.28	0.74	1,411	1,016	1.12	7.12	12.83	30	15.5	317	46,006	59,808	74,760	18.92	95%	70,755	Regional
D-080	2015	7465	27761_27760	Bluff/Cipole Sewer	10	262	0.03730	2.74	0.28	2.46	4,719	1,016	1.12	7.12	12.81	30	14.6	309	81,024	105,331	131,664	51.17	95%	124,617	Regional
D-080	2015	7467	27760_27759	Bluff/Cipole Sewer	10	424	0.00480	0.98	0.28	0.71	1,356	1,016	1.12	7.12	12.80	30	9.1	262	111,163	144,512	180,640	18.36	95%	170,953	Regional
D-080	2015	7469	27759_27758	Bluff/Cipole Sewer	10	343	0.01080	1.47	0.28	1.20	2,295	1,016	1.12	7.12	12.78	30	8.0	253	86,938	113,019	141,274	27.54	95%	133,711	Regional
D-080 Total						**2,546**													**1,220,313**	**1,586,407**	**1,983,009**		**95%**	**1,876,557**	
D-120	Existing	1433	21074_21142	East Tigard Trunk	12	124	0.00750	2.00	1.31	0.68	1,313	-	1.48	1.75	1.75	15	10.8	173	21,444	27,877	34,846	3.61	45%	15,574	-
D-120	Existing	1434	21142_21143	East Tigard Trunk	12	260	0.00300	1.26	1.31	-	-	-	1.48	1.75	1.75	15	9.1	162	42,045	54,659	68,323	2.29	45%	30,784	-
D-120	Existing	1435	21143_21144	East Tigard Trunk	12	326	0.00310	1.28	1.57	-	-	-	1.89	2.17	2.17	15	7.0	147	48,030	62,439	78,048	2.32	45%	35,104	-
D-120	Existing	1436	21144_21145	East Tigard Trunk	12	344	0.00290	1.24	1.57	-	-	-	1.89	2.17	2.17	15	5.5	137	47,173	61,325	76,656	2.25	45%	34,215	-
D-120	Existing	1437	21145_21146	East Tigard Trunk	12	391	0.00510	1.65	1.57	0.08	149	-	1.89	2.17	2.17	15	5.5	137	53,618	69,703	87,129	2.98	45%	38,873	-
D-120	Existing	1438	21146_21147	East Tigard Trunk	12	25	0.00160	0.92	1.57	-	-	-	1.89	2.16	2.16	15	6.0	141	3,513	4,567	5,709	1.67	45%	2,552	-
D-120 Total						**1,470**													**215,823**	**280,569**	**350,712**		**45%**	**157,102**	
D-170	Existing	944	04731_04732	Metzger Interceptor	12	169	0.00340	1.34	2.68	-	-	-	2.68	2.73	2.73	15	8.8	159	26,939	35,020	43,775	2.43	45%	19,660	-
D-170	Existing	945	04732_04736	Metzger Interceptor	12	95	0.00860	2.14	2.68	-	-	-	2.68	2.73	2.73	15	8.5	157	14,946	19,430	24,287	3.87	45%	10,831	-
D-170	Existing	946	04736_04742	Metzger Interceptor	12	228	0.00860	2.13	2.68	-	-	-	2.68	2.73	2.73	15	8.9	160	36,467	47,407	59,259	3.87	45%	26,576	-
D-170	Existing	947	04742_04745	Metzger Interceptor	12	364	0.00860	2.14	2.68	-	-	-	2.68	2.72	2.72	15	8.4	157	57,081	74,205	92,757	3.87	45%	41,459	-
D-170	Existing	948	04745_04748	Metzger Interceptor	12	396	0.00860	2.14	2.97	-	-	-	2.97	3.03	3.03	15	7.7	152	60,120	78,156	97,695	3.87	45%	43,715	-
D-170	Existing	949	04748_04760	Metzger Interceptor	12	128	0.00890	2.18	2.96	-	-	-	2.96	3.02	3.02	15	7.4	150	19,233	25,002	31,253	3.94	45%	13,965	-
D-170	Existing	832	04760_04765	Metzger Interceptor	12	194	0.01290	2.62	2.96	-	-	-	2.96	3.02	3.02	15	7.8	152	29,571	38,443	48,054	4.74	45%	21,495	-
D-170	Existing	833	04765_04837	Metzger Interceptor	12	302	0.00660	1.88	2.96	-	-	-	2.96	3.02	3.02	15	6.5	144	43,467	56,507	70,634	3.39	45%	31,508	-
D-170	Existing	838	04837_04844	Metzger Interceptor	12	323	0.00770	2.03	2.96	-	-	-	2.96	3.02	3.02	15	5.3	135	43,744	56,867	71,084	3.66	45%	31,670	-

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
D-170	Existing	839	04844_04845	Metzger Interceptor	12	149	0.00860	2.14	2.96	-	-	-	2.96	3.02	3.02	15	6.1	141	21,081	27,405	34,256	3.87	45%	15,323	-
D-170	Existing	840	04845_04847	Metzger Interceptor	12	309	0.00860	2.14	2.96	-	-	-	2.96	3.01	3.01	15	5.9	140	43,130	56,069	70,086	3.87	45%	31,302	-
D-170	Existing	841	04847_04848	Metzger Interceptor	12	280	0.00860	2.14	2.96	-	-	-	2.96	3.01	3.01	15	4.9	133	37,245	48,418	60,523	3.87	45%	27,041	-
D-170	Existing	842	04848_04849	Metzger Interceptor	12	221	0.00930	2.22	2.95	-	-	-	2.95	3.01	3.01	15	8.4	157	34,626	45,014	56,268	4.02	45%	25,188	-
D-170	Existing	843	04849_04855	Metzger Interceptor	15	223	0.00750	3.62	4.04	-	-	-	4.07	4.14	4.14	15	7.0	147	32,832	42,681	53,352	3.61	0%	(102)	-
D-170 Total						**3,381**													**500,482**	**650,626**	**813,283**		**42%**	**339,632**	
D-171	Existing	834	04826_04827	Metzger Interceptor	10	182	0.00400	0.90	1.14	-	-	-	1.17	1.18	1.18	12	9.1	143	26,040	33,852	42,315	1.46	38%	16,193	-
D-171	Existing	835	04827_04828	Metzger Interceptor	10	333	0.00400	0.90	1.14	-	-	-	1.17	1.18	1.18	12	17.6	196	65,132	84,672	105,840	1.46	38%	40,644	-
D-171	Existing	836	04828_04829	Metzger Interceptor	10	244	0.00400	0.89	1.14	-	-	-	1.17	1.18	1.18	12	15.8	184	44,917	58,392	72,989	1.46	39%	28,127	-
D-171	Existing	837	04829_04849	Metzger Interceptor	10	200	0.04560	3.03	1.14	1.89	3,616	-	1.17	1.18	1.18	12	11.8	160	31,903	41,474	51,842	4.91	38%	19,877	-
D-171 Total						**959**													**167,991**	**218,389**	**272,986**		**38%**	**104,841**	
D-220	2015	1897	11665_11666	Upper Tualatin Int	27	453	0.00100	6.32	4.78	1.54	2,960	-	7.70	10.72	67.50	72	8.2	686	310,976	404,268	505,335	86.52	93%	468,406	Regional
D-220	2015	1898	11666_11667	Upper Tualatin Int	27	481	0.00110	6.66	4.67	1.99	3,817	-	7.48	10.58	67.41	72	7.7	679	326,802	424,842	531,053	90.74	93%	492,081	Regional
D-220	2015	1899	11667_11668	Upper Tualatin Int	27	463	0.00110	6.66	4.56	2.10	4,023	-	7.29	10.54	67.33	72	7.7	680	314,700	409,110	511,388	90.74	93%	473,866	Regional
D-220	2015	1900	11668_11669	Upper Tualatin Int	27	87	0.00210	9.12	4.47	4.65	8,921	-	7.14	10.50	67.24	72	6.1	161	13,980	18,174	22,717	125.37	93%	21,064	Regional
D-220	2015	1901	11669_11670	Upper Tualatin Int	27	511	0.00100	6.34	4.93	1.41	2,694	-	7.66	11.06	67.74	72	6.9	1,858	949,403	1,234,224	1,542,780	86.52	93%	1,429,771	Regional
D-220	2015	1902	11670_11671	Upper Tualatin Int	27	500	0.00100	6.34	4.84	1.50	2,876	-	7.61	11.00	67.66	72	9.4	2,109	1,054,738	1,371,160	1,713,950	86.52	93%	1,588,275	Regional
D-220	2015	1903	11671_11672	Upper Tualatin Int	27	500	0.00100	6.34	4.83	1.52	2,907	-	7.55	10.94	67.58	72	9.4	2,109	1,054,738	1,371,160	1,713,950	86.52	93%	1,588,275	Regional
D-220	2015	1904	11672_11673	Upper Tualatin Int	27	237	0.00140	7.60	4.82	2.78	5,326	-	7.49	10.89	67.49	72	10.4	2,148	509,000	661,700	827,125	102.37	93%	765,731	Regional
D-220	2015	1905	11673_12145	Upper Tualatin Int	27	86	0.00030	3.75	4.82	-	-	-	7.47	10.87	67.41	72	11.0	2,176	187,146	243,290	304,113	47.39	92%	280,067	Regional
D-220	2015	1927	12145_11674	Upper Tualatin Int	27	244	0.00120	7.03	4.81	2.22	4,259	-	7.45	10.86	67.33	72	9.2	700	170,794	222,032	277,540	94.77	93%	256,941	Regional
D-220 Total						**3,562**													**4,892,277**	**6,359,960**	**7,949,950**		**93%**	**7,364,477**	
D-230	Existing	8236	06338_06340	King City Trunk	8	127	0.00590	0.60	0.81	-	-	-	0.81	0.84	0.84	10	9.4	131	16,629	21,618	27,023	1.09	45%	12,074	-
D-230	Existing	8165	06340_06940	King City Trunk	8	177	0.00590	0.60	0.81	-	-	-	0.81	0.84	0.84	10	10.3	137	24,220	31,486	39,357	1.09	45%	17,538	-
D-230	Existing	8160	06940_06342	King City Trunk	8	204	0.00590	0.60	0.81	-	-	-	0.81	0.84	0.84	10	11.4	143	29,195	37,953	47,441	1.09	45%	21,253	-
D-230	Existing	8163	06342_06343	King City Trunk	8	227	0.00590	0.60	0.81	-	-	-	0.81	0.84	0.84	10	12.7	150	34,088	44,315	55,394	1.09	45%	24,882	-
D-230 Total						**735**													**104,132**	**135,372**	**169,215**		**45%**	**75,746**	
D-240	Buildout	1488	15065_15648	Bull Mountain Trunk	12	35	0.03600	4.38	2.02	2.36	4,516	1,996	3.71	5.31	5.59	18	7.0	165	5,784	7,519	9,399	12.88	66%	6,203	-
D-240	Buildout	1490	15648_15643	Bull Mountain Trunk	12	88	0.02510	3.66	1.98	1.67	3,209	1,996	3.67	5.29	5.53	18	7.5	169	14,848	19,302	24,128	10.75	66%	15,920	-
D-240	Buildout	1489	15643_15064	Bull Mountain Trunk	12	265	0.03580	4.37	1.94	2.43	4,651	1,996	3.64	5.27	5.48	18	5.0	151	39,967	51,957	64,946	12.84	66%	42,866	-
D-240	Buildout	1487	15064_15063	Bull Mountain Trunk	12	220	0.01600	2.92	1.88	1.04	1,996	1,996	3.58	5.25	5.45	18	4.8	149	32,787	42,623	53,278	8.58	66%	35,158	-
D-240	Buildout	1486	15063_15062	Bull Mountain Trunk	15	449	0.01000	4.18	1.82	2.36	4,529	1,996	3.55	5.22	5.40	18	5.3	153	68,536	89,096	111,370	6.79	38%	42,699	-
D-240	Buildout	1485	15062_15061	Bull Mountain Trunk	15	300	0.02310	6.36	1.75	4.61	8,840	1,996	3.51	5.18	5.32	18	5.5	154	46,253	60,129	75,161	10.31	38%	28,780	-
D-240	Buildout	1484	15061_15060	Bull Mountain Trunk	15	151	0.01110	4.40	1.72	2.68	5,137	1,996	3.48	5.14	5.26	18	6.3	160	24,150	31,395	39,243	7.15	38%	15,088	-
D-240 Total						**1,508**													**232,323**	**302,021**	**377,526**		**49%**	**186,714**	
D-245	2015	8474	15074_15073	DLAT024	8	153	0.00400	0.49	0.27	0.23	432	426	2.41	4.05	4.04	18	29.6	795	121,598	158,077	197,596	4.29	88%	174,843	-
D-245	2015	8493	15073_15072	DLAT024	8	400	0.00400	0.49	0.27	0.23	433	426	2.41	4.05	4.03	18	35.7	933	373,158	485,106	606,382	4.29	88%	536,466	-
D-245	2015	8489	15072_15071	DLAT024	8	400	0.00400	0.49	0.27	0.23	433	426	2.40	4.04	4.03	18	39.8	1,026	410,267	533,348	666,685	4.29	88%	589,816	-
D-245	2015	8494	15071_15250	DLAT024	8	228	0.00400	0.49	0.27	0.23	432	426	2.39	4.03	4.02	18	28.5	771	175,839	228,590	285,738	4.29	88%	252,835	-
D-245	2015	8484	15250_15070	DLAT024	8	84	0.00400	0.50	0.27	0.23	439	426	2.38	4.03	4.02	18	19.1	252	21,159	27,507	34,384	4.29	88%	30,394	-
D-245	2015	8495	15070_15069	DLAT024	8	66	0.00390	0.49	0.27	0.22	426	426	2.38	4.02	4.01	18	16.9	236	15,587	20,264	25,329	4.24	88%	22,395	-
D-245	2015	8482	15069_15068	DLAT024	8	65	0.00400	0.49	0.27	0.23	433	426	2.38	4.02	4.00	18	22.2	628	40,841	53,094	66,367	4.29	88%	58,715	-
D-245 Total						**1,396**													**1,158,451**	**1,505,986**	**1,882,482**		**88%**	**1,665,465**	
D-250	2015	1911	11679_15345	Upper Tualatin Int	36	274	0.00030	6.91	9.72	-	-	-	13.82	18.90	75.41	84	9.3	878	240,676	312,878	391,098	71.48	90%	353,317	Regional
D-250	2015	1941	15345_11680	Upper Tualatin Int	36	260	0.00080	11.98	9.71	2.27	4,355	-	13.80	18.89	75.30	84	10.5	896	232,831	302,681	378,351	116.73	90%	339,510	Regional
D-250	2015	1912	11680_11681	Upper Tualatin Int	36	136	0.00070	11.72	9.70	2.01	3,858	-	13.80	18.89	75.19	84	11.1	905	123,123	160,059	200,074	109.19	89%	178,607	Regional
D-250	2015	1913	11681_11682	Upper Tualatin Int	36	71	0.00010	5.13	9.70	-	-	-	13.79	18.88	75.08	84	11.1	2,716	192,848	250,702	313,378	41.27	88%	274,443	Regional
D-250	2015	1914	11682_11683	Upper Tualatin Int	36	59	0.00050	9.74	9.69	0.05	105	-	13.78	18.88	74.98	84	11.2	2,719	160,441	208,573	260,716	92.28	89%	233,191	Regional
D-250	2015	1915	11683_11684	Upper Tualatin Int	36	86	0.00050	9.32	9.68	-	-	-	13.78	18.88	74.87	84	13.7	945	81,244	105,617	132,021	92.28	90%	118,691	Regional
D-250	2015	1916	11684_11685	Upper Tualatin Int	36	450	0.00050	9.77	9.93	-	-	-	14.02	19.15	75.10	84	15.9	977	439,611	571,494	714,368	92.28	89%	638,754	Regional
D-250	2015	1917	11685_11698	Upper Tualatin Int	36	501	0.00050	9.65	9.91	-	-	-	14.01	19.14	75.00	84	15.6	973	487,468	633,709	792,136	92.28	90%	709,294	Regional
D-250	2015	1923	11698_11699	Upper Tualatin Int	36	502	0.00050	9.64	9.89	-	-	-	13.99	19.13	74.76	84	14.9	962	482,760	627,588	784,485	92.28	90%	702,520	Regional
D-250	2015	1924	11699_11700	Upper Tualatin Int	36	500	0.00050	9.66	10.14	-	-	-	14.25	19.39	74.81	84	13.6	943	471,405	612,827	766,034	92.28	90%	685,841	Regional
D-250	2015	1925	11700_18010	Upper Tualatin Int	36	203	0.00050	9.59	10.14	-	-	-	14.24	19.38	74.58	84	13.3	938	190,395	247,514	309,392	92.28	90%	277,244	Regional
D-250	2015	1943	18010_11701	Upper Tualatin Int	36	293	0.00220	20.35	10.13	10.22	19,595	-	14.24	19.37	74.49	84	13.7	944	276,465	359,404	449,255	193.57	89%	402,026	Regional
D-250 Total						**3,335**													**3,379,266**	**4,393,046**	**5,491,307**		**89%**	**4,913,439**	
D-255	Buildout	1926	11701_11702	Upper Tualatin Int	42	515	0.00040	13.16	10.94	2.22	4,253	-	15.06	20.26	75.21	84	12.6	1,855	955,242	1,241,815	1,552,268	82.54	84%	1,304,776	Regional
D-255	Buildout	1948	11702_11703	Upper Tualatin Int	42	564	0.00040	13.16	11.05	2.11	4,039	-	15.18	20.39	75.14	84	11.3	1,816	1,024,342	1,331,645	1,664,556	82.54	84%	1,399,147	Regional
D-255	Buildout	1456	11703_16720	Upper Tualatin Int	42	246	0.00080	18.58	11.05	7.53	14,435	-	15.17	20.37	75.09	84	11.5	1,823	448,384	582,899	728,623	116.73	84%	612,633	Regional
D-255	Buildout	1497	16720_11710	Upper Tualatin Int	42	503	0.00020	9.19	11.23	-	-	-	15.36	20.59	75.35	84	11.7	1,827	919,094	1,194,822	1,493,528	58.36	84%	1,258,384	Regional
D-255	Buildout	1462	11710_11711	Upper Tualatin Int	42	482	0.00040	13.27	11.23	2.05	3,929	-	15.35	20.58	75.31	84	12.8	1,862	897,451	1,166,686	1,458,357	82.54	84%	1,223,806	Regional
D-255	Buildout	1463	11711_11712	Upper Tualatin Int	42	416	0.00040	13.17	11.21	1.96	3,761	-	15.35	20.56	75.25	84	13.0	1,868	776,886	1,009,952	1,262,440	82.54	84%	1,060,940	Regional
D-255	Buildout	1464	11712_11713	Upper Tualatin Int	42	586	0.00040	12.91	11.58	1.33	2,546	-	15.72	20.95	75.63	84	13.2	1,874	1,097,900	1,427,270	1,784,088	82.54	84%	1,505,010	Regional
D-255	Buildout	1444	11713_11714	Upper Tualatin Int	42	453	0.00040	12.99	11.58	1.41	2,702	-	15.72	20.94	75.53	84	12.9	1,865	844,685	1,098,091	1,372,613	82.54	84%	1,156,579	Regional
D-255 Total						**3,765**													**6,963,984**	**9,053,179**	**11,316,474**		**84%**	**9,521,276**	

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
D-260	Buildout	1563	11718_11719	Upper Tualatin Int	42	634	0.00040	12.94	12.02	0.92	1,761	-	16.16	21.43	75.96	84	16.7	990	627,591	815,868	1,019,835	82.54	84%	859,939	Regional
D-260	Buildout	1595	11719_11720	Upper Tualatin Int	42	696	0.00040	12.84	12.02	0.81	1,562	-	16.15	21.41	75.82	84	17.5	1,001	696,946	906,029	1,132,537	82.54	84%	956,416	Regional
D-260	Buildout	1300	11720_11721	Upper Tualatin Int	42	635	0.00040	13.19	12.17	1.02	1,948	-	16.30	21.53	75.92	84	15.3	968	614,447	798,781	998,477	82.54	84%	838,952	Regional
D-260 Total						**1,965**													**1,938,984**	**2,520,679**	**3,150,848**		**84%**	**2,655,307**	
D-270	Buildout	8496	97926_97925	Victoria Woods Trunk	8	271	0.00690	0.65	0.03	0.62	1,180	-	0.10	0.76	0.76	10	10.9	140	37,957	49,344	61,680	1.18	45%	27,620	-
D-270	Buildout	8500	97925_97924	Victoria Woods Trunk	8	268	0.00370	0.48	0.03	0.44	848	-	0.10	0.76	0.76	10	15.2	165	44,084	57,309	71,637	0.86	45%	32,022	-
D-270 Total						**538**													**82,041**	**106,653**	**133,317**		**45%**	**59,642**	
D-275	Buildout	8510	97116_97117	Victoria Woods Trunk	8	178	0.00430	0.52	0.03	0.48	924	-	0.10	0.76	0.76	12	7.3	130	23,122	30,059	37,573	1.51	66%	24,740	-
D-275	Buildout	8508	97117_97115	Victoria Woods Trunk	8	278	0.00210	0.36	0.03	0.33	627	-	0.10	0.75	0.75	12	9.6	146	40,670	52,871	66,089	1.05	66%	43,502	-
D-275	Buildout	8505	97115_97114	Victoria Woods Trunk	8	58	0.01250	0.87	0.03	0.84	1,611	-	0.10	0.75	0.75	12	10.1	150	8,631	11,221	14,026	2.57	66%	9,262	-
D-275	Buildout	8512	97114_97532	Victoria Woods Trunk	8	124	0.05920	1.90	0.03	1.87	3,587	-	0.10	0.75	0.75	12	10.3	151	18,737	24,358	30,447	5.60	66%	20,093	-
D-275	Buildout	8521	97532_97531	Victoria Woods Trunk	8	166	0.00950	0.76	0.03	0.73	1,396	-	0.10	0.75	0.75	12	11.5	158	26,152	33,997	42,496	2.24	66%	28,068	-
D-275	Buildout	8523	97531_97530	Victoria Woods Trunk	8	135	0.00640	0.62	0.03	0.59	1,133	-	0.10	0.75	0.75	12	11.8	160	21,538	28,000	35,000	1.84	66%	23,125	-
D-275	Buildout	8525	97530_97523	Victoria Woods Trunk	8	163	0.00650	0.63	0.03	0.60	1,148	-	0.10	0.75	0.75	12	14.0	173	28,061	36,479	45,599	1.86	66%	30,057	-
D-275	Buildout	8514	97523_97522	Victoria Woods Trunk	8	126	0.00470	0.54	0.03	0.51	971	-	0.10	0.75	0.75	12	14.4	175	22,148	28,792	35,990	1.58	66%	23,687	-
D-275	Buildout	8520	97522_97521	Victoria Woods Trunk	8	123	-	-	0.03	-	-	-	0.10	0.75	0.75	12	11.7	159	19,458	25,295	31,619	-	0%	-	-
D-275	Buildout	8517	97521_97520	Victoria Woods Trunk	8	136	0.00470	0.54	0.03	0.51	969	-	0.10	0.75	0.75	12	9.8	148	20,058	26,075	32,594	1.58	66%	21,478	-
D-275 Total						**1,485**													**228,575**	**297,147**	**371,434**		**60%**	**224,012**	
D-280	Buildout	7471	27758_27757	Bluff/Cipole Sewer	10	177	0.02720	2.34	0.28	2.06	3,958	1,016	1.12	7.12	12.76	30	13.0	296	52,333	68,033	85,041	43.70	95%	80,484	Regional
D-280	Buildout	1826	20784_21015	Tualatin Reservoir Trunk	15	289	0.00320	2.36	0.40	1.96	3,760	1,216	1.30	7.95	13.51	30	15.0	313	90,337	117,438	146,797	14.99	84%	123,673	Regional
D-280	Buildout	1877	21015_21014	Tualatin Reservoir Trunk	15	400	0.00250	2.09	0.40	1.69	3,245	1,216	1.30	7.95	13.50	30	14.5	309	123,530	160,589	200,736	13.25	84%	169,033	Regional
D-280	Buildout	1876	21014_21013	Tualatin Reservoir Trunk	15	209	0.00290	2.26	0.40	1.86	3,568	1,216	1.30	7.95	13.48	30	14.9	312	65,303	84,894	106,118	14.27	84%	89,308	Regional
D-280	Buildout	1875	21013_21012	Tualatin Reservoir Trunk	15	326	0.00240	2.05	0.52	1.52	2,919	1,216	1.42	8.07	13.58	30	13.9	304	98,950	128,635	160,794	12.98	84%	135,443	Regional
D-280	Buildout	1874	21012_21011	Tualatin Reservoir Trunk	15	87	0.01000	4.18	0.52	3.66	7,019	1,216	1.42	8.06	13.56	30	14.2	306	26,622	34,609	43,261	26.50	84%	36,430	Regional
D-280	Buildout	1873	21011_21010	Tualatin Reservoir Trunk	10	306	0.02650	2.31	0.52	1.79	3,427	1,216	1.42	8.06	13.55	30	12.1	288	88,148	114,592	143,240	43.13	95%	135,566	Regional
D-280	Buildout	1872	21010_21009	Tualatin Reservoir Trunk	10	65	0.25340	7.14	0.52	6.62	12,693	1,216	1.42	8.06	13.53	30	8.3	256	16,608	21,591	26,989	133.38	95%	25,543	Regional
D-280	Buildout	1871	21009_20766	Tualatin Reservoir Trunk	15	385	0.00960	4.09	0.52	3.57	6,840	1,216	1.42	8.06	13.51	30	8.9	261	100,412	130,536	163,170	25.96	84%	137,457	Regional
D-280	Buildout	1808	20766_20767	Tualatin Reservoir Trunk	15	345	0.00840	3.84	0.86	2.98	5,716	1,216	1.95	9.40	14.79	30	10.0	271	93,369	121,380	151,725	24.28	84%	127,715	Regional
D-280	Buildout	1809	20767_20768	Tualatin Reservoir Trunk	15	400	0.00810	3.78	0.86	2.92	5,591	1,216	1.95	9.40	14.79	30	10.1	271	108,545	141,108	176,385	23.85	84%	148,448	Regional
D-280	Buildout	1810	20768_20769	Tualatin Reservoir Trunk	15	500	0.00770	3.67	0.86	2.81	5,389	1,216	1.95	9.40	14.78	30	12.8	294	147,236	191,406	239,258	23.25	84%	201,474	Regional
D-280	Buildout	1811	20769_20770	Tualatin Reservoir Trunk	12	153	0.01800	3.10	0.86	2.24	4,293	1,216	1.95	9.39	14.78	30	15.2	629	96,265	125,144	156,431	35.55	91%	142,792	Regional
D-280	Buildout	1812	20770_20771	Tualatin Reservoir Trunk	12	416	0.01740	3.04	0.86	2.18	4,187	1,216	1.95	9.39	14.78	30	14.8	312	129,626	168,514	210,642	34.95	91%	192,294	Regional
D-280	Buildout	1813	20771_20772	Tualatin Reservoir Trunk	12	447	0.03900	4.56	0.86	3.70	7,092	1,216	1.95	9.38	14.77	30	18.4	342	152,824	198,671	248,339	52.33	91%	226,700	Regional
D-280 Total						**4,505**													**1,390,107**	**1,807,140**	**2,258,925**		**87%**	**1,972,359**	
D-285	Buildout	1814	20772_20773	Tualatin Reservoir Trunk	21	293	0.00130	3.74	1.00	2.75	5,267	1,216	2.64	10.82	16.20	39	20.1	476	139,336	181,137	226,422	19.23	81%	182,340	Regional
D-285	Buildout	1815	20773_20774	Tualatin Reservoir Trunk	21	286	0.00100	3.27	1.00	2.27	4,355	1,216	2.64	10.81	16.19	39	17.8	418	119,532	155,391	194,239	16.87	81%	156,604	Regional
D-285	Buildout	1816	20774_20775	Tualatin Reservoir Trunk	21	316	0.00130	3.74	1.00	2.74	5,262	1,216	2.63	10.80	16.19	39	19.0	429	135,618	176,303	220,378	19.23	81%	177,503	Regional
D-285	Buildout	1817	20775_20776	Tualatin Reservoir Trunk	21	338	0.00160	4.10	1.00	3.11	5,955	1,216	2.63	10.79	16.18	39	19.3	433	146,308	190,200	237,750	21.34	81%	192,039	Regional
D-285	Buildout	1818	20776_20777	Tualatin Reservoir Trunk	21	350	0.00160	4.07	1.00	3.07	5,890	1,216	2.63	10.78	16.16	39	16.0	400	140,088	182,114	227,643	21.34	81%	184,234	Regional
D-285	Buildout	1819	20777_20778	Tualatin Reservoir Trunk	21	475	0.00150	3.94	1.04	2.90	5,566	1,216	3.30	11.38	16.75	39	14.3	384	182,386	237,101	296,377	20.66	81%	239,851	Regional
D-285	Buildout	1820	20778_20779	Tualatin Reservoir Trunk	21	425	0.00160	4.11	1.11	3.00	5,745	1,216	3.49	11.55	16.90	39	14.7	388	165,005	214,506	268,133	21.34	81%	216,540	Regional
D-285	Buildout	1821	20779_20780	Tualatin Reservoir Trunk	21	427	0.00120	3.58	1.15	2.43	4,663	1,216	3.55	11.61	16.94	39	13.1	373	159,140	206,883	258,603	18.48	81%	208,479	Regional
D-285	Buildout	1822	20780_20736	Tualatin Reservoir Trunk	21	548	0.00130	3.75	1.15	2.60	4,979	1,216	3.55	11.61	16.93	39	13.7	378	207,299	269,489	336,861	19.23	81%	271,244	Regional
D-285 Total						**3,458**													**1,394,712**	**1,813,125**	**2,266,407**		**81%**	**1,828,834**	
D-290	Buildout	1869	21005_21006	Cipole/Bluff Trunk	10	500	0.00280	0.75	0.47	0.28	540	452	0.52	0.77	0.77	12	4.3	112	56,142	72,985	91,231	1.22	38%	35,000	-
D-290	Buildout	1870	21006_20722	Cipole/Bluff Trunk	10	500	0.00300	0.78	0.54	0.24	452	452	0.60	0.87	0.87	12	5.8	121	60,676	78,878	98,598	1.26	38%	37,815	-
D-290 Total						**1,000**													**116,818**	**151,864**	**189,829**		**38%**	**72,815**	
D-295	Buildout	1774	20724_20728	Cipole/Bluff Trunk	15	499	0.00150	1.64	1.38	0.26	503	452	1.94	2.18	2.18	18	9.6	184	91,827	119,375	149,219	2.63	37%	55,909	-
D-295	Buildout	1778	20728_20729	Cipole/Bluff Trunk	15	450	0.00170	1.72	1.38	0.34	655	452	1.93	2.17	2.17	18	9.7	184	82,858	107,716	134,645	2.80	39%	51,888	-
D-295	Buildout	1779	20729_20730	Cipole/Bluff Trunk	15	470	0.00160	1.68	1.37	0.31	591	452	1.93	2.17	2.17	18	11.7	198	93,294	121,283	151,603	2.71	38%	57,612	-
D-295	Buildout	1780	20730_20731	Cipole/Bluff Trunk	15	471	0.00160	1.68	1.37	0.31	592	452	1.93	2.17	2.17	18	12.4	204	96,052	124,867	156,084	2.71	38%	59,426	-
D-295	Buildout	1781	20731_20732	Cipole/Bluff Trunk	15	374	0.00200	1.89	1.37	0.52	988	452	1.93	2.17	2.17	18	12.1	202	75,361	97,970	122,462	3.03	38%	46,342	-
D-295 Total						**2,264**													**439,393**	**571,211**	**714,014**		**38%**	**271,177**	
D-310	Buildout	1956	16660_16989	Scholl Trunk	18	75	0.00410	4.37	1.81	2.57	4,926	-	2.62	4.68	17.59	36	7.8	292	21,935	28,516	35,645	27.59	84%	29,993	Regional
D-310	Buildout	1961	16989_16659	Scholl Trunk	18	20	0.02050	9.74	1.81	7.94	15,215	-	2.62	4.68	17.58	36	7.3	287	5,740	7,462	9,328	61.69	84%	7,855	Regional
D-310	Buildout	1955	16659_16658	Scholl Trunk	18	218	0.00190	2.99	1.81	1.18	2,264	-	2.62	4.68	17.57	36	7.5	290	63,159	82,106	102,633	18.78	84%	86,313	Regional
D-310	Buildout	1954	16658_16988	Scholl Trunk	18	127	0.00230	3.25	1.80	1.45	2,773	-	2.62	4.67	17.57	36	8.8	302	38,299	49,788	62,236	20.66	84%	52,443	Regional
D-310	Buildout	1960	16988_16987	Scholl Trunk	18	150	0.00170	2.83	1.80	1.03	1,970	-	2.62	4.67	17.56	36	10.0	313	46,893	60,961	76,201	17.77	84%	64,051	Regional
D-310	Buildout	1959	16987_16657	Scholl Trunk	18	66	0.00170	2.78	1.80	0.97	1,865	-	2.62	4.67	17.56	36	9.8	311	20,513	26,667	33,333	17.77	84%	28,121	Regional
D-310 Total						**656**													**196,539**	**255,501**	**319,376**		**84%**	**268,776**	
D-320	Buildout	1975	16653_16652	Scholl Trunk	18	251	0.00220	3.16	2.22	0.94	1,801	-	3.02	5.12	17.96	36	8.4	298	74,815	97,259	121,574	20.21	84%	102,591	Regional
D-320	Buildout	1974	16652_16651	Scholl Trunk	18	237	0.00240	3.37	2.21	1.15	2,207	-	3.02	5.12	17.95	36	15.3	362	85,775	111,507	139,384	21.11	84%	117,159	Regional
D-320	Buildout	1973	16651_16650	Scholl Trunk	18	426	0.00150	2.66	2.21	0.44	851	-	3.02	5.12	17.94	36	18.5	392	166,953	217,038	271,298	16.69	84%	228,091	Regional
D-320	Buildout	1972	16650_16649	Scholl Trunk	18	135	0.00390	4.22	2.21	2.01	3,857	-	3.02	5.11	17.93	36	17.4	382	51,573	67,044	83,806	26.91	84%	70,653	Regional
D-320	Buildout	1971	16649_16648	Scholl Trunk	18	162	0.00070	1.85	2.21	-	-	-	3.02	5.11	17.91	36	17.1	379	61,423	79,849	99,812	11.40	84%	83,607	Regional

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
D-320	Buildout	7830	-	Scholl Trunk	18	179	0.00080	1.90	2.73	-	-	-	3.53	6.11	18.91	36	15.7	366	65,624	85,311	106,639	12.19	84%	90,008	Regional
D-320	Buildout	2104	16648_16647	Scholl Trunk	18	310	0.06060	16.75	2.73	14.02	26,882	-	3.53	6.11	18.89	36	12.2	333	103,172	134,124	167,655	106.07	84%	141,177	Regional
D-320	Buildout	1232	16647_16646	Scholl Trunk	18	150	0.01960	9.53	2.73	6.80	13,029	-	3.53	6.11	18.88	36	10.2	314	47,138	61,279	76,599	60.32	84%	64,503	Regional
D-320	Buildout	1231	16646_16645	Scholl Trunk	18	253	0.00510	4.88	2.73	2.15	4,118	-	3.53	6.11	18.86	36	12.6	337	85,311	110,905	138,631	30.77	84%	116,657	Regional
D-320	Buildout	1230	16645_16644	Scholl Trunk	18	214	0.00350	4.03	2.73	1.30	2,491	-	3.53	6.10	18.85	36	11.6	328	70,124	91,162	113,952	25.49	84%	95,946	Regional
D-320	Buildout	1229	16644_16673	Scholl Trunk	18	366	0.00450	4.58	2.73	1.85	3,554	-	3.53	6.10	18.83	36	7.8	292	106,908	138,980	173,725	28.90	84%	146,185	Regional
D-320 Total						**2,684**													**918,815**	**1,194,459**	**1,493,074**		**84%**	**1,256,578**	
D-330	Buildout	1046	13885_13884	Scholl Trunk	27	330	0.00230	9.63	6.69	2.94	5,628	-	7.49	10.53	25.03	42	10.2	748	246,807	320,850	401,062	31.17	69%	277,188	Regional
D-330	Buildout	1045	13884_13883	Scholl Trunk	27	329	0.00200	8.99	6.69	2.30	4,403	-	7.49	10.51	25.00	42	12.8	801	263,427	342,455	428,068	29.07	69%	295,740	Regional
D-330	Buildout	1044	13883_13882	Scholl Trunk	27	115	0.00290	10.75	6.69	4.06	7,784	-	7.49	10.50	24.99	42	12.8	801	92,068	119,688	149,610	35.00	69%	103,675	Regional
D-330	Buildout	1043	13882_13881	Scholl Trunk	27	117	0.00200	8.89	6.69	2.21	4,234	-	7.49	10.50	24.98	42	16.6	877	102,614	133,398	166,747	29.07	69%	115,723	Regional
D-330	Buildout	1042	13881_13880	Scholl Trunk	27	184	0.00260	10.14	7.02	3.12	5,981	-	7.82	10.83	25.31	42	19.0	925	170,121	221,157	276,446	33.14	69%	191,870	Regional
D-330	Buildout	1041	13880_13879	Scholl Trunk	27	135	0.00270	10.50	7.02	3.48	6,678	-	7.81	10.82	25.30	42	13.4	812	109,581	142,455	178,069	33.77	69%	122,695	Regional
D-330	Buildout	1040	13879_13878	Scholl Trunk	27	255	0.00240	9.81	7.02	2.79	5,355	-	7.81	10.81	25.29	42	13.9	822	209,514	272,368	340,460	31.84	69%	235,549	Regional
D-330	Buildout	1039	13878_13877	Scholl Trunk	27	190	0.00250	10.08	7.02	3.07	5,878	-	7.81	10.79	25.28	42	12.9	802	152,438	198,170	247,712	32.50	69%	170,855	Regional
D-330	Buildout	1038	13877_13876	Scholl Trunk	27	405	0.00200	8.97	7.02	1.96	3,749	-	7.81	10.78	25.28	42	8.1	704	285,166	370,716	463,395	29.07	69%	320,362	Regional
D-330	Buildout	1037	13876_13875	Scholl Trunk	27	380	0.00200	8.97	7.01	1.96	3,753	-	7.80	10.76	25.26	42	6.8	680	258,225	335,693	419,616	29.07	69%	290,096	Regional
D-330	Buildout	1036	13875_13874	Scholl Trunk	27	226	0.00240	9.90	7.01	2.89	5,531	-	7.80	10.76	25.23	42	6.0	662	149,714	194,628	243,285	31.84	69%	167,671	Regional
D-330	Buildout	1035	13874_13873	Scholl Trunk	27	328	0.00230	9.66	7.01	2.65	5,077	-	7.80	10.75	25.22	42	7.2	686	224,946	292,429	365,537	31.17	69%	252,294	Regional
D-330	Buildout	1034	13873_13872	Scholl Trunk	27	349	0.00230	9.60	7.00	2.60	4,986	-	7.80	10.75	25.19	42	9.4	732	255,441	332,074	415,092	31.17	69%	287,185	Regional
D-330 Total						**3,343**													**2,520,060**	**3,276,079**	**4,095,098**		**69%**	**2,830,903**	
D-335	Buildout	1029	13868_13867	Scholl Trunk	27	329	0.00150	7.74	5.50	2.24	4,290	-	6.30	9.22	24.09	42	8.4	710	233,650	303,744	379,681	25.17	69%	262,910	Regional
D-335	Buildout	1028	13867_16379	Scholl Trunk	27	112	0.00140	7.58	5.50	2.08	3,989	-	6.30	9.22	24.01	42	8.1	704	78,849	102,504	128,130	24.32	69%	88,181	Regional
D-335	Buildout	1061	16379_16236	Scholl Trunk	27	39	0.00150	7.87	5.50	2.37	4,538	-	6.30	9.21	23.98	42	11.5	774	30,178	39,231	49,039	25.17	69%	33,710	Regional
D-335	Buildout	1060	16236_13866	Scholl Trunk	27	231	0.00140	7.47	5.50	1.97	3,769	-	6.30	9.21	23.95	42	11.6	775	179,072	232,794	290,993	24.32	69%	201,650	Regional
D-335	Buildout	1027	13866_13865	Scholl Trunk	27	401	0.00140	7.50	5.50	2.00	3,828	-	6.30	9.20	23.92	42	7.7	696	279,227	362,995	453,744	24.32	69%	313,865	Regional
D-335	Buildout	1026	13865_13864	Scholl Trunk	27	458	0.00140	7.50	5.58	1.92	3,686	-	6.37	9.29	23.95	42	8.0	703	322,160	418,808	523,510	24.32	69%	362,082	Regional
D-335	Buildout	1025	13864_13885	Scholl Trunk	27	283	0.00140	7.54	5.57	1.97	3,772	-	6.37	9.28	23.86	42	9.1	726	205,474	267,117	333,896	24.32	69%	230,343	Regional
D-335 Total						**1,853**													**1,328,610**	**1,727,193**	**2,158,992**		**69%**	**1,492,741**	
D-340	Existing	1004	10691_10692	Metzger Interceptor	30	240	0.00070	7.07	16.17	-	-	-	16.40	17.18	17.18	36	8.8	301	72,241	93,914	117,392	11.40	38%	44,576	Regional
D-340	Existing	1005	10692_10693	Metzger Interceptor	30	395	0.00280	14.08	16.16	-	-	-	16.39	17.17	17.17	36	8.9	302	119,413	155,237	194,046	22.80	38%	74,177	Regional
D-340	Existing	1006	10693_10694	Fanno Creek Interceptor	30	67	0.00400	16.87	16.15	0.71	1,365	-	16.38	17.17	17.17	36	11.1	323	21,624	28,111	35,138	27.25	38%	13,391	Regional
D-340	Existing	1007	10694_10696	Fanno Creek Interceptor	30	12	0.16920	109.28	16.15	93.13	178,538	-	16.38	17.16	17.16	36	12.0	331	3,974	5,166	6,457	177.23	38%	2,476	Regional
D-340 Total						**714**													**217,252**	**282,427**	**353,034**		**38%**	**134,620**	
D-345	Buildout	899	09446_09447	Metzger Interceptor	30	282	0.00280	14.06	13.80	0.26	497	-	14.03	14.58	14.58	33	8.2	275	77,611	100,894	126,118	18.08	22%	28,018	Regional
D-345	Buildout	900	09447_09448	Metzger Interceptor	30	283	0.00280	14.04	13.79	0.24	468	-	14.02	14.56	14.56	33	7.5	269	76,091	98,918	123,648	18.08	22%	27,637	Regional
D-345	Buildout	901	09448_09449	Metzger Interceptor	30	334	0.00280	14.09	13.78	0.31	594	-	14.01	14.56	14.56	33	7.6	270	90,147	117,191	146,488	18.08	22%	32,281	Regional
D-345	Buildout	1205	09449_09450	Metzger Interceptor	30	333	0.00250	13.18	14.23	-	-	-	14.44	15.22	15.22	33	11.0	300	99,934	129,914	162,393	17.08	23%	37,058	Regional
D-345	Buildout	1161	09450_09451	Metzger Interceptor	30	344	0.00290	14.40	14.22	0.18	337	-	14.43	15.21	15.21	33	13.1	319	109,890	142,857	178,572	18.40	22%	38,845	Regional
D-345	Buildout	1162	09451_10266	Metzger Interceptor	30	380	0.00280	14.03	14.21	-	-	-	14.42	15.20	15.20	33	10.2	879	333,968	434,158	542,698	18.08	22%	121,454	Regional
D-345	Buildout	1163	10266_10267	Metzger Interceptor	30	247	0.00280	14.04	14.80	-	-	-	15.01	15.81	15.81	33	8.5	278	68,773	89,405	111,756	18.08	22%	24,951	Regional
D-345	Buildout	1164	10267_10268	Metzger Interceptor	30	125	0.00280	14.06	14.79	-	-	-	14.99	15.79	15.79	33	8.1	274	34,268	44,548	55,686	18.08	22%	12,381	Regional
D-345	Buildout	1165	10268_10269	Metzger Interceptor	30	208	0.00280	14.15	14.79	-	-	-	14.99	15.79	15.79	33	8.5	278	57,896	75,264	94,080	18.08	22%	20,443	Regional
D-345	Buildout	1166	10269_10270	Metzger Interceptor	30	180	0.00280	14.00	14.78	-	-	-	14.98	15.78	15.78	33	11.1	301	54,195	70,454	88,068	18.08	23%	19,854	Regional
D-345	Buildout	1167	10270_10271	Metzger Interceptor	30	154	0.00290	14.36	14.78	-	-	-	14.98	15.77	15.77	33	10.6	296	45,645	59,338	74,173	18.40	22%	16,273	Regional
D-345	Buildout	993	10271_10264	Metzger Interceptor	30	476	0.00280	13.94	14.77	-	-	-	14.97	15.76	15.76	33	8.9	282	134,193	174,451	218,064	18.08	23%	49,940	Regional
D-345	Buildout	1003	10264_10691	Metzger Interceptor	30	298	0.00450	17.75	14.76	2.99	5,729	-	14.96	15.74	15.74	33	9.0	283	84,198	109,458	136,822	22.92	23%	30,858	Regional
D-345 Total						**3,644**													**1,266,809**	**1,646,852**	**2,058,565**		**22%**	**459,992**	
D-350	Existing	848	05043_05044	Elmwood Lateral	12	124	0.08250	6.63	5.52	1.10	2,118	-	5.53	5.75	5.75	21	7.9	189	Locust Street Re-route (See Project Data Sheet D-350 & D-351)						
D-350	Existing	849	05044_05045	Elmwood Lateral	12	312	0.06210	5.75	5.52	0.23	440	-	5.53	5.75	5.75	21	7.2	184							
D-350	Existing	850	05045_05048	Elmwood Lateral	12	126	0.06170	5.73	5.52	0.21	404	-	5.53	5.75	5.75	21	13.0	228							
D-350	Existing	851	05048_05050	Elmwood Lateral	12	250	0.05790	5.55	5.52	0.03	58	-	5.53	5.75	5.75	21	13.6	233							
D-350	Existing	852	05050_05076	Elmwood Lateral	12	102	0.03000	4.00	5.52	-	-	-	5.53	5.75	5.75	21	6.9	182							
D-350	Existing	853	05076_05077	Elmwood Lateral	12	146	0.04530	4.91	5.52	-	-	-	5.53	5.75	5.75	21	6.7	181							
D-350	Existing	854	05077_05085	Elmwood Lateral	12	214	0.04110	4.68	6.29	-	-	-	6.31	6.54	6.54	21	6.7	181							
D-350	Existing	855	05085_05088	Elmwood Lateral	12	104	0.02120	3.36	6.29	-	-	-	6.31	6.54	6.54	21	8.4	194							
D-350	Existing	856	05088_05089	Elmwood Lateral	12	149	0.02630	3.74	6.29	-	-	-	6.31	6.54	6.54	21	8.7	196							
D-350	Existing	857	05089_05100	Elmwood Lateral	12	312	0.00870	2.16	6.29	-	-	-	6.31	6.54	6.54	21	6.3	178							
D-350	Existing	858	05100_05101	Elmwood Lateral	12	198	0.00890	2.18	6.29	-	-	-	6.31	6.54	6.54	21	6.6	180							
D-350	Existing	859	05101_05104	Elmwood Lateral	12	310	0.00870	2.15	6.29	-	-	-	6.31	6.54	6.54	21	6.8	182							
D-350	Existing	860	05104_05105	Elmwood Lateral	12	183	0.01250	2.58	6.29	-	-	-	6.31	6.54	6.54	21	6.3	178							
D-350	Existing	861	05105_06616	Elmwood Lateral	12	349	0.01160	2.49	6.60	-	-	-	6.62	6.85	6.85	21	7.5	186							
D-350 Total						**2,879**													**-**	**-**	**-**		**-**	**-**	
D-351	Existing	873	06616_06618	Elmwood Lateral	15	181	0.00520	3.03	6.59	-	-	-	6.62	6.85	6.85	21	8.2	192	Locust Street Re-route (See Project Data Sheet D-350 & D-351)						
D-351	Existing	874	06618_06619	Elmwood Lateral	15	150	0.00550	3.11	6.59	-	-	-	6.62	6.85	6.85	21	8.1	191							

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
D-351	Existing	875	06619_06620	Elmwood Lateral	15	172	0.00540	3.08	6.59	-	-	-	6.62	6.85	6.85	21	7.7	188	Locust Street Re-route (See Project Data Sheet D-350 & D-351)						
D-351	Existing	876	06620_06621	Elmwood Lateral	15	228	0.00540	3.07	6.59	-	-	-	6.62	6.85	6.85	21	7.3	185							
D-351	Existing	877	06621_06626	Elmwood Lateral	15	400	0.00540	3.07	6.59	-	-	-	6.62	6.85	6.85	21	10.0	206							
D-351	Existing	878	06626_06627	Elmwood Lateral	15	219	0.00540	3.08	6.59	-	-	-	6.62	6.85	6.85	21	10.2	207							
D-351	Existing	879	06627_06628	Elmwood Lateral	15	146	0.00530	3.06	6.59	-	-	-	6.62	6.85	6.85	21	7.2	184							
D-351	Existing	880	06628_06633	Elmwood Lateral	15	265	0.00540	3.08	6.59	-	-	-	6.62	6.85	6.85	21	10.8	211							
D-351	Existing	881	06633_06634	Elmwood Lateral	15	276	0.00540	3.07	6.59	-	-	-	6.62	6.85	6.85	21	10.8	211							
D-351	Existing	882	06634_06635	Elmwood Lateral	15	330	0.01520	5.16	6.59	-	-	-	6.62	6.85	6.85	21	9.0	198							
D-351 Total						**2,367**													**-**	**-**	**-**		**-**	**-**	
D-410	Buildout	1103	19972_19971	SW Katherine Lateral	12	33	0.00090	0.70	1.70	-	-	-	1.71	1.83	1.83	15	8.9	160	5,279	6,863	8,579	1.25	44%	3,811	-
D-410	Buildout	1102	19971_19970	SW Katherine Lateral	12	152	0.00510	1.64	1.70	-	-	-	1.71	1.83	1.83	15	10.3	169	25,764	33,493	41,866	2.98	45%	18,788	-
D-410	Buildout	1101	19970_19969	SW Katherine Lateral	12	385	0.00500	1.63	1.70	-	-	-	1.71	1.83	1.83	15	12.0	181	69,760	90,687	113,359	2.95	45%	50,745	-
D-410	Buildout	1100	19969_19968	SW Katherine Lateral	12	329	0.00500	1.63	1.70	-	-	-	1.71	1.83	1.83	15	8.3	156	51,302	66,692	83,365	2.95	45%	37,191	-
D-410 Total						**899**													**152,104**	**197,735**	**247,169**		**45%**	**110,535**	
D-480	Existing	157	03368_03369	N. Brentwood Interceptor	10	223	0.00460	0.96	1.28	-	-	-	1.32	1.36	1.36		8.5	-	-	-	-	0.96	0%	-	no project
D-480	Existing	158	03369_03370	N. Brentwood Interceptor	10	42	0.00520	1.03	1.28	-	-	-	1.32	1.36	1.36		9.5	-	-	-	-	1.03	0%	-	no project
D-480	Existing	159	03370_03373	N. Brentwood Interceptor	10	96	0.00440	0.94	1.28	-	-	-	1.32	1.35	1.35		10.5	-	-	-	-	0.94	0%	-	no project
D-480	Existing	160	03373_03375	N. Brentwood Interceptor	10	203	0.00400	0.90	1.28	-	-	-	1.32	1.35	1.35		11.5	-	-	-	-	0.90	0%	-	no project
D-480	Existing	161	03375_03378	N. Brentwood Interceptor	10	430	0.01090	1.48	1.27	0.20	391	-	1.32	1.35	1.35		8.5	-	-	-	-	1.48	0%	-	no project
D-480 Total						**994**													**-**	**-**	**-**		**0%**	**-**	
D-485	Existing	153	03355_03360	N. Brentwood Interceptor	8	397	0.01240	0.87	1.04	-	-	-	1.08	1.11	1.11		11.0	-	-	-	-	0.87	0%	-	no project
D-485 Total						**397**													**-**	**-**	**-**		**0%**	**-**	
D-510	Existing	764	03050_03052	W. Tektronix Interceptor	8	105	0.01290	0.96	1.48	-	-	-	1.58	1.58	1.58	12	8.8	141	14,776	19,209	24,011	2.61	63%	15,182	-
D-510	Existing	765	03052_11437	W. Tektronix Interceptor	8	68	0.00500	0.55	1.48	-	-	-	1.57	1.58	1.58	12	8.4	137	9,339	12,141	15,176	1.63	66%	10,013	-
D-510	Existing	767	11437_16574	W. Tektronix Interceptor	8	307	0.00580	0.59	1.47	-	-	-	1.57	1.58	1.58	12	10.5	152	46,727	60,745	75,931	1.75	66%	50,186	-
D-510	Existing	771	16574_20924	W. Tektronix Interceptor	10	460	0.00670	1.16	1.47	-	-	-	1.57	1.57	1.57	12	11.6	158	72,850	94,706	118,382	1.88	38%	45,517	-
D-510	Existing	703	20924_20923	W. Tektronix Interceptor	10	501	0.01100	1.49	1.71	-	-	-	1.81	1.81	1.81	12	10.0	149	74,773	97,205	121,507	2.41	38%	46,522	-
D-510	Existing	741	20923_20922	W. Tektronix Interceptor	10	504	0.01100	1.49	1.71	-	-	-	1.81	1.81	1.81	12	10.0	149	75,221	97,787	122,234	2.41	38%	46,899	-
D-510	Existing	740	20922_20921	W. Tektronix Interceptor	10	400	0.01100	1.49	1.71	-	-	-	1.81	1.81	1.81	12	10.0	149	59,699	77,609	97,011	2.41	38%	37,195	-
D-510	Existing	453	20921_20911	W. Tektronix Interceptor	10	320	0.00830	1.30	1.71	-	-	-	1.81	1.81	1.81	12	11.6	158	50,571	65,743	82,179	2.10	38%	31,366	-
D-510 Total						**2,665**													**403,958**	**525,145**	**656,431**		**43%**	**282,880**	
D-520	Buildout	8452	54044_54043	DLAT006	12	229	0.00620	1.82	1.10	0.72	1,380	-	1.10	1.93	2.78	15	5.7	139	31,730	41,249	51,561	3.29	45%	23,046	-
D-520	Buildout	8450	54043_54042	DLAT006	12	43	0.00560	1.73	1.10	0.63	1,212	-	1.10	1.93	2.79	15	10.1	169	7,203	9,364	11,704	3.12	45%	5,220	-
D-520	Buildout	8447	54042_52521	DLAT006	12	596	0.00630	1.83	1.10	0.74	1,409	-	1.10	1.93	2.79	15	12.2	183	109,045	141,759	177,198	3.31	45%	79,152	-
D-520	Buildout	8453	52521_52520	DLAT006	12	610	0.00080	0.65	1.10	-	-	-	1.10	1.93	2.78	21	12.4	223	136,036	176,846	221,058	2.90	78%	171,634	-
D-520	Buildout	8455	52520_52519	DLAT006	12	584	0.00080	0.65	1.10	-	-	-	1.10	1.93	2.79	21	13.8	234	136,696	177,704	222,130	2.90	77%	171,922	-
D-520 Total						**2,062**													**420,709**	**546,922**	**683,652**		**66%**	**450,974**	
D-530	Existing	8121	58224_57262	DLAT014	8	239	0.00200	0.35	0.61	-	-	-	0.61	0.66	0.66	12	16.4	188	44,773	58,205	72,757	1.03	66%	47,962	-
D-530	Existing	8119	27262_58900	DLAT014	8	272	0.00200	0.35	0.61	-	-	-	0.61	0.66	0.66	12	19.4	208	56,490	73,436	91,796	1.03	66%	60,397	-
D-530	Existing	8117	58900_58588	DLAT014	8	334	0.00200	0.35	0.61	-	-	-	0.61	0.66	0.66	12	16.0	186	61,977	80,570	100,712	1.03	66%	66,643	-
D-530	Existing	8002	58588_13885	DLAT014	8	203	0.00200	0.35	0.61	-	-	-	0.61	0.66	0.66	12	9.6	147	29,795	38,734	48,417	1.03	66%	31,887	-
D-530 Total						**1,048**													**193,035**	**250,945**	**313,681**		**66%**	**206,888**	
D-540	2015	1946	20811_20812	Sherwood Rd Trunk	10	476	0.00060	0.34	0.93	-	-	-	1.12	1.12	1.12	15	4.9	133	63,186	82,142	102,678	1.02	67%	68,740	-
D-540	2015	1632	20812_20813	Sherwood Rd Trunk	10	133	0.00470	0.97	0.93	0.03	67	-	1.11	1.12	1.12	15	5.3	135	18,012	23,416	29,270	2.86	66%	19,356	-
D-540	2015	1633	20813_20814	Sherwood Rd Trunk	10	280	0.00400	0.90	0.98	-	-	-	1.20	1.20	1.20	15	5.3	136	37,959	49,346	61,683	2.64	66%	40,712	-
D-540	2015	1634	20814_21318	Sherwood Rd Trunk	10	272	0.00400	0.90	0.98	-	-	-	1.19	1.20	1.20	15	6.1	141	38,465	50,004	62,505	2.64	66%	41,132	-
D-540	2015	1668	21318_20815	Sherwood Rd Trunk	10	98	0.00410	0.91	0.98	-	-	-	1.19	1.20	1.20	15	6.7	145	14,258	18,536	23,170	2.67	66%	15,305	-
D-540	2015	1635	20815_20807	Sherwood Rd Trunk	10	430	0.00430	0.93	0.98	-	-	-	1.19	1.20	1.20	15	7.5	301	129,599	168,478	210,598	2.74	66%	139,354	-
D-540	2015	1629	20807_20808	Sherwood Rd Trunk	12	56	0.00840	2.11	1.55	0.57	1,084	-	1.75	1.78	1.78	15	8.7	159	8,896	11,565	14,456	3.82	45%	6,464	-
D-540	2015	1630	20808_20809	Sherwood Rd Trunk	12	295	0.00400	1.46	1.55	-	-	-	1.75	1.78	1.78	15	8.1	155	45,609	59,291	74,114	2.64	45%	33,135	-
D-540	2015	1631	20809_20810	Sherwood Rd Trunk	12	379	0.00430	1.51	1.54	-	-	-	1.74	1.78	1.78	15	8.5	157	59,627	77,515	96,893	2.74	45%	43,460	-
D-540 Total						**2,419**													**415,611**	**540,294**	**675,367**		**60%**	**407,658**	
D-550	Existing	8232	15946_15945	DLAT022	8	297	0.00360	0.47	0.77	-	-	-	0.21	0.22	0.22	12	7.6	132	38,991	50,689	63,361	1.38	66%	41,902	-
D-550	Existing	8242	15945_15944	DLAT022	8	353	0.00430	0.51	0.77	-	-	-	0.21	0.22	0.22	12	13.9	172	60,741	78,963	98,704	1.51	66%	65,116	-
D-550	Existing	8213	15944_52710	DLAT022	8	177	0.00790	0.70	0.77	-	-	-	0.21	0.22	0.22	12	14.1	174	30,713	39,927	49,909	2.05	66%	32,919	-
D-550	Existing	8562	52710_15943	DLAT022	8	27	0.01320	0.90	0.77	0.13	245	-	0.21	0.22	0.22	12	9.3	145	3,932	5,112	6,390	2.64	66%	4,214	-
D-550 Total						**853**													**134,378**	**174,692**	**218,364**		**66%**	**144,151**	
D-560	Existing	8552	21773_21772	Borland Sewer	8	134	0.00380	0.48	0.61	-	-	-	0.73	1.18	1.18	12	8.2	136	18,164	23,613	29,516	1.42	66%	19,464	-
D-560	Existing	8559	21772_21771	Borland Sewer	8	206	0.00190	0.34	0.61	-	-	-	0.73	1.18	1.18	12	10.7	153	31,502	40,952	51,190	1.00	66%	33,786	-
D-560	Existing	8537	21771_21770	Borland Sewer	8	382	0.00420	0.51	0.61	-	-	-	0.73	1.18	1.18	12	10.7	153	58,424	75,951	94,939	1.49	66%	62,785	-
D-560	Existing	8540	21770_21769	Borland Sewer	8	262	0.00260	0.40	0.61	-	-	-	0.73	1.18	1.18	12	8.5	138	36,127	46,966	58,707	1.17	66%	38,768	-
D-560 Total						**984**													**144,217**	**187,482**	**234,353**		**66%**	**154,803**	
D-565	Buildout	8542	21769_96870	Borland Sewer	8	231	0.01010	0.79	0.61	0.17	332	-	0.73	1.18	1.18	12	10.6	153	35,307	45,899	57,374	2.31	66%	37,889	-
D-565	Buildout	8551	96870_96868	Borland Sewer	8	278	0.01600	0.99	0.61	0.38	725	-	0.73	1.18	1.18	12	12.5	163	45,428	59,056	73,820	2.91	66%	48,726	-
D-565	Buildout	8549	96868_21766	Borland Sewer	8	264	0.01400	0.93	0.61	0.32	606	-	0.73	1.17	1.17	12	10.0	149	39,345	51,149	63,936	2.72	66%	42,172	-

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
D-565	Buildout	8547	21766_21765	Borland Sewer	8	169	0.00680	0.65	0.61	0.04	68	-	0.73	1.17	1.17	12	7.0	128	21,693	28,202	35,252	1.90	66%	23,253	-
D-565 Total						**943**													**141,774**	**184,306**	**230,383**		**66%**	**152,040**	
D-570	Buildout	1614	20791_20792	Nyberg Trunk	18	115	0.00160	2.69	3.27	-	-	-	3.53	4.16	4.16	24	11.4	235	27,058	35,175	43,969	5.85	54%	23,721	Regional
D-570	Buildout	1615	20792_20793	Nyberg Trunk	18	290	0.00160	2.68	3.26	-	-	-	3.53	4.15	4.15	24	9.5	220	63,773	82,904	103,631	5.85	54%	56,115	Regional
D-570	Buildout	1616	20793_20794	Nyberg Trunk	18	400	0.00160	2.76	3.26	-	-	-	3.53	4.15	4.15	24	8.0	209	83,553	108,619	135,773	5.85	53%	71,585	Regional
D-570	Buildout	1617	20794_20806	Nyberg Trunk	18	352	0.00100	2.18	3.26	-	-	-	3.53	4.15	4.15	24	8.0	208	73,347	95,351	119,189	4.62	53%	63,075	Regional
D-570	Buildout	1628	20806_20796	Nyberg Trunk	18	414	0.00130	2.48	3.32	-	-	-	3.59	4.21	4.21	24	7.9	208	85,974	111,766	139,707	5.27	53%	73,953	Regional
D-570	Buildout	1618	20796_20797	Nyberg Trunk	18	307	0.00160	2.69	3.31	-	-	-	3.58	4.20	4.20	24	7.4	204	62,670	81,470	101,838	5.85	54%	54,965	Regional
D-570	Buildout	1619	20797_20798	Nyberg Trunk	18	407	0.00380	4.21	3.31	0.90	1,729	-	3.58	4.20	4.20	24	6.2	195	79,235	103,006	128,757	9.01	53%	68,549	Regional
D-570	Buildout	1620	20798_20799	Nyberg Trunk	18	395	0.00190	3.00	3.31	-	-	-	3.58	4.19	4.19	24	6.2	389	153,519	199,575	249,468	6.37	53%	131,829	Regional
D-570	Buildout	1621	20799_20800	Nyberg Trunk	18	502	0.00160	2.70	3.31	-	-	-	3.58	4.19	4.19	24	7.5	204	102,515	133,270	166,587	5.85	54%	89,672	Regional
D-570	Buildout	1622	20800_20801	Nyberg Trunk	18	475	0.00070	1.82	3.30	-	-	-	3.57	4.18	4.18	24	8.6	213	101,120	131,456	164,320	3.87	53%	86,955	Regional
D-570	Buildout	1623	20801_20802	Nyberg Trunk	18	154	0.00200	3.05	3.30	-	-	-	3.57	4.18	4.18	24	8.6	213	32,778	42,611	53,264	6.54	53%	28,383	Regional
D-570	Buildout	1624	20802_20803	Nyberg Trunk	18	93	0.00320	3.86	3.52	0.34	653	-	3.80	4.40	4.40	24	10.3	226	21,064	27,383	34,229	8.27	53%	18,229	Regional
D-570	Buildout	1625	20803_20804	Nyberg Trunk	18	338	0.00090	2.06	3.52	-	-	-	3.80	4.40	4.40	24	11.8	238	80,428	104,556	130,695	4.38	53%	69,264	Regional
D-570	Buildout	1626	20804_22302	Nyberg Trunk	18	445	0.00200	3.01	3.52	-	-	-	3.80	4.40	4.40	24	14.2	257	114,512	148,866	186,083	6.54	54%	100,427	Regional
D-570 Total						**4,687**													**1,081,545**	**1,406,008**	**1,757,511**		**53%**	**936,721**	
D-600	Existing	1727	12123_12122	Lower Tualatin Interceptor	30	412	0.00070	7.86	12.02	-	-	-	15.87	24.80	29.84	-	17.3	-	Refer to Lower Tualatin Pump Station Improvements (Project Data Sheet D-600)						
D-600	Existing	1726	12122_12121	Lower Tualatin Interceptor	30	488	0.00100	7.17	12.02	-	-	-	15.87	24.78	29.82	-	17.3	-							
D-600	Existing	1725	12121_11876	Lower Tualatin Interceptor	30	443	0.00100	8.24	12.01	-	-	-	15.87	24.76	29.81	-	18.6	-							
D-600	Existing	1719	11876_11877	Lower Tualatin Interceptor	30	500	0.00050	6.18	12.65	-	-	-	16.49	25.40	30.56	-	20.2	-							
D-600	Existing	1720	11877_11878	Lower Tualatin Interceptor	30	450	0.00090	8.02	12.64	-	-	-	16.48	25.37	30.55	-	20.7	-							
D-600	Existing	1722	11879_11880	Lower Tualatin Interceptor	30	84	0.00430	17.39	12.81	4.59	8,791	-	16.65	25.55	30.72	-	23.9	-							
D-600	Existing	1723	11880_11837	Lower Tualatin Interceptor	30	410	0.00110	8.80	12.80	-	-	-	16.65	25.55	30.72	66	21.5	1,137	466,340	606,242	757,803	71.95	88%	665,064	Regional
D-600	Existing	1718	11837_11881	Lower Tualatin Interceptor	30	452	0.00070	6.85	13.06	-	-	-	16.93	25.82	30.99	66	20.9	1,102	498,090	647,517	809,396	57.39	88%	712,829	Regional
D-600	Existing	1724	11881_11882	Lower Tualatin Interceptor	30	253	0.00020	4.09	13.06	-	-	-	16.93	25.81	30.97	66	21.3	1,130	286,013	371,817	464,771	30.68	87%	402,822	Regional
D-600	Existing	1951	11882_10849	Lower Tualatin Interceptor	30	245	0.00020	3.80	13.06	-	-	-	16.93	25.80	30.96	66	20.6	992	243,124	316,062	395,077	30.68	88%	346,161	Regional
D-600	Existing	1293	10849_10847	Lower Tualatin Interceptor	30	250	0.00440	17.55	13.05	4.49	8,616	-	16.92	25.78	30.95	66	20.8	1,052	262,877	341,740	427,174	143.90	88%	375,089	Regional
D-600 Total						**3,987**													**1,756,444**	**2,283,377**	**2,854,221**		**88%**	**2,501,965**	
F-010	Buildout	227	20408_20407	16th/Pacific Ave Trunk	10	334	0.00810	1.28	0.58	0.69	1,325	1,274	1.24	1.67	1.67	15	9.1	162	54,091	70,319	87,898	3.76	66%	58,039	-
F-010	Buildout	226	20407_20405	16th/Pacific Ave Trunk	10	356	0.00780	1.25	0.58	0.66	1,274	1,274	1.24	1.67	1.67	15	8.9	161	57,146	74,290	92,862	3.69	66%	61,382	-
F-010	Buildout	225	20405_20404	16th/Pacific Ave Trunk	10	11	0.00910	1.35	0.58	0.77	1,474	1,274	1.24	1.67	1.67	15	8.5	157	1,730	2,249	2,812	3.98	66%	1,856	-
F-010	Buildout	224	20404_20403	16th/Pacific Ave Trunk	12	242	0.00480	1.60	0.58	1.01	1,942	1,274	1.24	1.67	1.67	15	8.0	154	37,332	48,532	60,665	2.89	45%	27,144	-
F-010	Buildout	223	20403_20402	16th/Pacific Ave Trunk	12	33	0.00360	1.39	0.58	0.81	1,547	1,274	1.24	1.67	1.67	15	8.0	154	5,080	6,603	8,254	2.50	44%	3,667	-
F-010 Total						**976**													**155,379**	**201,993**	**252,491**		**60%**	**152,087**	
F-020	2015	6147	25143_25142	FLAT006	8	103	0.00400	0.49	0.03	0.46	888	762	0.58	0.64	0.64	10	6.0	110	11,341	14,744	18,429	0.90	45%	8,269	-
F-020	2015	6145	25142_25141	FLAT006	8	192	0.00400	0.50	0.03	0.47	892	762	0.58	0.64	0.64	10	5.9	109	21,012	27,316	34,145	0.90	45%	15,246	-
F-020	2015	6143	25141_25140	FLAT006	8	144	0.00300	0.43	0.03	0.40	762	762	0.58	0.64	0.64	10	5.6	108	15,534	20,195	25,243	0.78	45%	11,318	-
F-020	2015	6139	25140_25139	FLAT006	8	15	0.00400	0.49	0.03	0.46	890	762	0.58	0.64	0.64	10	5.2	106	1,589	2,066	2,583	0.90	45%	1,155	-
F-020	2015	6142	25139_25138	FLAT006	8	235	0.00400	0.49	0.03	0.46	890	762	0.58	0.64	0.64	10	5.2	106	24,859	32,317	40,397	0.90	45%	18,066	-
F-020	2015	6136	25138_25137	FLAT006	8	450	0.00400	0.49	0.03	0.46	890	762	0.58	0.64	0.64	10	7.6	119	53,478	69,522	86,902	0.90	45%	38,864	-
F-020	2015	6148	25137_22090	FLAT006	8	174	0.00400	0.50	0.03	0.47	894	762	0.58	0.64	0.64	10	9.5	132	22,960	29,848	37,309	0.90	45%	16,605	-
F-020	2015	96	22090_22089	12th Avenue Trunk (West)	10	483	0.00600	1.10	0.80	0.31	587	587	1.67	1.62	1.62	15	9.6	165	79,667	103,567	129,459	3.23	66%	85,346	-
F-020 Total						**1,796**													**230,442**	**299,574**	**374,468**		**52%**	**194,868**	
F-110	Buildout	6190	78758_78827	-	8	327	0.00300	0.43	0.001	0.43	820	820	0.45	0.68	0.68	10	16.8	176	57,540	74,802	93,502	0.78	45%	41,845	-
F-110	Buildout	6187	78827_78757	-	8	142	0.00300	0.43	0.001	0.43	825	820	0.45	0.68	0.68	10	16.0	170	24,148	31,392	39,240	0.78	44%	17,430	-
F-110	Buildout	6191	78757_19120	-	8	450	0.00300	0.43	0.001	0.43	820	820	0.45	0.68	0.68	10	13.2	153	69,040	89,752	112,190	0.78	45%	50,208	-
F-110	Buildout	216	19120_19076	16th/Pacific Ave Trunk	8	135	0.02280	1.18	0.23	0.96	1,832	1,274	0.77	1.14	1.14	10	9.1	129	17,418	22,644	28,304	2.14	45%	12,648	-
F-110 Total						**1,054**													**168,145**	**218,589**	**273,236**		**45%**	**122,131**	
F-210	Buildout	267	15785_15784	Gaston South	12	342	0.00250	1.16	0.20	0.95	1,830	1,681	0.32	1.35	1.35	15	6.2	142	48,550	63,115	78,893	2.09	45%	35,146	-
F-210	Buildout	266	15784_15783	Gaston South	12	500	0.00220	1.08	0.20	0.88	1,688	1,681	0.32	1.35	1.35	15	7.7	152	76,011	98,814	123,518	1.96	45%	55,194	-
F-210	Buildout	265	15783_15782	Gaston South	12	229	0.00220	1.08	0.20	0.88	1,681	1,681	0.32	1.35	1.35	15	10.0	168	38,395	49,913	62,391	1.96	45%	28,024	-
F-210	Buildout	264	15782_15781	Gaston South	12	400	0.00280	1.22	0.20	1.02	1,956	1,681	0.32	1.35	1.35	15	12.8	187	74,708	97,120	121,400	2.21	45%	54,275	-
F-210 Total						**1,471**													**237,663**	**308,962**	**386,203**		**45%**	**172,639**	
H-010	Buildout	72	12279_12280	Hillsboro Interceptor	30	436	0.00060	6.49	6.91	-	-	-	6.96	9.22	9.22	48	17.1	512	223,305	290,297	362,871	22.73	71%	259,296	Regional
H-010	Buildout	232	12280_12281	Hillsboro Interceptor	30	492	0.00060	6.45	6.90	-	-	-	6.96	9.21	9.21	48	17.1	512	252,119	327,755	409,694	22.73	72%	293,430	Regional
H-010	Buildout	225	12281_12282	Hillsboro Interceptor	30	125	0.00060	6.72	7.00	-	-	-	7.06	9.32	9.32	48	13.3	471	58,911	76,584	95,730	22.73	70%	67,421	Regional
H-010	Buildout	224	12282_12283	Hillsboro Interceptor	30	433	0.00060	6.38	7.07	-	-	-	7.15	9.40	9.40	48	12.7	465	201,334	261,735	327,169	22.73	72%	235,281	Regional
H-010	Buildout	223	12283_12284	Hillsboro Interceptor	30	500	0.00060	6.51	7.06	-	-	-	7.15	9.40	9.40	48	12.6	464	231,949	301,533	376,916	22.73	71%	269,000	Regional
H-010	Buildout	222	12284_12285	Hillsboro Interceptor	30	244	0.00060	6.59	7.05	-	-	-	7.15	9.40	9.40	48	8.8	423	103,255	134,232	167,790	22.73	71%	119,163	Regional
H-010	Buildout	221	12285_12286	Hillsboro Interceptor	30	235	0.00060	6.48	7.05	-	-	-	7.15	9.40	9.40	48	7.8	825	193,925	252,102	315,128	22.73	71%	225,225	Regional
H-010	Buildout	220	12286_12287	Hillsboro Interceptor	30	391	0.00060	6.72	7.05	-	-	-	7.15	9.39	9.39	48	14.4	484	189,144	245,887	307,359	22.73	70%	216,511	Regional
H-010	Buildout	219	12287_12288	Hillsboro Interceptor	30	172	0.00050	6.08	7.04	-	-	-	7.14	9.39	9.39	48	22.2	2,762	475,114	617,649	772,061	20.75	71%	545,920	Regional
H-010	Buildout	218	12288_12289	Hillsboro Interceptor	30	178	0.00060	6.60	7.03	-	-	-	7.14	9.39	9.39	48	19.8	542	96,513	125,467	156,834	22.73	71%	111,262	Regional
H-010	Buildout	217	12289_12290	Hillsboro Interceptor	30	264	0.00190	11.45	7.03	4.42	8,476	-	7.14	9.39	9.39	48	12.1	459	121,187	157,544	196,929	40.45	72%	141,200	Regional

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
H-010 Total						**3,470**													**2,146,757**	**2,790,784**	**3,488,481**		**71%**	**2,483,708**	
H-015	Buildout	88	12263_12264	Hillsboro Interceptor	30	189	0.00070	6.97	6.01	0.96	1,844	-	6.01	8.26	8.26	42	6.7	338	63,882	83,047	103,808	17.20	59%	61,745	Regional
H-015	Buildout	87	12264_12265	Hillsboro Interceptor	30	301	0.00100	8.53	6.00	2.53	4,843	-	6.01	8.25	8.25	42	5.0	322	96,777	125,809	157,262	20.55	59%	92,020	Regional
H-015	Buildout	86	12265_12266	Hillsboro Interceptor	30	311	0.00070	6.90	5.99	0.91	1,754	-	5.99	8.25	8.25	42	7.6	348	108,200	140,660	175,825	17.20	60%	105,235	Regional
H-015	Buildout	85	12266_12267	Hillsboro Interceptor	30	222	0.00070	7.13	6.15	0.98	1,876	-	6.16	8.41	8.41	42	11.1	383	84,948	110,432	138,040	17.20	59%	80,784	Regional
H-015	Buildout	84	12267_12268	Hillsboro Interceptor	30	145	0.00140	9.87	6.15	3.72	7,125	-	6.16	8.41	8.41	42	11.7	389	56,349	73,254	91,567	24.32	59%	54,415	Regional
H-015	Buildout	83	12268_12269	Hillsboro Interceptor	30	75	0.00200	11.88	6.15	5.73	10,992	-	6.16	8.41	8.41	42	12.1	393	29,438	38,269	47,837	29.07	59%	28,282	Regional
H-015	Buildout	82	12269_12270	Hillsboro Interceptor	30	490	0.00090	7.96	6.15	1.81	3,478	-	6.15	8.41	8.41	42	11.3	385	188,488	245,035	306,293	19.50	59%	181,231	Regional
H-015	Buildout	81	12270_12271	Hillsboro Interceptor	30	197	0.00120	9.08	6.14	2.94	5,629	-	6.15	8.41	8.41	42	9.0	362	71,248	92,622	115,778	22.51	60%	69,094	Regional
H-015	Buildout	80	12271_12272	Hillsboro Interceptor	30	443	0.00090	7.98	6.15	1.84	3,521	-	6.15	8.41	8.41	42	7.0	342	151,436	196,867	246,084	19.50	59%	145,328	Regional
H-015	Buildout	79	12272_12273	Hillsboro Interceptor	30	497	0.00090	7.99	6.14	1.85	3,548	-	6.15	8.40	8.40	42	7.5	346	172,208	223,870	279,838	19.50	59%	165,104	Regional
H-015	Buildout	78	12273_12274	Hillsboro Interceptor	30	337	0.00100	8.44	6.17	2.27	4,348	-	6.18	8.43	8.43	42	6.8	340	114,417	148,742	185,928	20.55	59%	109,589	Regional
H-015	Buildout	77	12274_12275	Hillsboro Interceptor	30	401	0.00070	7.02	6.17	0.85	1,634	-	6.18	8.44	8.44	42	7.0	341	136,856	177,913	222,391	17.20	59%	131,593	Regional
H-015	Buildout	76	12275_12276	Hillsboro Interceptor	30	382	0.00120	9.32	6.16	3.16	6,051	-	6.18	8.43	8.43	42	8.4	356	135,934	176,715	220,893	22.51	59%	129,461	Regional
H-015	Buildout	75	12276_12277	Hillsboro Interceptor	30	220	0.00070	6.94	6.16	0.78	1,497	-	6.18	8.43	8.43	42	8.7	359	78,943	102,626	128,283	17.20	60%	76,529	Regional
H-015	Buildout	74	12277_12278	Hillsboro Interceptor	30	345	0.00100	8.34	6.15	2.19	4,203	-	6.17	8.42	8.42	42	11.8	390	134,386	174,702	218,377	20.55	59%	129,758	Regional
H-015	Buildout	73	12278_12279	Hillsboro Interceptor	30	137	0.00190	11.57	6.14	5.44	10,422	-	6.17	8.42	8.42	42	15.2	425	58,165	75,615	94,519	28.33	59%	55,903	Regional
H-015 Total						**4,692**													**1,681,676**	**2,186,178**	**2,732,723**		**59%**	**1,616,070**	
H-100	2015	6319	26125_26124	HLAT003	8	500	0.00400	0.49	0.06	0.43	827	726	0.82	1.09	1.09	12	7.2	130	64,804	84,246	105,307	1.46	66%	69,509	-
H-100	2015	6314	26124_26123	HLAT003	8	68	0.00400	0.49	0.06	0.43	825	726	0.82	1.09	1.09	12	9.2	144	9,791	12,728	15,910	1.46	66%	10,516	-
H-100	2015	6312	26123_23553	HLAT003	8	72	0.00400	0.50	0.06	0.43	831	726	0.82	1.09	1.09	12	10.4	152	10,921	14,197	17,746	1.46	66%	11,690	-
H-100	2015	6307	23553_23552	HLAT003	8	122	0.00800	0.70	0.06	0.64	1,224	726	0.82	1.09	1.09	12	12.8	165	20,080	26,104	32,630	2.06	66%	21,510	-
H-100	2015	6300	23552_23551	HLAT003	8	133	0.00560	0.59	0.06	0.52	1,006	726	0.82	1.09	1.09	12	14.8	177	23,594	30,672	38,340	1.72	66%	25,254	-
H-100	2015	6311	23551_23549	HLAT003	8	499	0.00610	0.61	0.23	0.38	726	726	0.98	1.25	1.25	12	13.6	170	84,880	110,345	137,931	1.80	66%	91,138	-
H-100	2015	6309	23549_23548	HLAT003	10	150	0.00390	0.89	0.23	0.66	1,262	726	0.98	1.25	1.25	12	11.1	156	23,341	30,344	37,930	1.44	38%	14,439	-
H-100	2015	6303	23548_23547	HLAT003	10	92	0.00260	0.72	0.23	0.49	945	726	0.98	1.25	1.25	12	9.0	142	13,074	16,996	21,245	1.17	38%	8,124	-
H-100	2015	6306	23547_14581	HLAT003	10	60	0.00520	1.02	0.23	0.79	1,512	726	0.98	1.25	1.25	12	10.6	153	9,166	11,916	14,894	1.66	39%	5,740	-
H-100 Total						**1,696**													**259,651**	**337,546**	**421,933**		**61%**	**257,919**	
H-210	2015	6477	26223_26222	West Union Trunk	8	401	0.00400	0.49	-	0.49	947	64	0.16	0.45	0.45	12	13.1	167	66,770	86,801	108,502	1.46	66%	71,665	-
H-210	2015	6475	26222_26221	West Union Trunk	8	522	0.00340	0.46	-	0.46	882	64	0.54	1.10	1.10	12	14.1	173	90,562	117,731	147,163	1.34	66%	96,727	-
H-210	2015	6473	26221_26220	West Union Trunk	8	450	0.00400	0.49	-	0.49	949	64	0.54	1.10	1.10	12	14.6	176	79,339	103,140	128,925	1.46	66%	85,098	-
H-210	2015	6466	26220_64798	West Union Trunk	8	212	0.00310	0.44	0.40	0.03	64	64	0.90	1.40	1.40	12	14.8	178	37,649	48,944	61,180	1.28	66%	40,331	-
H-210	2015	6469	64798_26219	West Union Trunk	8	238	0.00480	0.54	0.40	0.14	266	64	0.90	1.40	1.40	12	15.0	179	42,509	55,262	69,077	1.59	66%	45,598	-
H-210	2015	6481	26219_26224	West Union Trunk	8	185	0.00340	0.45	0.40	0.05	95	64	0.89	1.40	1.40	12	15.4	181	33,559	43,627	54,533	1.34	66%	36,132	-
H-210	2015	6479	26224_26218	West Union Trunk	8	260	0.00380	0.48	0.40	0.08	150	64	0.89	1.40	1.40	12	15.9	185	48,089	62,515	78,144	1.42	66%	51,672	-
H-210 Total						**2,268**													**398,477**	**518,020**	**647,525**		**66%**	**427,223**	
H-220	Buildout	6460	23510_12944	Old West Union Rd Trunk	8	95	0.00360	0.47	0.06	0.41	779	684	0.27	0.48	2.49	18	8.7	177	16,834	21,884	27,355	4.07	88%	24,208	-
H-220	Buildout	6431	12944_12941	Old West Union Rd Trunk	8	269	0.00290	0.42	0.06	0.36	684	684	0.27	0.48	2.49	18	8.1	346	93,043	120,956	151,195	3.65	89%	133,875	-
H-220	Buildout	6099	12941_12940	McKay Creek Trunk	8	237	0.00470	0.54	0.80	-	-	-	0.49	0.71	2.62	18	8.6	176	41,826	54,374	67,967	4.65	88%	60,105	-
H-220 Total						**601**													**151,702**	**197,213**	**246,517**		**89%**	**218,188**	
H-320	Buildout	6227	75850_68794	HLAT004	10	78	0.00210	0.64	-	0.64	1,232	1,232	0.96	2.15	2.15	18	10.6	191	14,909	19,381	24,226	3.11	79%	19,219	-
H-320	Buildout	6225	68794_69033	HLAT004	10	122	0.00280	0.75	-	0.75	1,437	1,232	0.96	2.15	2.15	18	10.5	380	46,349	60,254	75,318	3.59	79%	59,599	-
H-320	Buildout	6241	69033_69036	HLAT004	18	416	0.00170	2.81	0.31	2.50	4,800	1,232	1.70	3.75	3.75	24	10.6	457	190,305	247,397	309,246	6.03	53%	164,991	Regional
H-320	Buildout	6239	69036_68197	HLAT004	18	450	0.00170	2.81	0.31	2.51	4,808	1,232	1.70	3.75	3.75	24	11.0	464	208,613	271,197	338,997	6.03	53%	180,646	Regional
H-320	Buildout	6237	68197_69198	HLAT004	18	356	0.00170	2.82	0.75	2.07	3,961	1,232	2.09	4.17	4.17	24	10.0	448	159,394	207,212	259,015	6.03	53%	137,942	Regional
H-320	Buildout	6235	68198_69196	HLAT004	18	213	0.00170	2.80	0.75	2.05	3,926	1,232	2.09	4.17	4.17	24	8.7	214	45,570	59,241	74,051	6.03	54%	39,675	Regional
H-320	Buildout	6233	68196_69195	HLAT004	18	252	0.00170	2.81	0.75	2.06	3,952	1,232	2.08	4.17	4.17	24	9.0	216	54,497	70,846	88,557	6.03	53%	47,248	Regional
H-320	Buildout	6231	68195_69194	HLAT004	18	247	0.00170	2.81	0.78	2.02	3,874	1,232	2.12	4.27	4.27	24	10.2	225	55,673	72,375	90,469	6.03	53%	48,345	Regional
H-320	Buildout	6229	68194_69193	HLAT004	18	253	0.00210	3.11	0.78	2.33	4,467	1,232	2.12	4.27	4.27	24	13.0	248	62,733	81,552	101,941	6.70	53%	54,534	Regional
H-320	Buildout	6198	68193_801130	HLAT004	18	200	0.00100	2.15	0.78	1.37	2,623	1,232	2.12	4.27	4.27	24	16.8	277	55,436	72,067	90,084	4.62	53%	48,139	Regional
H-320	Buildout	6195	801130_68192	HLAT004	18	70	0.00600	5.27	0.78	4.49	8,604	1,232	2.11	4.26	4.26	24	17.2	280	19,628	25,516	31,895	11.32	53%	17,045	Regional
H-320	Buildout	6228	68192_12178	HLAT004	18	492	0.00120	2.34	0.78	1.55	2,977	1,232	2.11	4.26	4.26	24	12.9	247	121,511	157,965	197,456	5.06	54%	106,345	Regional
H-320 Total						**3,149**													**1,034,619**	**1,345,005**	**1,681,256**		**55%**	**923,728**	
R-020	2015	1779	08204_08172	198th Avenue Lateral	10	253	0.00360	0.85	0.68	0.17	333	-	0.94	1.34	1.34	15	6.4	143	36,251	47,126	58,908	2.50	66%	38,876	-
R-020	2015	1772	08172_08173	198th Avenue Lateral	10	325	0.00880	1.33	0.91	0.42	811	-	1.17	1.57	1.57	15	6.5	144	46,866	60,926	76,157	3.91	66%	50,255	-
R-020	2015	1773	08173_08174	198th Avenue Lateral	10	162	0.00880	1.33	0.91	0.42	808	-	1.17	1.56	1.56	15	5.2	135	21,863	28,421	35,527	3.91	66%	23,467	-
R-020	2015	1774	08174_08175	198th Avenue Lateral	10	163	0.00880	1.33	0.91	0.43	817	-	1.16	1.55	1.55	15	4.9	133	21,643	28,136	35,170	3.91	66%	23,185	-
R-020	2015	1775	08175_08176	198th Avenue Lateral	10	185	0.00290	0.76	0.91	-	-	-	1.16	1.55	1.55	15	5.3	136	25,174	32,726	40,908	2.25	66%	27,079	-
R-020	2015	1776	08176_08177	198th Avenue Lateral	10	140	0.00150	0.55	0.91	-	-	-	1.16	1.55	1.55	15	6.2	142	19,879	25,843	32,303	1.62	66%	21,315	-
R-020	2015	1777	08177_08178	198th Avenue Lateral	10	75	0.00320	0.80	0.91	-	-	-	1.16	1.55	1.55	15	5.7	139	10,402	13,523	16,903	2.36	66%	11,154	-
R-020	2015	1778	08178_08179	198th Avenue Lateral	10	265	0.00400	0.89	0.91	-	-	-	1.16	1.55	1.55	15	6.4	143	37,916	49,291	61,614	2.64	66%	40,757	-
R-020	2015	1804	08179_08018	198th Avenue Lateral	10	325	0.01320	1.63	0.91	0.72	1,388	-	1.16	1.55	1.55	15	6.2	142	46,103	59,934	74,918	4.79	66%	49,440	-
R-020	2015	1421	08018_08017	198th Avenue Lateral	10	325	0.00880	1.33	0.91	0.43	815	-	1.16	1.54	1.54	15	5.2	135	43,838	56,990	71,237	3.91	66%	47,009	-
R-020	2015	1420	08017_08016	198th Avenue Lateral	10	345	0.01100	1.49	0.91	0.58	1,116	-	1.16	1.54	1.54	15	5.9	140	48,354	62,860	78,575	4.38	66%	51,866	-
R-020	2015	1419	08016_08015	198th Avenue Lateral	12	173	0.00620	1.81	1.09	0.72	1,387	-	1.35	1.73	1.73	15	8.0	154	26,635	34,626	43,282	3.29	45%	19,379	-

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
R-020	2015	1418	08015_07933	198th Avenue Lateral	12	193	0.00560	1.73	1.09	0.64	1,217	-	1.35	1.73	1.73	15	8.1	154	29,813	38,757	48,446	3.12	45%	21,668	-
R-020 Total						**2,929**													**414,737**	**539,158**	**673,948**		**63%**	**425,450**	
R-110	Existing	1184	20681_20680	Hall Blvd Lateral	15	249	0.00230	2.02	3.39	-	-	-	3.39	3.49	3.49	18	9.1	180	44,780	58,214	72,768	3.25	38%	27,614	-
R-110	Existing	1183	20680_20679	Hall Blvd Lateral	15	119	0.00340	2.46	3.39	-	-	-	3.39	3.49	3.49	18	8.0	172	20,504	26,655	33,318	3.96	38%	12,637	-
R-110	Existing	1182	20679_20678	Hall Blvd Lateral	15	40	0.00320	2.39	3.39	-	-	-	3.39	3.49	3.49	18	9.1	180	7,192	9,350	11,687	3.84	38%	4,424	-
R-110	Existing	1181	20678_20677	Hall Blvd Lateral	15	140	0.00310	2.35	3.39	-	-	-	3.39	3.49	3.49	18	8.4	175	24,507	31,859	39,824	3.78	38%	15,100	-
R-110	Existing	1180	20677_20676	Hall Blvd Lateral	15	131	0.00270	2.16	3.39	-	-	-	3.39	3.49	3.49	18	9.6	184	24,112	31,345	39,181	3.53	39%	15,148	-
R-110	Existing	1179	20676_20675	Hall Blvd Lateral	15	265	0.00300	2.28	3.39	-	-	-	3.39	3.49	3.49	18	9.7	185	48,908	63,580	79,476	3.72	39%	30,617	-
R-110	Existing	1178	20675_20674	Hall Blvd Lateral	15	102	0.00430	2.75	3.39	-	-	-	3.39	3.49	3.49	18	7.0	165	16,813	21,856	27,320	4.45	38%	10,448	-
R-110	Existing	1177	20674_20673	Hall Blvd Lateral	15	127	0.00300	2.29	3.39	-	-	-	3.39	3.49	3.49	18	7.5	169	21,423	27,851	34,813	3.72	38%	13,375	-
R-110	Existing	1176	20673_20672	Hall Blvd Lateral	15	130	0.00300	2.29	3.39	-	-	-	3.39	3.49	3.49	18	9.3	182	23,616	30,701	38,376	3.72	38%	14,711	-
R-110	Existing	1175	20672_18342	Hall Blvd Lateral	15	247	0.00400	2.65	3.39	-	-	-	3.39	3.49	3.49	18	11.0	193	47,784	62,120	77,649	4.29	38%	29,717	-
R-110	Existing	1273	20690_20689	Hall Blvd Lateral	15	289	0.00270	2.19	2.62	-	-	-	2.62	2.71	2.71	18	8.9	179	51,633	67,123	83,904	3.53	38%	31,854	-
R-110	Existing	1272	20689_20688	Hall Blvd Lateral	15	323	0.00540	3.08	3.39	-	-	-	3.40	3.49	3.49	18	10.2	188	60,640	78,832	98,540	4.99	38%	37,673	-
R-110	Existing	1271	20688_20687	Hall Blvd Lateral	15	180	0.00330	2.42	3.39	-	-	-	3.40	3.49	3.49	18	10.3	189	34,018	44,224	55,280	3.90	38%	21,018	-
R-110	Existing	1293	20687_20686	Hall Blvd Lateral	15	133	0.00330	2.41	3.39	-	-	-	3.40	3.49	3.49	18	10.6	191	25,354	32,961	41,201	3.90	38%	15,761	-
R-110	Existing	1189	20686_20685	Hall Blvd Lateral	15	328	0.00300	2.29	3.39	-	-	-	3.40	3.49	3.49	18	11.8	199	65,295	84,884	106,104	3.72	38%	40,820	-
R-110	Existing	1188	20685_20684	Hall Blvd Lateral	15	35	0.00110	1.41	3.39	-	-	-	3.40	3.49	3.49	18	11.5	198	6,914	8,988	11,235	2.25	37%	4,172	-
R-110	Existing	1187	20684_20683	Hall Blvd Lateral	15	201	0.00280	2.21	3.39	-	-	-	3.40	3.49	3.49	18	11.6	198	39,798	51,737	64,671	3.59	38%	24,891	-
R-110	Existing	1186	20683_20682	Hall Blvd Lateral	15	134	0.00150	1.62	3.39	-	-	-	3.39	3.49	3.49	18	11.7	199	26,651	34,647	43,309	2.63	39%	16,674	-
R-110	Existing	1185	20682_20681	Hall Blvd Lateral	15	240	0.00150	1.62	3.39	-	-	-	3.39	3.49	3.49	18	10.8	192	46,096	59,924	74,905	2.63	38%	28,710	-
R-110 Total						**3,413**													**636,039**	**826,850**	**1,033,563**		**38%**	**395,363**	
R-115	Existing	1139	18262_18261	Hall Blvd Lateral	10	293	0.00310	0.79	0.53	0.26	495	-	0.53	0.53	0.53	15	13.7	193	56,417	73,342	91,678	2.32	66%	60,631	-
R-115	Existing	1137	18260_18259	Hall Blvd Lateral	10	413	0.00290	0.76	0.32	0.45	860	-	0.32	0.32	0.32	15	12.1	182	75,240	97,812	122,265	2.25	66%	80,652	-
R-115	Existing	1136	18259_18258	Hall Blvd Lateral	10	409	0.00280	0.75	0.32	0.44	836	-	0.32	0.32	0.32	15	10.1	168	68,741	89,363	111,703	2.21	66%	73,632	-
R-115	Existing	1135	18258_18243	Hall Blvd Lateral	10	15	0.03000	2.46	0.32	2.14	4,106	-	0.32	0.32	0.32	15	8.3	156	2,345	3,049	3,811	7.23	66%	2,515	-
R-115	Existing	1140	18263_18262	Hall Blvd Lateral	10	322	0.00150	0.55	-	0.55	1,061	-	-	-	-	15	13.7	193	62,187	80,843	101,054	1.62	66%	66,438	-
R-115	Existing	1138	18261_18260	Hall Blvd Lateral	10	315	0.00700	1.19	0.53	0.66	1,261	-	0.53	0.53	0.53	15	12.0	181	57,119	74,254	92,818	3.49	66%	61,287	-
R-115 Total						**1,767**													**322,049**	**418,663**	**523,329**		**66%**	**345,156**	
R-120	2015	1105	12453_12454	Beaverton Interceptor	24	202	0.00190	6.36	8.03	-	-	-	8.05	8.19	8.19	27	10.6	253	51,150	66,496	83,119	8.72	27%	22,545	Regional
R-120	2015	1106	12454_12455	Beaverton Interceptor	24	197	0.00200	6.52	8.03	-	-	-	8.04	8.19	8.19	27	9.1	242	47,600	61,880	77,350	8.95	27%	20,984	Regional
R-120	2015	1107	12455_12456	Beaverton Interceptor	24	127	0.00230	7.00	8.03	-	-	-	8.04	8.19	8.19	27	9.2	484	61,456	79,893	99,866	9.59	27%	26,988	Regional
R-120	2015	1108	12456_12457	Beaverton Interceptor	24	397	0.00200	6.54	8.03	-	-	-	8.04	8.19	8.19	27	9.9	248	98,462	128,001	160,001	8.95	27%	43,105	Regional
R-120	2015	1109	12457_12458	Beaverton Interceptor	24	175	0.00190	6.46	8.03	-	-	-	8.04	8.19	8.19	27	11.2	775	135,651	176,346	220,433	8.72	26%	57,178	Regional
R-120	2015	1110	12458_12459	Beaverton Interceptor	24	435	0.00200	6.55	8.61	-	-	-	8.62	8.81	8.81	27	12.5	269	117,048	152,163	190,204	8.95	27%	50,898	Regional
R-120	2015	1111	12459_12460	Beaverton Interceptor	24	275	0.00170	6.12	8.61	-	-	-	8.62	8.80	8.80	27	13.4	276	75,968	98,758	123,448	8.25	26%	31,829	Regional
R-120	2015	1112	12460_12461	Beaverton Interceptor	24	215	0.00290	7.93	8.61	-	-	-	8.62	8.80	8.80	27	12.9	272	58,521	76,077	95,097	10.77	26%	25,083	Regional
R-120	2015	1113	12461_12462	Beaverton Interceptor	24	295	0.00790	13.02	8.61	4.42	8,466	-	8.62	8.80	8.80	27	12.9	272	80,248	104,322	130,403	17.78	27%	34,904	Regional
R-120	2015	1114	12462_13408	Beaverton Interceptor	24	127	0.01310	16.75	8.61	8.15	15,620	-	8.62	8.80	8.80	27	14.0	281	35,687	46,393	57,991	22.90	27%	15,565	Regional
R-120	2015	1119	13408_13407	Beaverton Interceptor	24	130	0.00400	9.27	8.60	0.66	1,271	-	8.62	8.80	8.80	27	16.8	304	39,555	51,422	64,278	12.65	27%	17,200	Regional
R-120	2015	1118	13407_12463	Beaverton Interceptor	24	345	0.00100	4.67	8.60	-	-	-	8.62	8.80	8.80	27	13.4	276	95,319	123,915	154,894	6.33	26%	40,625	Regional
R-120	2015	1115	12463_10869	Beaverton Interceptor	24	109	0.07390	39.85	8.60	31.24	59,899	-	8.61	8.79	8.79	27	11.6	262	28,512	37,066	46,332	54.39	27%	12,387	Regional
R-120 Total						**3,029**													**925,179**	**1,202,732**	**1,503,415**		**27%**	**399,291**	
R-125	2015	1158	18390_18389	Murray Blvd Interceptor	15	160	0.00200	1.87	2.40	-	-	-	2.40	2.44	2.44	18	9.4	182	29,152	37,898	47,372	3.03	38%	18,158	-
R-125	2015	1157	18389_18388	Murray Blvd Interceptor	15	160	0.00210	1.93	2.40	-	-	-	2.40	2.44	2.44	18	8.6	177	28,271	36,753	45,941	3.11	38%	17,443	-
R-125	2015	1156	18388_18387	Murray Blvd Interceptor	15	108	0.00230	2.01	2.40	-	-	-	2.40	2.44	2.44	18	8.1	173	18,697	24,306	30,383	3.25	38%	11,590	-
R-125	2015	1155	18387_18386	Murray Blvd Interceptor	15	180	0.00200	1.87	2.40	-	-	-	2.40	2.44	2.44	18	8.5	176	31,651	41,146	51,432	3.03	38%	19,715	-
R-125	2015	1154	18386_18385	Murray Blvd Interceptor	15	26	0.00190	1.83	2.40	-	-	-	2.40	2.44	2.44	18	8.8	178	4,628	6,016	7,520	2.96	38%	2,856	-
R-125	2015	1153	18385_18384	Murray Blvd Interceptor	15	302	0.00200	1.88	2.40	-	-	-	2.40	2.44	2.44	18	13.1	209	63,045	81,958	102,447	3.03	38%	38,964	-
R-125	2015	1152	18384_18367	Murray Blvd Interceptor	15	292	0.00270	2.16	2.40	-	-	-	2.40	2.44	2.44	18	18.0	244	71,175	92,527	115,659	3.53	39%	44,715	-
R-125 Total						**1,228**													**246,618**	**320,603**	**400,754**		**38%**	**153,441**	
R-140	Existing	8971	08157_08156	RLAT008	8	150	0.00490	0.55	0.78	-	-	-	3.01	4.09	4.70	21	7.1	184	27,547	35,811	44,764	7.17	92%	41,330	-
R-140	Existing	8980	08156_08147	RLAT008	8	403	0.00630	0.62	0.78	-	-	-	3.01	4.09	4.70	21	7.2	184	74,343	96,646	120,807	8.12	92%	111,547	-
R-140	Existing	8992	08147_08146	RLAT008	8	326	0.00850	0.72	0.78	-	-	-	3.01	4.08	4.69	21	7.5	186	60,749	78,974	98,718	9.44	92%	91,169	-
R-140	Existing	8982	08146_08140	RLAT008	8	107	0.01710	1.02	0.78	0.25	473	-	3.01	4.08	4.69	21	7.5	186	19,947	25,931	32,414	13.39	92%	29,935	-
R-140	Existing	8989	08140_08139	RLAT008	8	188	0.01700	1.02	0.78	0.24	464	-	3.14	4.54	10.97	27	7.4	227	42,737	55,558	69,448	26.09	96%	66,734	Regional
R-140	Existing	8986	08139_08138	RLAT008	8	81	0.00590	0.60	0.78	-	-	-	3.13	4.54	10.96	27	7.4	227	18,417	23,942	29,927	15.37	96%	28,753	Regional
R-140	Existing	8993	08138_08137	RLAT008	8	181	0.00480	0.54	0.78	-	-	-	3.13	4.53	10.95	27	8.8	238	43,163	56,112	70,140	13.86	96%	67,394	Regional
R-140	Existing	8990	08137_08135	RLAT008	8	175	0.01470	0.95	0.78	0.17	329	-	3.13	4.53	10.94	27	9.6	245	42,887	55,753	69,691	24.26	96%	66,966	Regional
R-140	Existing	8363	08135_55970	RLAT008	8	551	0.00370	0.47	0.78	-	-	-	3.13	4.53	10.93	27	13.2	275	151,557	197,025	246,281	12.17	96%	236,672	Regional
R-140 Total						**2,162**													**481,347**	**625,751**	**782,189**		**95%**	**740,500**	
R-145	2015	8835	55852_22794	RLAT008	8	57	0.02000	1.11	-	1.11	2,120	-	1.71	2.39	3.05	15	7.5	150	8,516	11,071	13,838	5.90	81%	11,245	-
R-145	2015	8825	22794_22793	RLAT008	8	124	0.06730	2.03	-	2.03	3,894	-	1.71	2.39	3.05	15	9.1	162	20,040	26,052	32,564	10.83	81%	26,455	-
R-145	2015	8803	22793_22792	RLAT008	8	117	0.02090	1.13	-	1.13	2,171	-	1.71	2.38	3.05	15	9.7	166	19,402	25,222	31,528	6.03	81%	25,610	-
R-145	2015	8829	22792_22791	RLAT008	8	98	0.00720	0.67	-	0.67	1,277	-	1.70	2.38	3.05	15	9.6	165	16,168	21,018	26,272	3.54	81%	21,331	-

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
R-145	2015	8847	22791_22790	RLAT008	8	100	0.01100	0.82	-	0.82	1,574	-	1.70	2.38	3.05	15	11.2	176	17,555	22,821	28,527	4.38	81%	23,175	-
R-145	2015	8868	22790_22789	RLAT008	8	81	0.01320	0.90	-	0.90	1,725	-	1.70	2.38	3.05	15	12.4	184	14,908	19,380	24,226	4.79	81%	19,679	-
R-145	2015	8866	22789_22788	RLAT008	8	434	0.05050	1.76	-	1.76	3,372	-	1.70	2.38	3.04	15	12.5	185	80,246	104,320	130,400	9.38	81%	105,940	-
R-145	2015	8849	22788_22787	RLAT008	8	91	0.01930	1.09	-	1.09	2,087	-	1.69	2.37	3.04	15	12.1	182	16,563	21,532	26,915	5.80	81%	21,861	-
R-145	2015	8839	22787_22786	RLAT008	8	216	0.12870	2.81	0.32	2.49	4,773	-	2.00	2.74	3.41	15	9.1	161	34,834	45,285	56,606	14.97	81%	45,990	-
R-145	2015	8820	22786_22785	RLAT008	8	75	0.41920	5.07	0.32	4.75	9,107	-	2.00	2.74	3.40	15	8.2	155	11,659	15,157	18,946	27.02	81%	15,392	-
R-145	2015	8823	22785_22781	RLAT008	8	125	0.33590	4.54	0.32	4.22	8,089	-	2.00	2.74	3.40	15	12.8	187	23,338	30,339	37,924	24.19	81%	30,810	-
R-145	2015	8831	22781_22780	RLAT008	8	215	0.01050	0.80	0.32	0.48	929	-	1.99	2.73	3.40	15	12.8	186	40,097	52,126	65,158	4.28	81%	52,932	-
R-145	2015	8806	22780_22779	RLAT008	8	69	0.18060	3.33	0.32	3.01	5,768	-	1.99	2.73	3.39	15	7.5	151	10,419	13,545	16,931	17.73	81%	13,755	-
R-145	2015	8832	22779_22778	RLAT008	8	168	0.10860	2.58	0.32	2.26	4,337	-	1.99	2.73	3.39	15	6.6	145	24,329	31,627	39,534	13.75	81%	32,117	-
R-145	2015	8834	22778_22777	RLAT008	8	273	0.10110	2.49	0.32	2.17	4,161	-	1.99	2.72	3.39	15	7.8	153	41,678	54,182	67,727	13.27	81%	55,026	-
R-145	2015	8815	22777_22776	RLAT008	8	59	0.32120	4.44	0.32	4.12	7,895	-	1.99	2.72	3.38	15	7.5	150	8,879	11,543	14,428	23.65	81%	11,722	-
R-145	2015	8809	22776_22760	RLAT008	8	77	0.01440	0.94	0.32	0.62	1,193	-	1.99	2.72	3.38	15	7.0	147	11,347	14,751	18,439	5.01	81%	14,978	-
R-145	2015	8861	22760_22759	RLAT008	8	20	1.49500	9.57	0.32	9.25	17,739	-	1.98	2.71	3.37	15	6.0	141	2,817	3,662	4,577	51.02	81%	3,719	-
R-145	2015	8863	22759_22758	RLAT008	8	159	0.01420	0.93	0.32	0.61	1,175	-	1.98	2.71	3.37	15	5.4	137	21,733	28,254	35,317	4.97	81%	28,706	-
R-145	2015	8843	22758_22757	RLAT008	8	103	0.08640	2.30	0.32	1.98	3,802	-	1.98	2.71	3.37	15	5.4	136	14,026	18,234	22,793	12.27	81%	18,517	-
R-145	2015	8841	22757_14749	RLAT008	8	95	0.20930	3.58	0.32	3.26	6,256	-	1.98	2.70	3.36	15	9.4	164	15,540	20,202	25,253	19.09	81%	20,517	-
R-145	2015	8978	14749_14748	RLAT008	8	400	0.03000	1.36	0.32	1.04	1,990	-	2.56	3.63	4.28	15	9.3	163	65,270	84,850	106,063	7.23	81%	86,166	-
R-145	2015	8994	14748_09992	RLAT008	8	300	0.03000	1.36	0.32	1.04	1,990	-	2.56	3.63	4.27	15	7.3	449	134,617	175,002	218,752	7.23	81%	177,714	-
R-145	2015	8998	09992_09991	RLAT008	8	190	0.03000	1.36	0.32	1.04	1,990	-	2.56	3.63	4.27	15	9.7	166	31,455	40,892	51,115	7.23	81%	41,526	-
R-145	2015	8996	09991_09989	RLAT008	8	157	0.03000	1.36	0.32	1.04	1,990	-	2.56	3.63	4.26	15	9.9	167	26,211	34,074	42,593	7.23	81%	34,602	-
R-145	2015	8975	09989_09988	RLAT008	8	30	0.03630	1.49	0.32	1.17	2,252	-	2.56	3.63	4.26	15	8.7	159	4,774	6,206	7,757	7.95	81%	6,301	-
R-145	2015	8985	09988_08159	RLAT008	8	152	0.01420	0.93	0.32	0.62	1,183	-	2.55	3.62	4.25	15	7.4	150	22,831	29,681	37,101	4.97	81%	30,132	-
R-145	2015	8973	08159_08157	RLAT008	8	141	0.03210	1.40	0.32	1.08	2,078	-	2.55	3.62	4.24	15	7.4	150	21,128	27,467	34,334	7.48	81%	27,899	-
R-145 Total						**4,126**													**760,381**	**988,495**	**1,235,619**		**81%**	**1,003,817**	
R-240	Buildout	350	13786_13785	Bendemeer Trunk	18	455	0.00160	2.76	1.21	1.55	2,974	1,208	2.36	4.00	4.00	24	12.3	242	110,214	143,278	179,097	5.85	53%	94,466	Regional
R-240	Buildout	349	13785_13784	Bendemeer Trunk	18	550	0.00160	2.69	1.21	1.48	2,837	1,208	2.36	4.00	4.00	24	17.9	286	157,197	204,356	255,445	5.85	54%	137,870	Regional
R-240	Buildout	348	13784_13783	Bendemeer Trunk	18	526	0.00160	2.70	1.21	1.49	2,866	1,208	2.36	4.00	4.00	24	20.7	541	284,649	370,043	462,554	5.85	54%	248,681	Regional
R-240	Buildout	8756	13783_63607	Bendemeer Re-Route	18	61	0.00110	2.30	1.20	1.10	2,110	-	2.36	3.99	3.99	24	20.2	356	21,708	28,220	35,275	4.85	52%	18,500	Regional
R-240 Total						**1,592**													**573,767**	**745,897**	**932,371**		**54%**	**499,518**	
R-241	Buildout	351	13787_13786	Bendemeer Trunk	12	250	0.04680	4.99	0.23	4.76	9,124	1,208	1.29	2.23	2.23	18	8.6	176	44,084	57,310	71,637	14.68	66%	47,275	-
R-241	Buildout	353	13789_13788	Bendemeer Trunk	12	359	0.00250	1.16	0.30	0.86	1,650	1,208	1.29	2.24	2.24	18	20.4	383	137,601	178,881	223,601	3.39	66%	147,012	-
R-241	Buildout	352	13788_13787	Bendemeer Trunk	12	500	0.00240	1.13	0.27	0.86	1,657	1,208	1.29	2.23	2.23	18	14.4	218	108,900	141,570	176,962	3.32	66%	116,783	-
R-241 Total						**1,109**													**290,585**	**377,761**	**472,201**		**66%**	**311,071**	
R-242	Buildout	360	13798_13797	E. Country Haven Lateral	12	408	0.00250	1.15	0.71	0.45	857	801	0.73	1.44	1.44	15	10.4	170	69,544	90,407	113,008	2.09	45%	50,519	-
R-242	Buildout	359	13797_13796	E. Country Haven Lateral	12	514	0.00240	1.12	0.71	0.42	801	801	0.73	1.44	1.44	15	9.2	162	83,487	108,533	135,666	2.04	45%	61,074	-
R-242	Buildout	358	13796_13786	E. Country Haven Lateral	12	520	0.00240	1.13	0.71	0.42	806	801	0.73	1.44	1.44	15	9.4	164	85,098	110,627	138,284	2.04	45%	62,077	-
R-242 Total						**1,442**													**238,129**	**309,567**	**386,959**		**45%**	**173,670**	
R-250	2015	8771	75316_75315	Bendemeer Re-Route	8	55	0.00400	0.49	0.84	-	-	-	0.88	1.24	1.24	15	15.3	204	11,196	14,555	18,194	2.64	81%	14,782	-
R-250	2015	8773	75315_75314	Bendemeer Re-Route	10	240	0.00280	0.75	0.84	-	-	-	0.88	1.24	1.24	15	14.9	201	48,195	62,653	78,316	2.21	66%	51,716	-
R-250	2015	8775	75314_75313	Bendemeer Re-Route	10	190	0.00280	0.75	0.84	-	-	-	0.88	1.24	1.24	15	13.6	192	36,539	47,501	59,376	2.21	66%	39,226	-
R-250	2015	8777	75313_75312	Bendemeer Re-Route	10	278	0.00280	0.75	0.84	-	-	-	0.88	1.24	1.24	15	12.4	184	51,204	66,565	83,206	2.21	66%	54,872	-
R-250	2015	8779	75312_75311	Bendemeer Re-Route	10	225	0.00280	0.75	0.84	-	-	-	0.88	1.24	1.24	15	11.0	174	39,231	51,000	63,750	2.21	66%	42,079	-
R-250	2015	8781	75311_75310	Bendemeer Re-Route	10	60	0.00050	0.32	0.84	-	-	-	0.88	1.24	1.24	15	10.6	172	10,319	13,414	16,768	0.93	66%	11,068	-
R-250	2015	8783	75310_76021	Bendemeer Re-Route	10	25	0.00440	0.94	0.84	0.10	199	-	0.88	1.24	1.24	15	10.3	170	4,243	5,516	6,896	2.77	66%	4,551	-
R-250	2015	8869	76021_13800	Bendemeer Re-Route	10	10	(0.06600)	-	0.84	-	-	-	0.88	1.24	1.24	15	9.5	164	1,641	2,134	2,667	-	0%	-	-
R-250	2015	8785	13800_13802	Bendemeer Re-Route	10	421	0.00290	0.76	0.84	-	-	-	0.88	1.24	1.24	15	9.3	163	68,739	89,361	111,701	2.25	66%	73,876	-
R-250 Total						**1,504**													**271,307**	**352,699**	**440,874**		**66%**	**292,170**	
R-260	Existing	1856	20197_20198	26th Street Lateral	10	225	0.00330	0.82	1.06	-	-	-	1.06	1.06	1.06	12	11.9	160	35,947	46,731	58,414	1.32	38%	22,224	-
R-260	Existing	1857	20198_20199	26th Street Lateral	10	210	0.00240	0.69	1.06	-	-	-	1.06	1.06	1.06	12	11.5	158	33,111	43,045	53,806	1.13	39%	20,759	-
R-260	Existing	1858	20199_20200	26th Street Lateral	10	280	0.00290	0.76	1.06	-	-	-	1.06	1.06	1.06	12	10.7	153	42,828	55,677	69,596	1.24	38%	26,720	-
R-260	Existing	1859	20200_20201	26th Street Lateral	10	350	0.00300	0.78	1.06	-	-	-	1.06	1.06	1.06	12	10.6	153	53,399	69,418	86,773	1.26	38%	33,280	-
R-260	Existing	1860	20201_20202	26th Street Lateral	10	293	0.01120	1.50	1.06	0.44	847	-	1.06	1.06	1.06	12	10.8	153	44,972	58,464	73,080	2.44	38%	28,036	-
R-260	Existing	2005	20202_20203	26th Street Lateral	10	500	0.00390	0.89	1.06	-	-	-	1.06	1.06	1.06	12	10.4	151	75,698	98,408	123,010	1.44	38%	46,770	-
R-260	Existing	1883	20203_20204	26th Street Lateral	10	423	0.01130	1.51	1.26	0.25	482	-	1.26	1.28	1.28	12	9.3	144	60,949	79,234	99,042	2.45	38%	37,979	-
R-260	Existing	1884	20204_20205	26th Street Lateral	10	115	0.00500	1.01	1.26	-	-	-	1.26	1.28	1.28	12	8.9	142	16,304	21,195	26,494	1.63	38%	10,088	-
R-260 Total						**2,396**													**363,209**	**472,171**	**590,214**		**38%**	**225,858**	
R-270	Existing	9132	88278_88220	Hall Blvd Lateral	8	268	0.00400	0.49	1.33	-	-	-	1.33	1.33	1.33	15	9.2	162	43,530	56,589	70,737	2.64	81%	57,543	-
R-270	Existing	9152	88220_86430	Hall Blvd Lateral	8	193	0.02090	1.13	1.33	-	-	-	1.33	1.33	1.33	15	10.0	168	32,392	42,109	52,636	6.03	81%	42,767	-
R-270	Existing	9150	86430_86593	Hall Blvd Lateral	8	100	0.01970	1.10	1.33	-	-	-	1.33	1.33	1.33	15	8.5	158	15,763	20,492	25,615	5.86	81%	20,810	-
R-270	Existing	9148	86593_85225	Hall Blvd Lateral	8	121	0.01520	0.97	1.33	-	-	-	1.33	1.33	1.33	15	8.4	157	18,942	24,625	30,781	5.14	81%	24,999	-
R-270	Existing	9146	85225_87200	Hall Blvd Lateral	8	139	0.01480	0.95	1.33	-	-	-	1.33	1.33	1.33	15	8.9	160	22,246	28,920	36,150	5.08	81%	29,365	-
R-270	Existing	9144	87200_84465	Hall Blvd Lateral	8	119	0.00410	0.50	1.33	-	-	-	1.33	1.33	1.33	15	8.6	159	18,816	24,461	30,576	2.67	81%	24,825	-

Appendix N. Summary of Gravity Sewer Capital Improvement Project Costs

Project ID	CIP Timing	Model G_ID	Manholes Nos. Up_Dn	Lateral Name	Existing Diameter, inches	Length, ft	Slope	Full-pipe Capacity, mgd	Peak Wet Weather Existing (2006) Flow, mgd	Peak Wet Weather Remaining Capacity, mgd	EDUs Remaining	Limiting Reach EDUs Remaining	Peak Wet Weather 2015 Flow, mgd	Peak Wet Weather Study Area Buildout Flow, mgd	Peak Wet Weather Buildout + Flow, mgd	Recommended Diameter, inches	Average Depth, ft	Unit Cost, $/LF	Base Construction Cost (Replacement; w/o Contingency), $	Construction Cost (Replacement; w/ Contingency), $	Total Project Cost, $	Capacity at Replacement Diameter, mgd	Portion of Improvement Allotted to SDC	SDC Improvement Cost, $	Future Local/ Regional
R-270	Existing	9142	84465_84935	Hall Blvd Lateral	8	132	0.00700	0.65	1.33	-	-	-	1.33	1.33	1.33	15	8.3	157	20,713	26,926	33,658	3.49	81%	27,368	-
R-270	Existing	9140	84935_85948	Hall Blvd Lateral	8	160	0.00390	0.49	1.33	-	-	-	1.33	1.33	1.33	15	8.4	157	25,065	32,585	40,731	2.61	81%	33,098	-
R-270	Existing	9138	85948_88423	Hall Blvd Lateral	8	93	0.00350	0.46	1.33	-	-	-	1.33	1.33	1.33	15	8.2	156	14,490	18,837	23,546	2.47	81%	19,122	-
R-270	Existing	9136	88423_20694	Hall Blvd Lateral	8	70	0.00910	0.75	1.33	-	-	-	1.33	1.33	1.33	15	8.7	159	11,113	14,447	18,058	3.98	81%	14,662	-
R-270	Existing	9134	20694_84950	Hall Blvd Lateral	12	111	0.00450	1.55	1.33	0.22	429	-	1.33	1.33	1.33	15	9.9	167	18,505	24,056	30,070	2.80	45%	13,430	-
R-270	Existing	9153	84950_20693	Hall Blvd Lateral	12	90	0.00290	1.24	1.33	-	-	-	1.33	1.33	1.33	15	10.0	168	15,148	19,692	24,615	2.25	45%	11,043	-
R-270 Total						**1,596**													**256,722**	**333,739**	**417,173**		**76%**	**319,032**	
Grand Total						**138,331**													**54,260,173**	**70,538,224**	**88,172,781**		**73%**	**64,568,540**	

APPENDIX Q

Hillsboro Trunk Short Term Flow Control
Recalibration of Hillsboro East Interceptor (HEI) Collection System
PMA Engineering; 4/14/08

TECHNICAL MEMORANDUM
Hillsboro Trunk Short Term Flow Control
PMA Engineering / 601 Main Street, Suite 203 / Vancouver, WA 98660 / (360) 993-0635

TO:	Andy Braun, P.E., Capital Program Manager, Clean Water Services
FROM:	Paula M. Arsenault, P.E., PMA Engineering
COPIES:	Jeff Pelz, P.E., West Yost & Associates
	Jim Gilmer, P.E., David Evans & Associates
DATE:	April 14, 2008
PROJECT:	Hillsboro Trunk Short Term Flow Control
SUBJECT:	Recalibration of Hillsboro East Interceptor (HEI) Collection System

OVERVIEW OF EVALUATION

The purpose of this effort was to recalibrate the Hillsboro East Interceptor (HEI) collection system within the Rock Creek Hydra model to current conditions and reflecting the significant amount of sewer repair and rehabilitation work that Clean Water Services (CWS) has completed. This will improve the accuracy of the model in predicting flows during design storm conditions. PMA obtained the current version of the Rock Creek model from West-Yost & Associates (consultant for updating CWS's *Sanitary Sewer Master Plan*) and calibrated the HEI collection system to current dry- and wet-weather conditions. The calibrated model will be used by West Yost & Associates to identify whether potential sewer relief options are needed during the 5-year 24-hour design storm event.

The CWS collection system has had inflow contributions resulting from rooftop and patio drain connections, cross-connections between storm and sewer systems, and other sources such as stream flows entering the system. During 2006 (through mid-January of 2007), CWS completed substantial repairs to reduce inflow/infiltration contributions to the system within the HEI subsystem. The objective was to modify the model to reflect those improvements.

AVAILABLE FLOW METER DATA

There were several temporary and permanent flow monitor locations on the Hillsboro East Interceptor and contributing laterals where dry- and wet-season data were collected between early 2006 and January 2008 as follows:

Table 1. Temporary & Permanent Flow Monitor Sites in the Hillsboro East Interceptor Collection System

MH	Install Location	Lateral Name	Direction from MH	Status
09877	Morse Bros. along Turner Creek (27")	HEI	Unknown (Assumed Downstream)	Temporary
12315	Rock Creek Path (18")	Quail Circle Lateral	Upstream	Temporary
12323	35th Ave. off of Willow St. (18")	37th Avenue Trunk	Upstream	Temporary
12332	Willow St. off SE 32nd Ave. (18") (re-located to 70224)	HEI	Downstream	Permanent
12383	24th Ave. north of Maple St. (18")	HEI	Downstream	Permanent
12424	Baseline Rd. off NE 18th Ave. (18")	HEI	Downstream	Permanent
19882	TV Highway near 32nd Ave. (12")	TV Highway Interceptor	Downstream	Permanent
20206	E Main Street (12")	26th Street Lateral	Downstream	Temporary
20238	18th Ave. off of Grant St. (12")	Cornell Road Lateral	Downstream	Temporary
20276	Grand St. near Delsey St. (10")	HEI	Downstream	Temporary
20283	12th Ave. off of Cornell Rd. (15")	HEI	Unknown (Assumed Downstream)	Temporary
70224	Willow St. off SE 32nd Ave. (18") (re-located from 12332)	HEI	Upstream	Permanent

In addition, rainfall data were available for three relevant gages: Hillsboro WWTP (HWR), Rock Creek WWTP (RCR) and Turner Creek (TCR).

Figure 1 illustrates the locations of the flow meter sites and modeled sewers. Site 19901 was not included in the analysis because the Drake Lateral connection was moved from the HEI to the Rock Creek Trunk and is therefore no longer a part of the HEI collection system.

DATA COLLECTION AND REVIEW

Recent hourly flow and rainfall records for the sites listed in Table 1 were obtained from CWS. CWS indicated that all major sewer repair work was completed as of mid-January 2007, so calibration events were selected from the flow meter and rain gage records from mid-January 2007 to January 2008. Information was also obtained regarding events within the calibration period during which unusual operating circumstances occurred that should be excluded from the calibration event selection process. For instance, in early December of 2006 an SSO occurred because of an unexpected diversion from the Hillsboro system at 9th Avenue. On December 3 of 2007, a pump at the Rock Creek Influent Pump Station was out of service that caused backups throughout the system.

Due to these unusual circumstances, these events were not selected for calibration purposes.

PMA obtained the current Rock Creek Hydra model and appurtenant files from West Yost & Associates. Because WYA completely changed the method for defining sanitary flow injections, PMA travelled to Davis, California to work with the WYA modelers to become familiar with the revised model setup and methods.

FLOW DATA ANALYSIS

The flow data files were initially reviewed to remove negative values, partial days of data and periods when instrument or level adjustments caused significant flow changes or erroneous data. The date and time formatting was revised and rainfall data was added to the flow data files. Flow and rainfall data were then copied into and processed in a wet-season data template similar to that developed during the *2000 Master Plan Update* effort. The spreadsheet template contains macros that transpose the data and update named ranges and equations.

Monthly graphs of the hourly flow and rainfall data were generated in order to review the data and to define the dry-season period for each meter. The periods selected as representing dry-season conditions were then moved to a dry-season spreadsheet tool in which average weekday and weekend flows, and the diurnal pattern are computed. This information was copied into the wet-season spreadsheet tool wherein the infiltration and inflow (I/I) is separated from the base sanitary flow, and seasonal infiltration is separated from rainfall-dependent infiltration and inflow (RDII).

West Yost & Associates developed a complex spreadsheet tool to generate sanitary flow injections to the model. Essentially, a land use polygon (LU Layer) was generated for each sewershed (SE Layer) included in the model. WYA determined the land use within each LU polygon based on parcel data obtained from Metro and the constituent cities. Where available, parcel data from the cities were used and the city land use codes were converted to Metro land use codes to create a uniform coding system.

Rather than using a population-based flow-generation method, as was the case for the *2000 Master Plan Update* effort, WYA set up the LU database to employ an area-based unit flow method. The RES_POP and VIS_POP fields in the LU database contain developed residential and non-residential developed area, respectively, and the RES_CPC and VIS_CPS fields contain unit flows in gallons per acre per day (gpad). Therefore, the 2007 flow meter data for the HEI collection system was analyzed in a similar manner.

PMA set up a spreadsheet table to summarize information included in the WYA Land Use Layer for existing conditions covering the HEI collection system (called *LU_Ex17 HEI Analysis.xls*), which is presented as Table 1. The purpose was to associate the land use information to the sewersheds, determine representative meter assignments for calibration purposes, and to compute developed acreage within the flow meter collection boundaries. The total developed acreage determined by WYA was used to compute unit flows in gpad within the dry-season flow data spreadsheet tools for each flow monitor. These unit flows were then input to the Land Use database (*LU_Ex17.dbf*) and served as the initial values for dry-season model calibration. Following dry-season calibration, the

final unit flow assignments and adjustment percentages (RES_ACTIVE and VIS_ACTIVE) were added to the table in order to provide summary information for WYA. Consistent with WYA's approach, the dry-season weekday unit flows computed from the 2007 flow data was entirely allocated as sanitary base flow. Therefore, the model no longer includes dry-season infiltration as a component.

Within the model AutoCAD drawing, the flow meter boundaries were delineated based on the sewershed boundaries. Two tables were set up to compute accumulated total and developed area upstream of each meter, which are shown in Tables 2 and 3. The total collection area was copied into both the dry- and wet-season flow data spreadsheet tools, and the accumulated developed area was entered into the dry-season data table in order to compute unit weekday base flow in gpad.

The flow monitor summary data table (*RC Monitor Defect Summary.xls*) was modified to include the 2007 HEI flow meters. This spreadsheet is linked to a spreadsheet, *RC Wet Season I-I Inputs.xls* that computes inputs to the I/I defects database, *DefectWE.dbf*, which represents I/I for existing land use and population conditions and moderate antecedent conditions. The I/I inputs in spreadsheet tool are copied to the database. All calibration adjustments are made in the spreadsheets rather than using the TWEAK factors in the Defects database.

MODEL REFINEMENTS

All of the 2007 flow meter locations were added to the model AutoCAD drawing in order to determine if pipe additions or sewershed subdivisions were required. No pipe additions were needed to accommodate flow meter locations, and only one sewershed (G_ID No. 244) was subdivided to generate a new sewershed (G_ID No. 468).

MODEL CALIBRATION

This task involved multiple components that improved model accuracy in the vicinity of the Hillsboro East Interceptor. Calibration to dry-season conditions was performed prior to calibrating the model to selected wet-season storm events. This is because errors in modeling sanitary flows would be carried forth into the analysis of storm event flows. Once the model was calibrated to dry-season conditions, wet-season calibration involved adjusting inputs to the Defects database from which I/I flows are injected to the model. The model was calibrated to selected storm events representing dry (fall season), wet (winter season) and moderate (spring season) antecedent conditions.

Dry-Season Calibration

An iterative process was used to calibrate the model whereby model inputs were adjusted (Land Use Layer), the model was run and the results graphed such that the model was calibrated to within a reasonable level of accuracy. This calibration process involved adjusting sanitary flow quantities and diurnal patterns. In addition, monitor-specific diurnal curves were created to achieve a better match between metered and modeled hydrograph shapes where needed. The four diurnal curves representing median weekday conditions that were developed for the *1995 Collection System Needs*

Analysis were used in addition to the monitor-specific diurnal curves.

The calibrated unit flows (RES_CPC and VIS_CPC) and calibrated percent actives (RES_ACTIVE and COM_ACTIVE) from calibration to 2007 dry-season flows were copied from the LU_Ex17 Layer into the summary table, *LU_Ex17 HEI Analysis.xls*, to provide West Yost & Associates with a summary of the final model inputs. The unit flows and percent actives were uniformly assigned to the LU polygons within each flow meter boundary, as shown in Table 1.

The results of the dry-season calibration process are presented in Figures 2 to 13. Modeled volumes and peak flows were all within 10 percent of metered values.

Wet-Season Model Calibration

Calibration spreadsheet tools were set up and model runs were completed initially for seven events selected from the flow meter data representing a variety of antecedent conditions. Based on these initial model runs, it was apparent that a significant amount of infiltration remains in the HEI collection system and that the system is highly sensitive to antecedent conditions. In addition, it is apparent that the majority of inflow problems have been corrected by the District's rehabilitation program. Among the events analyzed, three events were selected to represent dry-to-moderate, wet and moderate antecedent conditions, respectively: November 18-20, 2007, January 2-4, 2008 and March 24-25, 2008. The former two events were three days in duration and run using a 20-minute time step, while the March event was 2 days in duration and run with a 15-minute step. Rainfall data for all three gauges was used and input in hourly intensity.

Calibration to November 18-20, 2007 (Dry to Moderate Antecedent Conditions)
The month of November 2007 was relatively dry until mid-month. This 3-day event was preceded by 1.18 inches of rainfall between November 15 and 17. Hyetographs for the three nearby rain gauges are shown in Figure 14, which indicates that rainfall was relatively consistent among the gauges. Total rainfall for the 72-hour period was 1.31 inches at gauge TCR and 1.26 inches at gauge RCR. Comparative graphical results showing modeled and metered flows are presented in Figures 15 to 22. No data were available for meters 12332 (relocated to 70224) and 19882. Data for sites 20206 and 20283 were suspect and therefore not used in the analysis. In general, the data for these latter sites were determined to be unreliable for the majority of the metering period. Reasonable agreement was achieved between modeled and metered flows.

Calibration to January 2-4, 2008 (Wet Antecedent Conditions)
The January 2-4 storms were preceded by 10.5 inches of rainfall during the month of December 2007 as measured at gauge TCR, creating wet antecedent conditions. Compared to the November event, there was a significant increase in seasonal infiltration and rainfall-dependent infiltration, particularly the former. The hetographs are shown in Figure 23 and hydrograph results are presented in Figures 24 to 28 for meters with available and reliable data. At gauge TCR, a total rainfall depth of 1.24 inches was measured during the period, while 1.23 inches was measured at gauge RCR. Comparing the results for meter No. 09877, infiltration during this event was over twice the amount of infiltration that occurred during the November 18-20, 2007 event.

Calibration to March 24-25, 2007 (Moist to Moderate Antecedent Conditions)
Initially, this event was run using the Defects database set up to simulate dry-to-moderate antecedent conditions. However, it was evident that a higher rate of seasonal (constant) and rainfall-dependent infiltration is present during the spring season relative to the fall season. The month of March 2007 was not particularly wet with only 1.22 inches of rainfall preceding the March 24-25, 2007 event, during which 0.74 inches of total depth was recorded at gauge TCR. Therefore, this event was considered to have moist-to-moderate antecedent conditions. Hyetographs are shown in Figure 29 and comparative graphical results are presented in Figures 30 to 35. Reasonable agreement was achieved at most of the flow meters for the initial portion of the event, except at meter 09877. Further adjustments to increase the rainfall-dependent infiltration between meters 12383 and 09877 were estimated to be unreasonable, and reliable data were not available for meter 12323 during this event.

DESIGN STORM ANALYSIS

In order to test the system under design storm conditions, the model was run using the District's 5-year 24-hour storm event using the Defects databases representing moderate and dry-to-moderate (fall season) and moderate (spring season) antecedent conditions. The model was run using a 15-minute time step for 48 hours with the SHUFFLE function turned on.

Under the dry-to-moderate antecedent condition assumption, the collection system conveyed the design storm almost entirely within the crown of the pipe network. Minor surcharging occurred between manholes 12386 and 20696. During the design storm under moist-to-moderate antecedent conditions, surcharging occurred between manholes 12388 and 20696.

Given the significant amount of infiltration remaining in the system, it is recommended that CWS continue the rehabilitation work on manholes and services laterals within the HEI collection system.

FIGURES

Figure 1. 2007 Flow Monitor Locations in Vicinity of the Hillsboro East Interceptor
Figure 2. 2007 Dry Season Flow Comparison - 20276 - Rock Creek - HEI
Figure 3. 2007 Dry Season Flow Comparison - 20283 - Rock Creek - HEI
Figure 4. 2007 Dry Season Flow Comparison - 20238 - Rock Creek - HEI
Figure 5. 2007 Dry Season Flow Comparison - 12424 - Rock Creek - HEI
Figure 6. 2007 Dry Season Flow Comparison - 20206 - Rock Creek - HEI
Figure 7. 2007 Dry Season Flow Comparison - 12383 - Rock Creek - HEI
Figure 8. 2007 Dry Season Flow Comparison - 12332 - Rock Creek - HEI
Figure 9. 2007 Dry Season Flow Comparison - 70224 - Rock Creek - HEI
Figure 10. 2007 Dry Season Flow Comparison - 12323 - Rock Creek - HEI
Figure 11. 2007 Dry Season Flow Comparison - 19882 - Rock Creek - HEI
Figure 12. 2007 Dry Season Flow Comparison - 09877 - Rock Creek - HEI
Figure 13. 2007 Dry Season Flow Comparison - 12315 - Rock Creek - HEI
Figure 14. Rain Gauge Data for November 18-20, 2007 Storms
Figure 15. Metered vs. Modeled Flow - Rock Creek Meter 20276 - November 18-20, 2007
Figure 16. Metered vs. Modeled Flow - Rock Creek Meter 20238 - November 18-20, 2007
Figure 17. Metered vs. Modeled Flow - Rock Creek Meter 12424 - November 18-20, 2007
Figure 18. Metered vs. Modeled Flow - Rock Creek Meter 12383 - November 18-20, 2007
Figure 19. Metered vs. Modeled Flow - Rock Creek Meter 70224 - November 18-20, 2007
Figure 20. Metered vs. Modeled Flow - Rock Creek Meter 12323 - November 18-20, 2007
Figure 21. Metered vs. Modeled Flow - Rock Creek Meter 09877 - November 18-20, 2007
Figure 22. Metered vs. Modeled Flow - Rock Creek Meter 12315 - November 18-20, 2007
Figure 23. Rain Gauge Data for January 2-4, 2008 Storms
Figure 24. Metered vs. Modeled Flow - Rock Creek Meter 20276 - January 2-4, 2008
Figure 25. Metered vs. Modeled Flow - Rock Creek Meter 20238 - January 2-4, 2008
Figure 26. Metered vs. Modeled Flow - Rock Creek Meter 70224 - January 2-4, 2008
Figure 27. Metered vs. Modeled Flow - Rock Creek Meter 12323 - January 2-4, 2008
Figure 28. Metered vs. Modeled Flow - Rock Creek Meter 09877 - January 2-4, 2008
Figure 29. Rain Gauge Data for March 24-25, 2008 Storm
Figure 30. Metered vs. Modeled Flow - Rock Creek Meter 20276 - March 24-25, 2007
Figure 31. Metered vs. Modeled Flow - Rock Creek Meter 20238 - March 24-25, 2007
Figure 32. Metered vs. Modeled Flow - Rock Creek Meter 12424 - March 24-25, 2007
Figure 33. Metered vs. Modeled Flow - Rock Creek Meter 12383 - March 24-25, 2007
Figure 34. Metered vs. Modeled Flow - Rock Creek Meter 19882 - March 24-25, 2007
Figure 35. Metered vs. Modeled Flow - Rock Creek Meter 09876 - March 24-25, 2007

Figure 1. 2007 Flow Monitor Locations in Vicinity of the Hillsboro East Interceptor

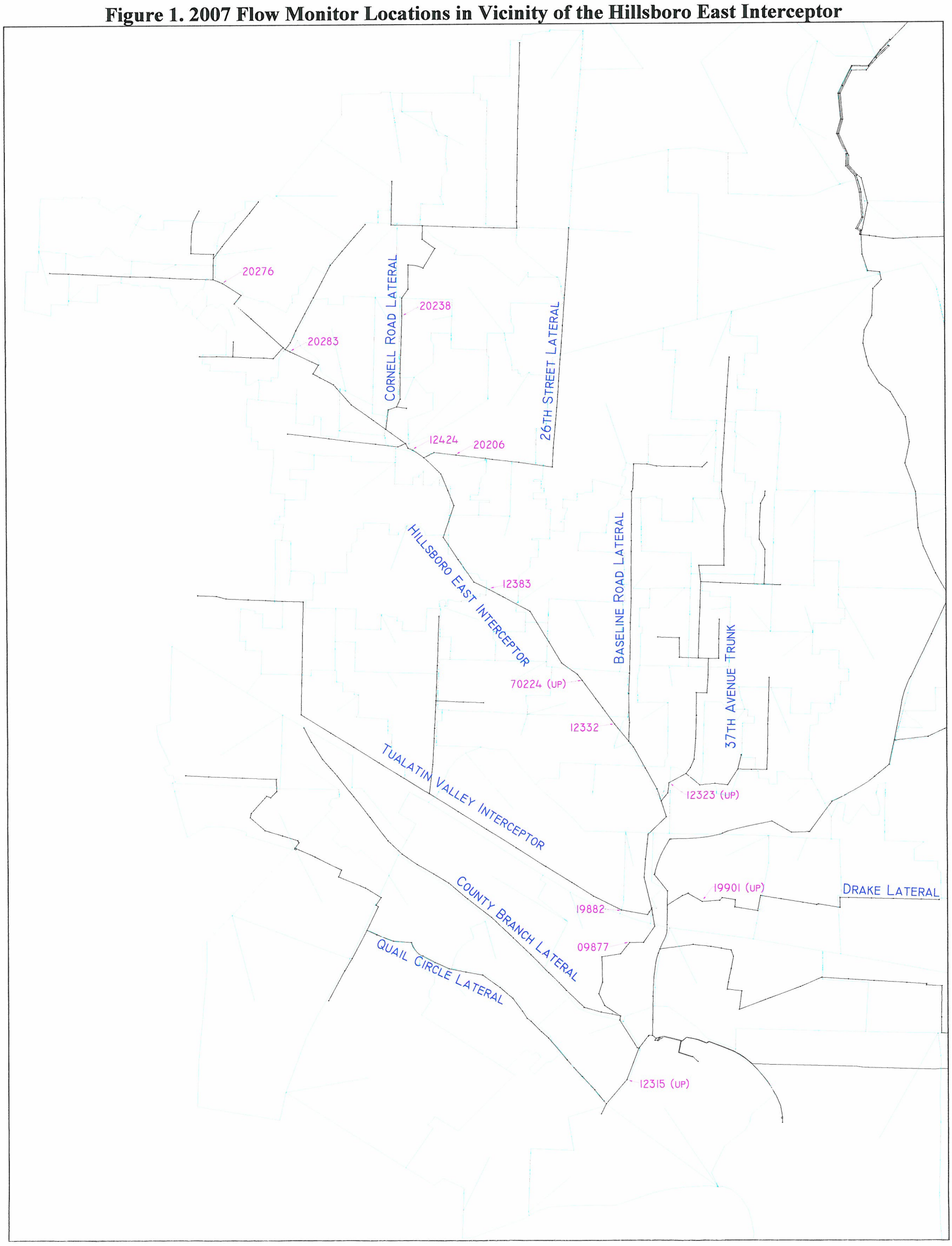


Figure 2

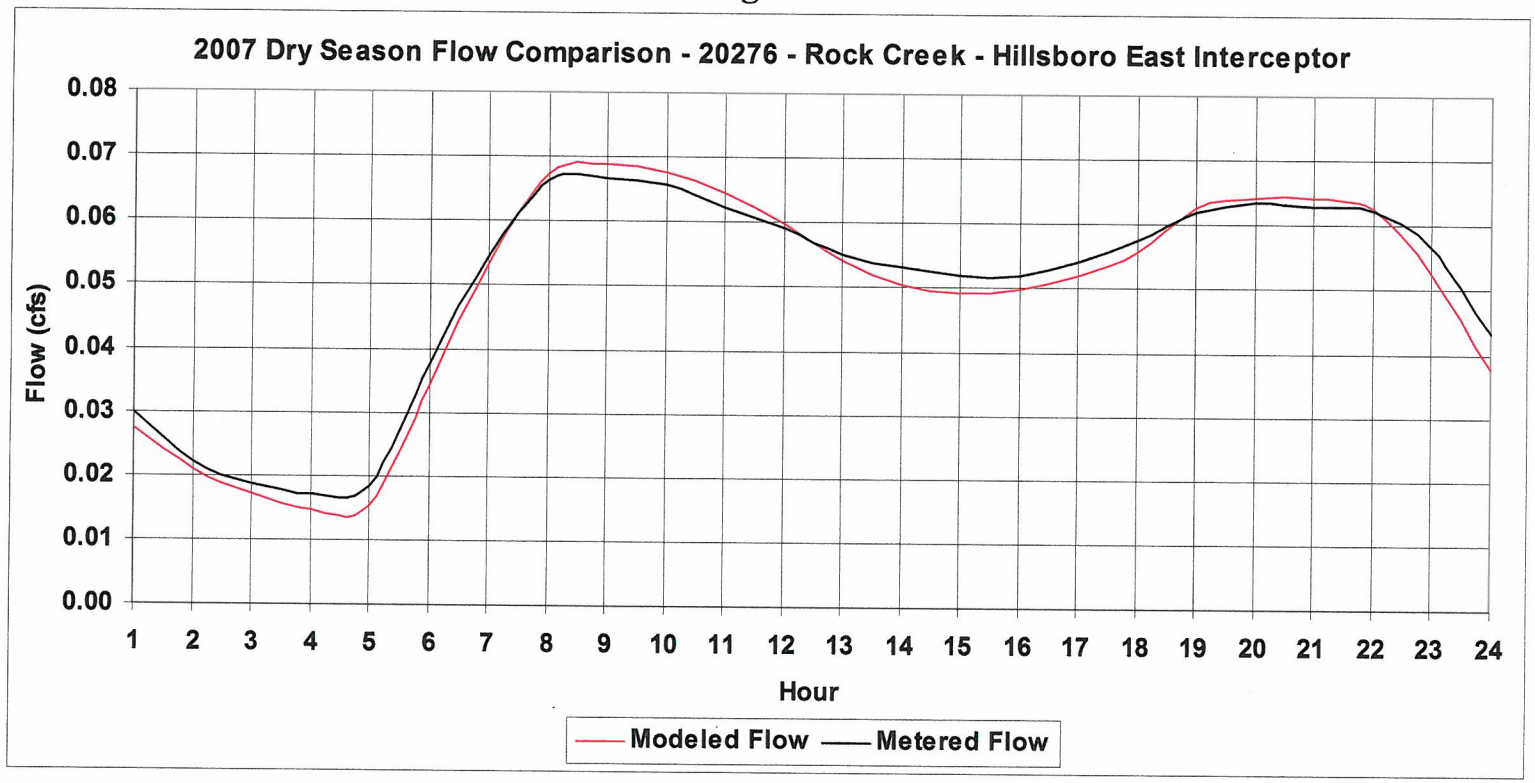

2007 Dry Season Flow Comparison - 20276 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0.00
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 3

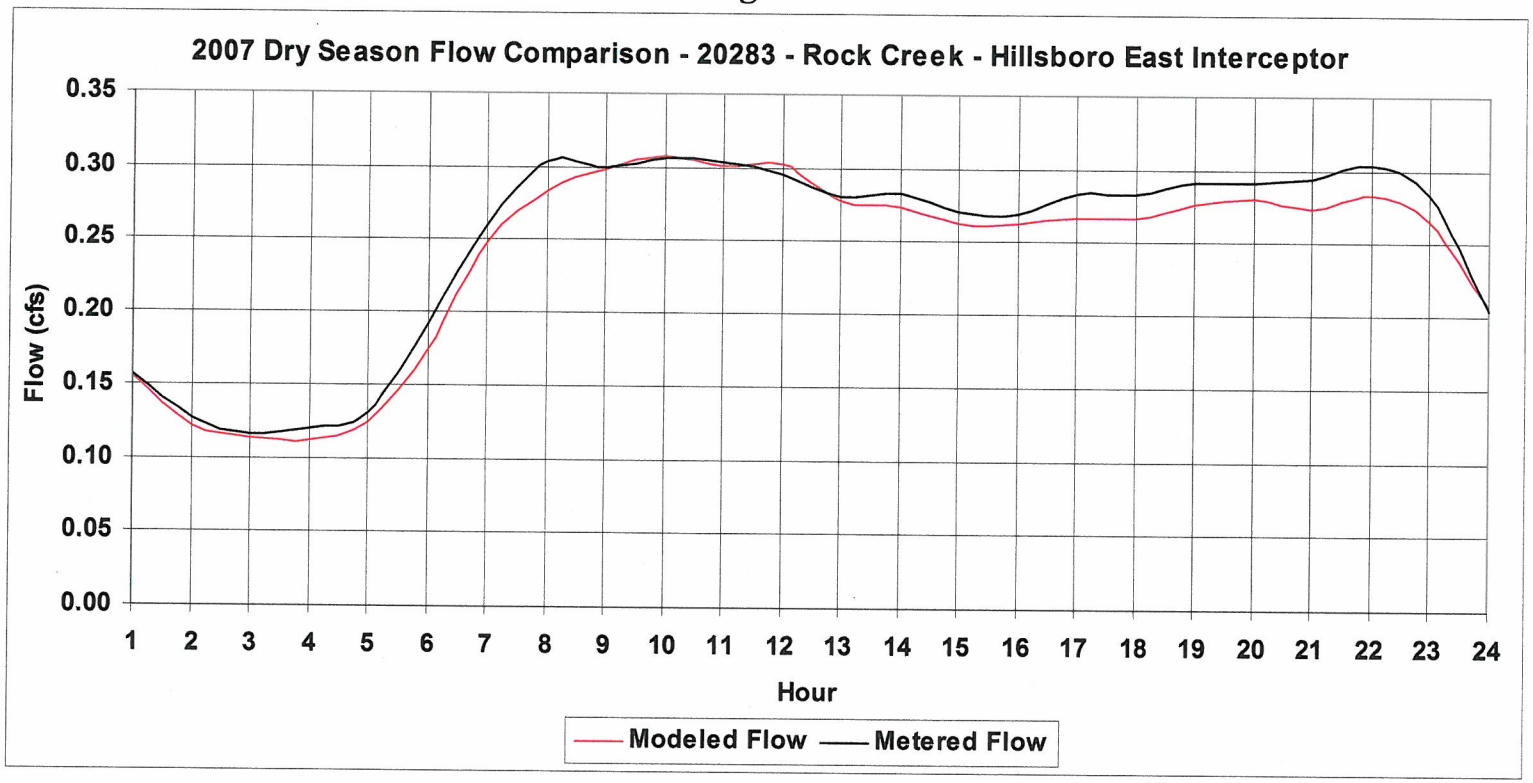

2007 Dry Season Flow Comparison - 20283 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 4

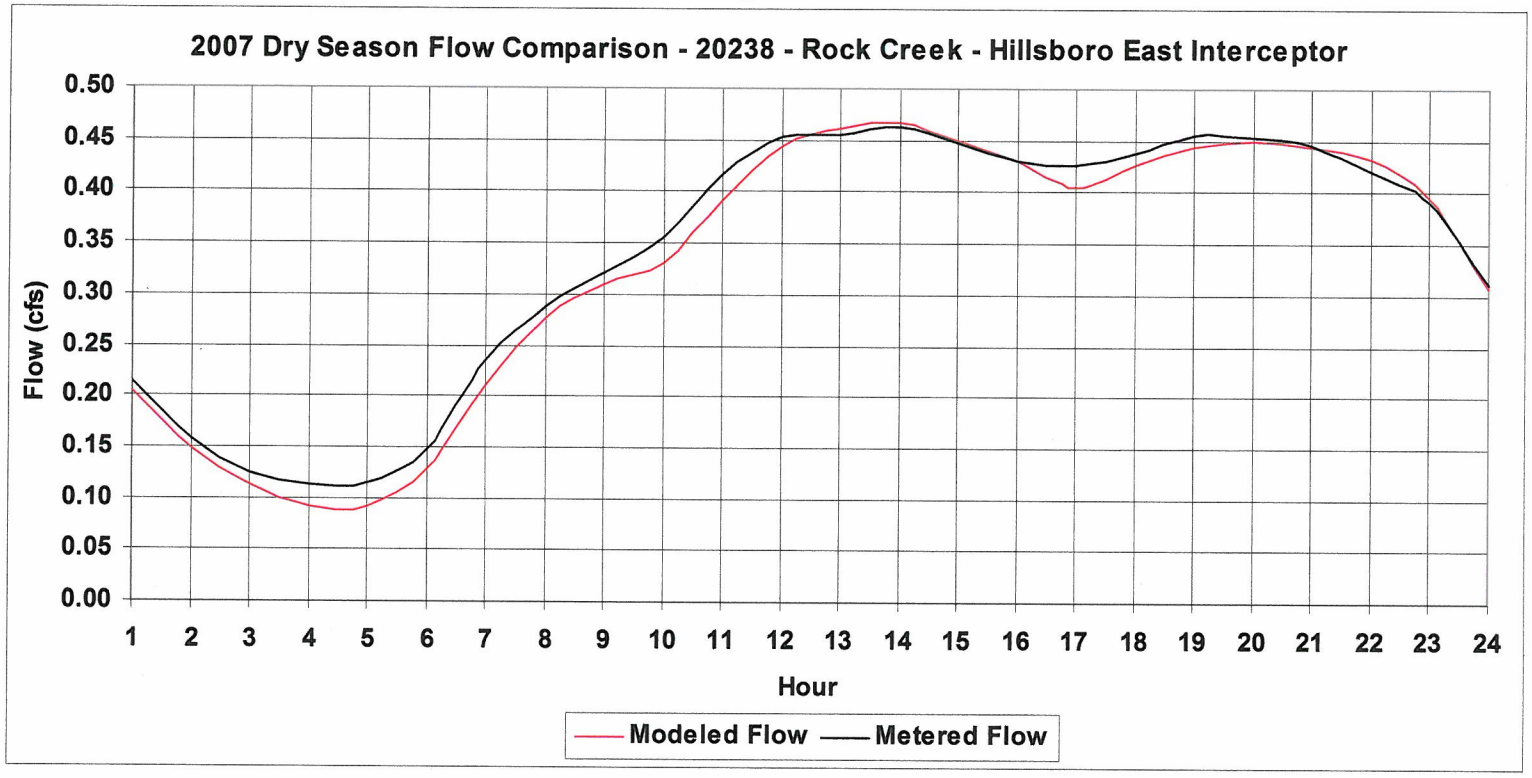

2007 Dry Season Flow Comparison - 20238 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
0.50
0.45
0.40
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 5

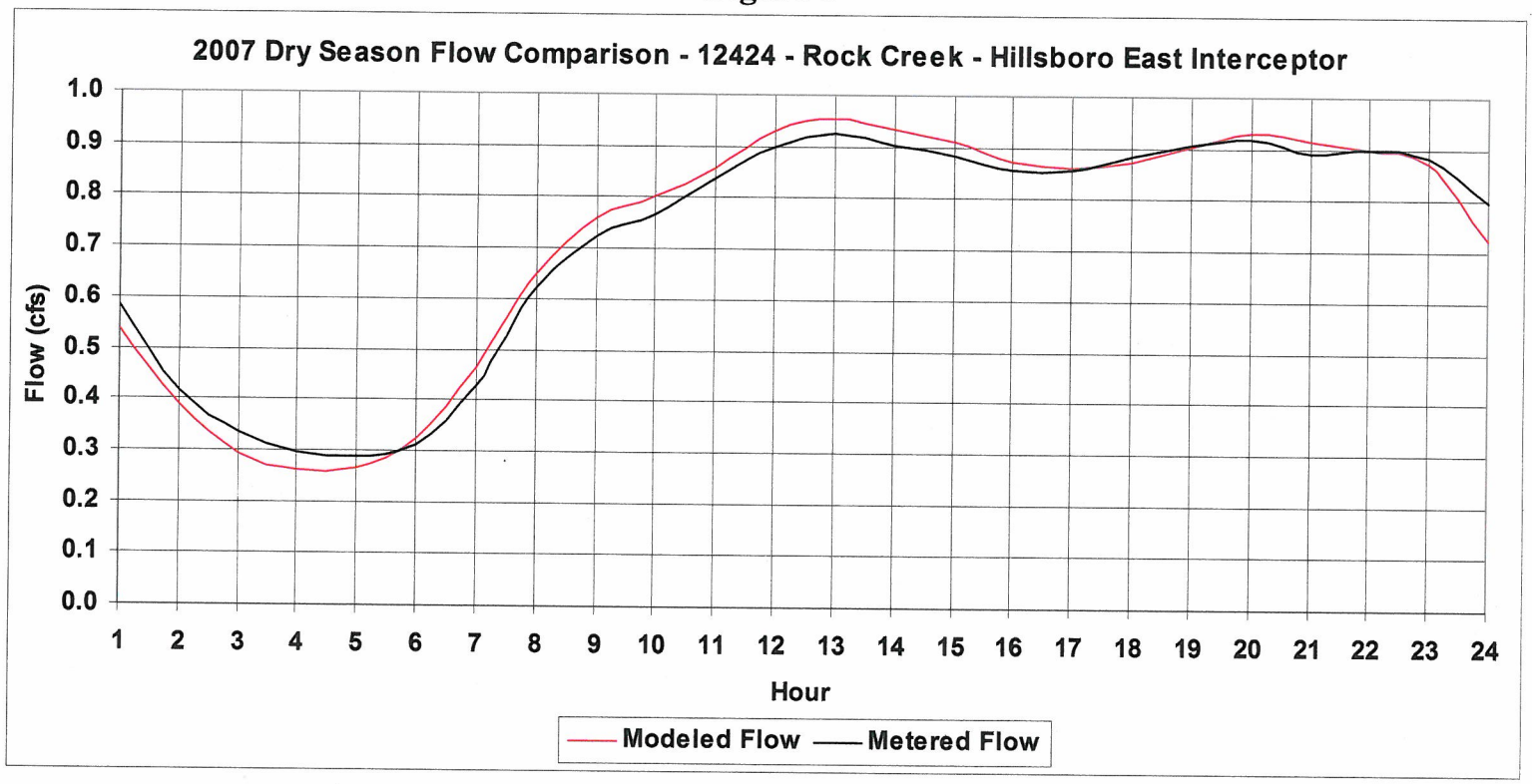

2007 Dry Season Flow Comparison - 12424 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 6

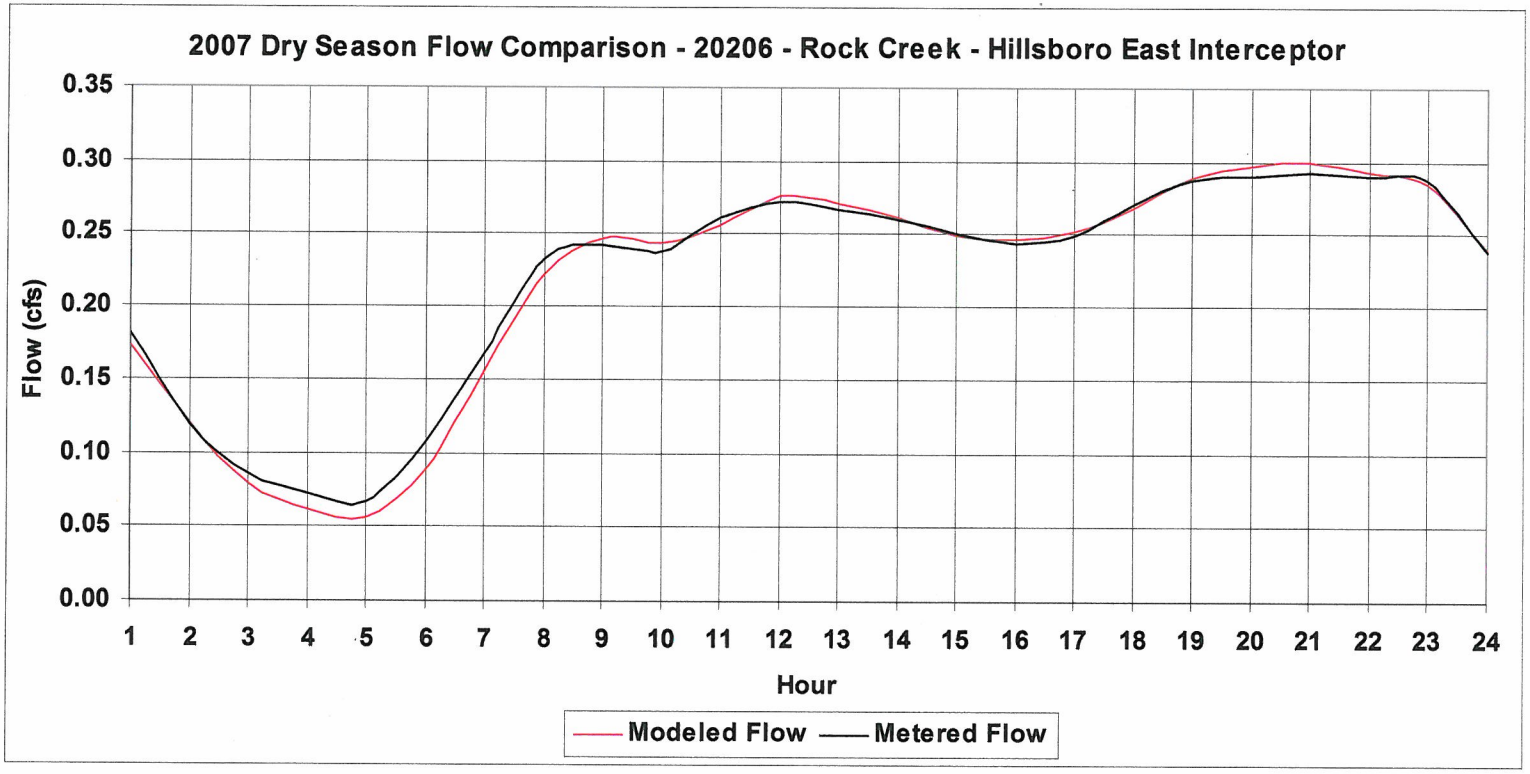

2007 Dry Season Flow Comparison - 20206 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 7

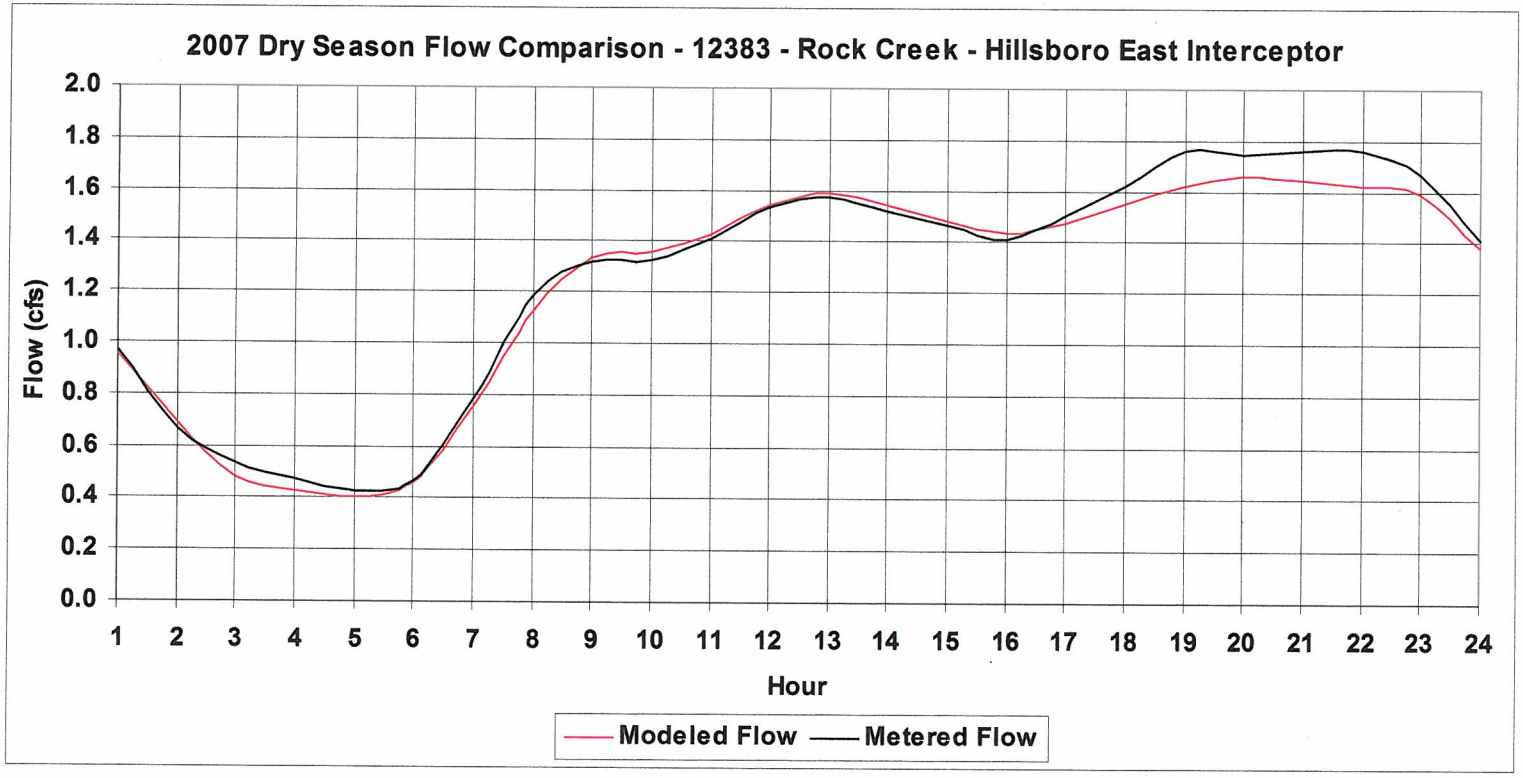

2007 Dry Season Flow Comparison - 12383 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
2.0
1.8
1.6
1.4
1.2
1.0
0.8
0.6
0.4
0.2
0.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 8

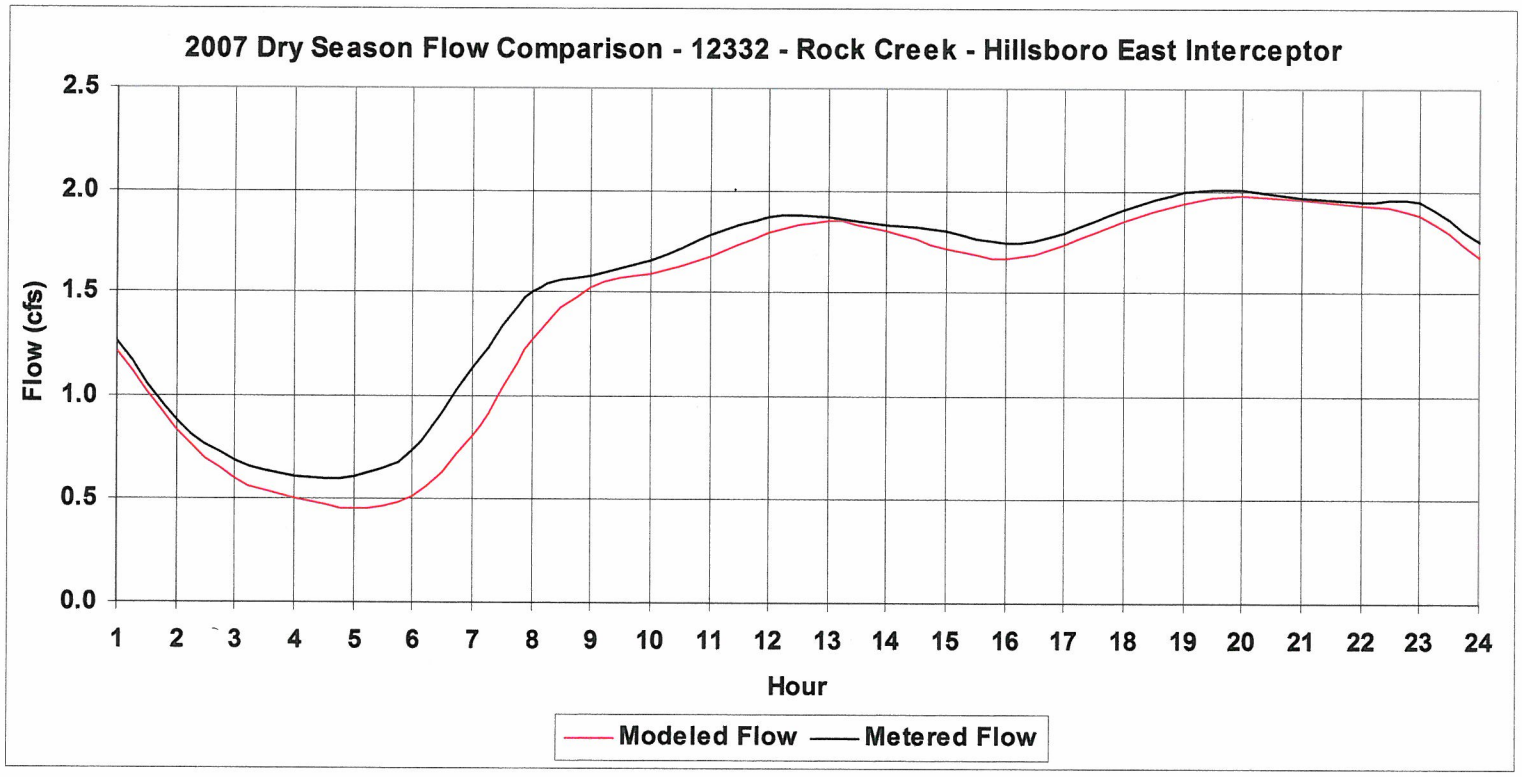

2007 Dry Season Flow Comparison - 12332 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
2.5
2.0
1.5
1.0
0.5
0.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 9

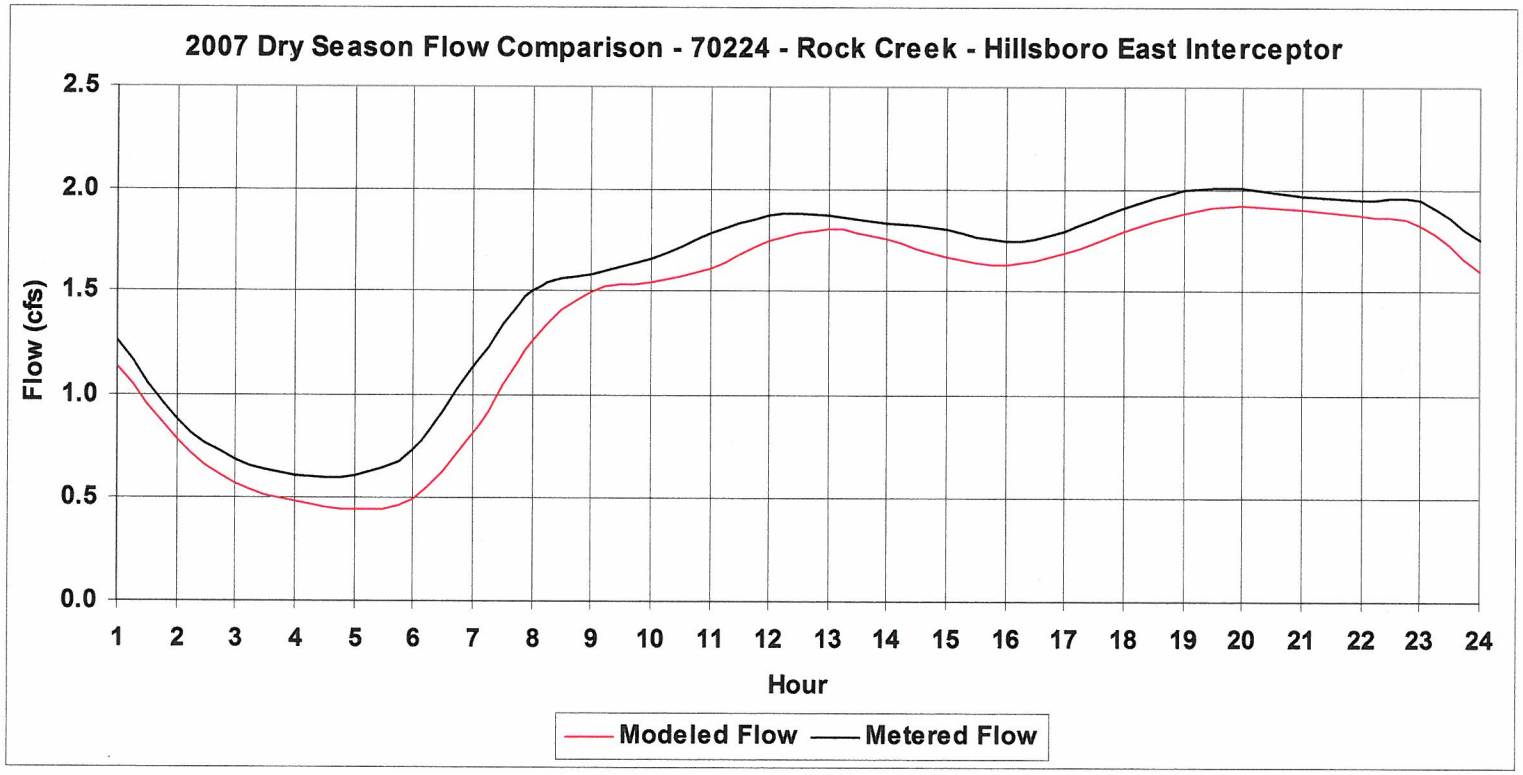

2007 Dry Season Flow Comparison - 70224 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
2.5
2.0
1.5
1.0
0.5
0.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 10

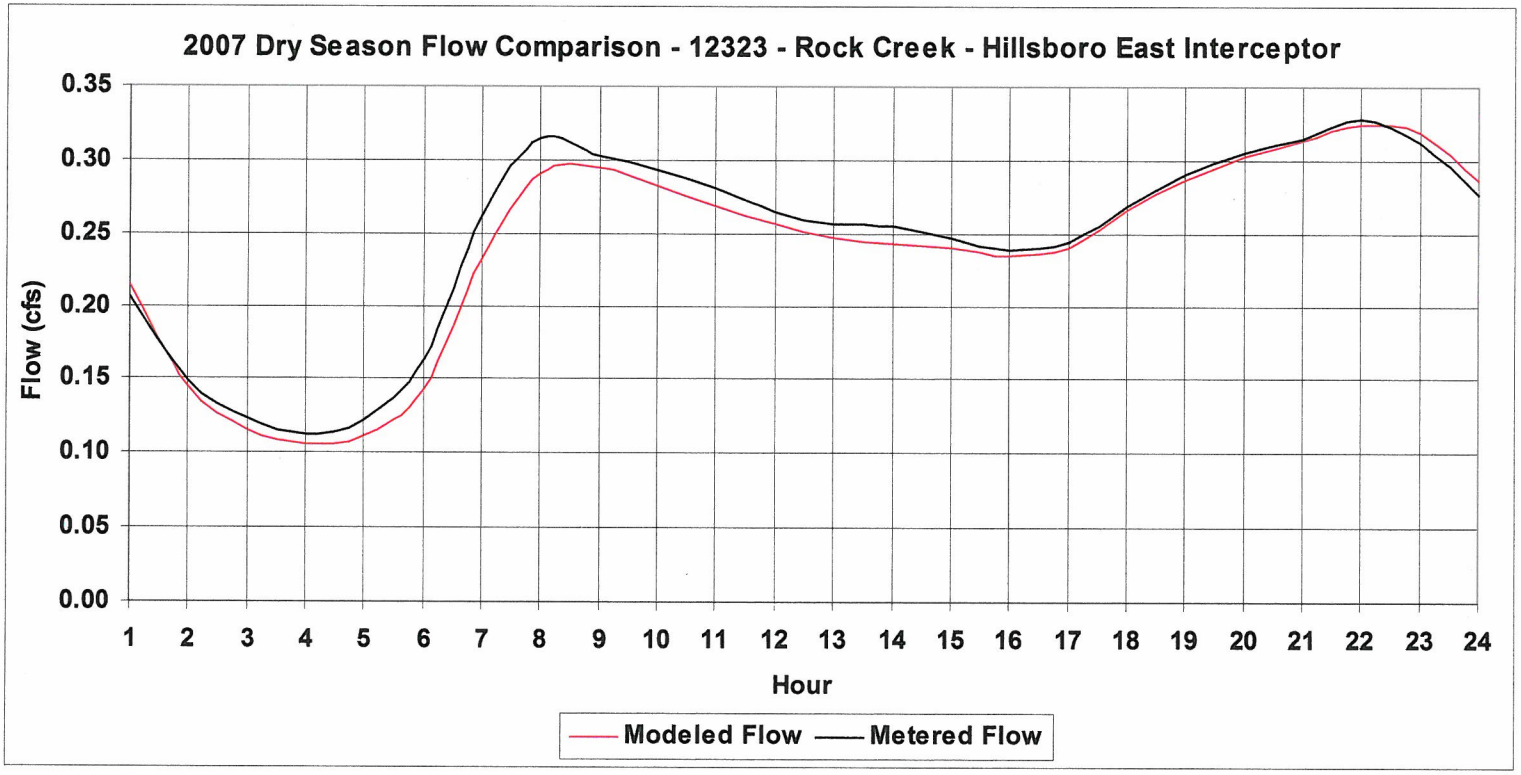

2007 Dry Season Flow Comparison - 12323 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 11

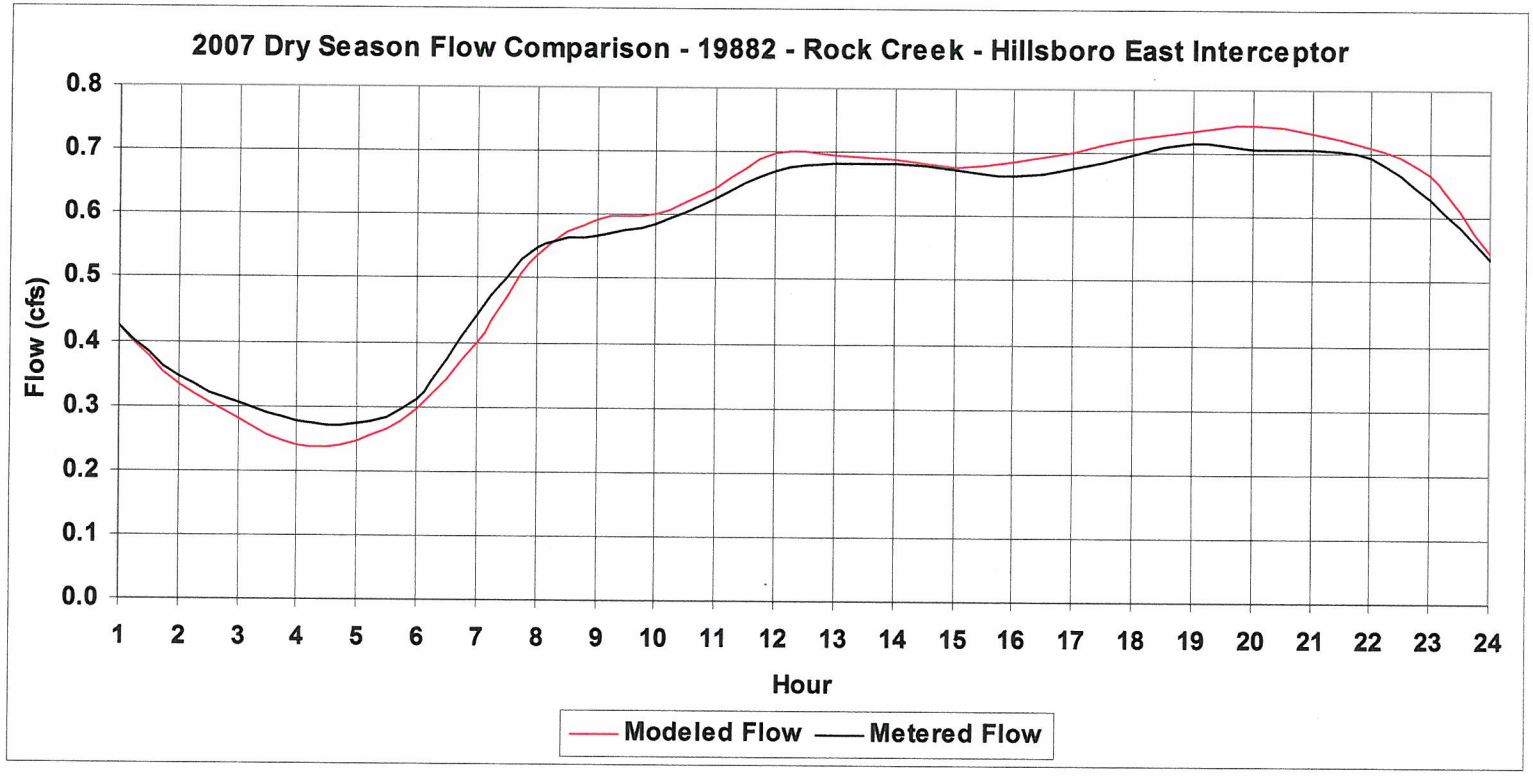

2007 Dry Season Flow Comparison - 19882 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 12

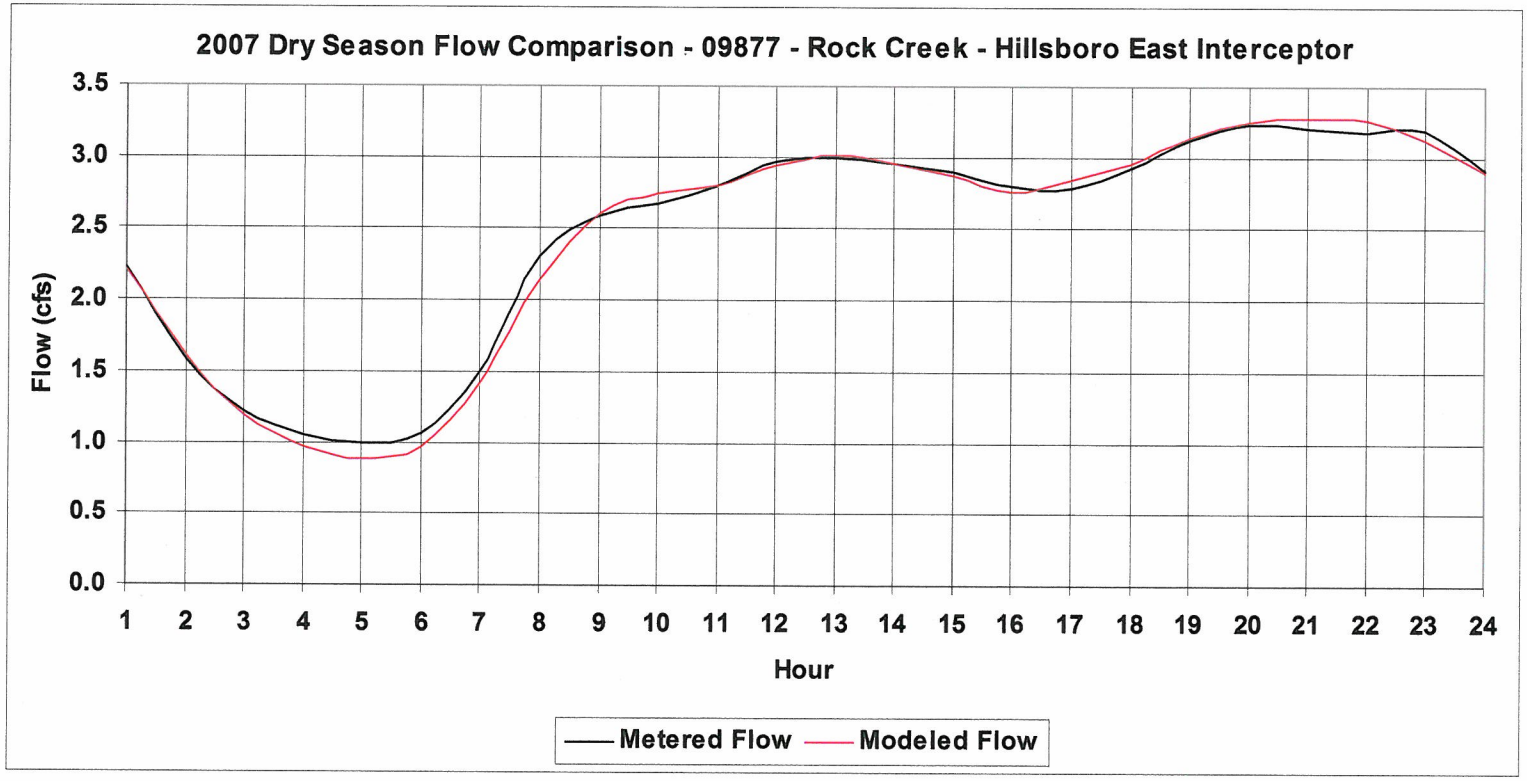

2007 Dry Season Flow Comparison - 09877 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
3.5
3.0
2.5
2.0
1.5
1.0
0.5
0.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Metered Flow
Modeled Flow

Figure 13

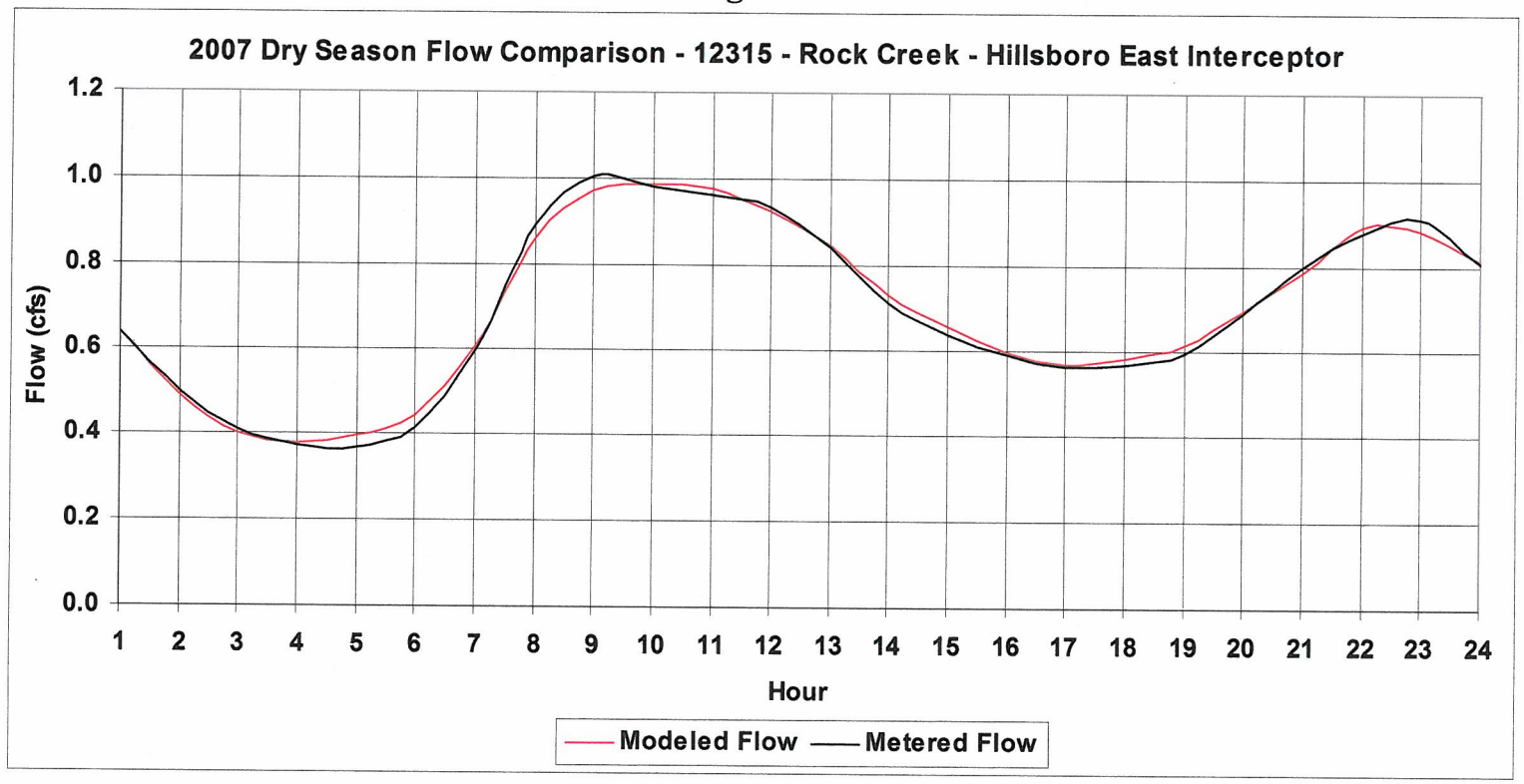

2007 Dry Season Flow Comparison - 12315 - Rock Creek - Hillsboro East Interceptor
Flow (cfs)
1.2
1.0
0.8
0.6
0.4
0.2
0.0
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
Hour
Modeled Flow
Metered Flow

Figure 14

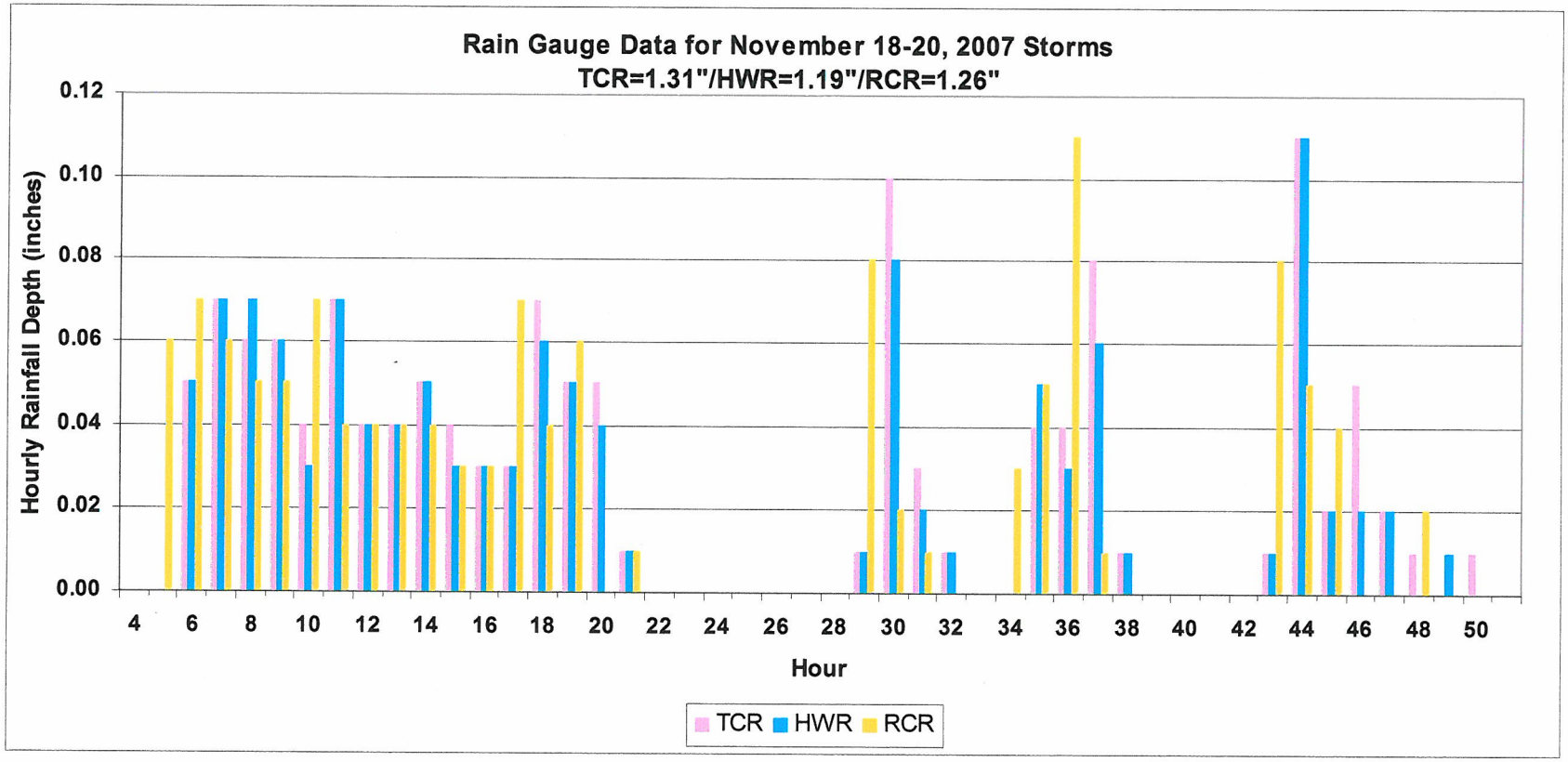

Rain Gauge Data for November 18-20, 2007 Storms
TCR=1.31"/HWR=1.19"/RCR=1.26"
Hourly Rainfall Depth (inches)
0.12
0.10
0.08
0.06
0.04
0.02
0.00
4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50
Hour
TCR
HWR
RCR

Figure 15

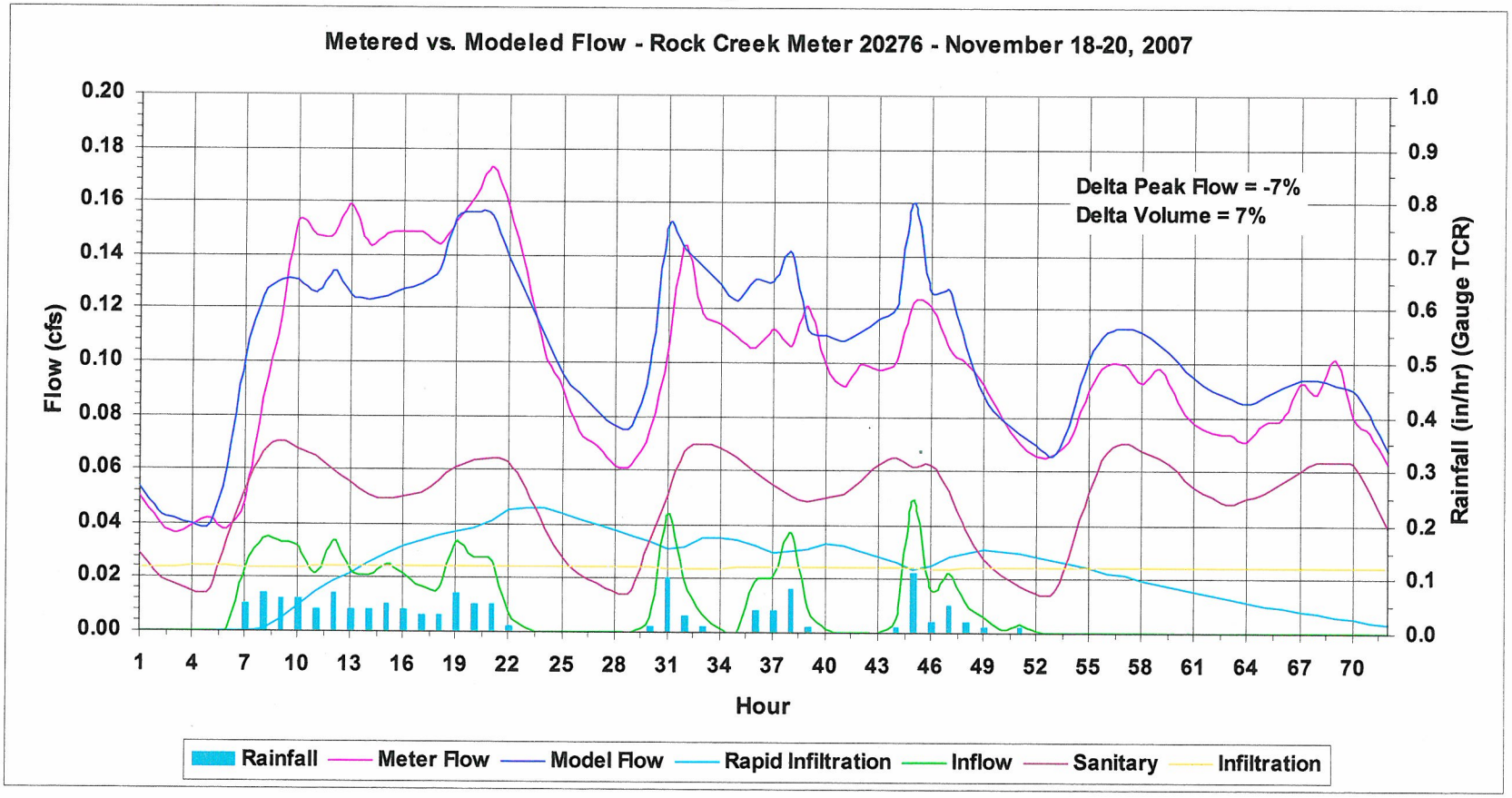

Metered vs. Modeled Flow - Rock Creek Meter 20276 - November 18-20, 2007
Delta Peak Flow = -7%
Delta Volume = 7%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
0.20
0.18
0.16
0.14
0.12
0.10
0.08
0.06
0.04
0.02
0.00
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 16

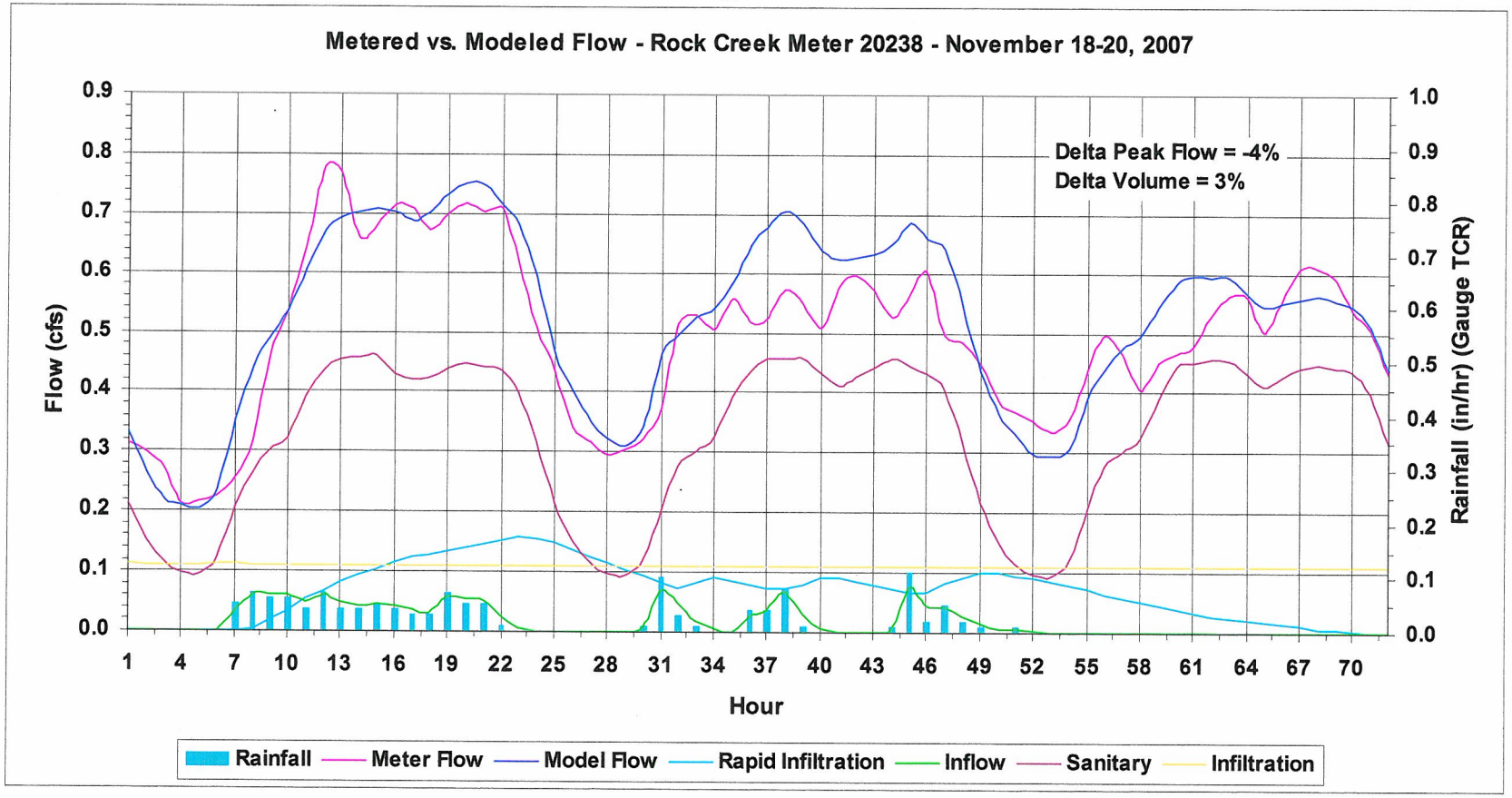

Metered vs. Modeled Flow - Rock Creek Meter 20238 - November 18-20, 2007
Delta Peak Flow = -4%
Delta Volume = 3%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
0.0
0.1
0.2
0.3
0.4
0.5
0.6
0.7
0.8
0.9
1.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 17

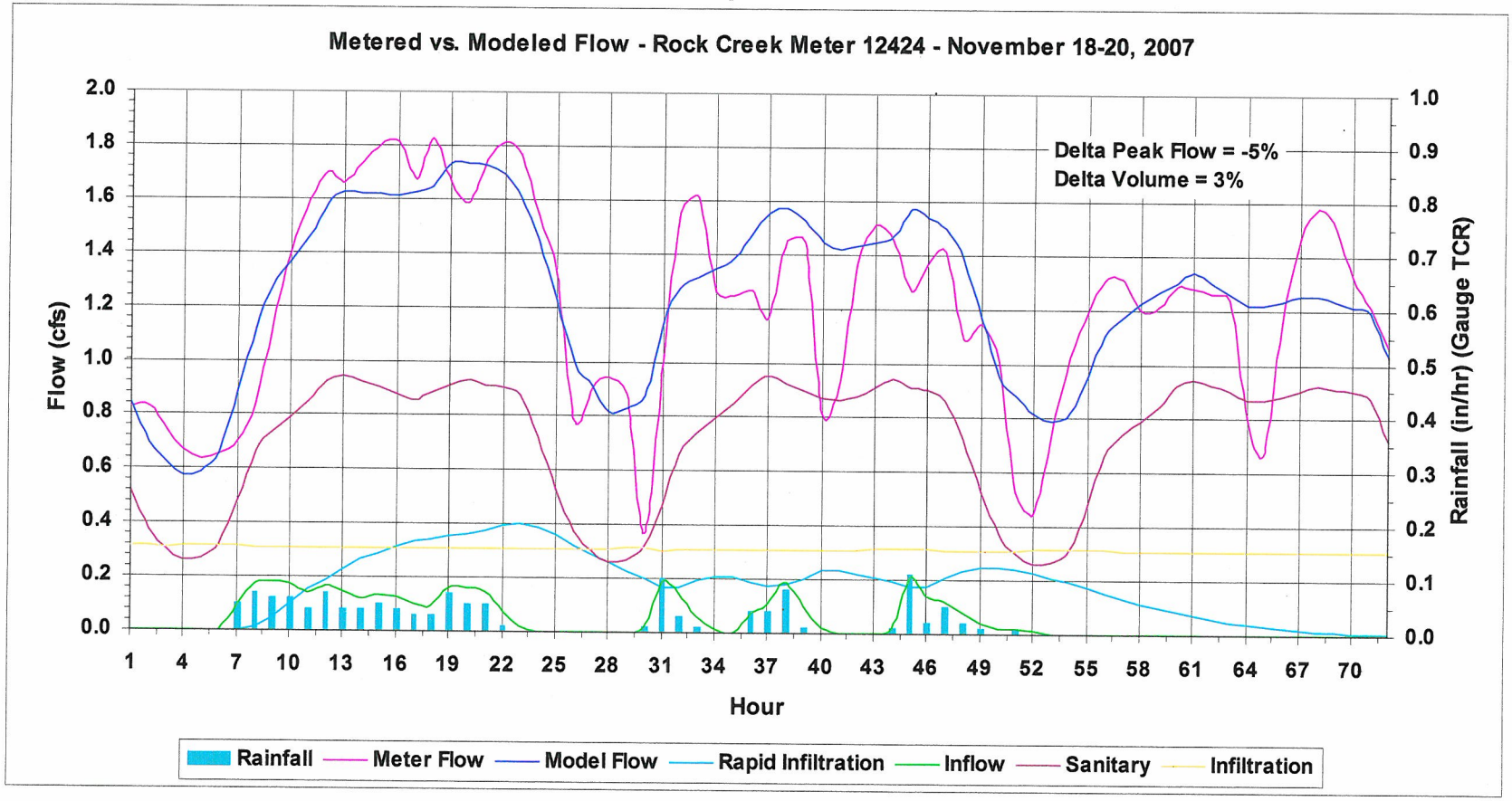

Metered vs. Modeled Flow - Rock Creek Meter 12424 - November 18-20, 2007
Delta Peak Flow = -5%
Delta Volume = 3%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 18

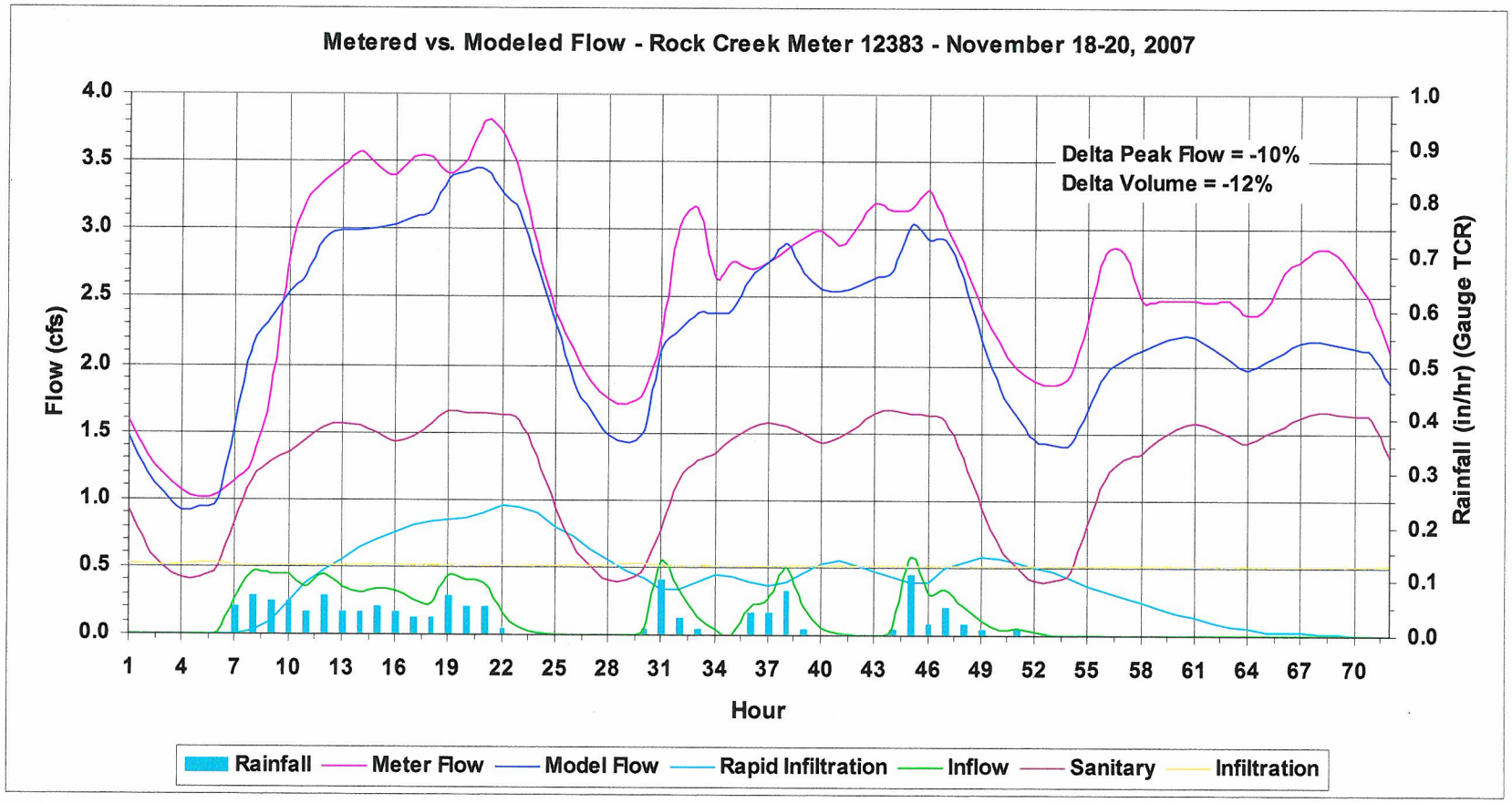

Metered vs. Modeled Flow - Rock Creek Meter 12383 - November 18-20, 2007
Delta Peak Flow = -10%
Delta Volume = -12%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 19

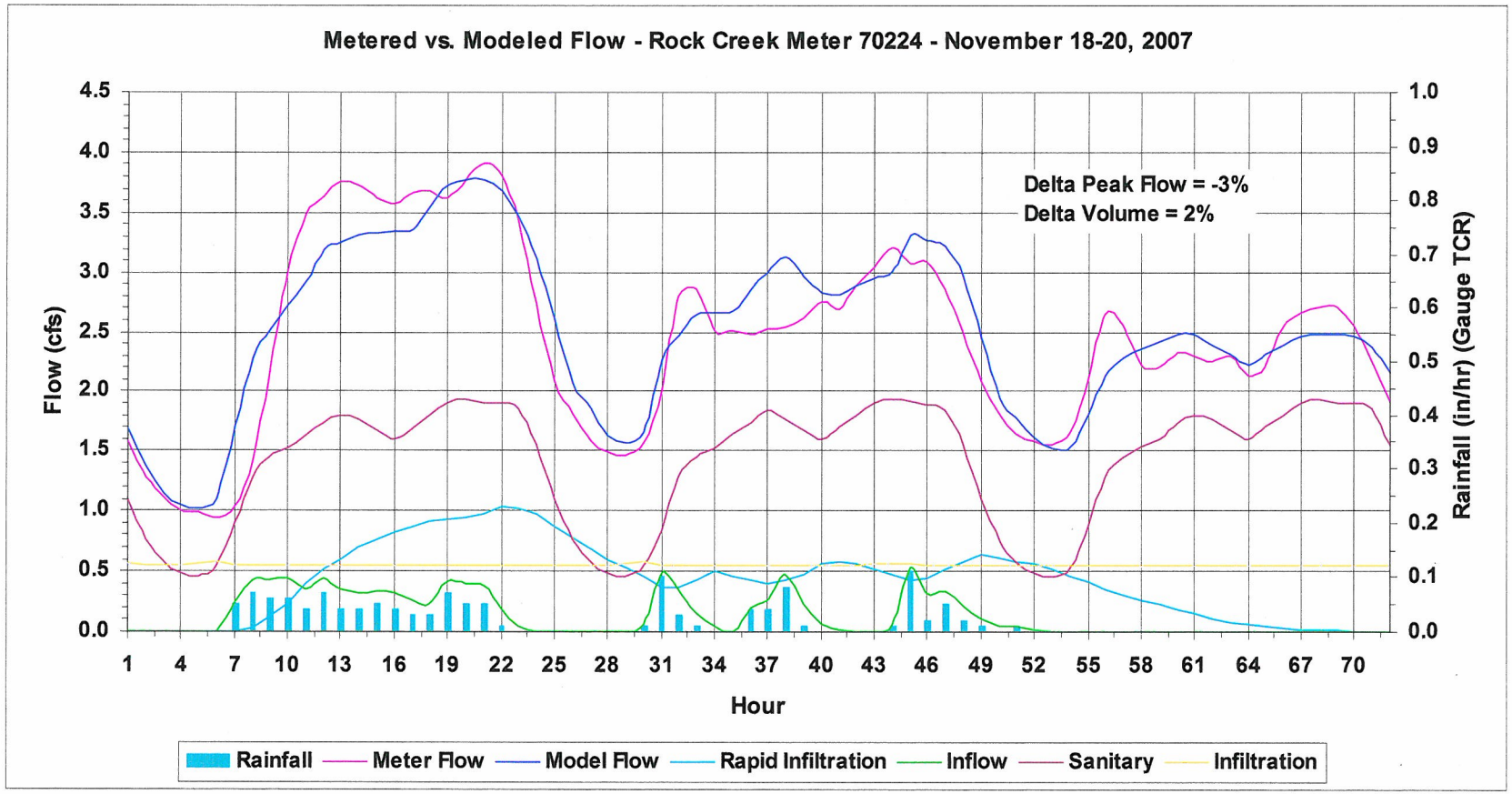

Metered vs. Modeled Flow - Rock Creek Meter 70224 - November 18-20, 2007
Delta Peak Flow = -3%
Delta Volume = 2%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
4.5
4.0
3.5
3.0
2.5
2.0
1.5
1.0
0.5
0.0
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 20

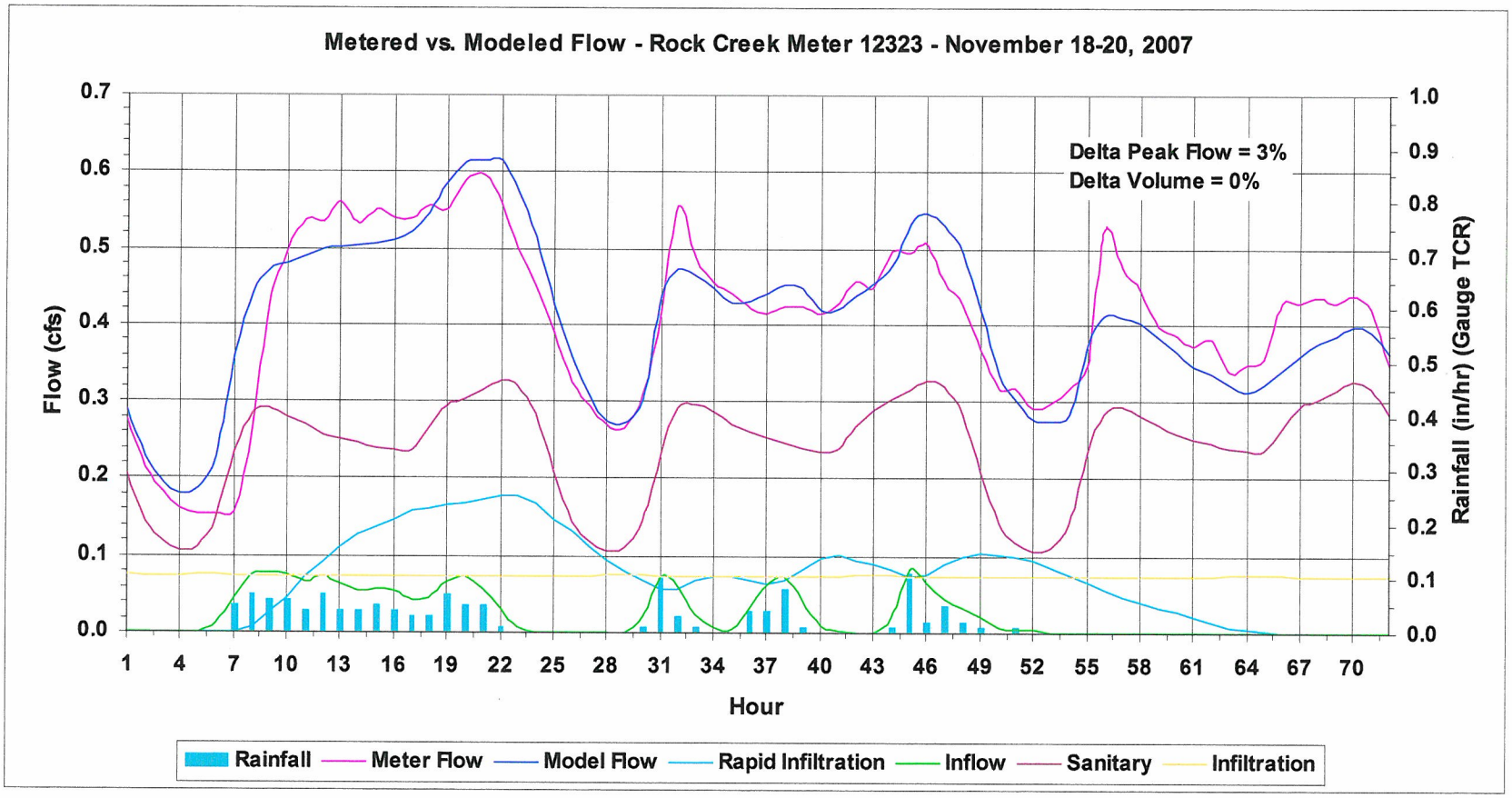

Metered vs. Modeled Flow - Rock Creek Meter 12323 - November 18-20, 2007
Delta Peak Flow = 3%
Delta Volume = 0%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
0.0
0.1
0.2
0.3
0.4
0.5
0.6
0.7
0.8
0.9
1.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 21

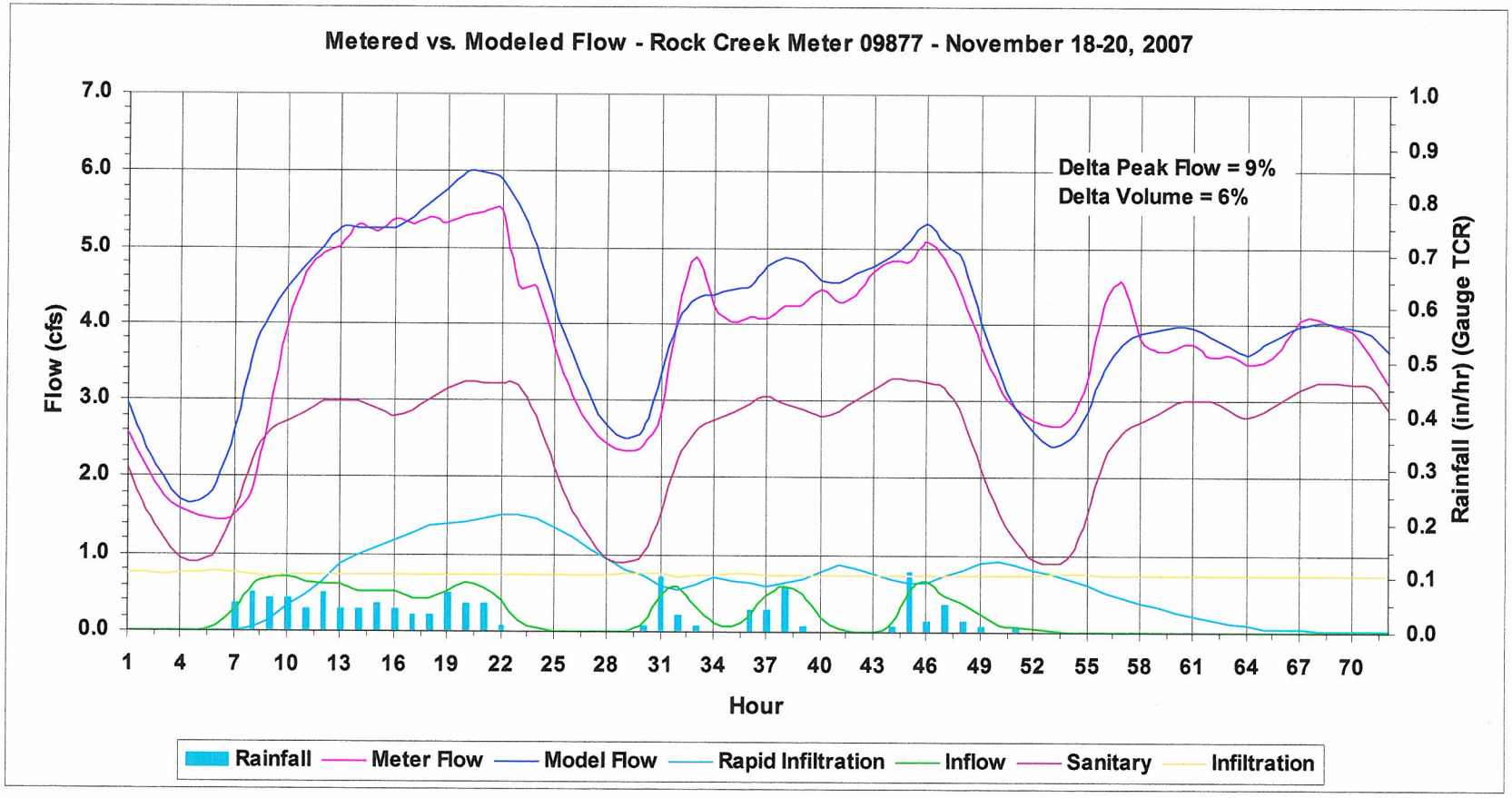

Metered vs. Modeled Flow - Rock Creek Meter 09877 - November 18-20, 2007
Delta Peak Flow = 9%
Delta Volume = 6%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
7.0
6.0
5.0
4.0
3.0
2.0
1.0
0.0
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 22

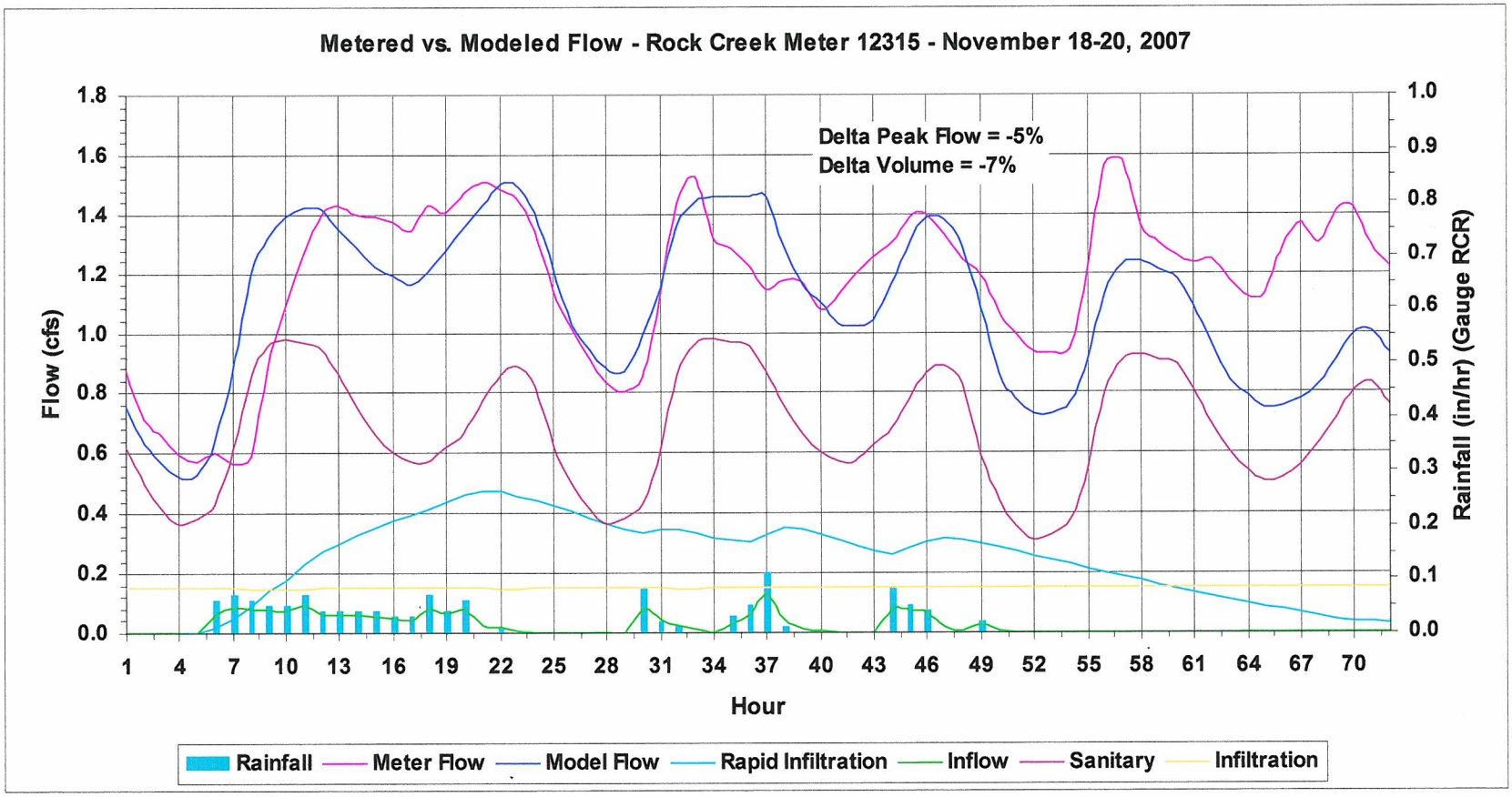

Metered vs. Modeled Flow - Rock Creek Meter 12315 - November 18-20, 2007
Delta Peak Flow = -5%
Delta Volume = -7%
Flow (cfs)
Rainfall (in/hr) (Gauge RCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 23

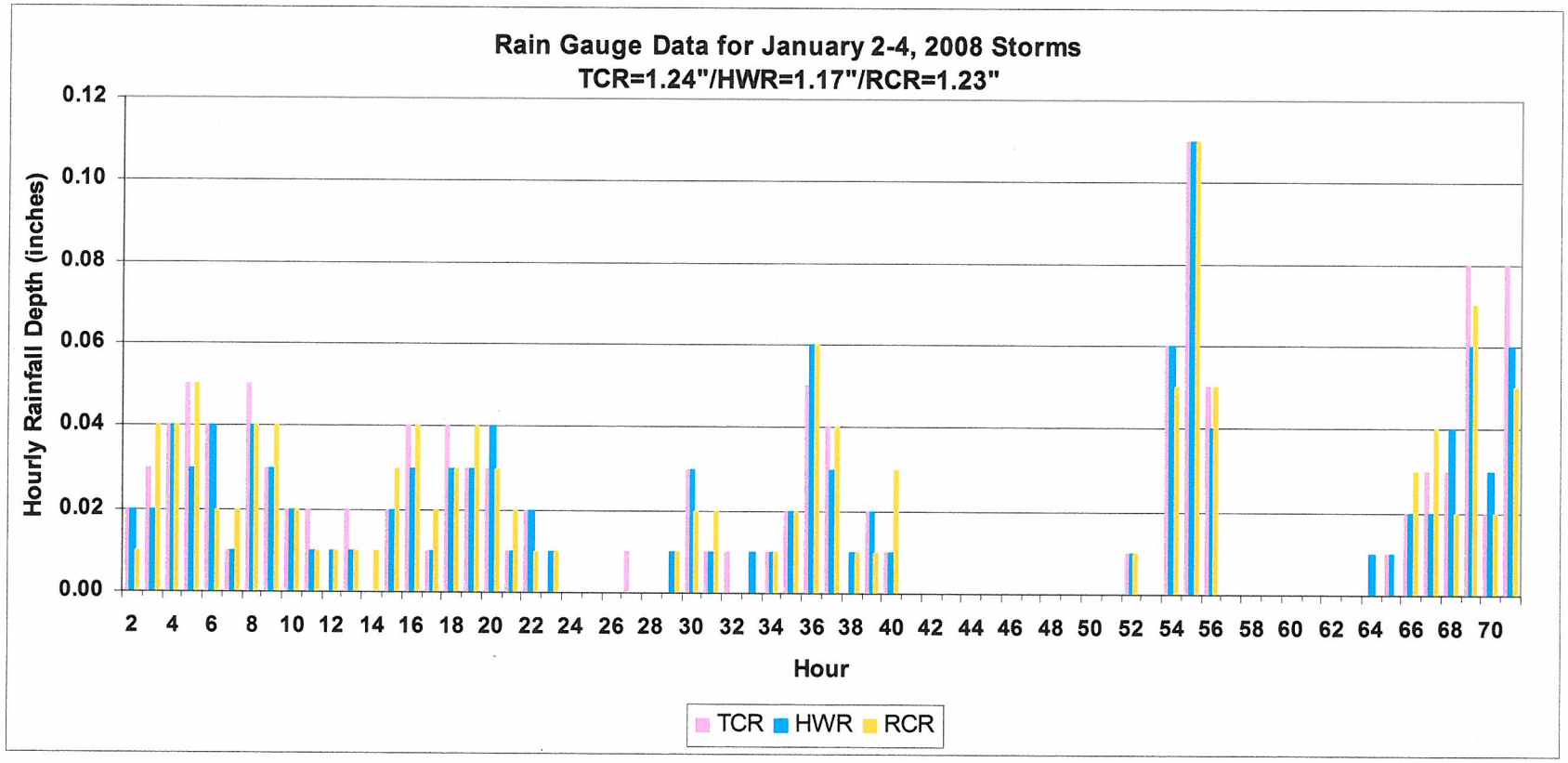

Rain Gauge Data for January 2-4, 2008 Storms
TCR=1.24"/HWR=1.17"/RCR=1.23"
Hourly Rainfall Depth (inches)
0.12
0.10
0.08
0.06
0.04
0.02
0.00
2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70
Hour
TCR
HWR
RCR

Figure 24

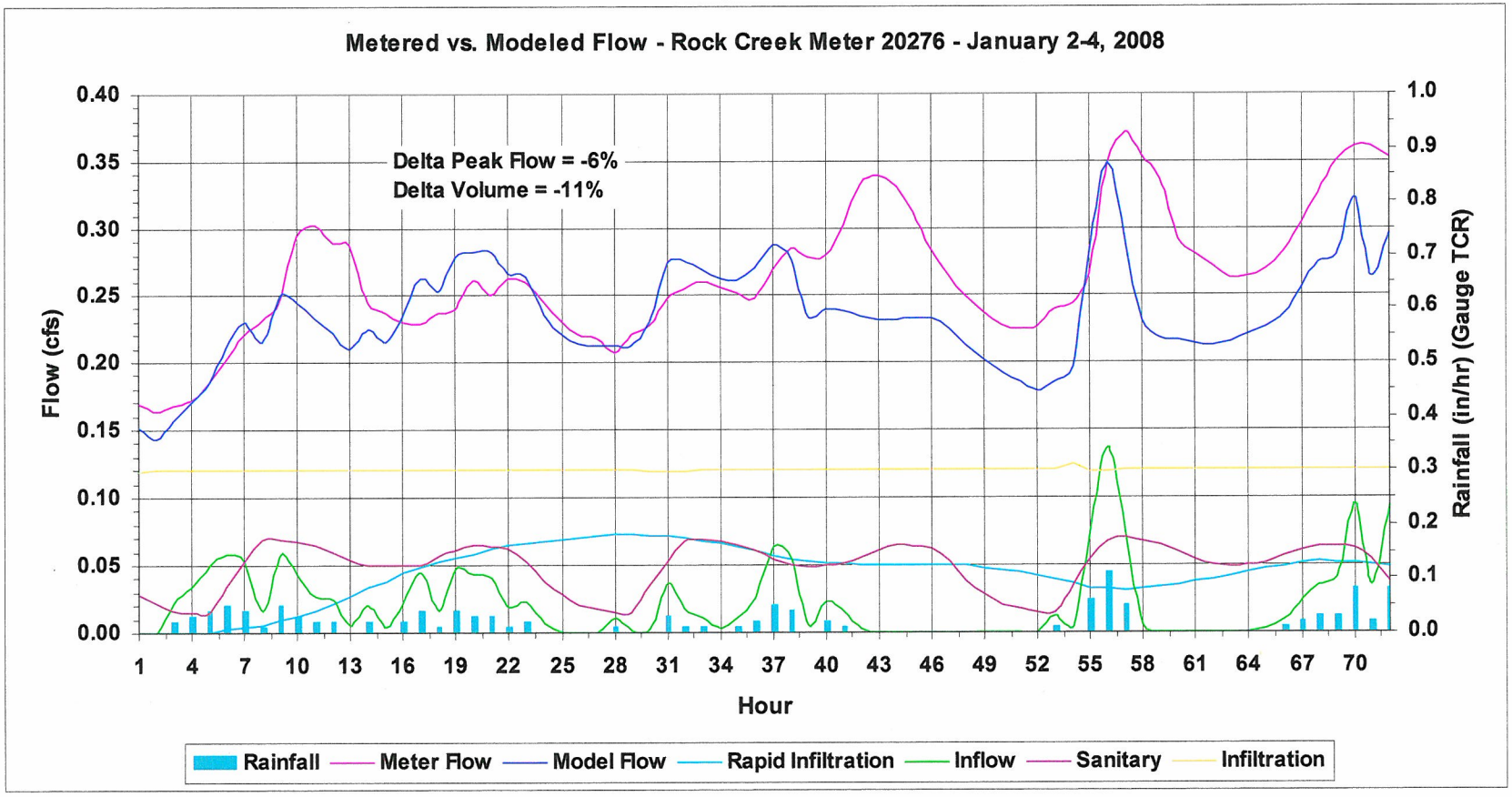

Metered vs. Modeled Flow - Rock Creek Meter 20276 - January 2-4, 2008
Delta Peak Flow = -6%
Delta Volume = -11%
Flow (cfs)
0.40
0.35
0.30
0.25
0.20
0.15
0.10
0.05
0.00
Rainfall (in/hr) (Gauge TCR)
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 25

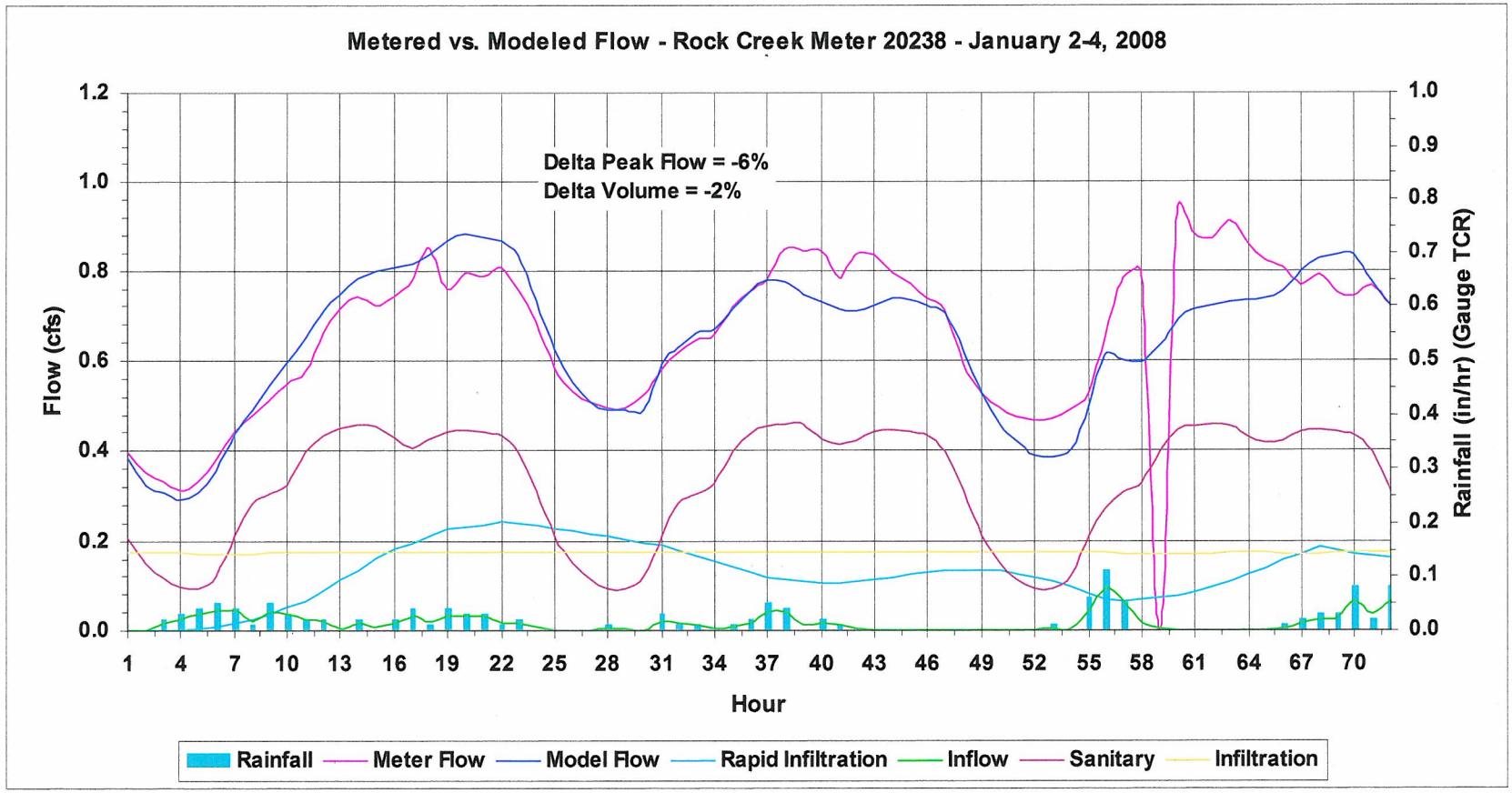

Metered vs. Modeled Flow - Rock Creek Meter 20238 - January 2-4, 2008
Delta Peak Flow = -6%
Delta Volume = -2%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 26

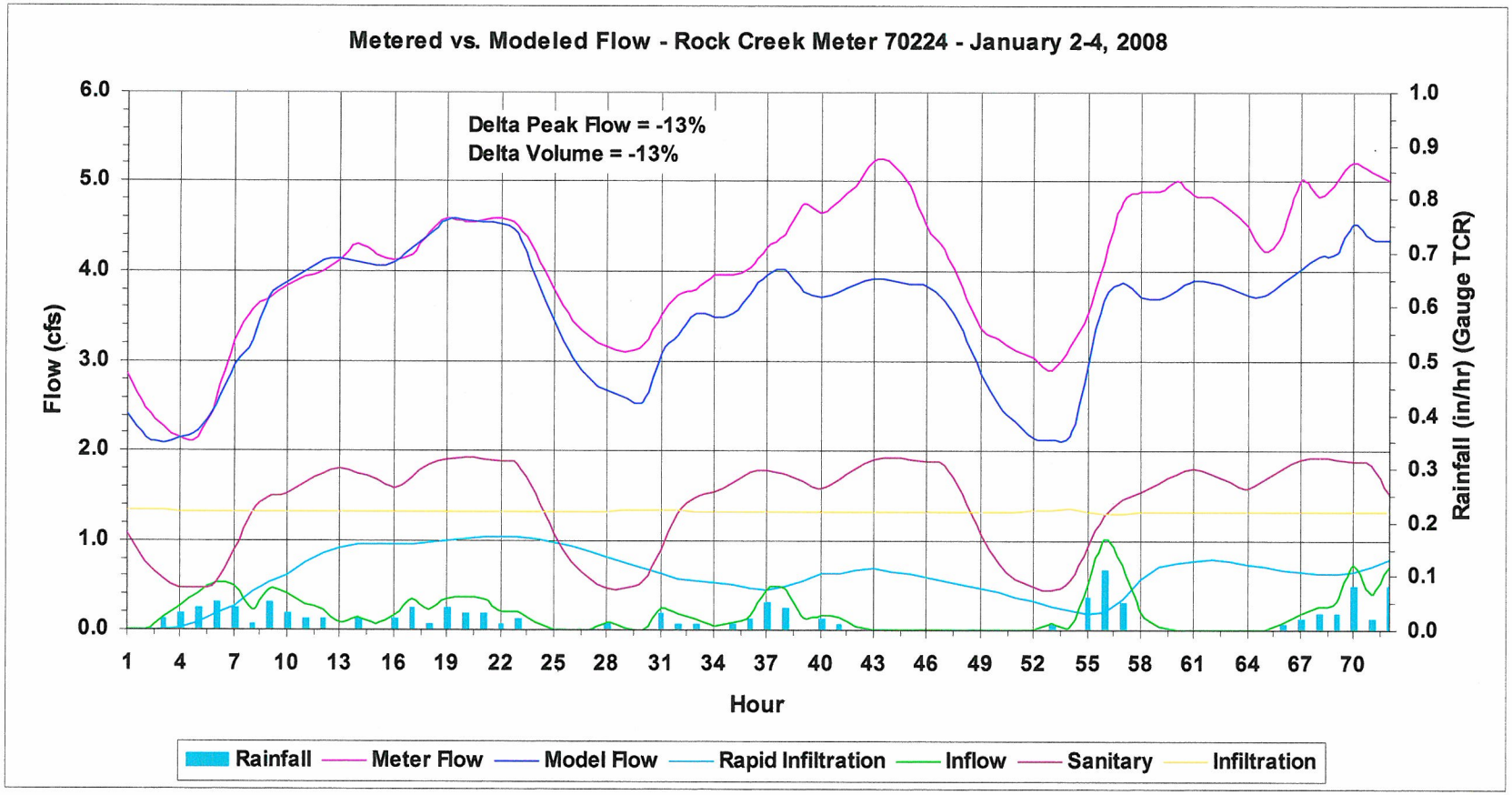

Metered vs. Modeled Flow - Rock Creek Meter 70224 - January 2-4, 2008
Delta Peak Flow = -13%
Delta Volume = -13%
Flow (cfs)
6.0
5.0
4.0
3.0
2.0
1.0
0.0
Rainfall (in/hr) (Gauge TCR)
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 27

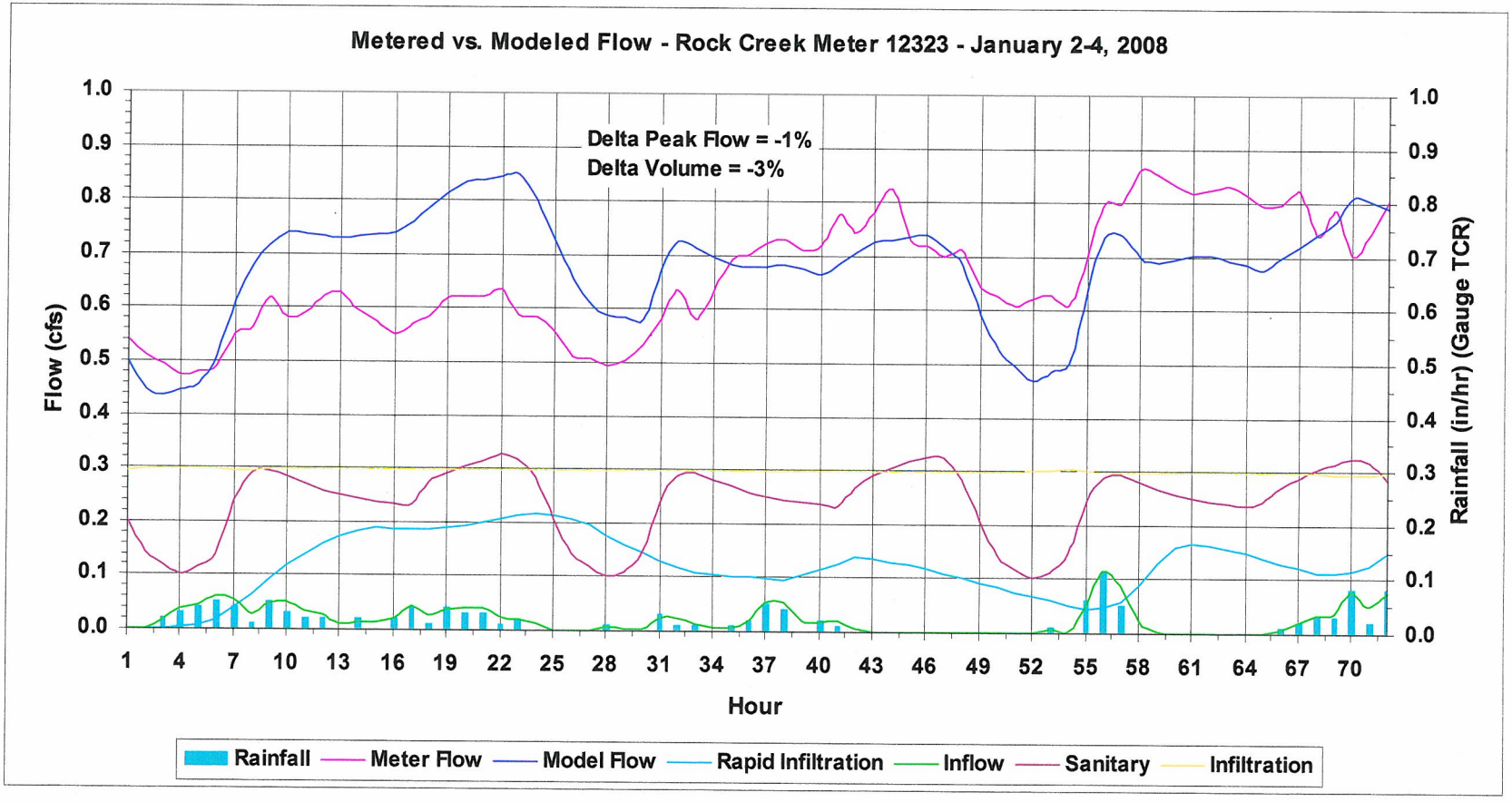

Metered vs. Modeled Flow - Rock Creek Meter 12323 - January 2-4, 2008
Delta Peak Flow = -1%
Delta Volume = -3%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 4 7 10 13 16 19 22 25 28 31 34 37 40 43 46 49 52 55 58 61 64 67 70
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 28

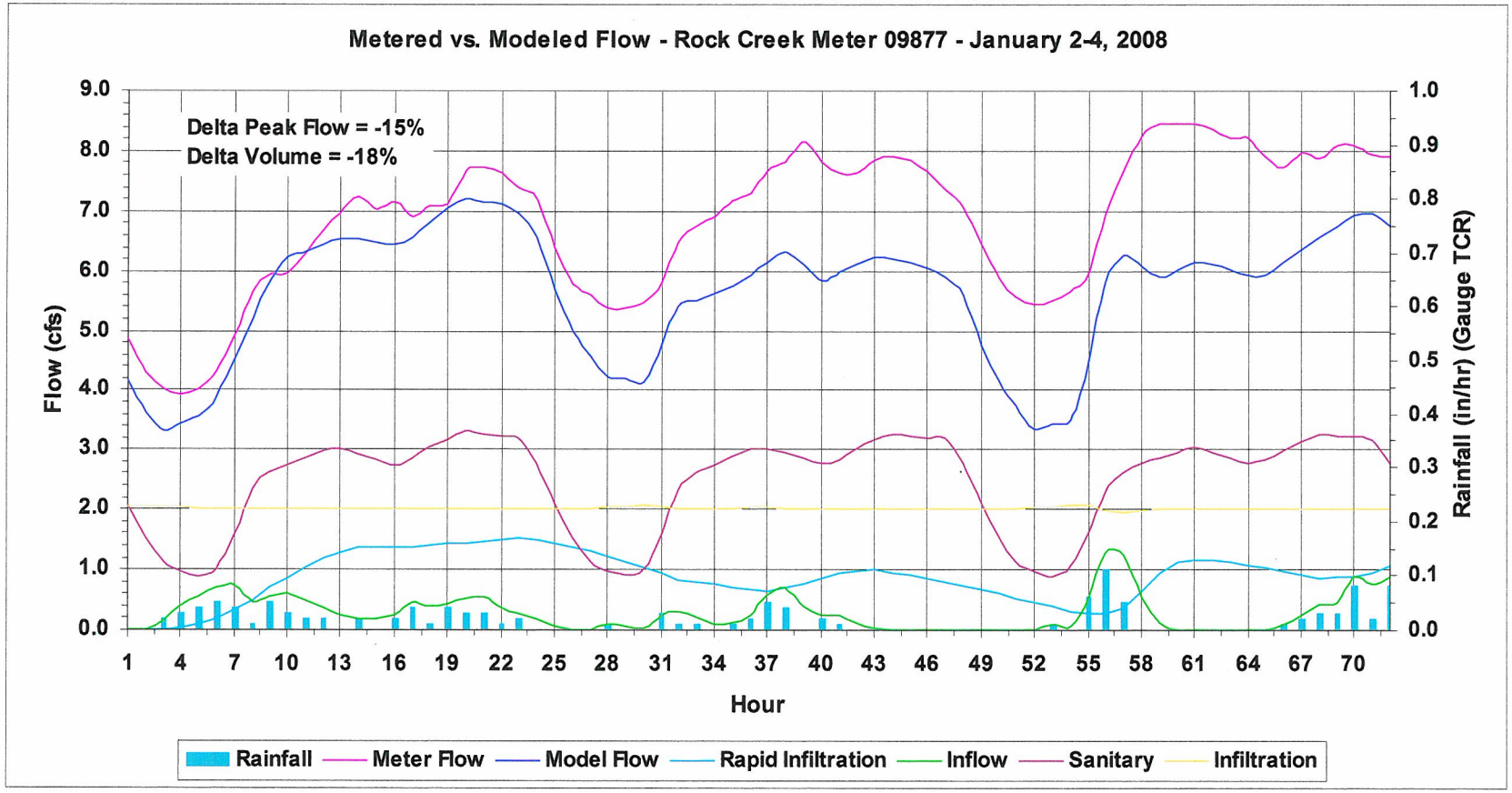

Metered vs. Modeled Flow - Rock Creek Meter 09877 - January 2-4, 2008
Delta Peak Flow = -15%
Delta Volume = -18%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 29

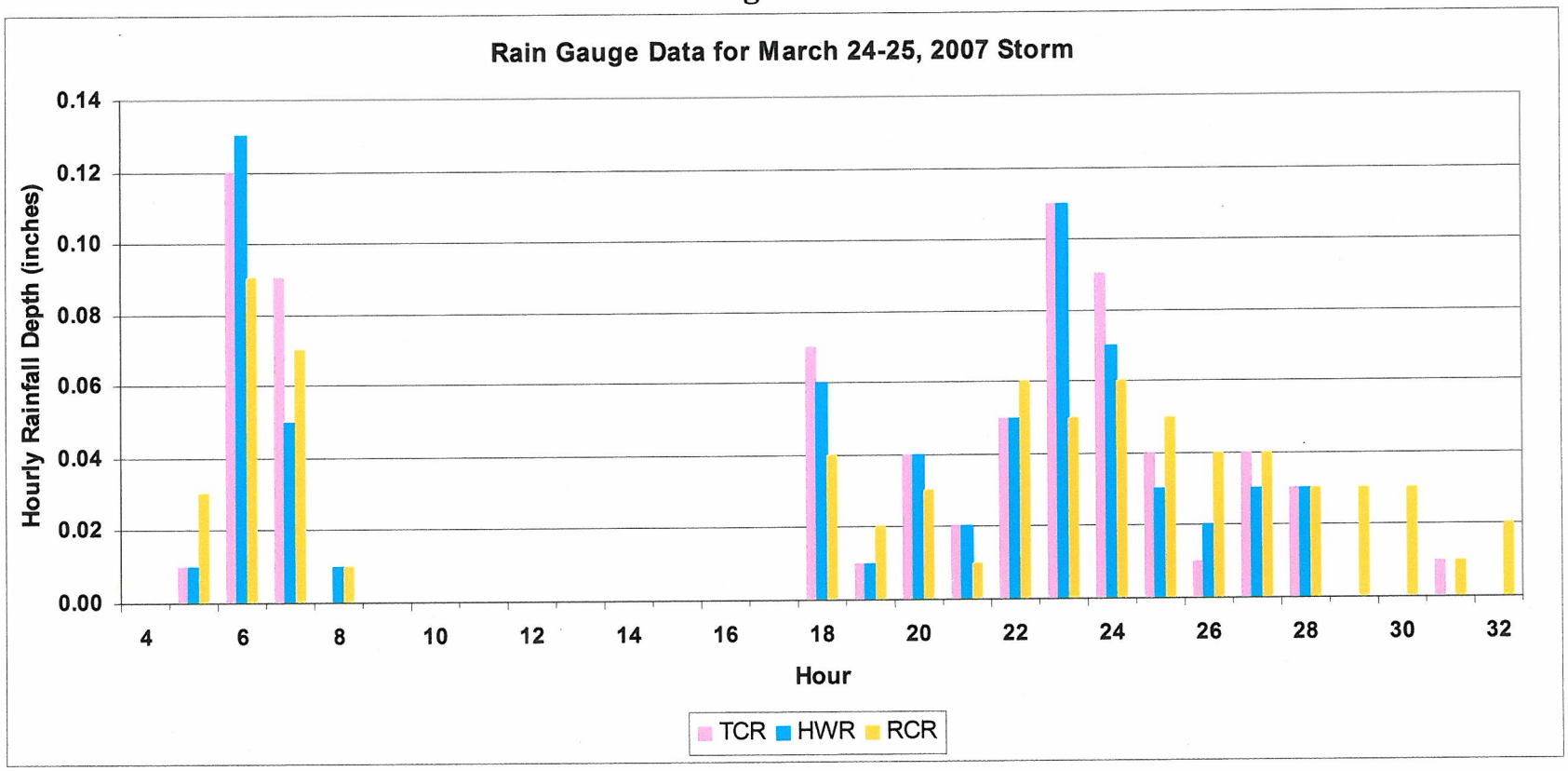

Rain Gauge Data for March 24-25, 2007 Storm
Hourly Rainfall Depth (inches)
0.14
0.12
0.10
0.08
0.06
0.04
0.02
0.00
4
6
8
10
12
14
16
18
20
22
24
26
28
30
32
Hour
TCR
HWR
RCR

Figure 30

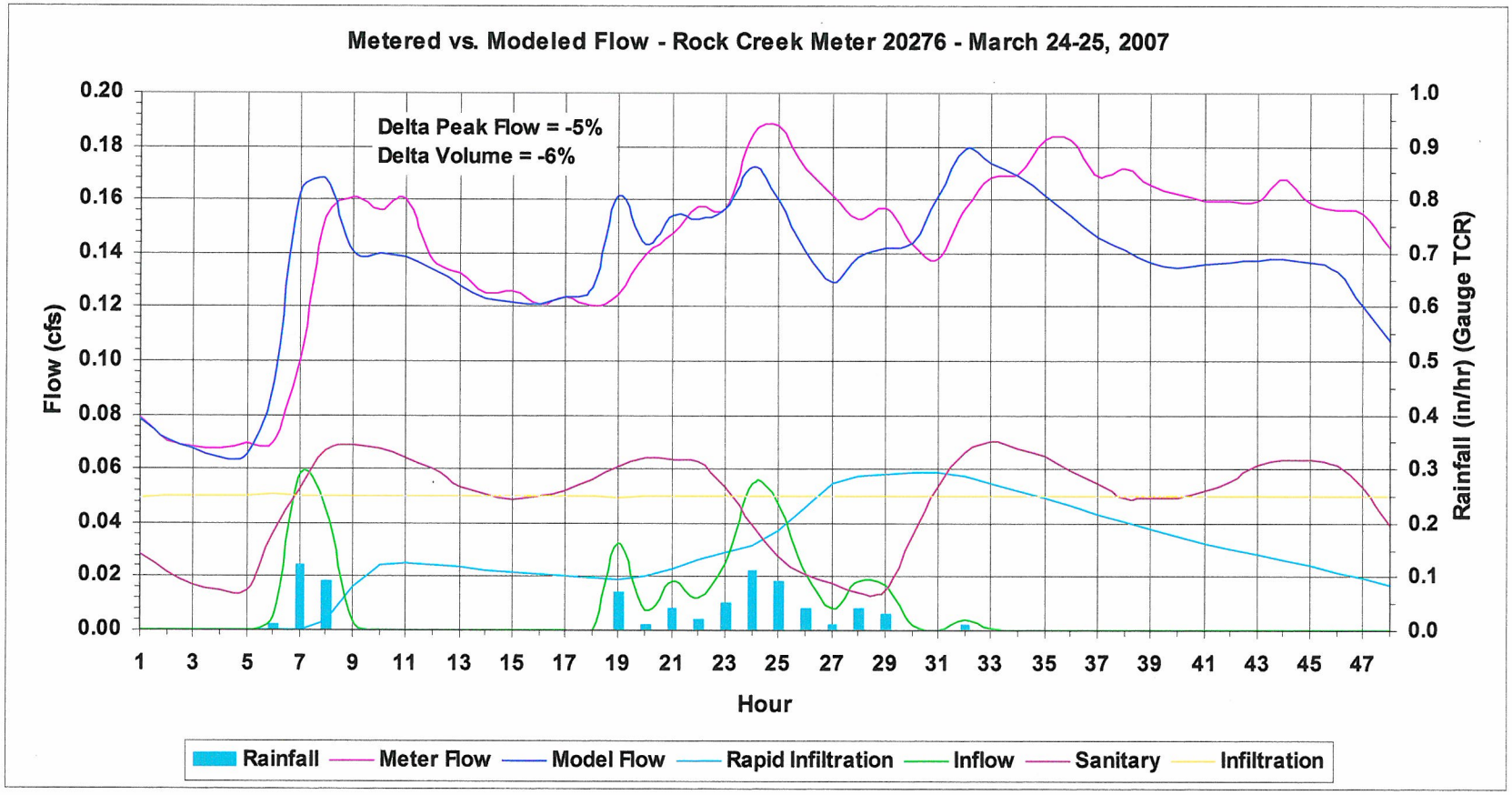

Metered vs. Modeled Flow - Rock Creek Meter 20276 - March 24-25, 2007
Delta Peak Flow = -5%
Delta Volume = -6%
Flow (cfs)
0.20
0.18
0.16
0.14
0.12
0.10
0.08
0.06
0.04
0.02
0.00
Rainfall (in/hr) (Gauge TCR)
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
1 3 5 7 9 11 13 15 17 19 21 23 25 27 29 31 33 35 37 39 41 43 45 47
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 31

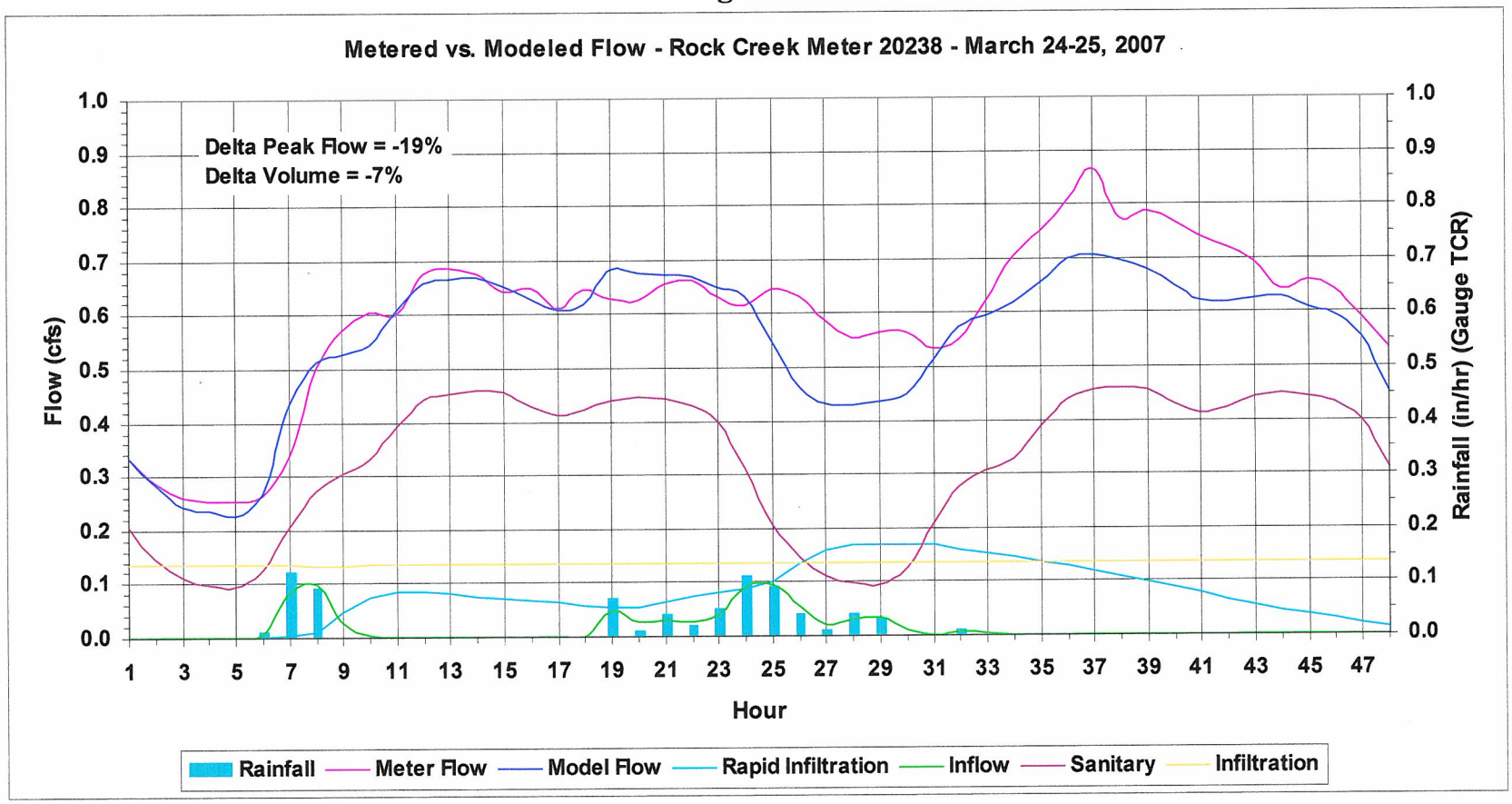

Metered vs. Modeled Flow - Rock Creek Meter 20238 - March 24-25, 2007
Delta Peak Flow = -19%
Delta Volume = -7%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 32

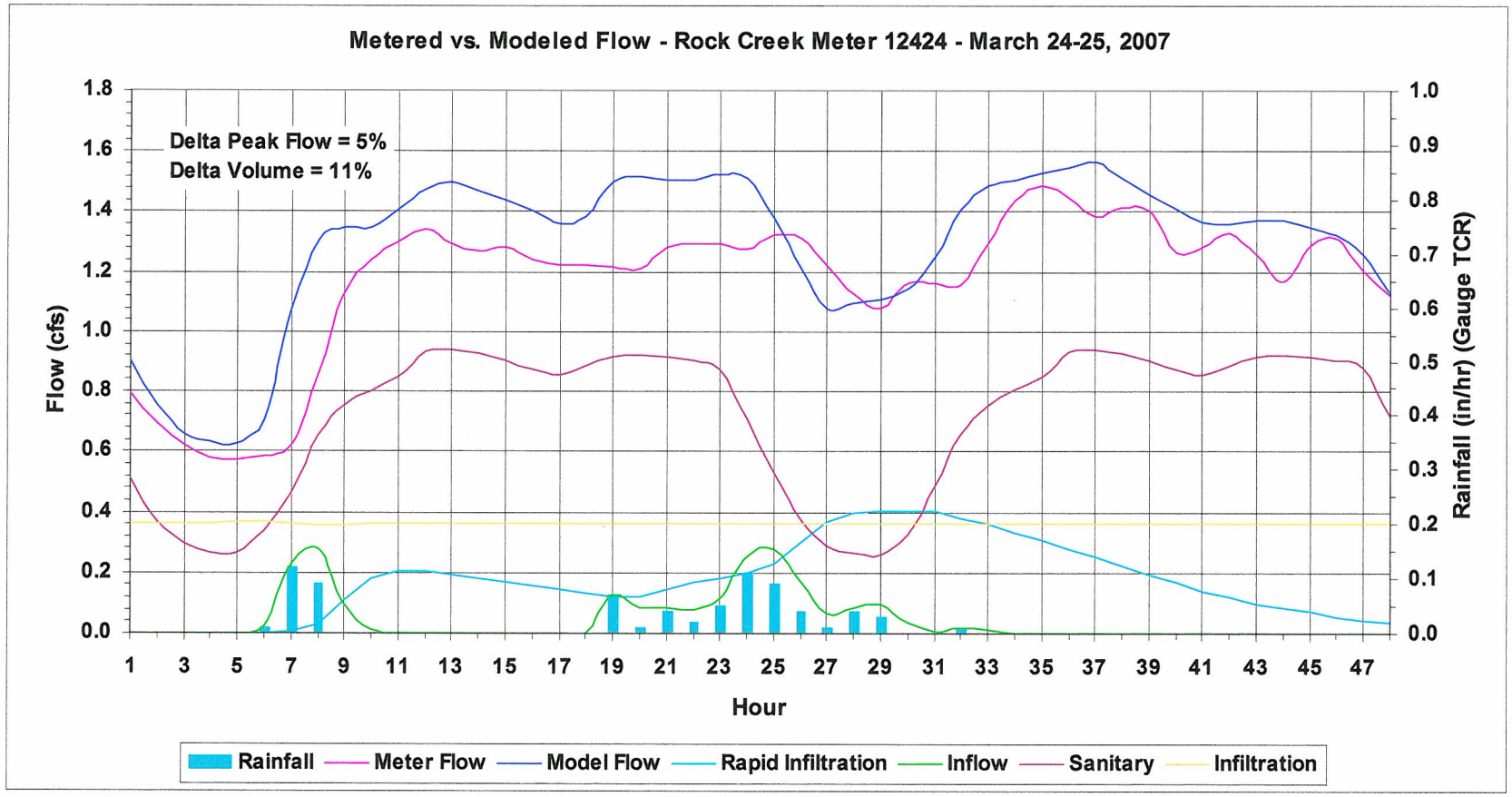

Metered vs. Modeled Flow - Rock Creek Meter 12424 - March 24-25, 2007
Delta Peak Flow = 5%
Delta Volume = 11%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 33

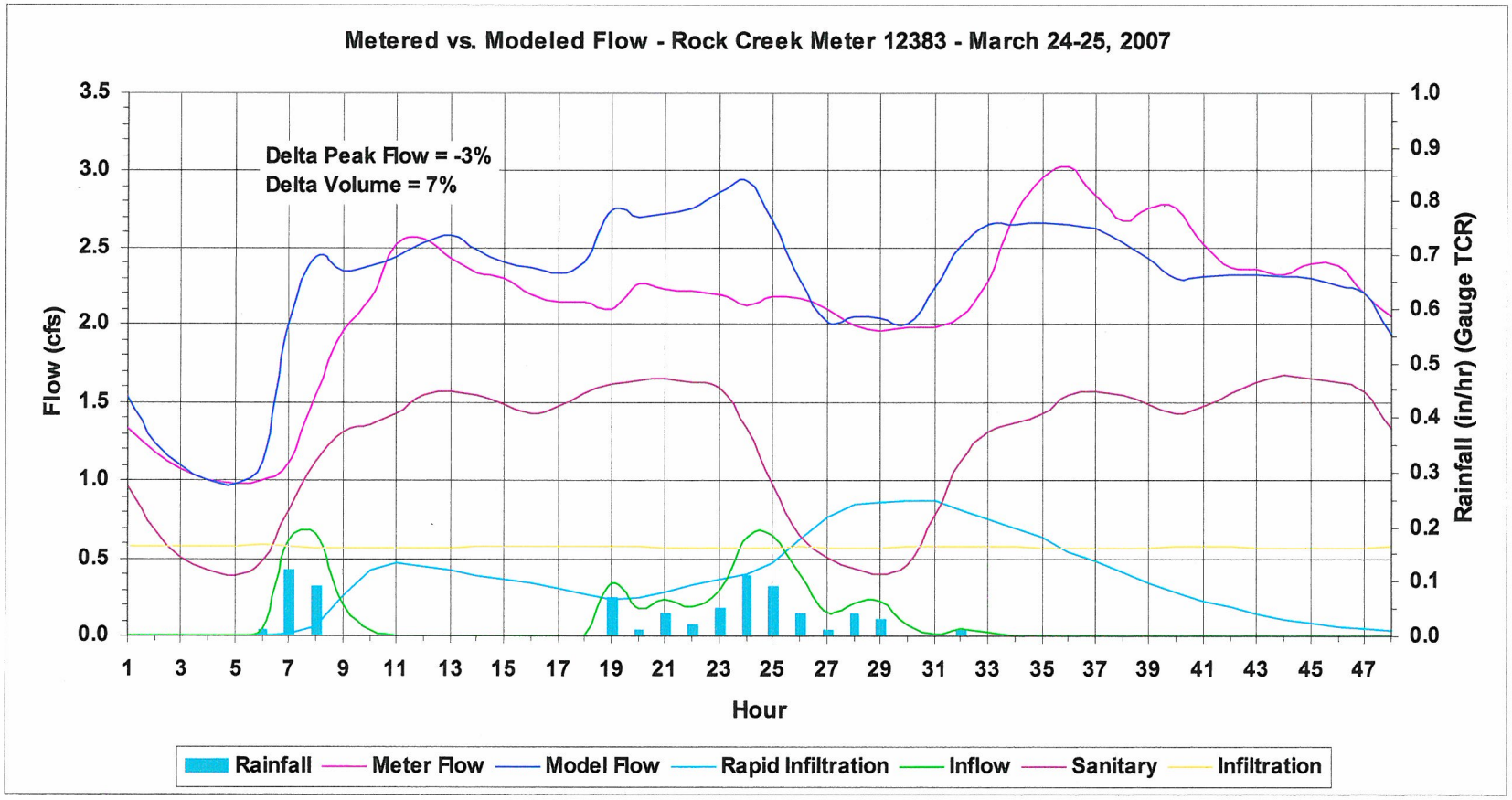

Metered vs. Modeled Flow - Rock Creek Meter 12383 - March 24-25, 2007
Delta Peak Flow = -3%
Delta Volume = 7%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 34

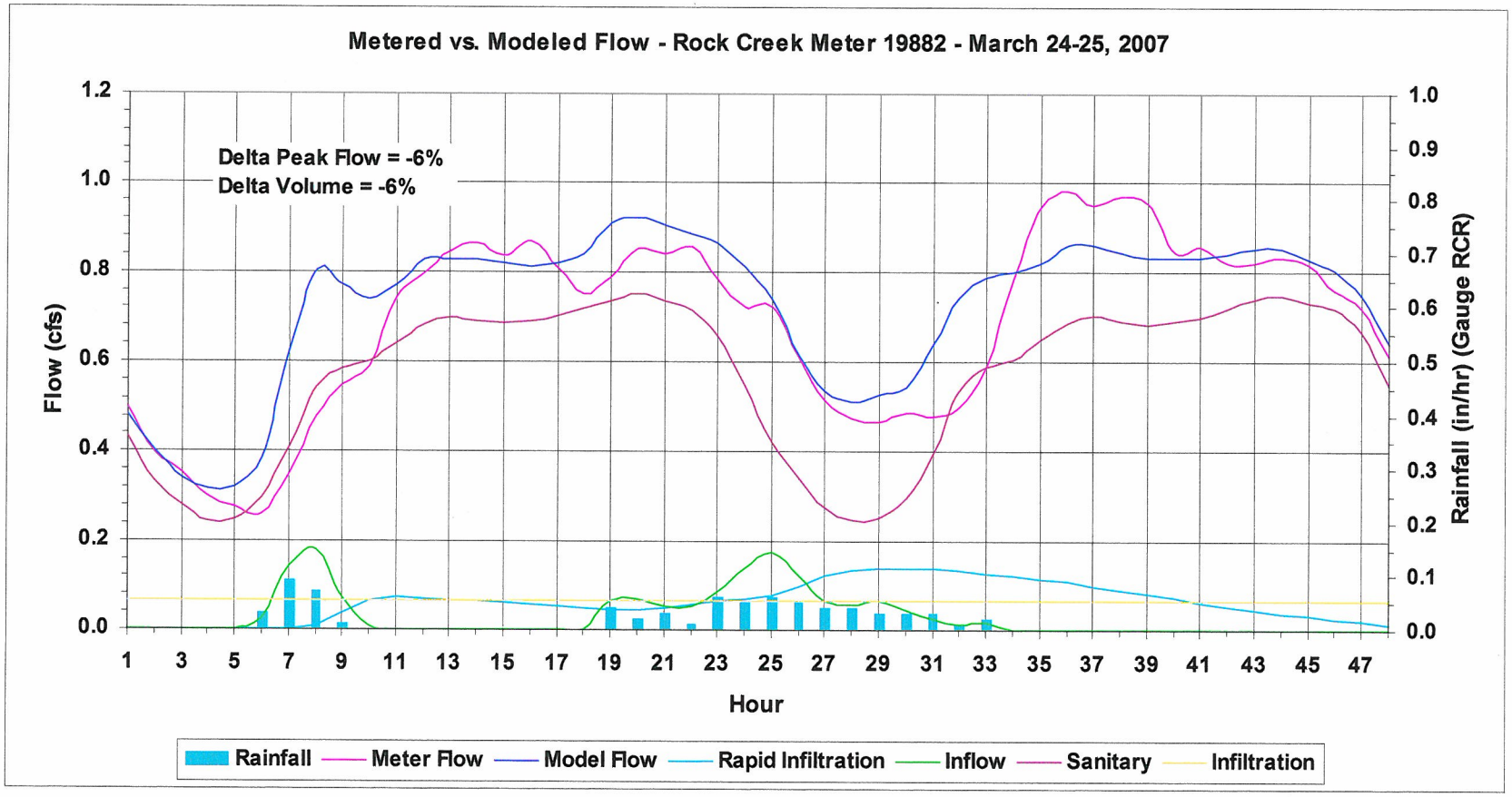
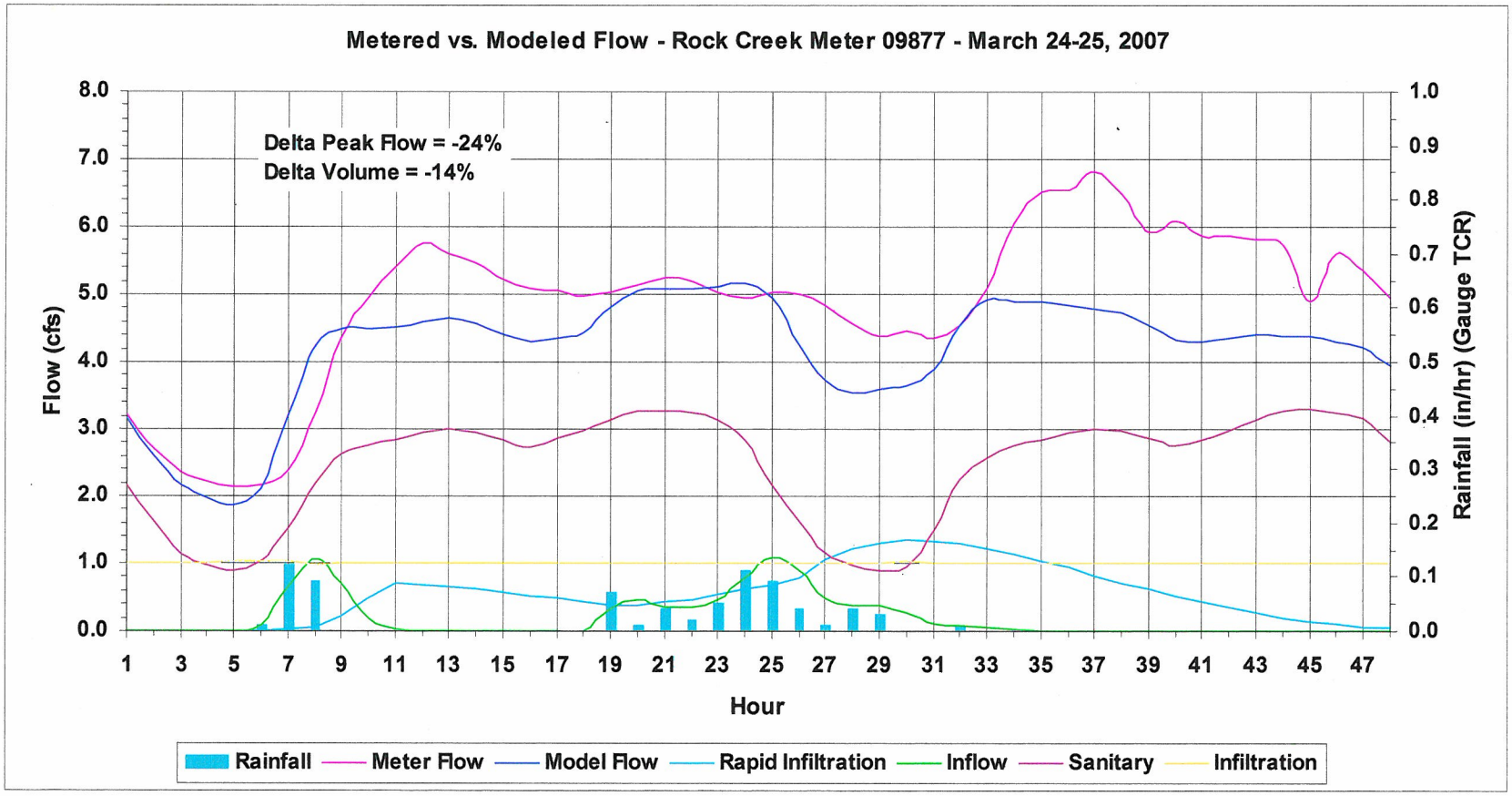

Metered vs. Modeled Flow - Rock Creek Meter 19882 - March 24-25, 2007
Delta Peak Flow = -6%
Delta Volume = -6%
Flow (cfs)
Rainfall (in/hr) (Gauge RCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

Figure 35


Metered vs. Modeled Flow - Rock Creek Meter 09877 - March 24-25, 2007
Delta Peak Flow = -24%
Delta Volume = -14%
Flow (cfs)
Rainfall (in/hr) (Gauge TCR)
Hour
Rainfall
Meter Flow
Model Flow
Rapid Infiltration
Inflow
Sanitary
Infiltration

TABLES

Table 1. Evaluation and Revisions to Land Use Layer for Existing Conditions - Hillsboro East Interceptor (Rock Creek Basin)
Table 2. 2007 RC HEI Monitor Areas & Sequence Summary
Table 3. 2007 RC HEI Monitor Areas & Sequence Summary - Developed

Evaluation and Revisions to Land Use Layer for Existing Conditions - Hillsboro East Interceptor (Rock Creek Basin)

West-Yost Land Use Layer - Existing System																		Flow Data Analysis & Model Calibration				
G_ID	LU_AREA (Total Area)	RES_POP (Developed Acres)	RES_CPC	RES_DIU	VIS_POP (Developed Acres)	VIS_CPC	VIS_DIU	LU_GIO GIS_KEY	SE_GID	SE Area	Meter	Total Acres	RES Acres	COM Acres	Residual Acres Developed	% RES Acres	% COM Acres	Total Unit Flow (gpad)	Calibrated RES_CPC	Calibrated RES_ACTIVE	Calibrated VIS_CPC	Calibrated VIS_ACTIVE
117	58.21	14.54	2013.15	DIU_3WDMed	21.46	787.07	DIU_4WDMed	116	387	58.22	0								916	100%	916	100%
123	40.13	14.97	754.17	DIU_4WDMed	18.70	1097.70	DIU_12325	122	73	40.13	0							(Average)	916	100%	916	100%
392	61.24	18.85	2013.15	DIU_3WDMed	33.13	1099.55	DIU_4WDMed	391	272	61.24	0	159.58	48.36	73.29	121.65	40%	60%	916	916	100%	916	100%
116	13.42	4.57	277.14	DIU_1WDMed	0.95	0.00	DIU_4WDMed	115	388	13.42	09877								1022	100%	1022	100%
124	37.10	24.90	277.14	DIU_1WDMed	5.57	0.00	DIU_4WDMed	123	283	37.10	09877								1022	100%	1022	100%
125	46.67	30.90	277.14	DIU_1WDMed	0.80	0.00	DIU_4WDMed	124	385	46.67	09877								1022	100%	1022	100%
136	24.31	16.24	277.14	DIU_1WDMed	1.12	0.00	DIU_4WDMed	135	382	24.31	09877								1022	100%	1022	100%
400	24.38	18.32	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	399	281	24.38	09877								1022	100%	1022	100%
427	31.20	24.85	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	426	316	31.20	09877	177.06	119.78	8.44	128.22	93%	7%	1022	1022	100%	1022	100%
50	86.63	45.68	277.14	DIU_1WDMed	9.82	953.56	DIU_4WDMed	49	216	86.57	12315								862	95%	862	95%
52	58.81	2.82	277.14	DIU_1WDMed	41.92	199.52	DIU_4WDMed	51	215	58.82	12315								862	95%	862	95%
72	38.56	30.71	277.14	DIU_4WDMed	3.59	0.00	DIU_12325	71	422	38.56	12315								862	95%	862	95%
118	29.23	15.39	277.14	DIU_1WDMed	13.04	0.00	DIU_4WDMed	117	386	29.23	12315								862	95%	862	95%
119	41.55	33.09	957.26	DIU_3WDMed	8.16	0.00	DIU_4WDMed	118	258	41.55	12315								862	95%	862	95%
120	145.57	73.21	452.76	DIU_3WDMed	48.98	1099.55	DIU_4WDMed	119	77	145.58	12315								862	95%	862	95%
121	26.46	14.57	277.14	DIU_1WDMed	0.17	0.00	DIU_4WDMed	120	107	26.46	12315								862	95%	862	95%
122	38.11	31.04	1278.96	DIU_3WDMed	0.00	0.00	DIU_4WDMed	121	204	38.11	12315								862	95%	862	95%
397	64.33	36.48	2609.86	DIU_4WDMed	2.62	919.87	DIU_12325	396	278	64.33	12315								862	95%	862	95%
398	60.63	31.95	277.21	DIU_4WDMed	0.02	0.00	DIU_12325	397	279	60.63	12315								862	95%	862	95%
399	106.52	66.83	342.41	DIU_4WDMed	0.04	0.00	DIU_12325	398	280	106.52	12315	696.39	381.77	128.36	510.13	75%	25%	862	862	95%	862	95%
115	20.41	14.52	277.30	DIU_1WDMed	0.00	0.00	DIU_4WDMed	114	389	20.41	12323								643	100%	643	100%
135	18.61	11.88	277.14	DIU_1WDMed	1.00	0.00	DIU_4WDMed	134	312	18.61	12323								643	100%	643	100%
137	44.11	33.19	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	136	251	44.11	12323								643	100%	643	100%
138	35.42	27.67	471.61	DIU_3WDMed	0.00	0.00	DIU_4WDMed	137	284	35.43	12323								643	100%	643	100%
139	29.32	18.19	277.14	DIU_1WDMed	2.51	0.00	DIU_4WDMed	138	381	29.32	12323								643	100%	643	100%
141	18.80	14.68	554.11	DIU_3WDMed	0.00	0.00	DIU_4WDMed	140	315	18.81	12323								643	100%	643	100%
142	14.29	3.52	277.14	DIU_1WDMed	9.63	1099.55	DIU_4WDMed	141	380	14.29	12323								643	100%	643	100%
143	39.95	33.72	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	142	247	39.95	12323								643	100%	643	100%
379	28.18	21.54	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	378	250	28.19	12323								643	100%	643	100%
424	35.31	23.64	277.14	DIU_1WDMed	0.91	0.00	DIU_4WDMed	423	311	35.31	12323								643	100%	643	100%
425	19.06	14.32	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	424	313	19.05	12323								643	100%	643	100%
426	16.62	12.34	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	425	314	16.62	12323	320.09	229.21	14.05	243.26	94%	6%	643	643	100%	643	100%
133	59.70	45.20	910.63	DIU_3WDMed	1.92	0.00	DIU_4WDMed	132	252	59.70	12383								927	120%	927	120%
134	65.38	53.15	2105.09	DIU_3WDMed	1.62	0.00	DIU_4WDMed	133	253	65.39	12383								927	120%	927	120%
146	39.70	28.33	471.28	DIU_3WDMed	0.39	0.00	DIU_4WDMed	145	379	39.70	12383								927	120%	927	120%
147	18.26	11.09	316.98	DIU_1WDMed	1.50	0.00	DIU_4WDMed	146	378	18.26	12383	183.05	137.77	5.43	143.20	96%	4%	927	927	120%	927	120%
107	33.53	24.77	2567.71	DIU_1WDMed	0.09	0.00	DIU_4WDMed	106	267	33.53	12424								920	100%	920	100%
149	7.77	3.51	1786.19	DIU_1WDMed	1.84	0.00	DIU_4WDMed	148	377	7.77	12424								920	100%	920	100%
150	22.03	16.24	1909.93	DIU_3WDMed	1.45	0.00	DIU_4WDMed	149	376	22.03	12424								920	100%	920	100%
157	30.73	22.59	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	156	266	30.73	12424								920	100%	920	100%
376	16.51	10.02	557.37	DIU_3WDMed	2.30	52.25	DIU_4WDMed	375											920	100%	920	100%
377	26.35	12.25	277.14	DIU_1WDMed	7.79	1099.55	DIU_4WDMed	376	245	26.35	12424								920	100%	920	100%
430	15.06	11.33	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	429	322	15.06	12424								920	100%	920	100%
431	10.49	6.32	277.14	DIU_1WDMed	0.10	0.00	DIU_4WDMed	430	323	10.49	12424	162.47	107.03	13.57	120.60	89%	11%	920	920	100%	920	100%

Evaluation and Revisions to Land Use Layer for Existing Conditions - Hillsboro East Interceptor (Rock Creek Basin)

West-Yost Land Use Layer - Existing System																		Flow Data Analysis & Model Calibration				
G_ID	LU_AREA (Total Area)	RES_POP (Developed Acres)	RES_CPC	RES_DIU	VIS_POP (Developed Acres)	VIS_CPC	VIS_DIU	GIS_KEY (LU-GID)	SE_GID	SE Area	Meter	Total Acres	RES Acres	COM Acres	Residual Acres Developed	% RES Acres	% COM Acres	Total Unit Flow (gpad)	Calibrated RES_CPC	Calibrated RES_ACTIVE	Calibrated VIS_CPC	Calibrated VIS_ACTIVE
129	52.10	23.26	1202.79	DIU_3WDMed	13.81	1099.55	DIU_4WDMed	128	383	52.11	19882								1747	105%	1747	105%
130	43.64	23.75	277.14	DIU_1WDMed	10.37	1099.55	DIU_4WDMed	129	384	43.63	19882								1747	105%	1747	105%
131	26.94	20.53	461.89	DIU_3WDMed	0.00	0.00	DIU_4WDMed	130	286	26.94	19882								1747	105%	1747	105%
390	77.94	2.14	277.14	DIU_1WDMed	55.19	1099.55	DIU_4WDMed	389	270	77.94	19882								1747	105%	1747	105%
402	36.82	29.48	1858.75	DIU_68368	0.00	0.00	DIU_4WDMed	401	287	36.82	19882								1747	105%	1747	105%
429	28.47	14.40	277.14	DIU_1WDMed	10.00	1099.55	DIU_4WDMed	428	320	28.47	19882	265.91	113.56	89.37	202.93	56%	44%	1747	1747	105%	1747	105%
144	96.32	72.63	555.25	DIU_3WDMed	0.00	0.00	DIU_4WDMed	143	246	96.31	20206								610	105%	610	105%
145	145.73	103.10	2333.91	DIU_3WDMed	17.71	1099.55	DIU_4WDMed	144	241	145.73	20206								610	105%	610	105%
148	52.29	24.68	1419.90	DIU_3WDMed	10.13	609.49	DIU_4WDMed	147	321	52.29	20206	294.34	200.41	27.84	228.25	88%	12%	610	610	105%	610	105%
108	88.29	3.48	278.35	DIU_1WDMed	55.46	1096.87	DIU_4WDMed	107	393	88.29	20238								1137	110%	1137	110%
152	57.06	28.03	1324.21	DIU_3WDMed	20.51	1099.55	DIU_4WDMed	151	242	55.66	20238								1137	110%	1137	110%
375	52.29	36.85	1374.28	DIU_3WDMed	4.19	1099.55	DIU_4WDMed	374	243	52.29	20238								1137	110%	1137	110%
376	51.75	31.74	557.37	DIU_3WDMed	7.28	52.25	DIU_4WDMed	375	244	51.75	20238								1137	110%	1137	110%
									468	16.51	20238	249.39	100.10	87.44	187.54	53%	47%	1137	1137	110%	1137	110%
73	11.47	2.36	277.14	DIU_68368	8.03	1099.55	DIU_68368	72	421	11.47	20276								297	100%	297	100%
155	12.30	9.14	277.14	DIU_68368	0.00	0.00	DIU_68368	154	374	12.31	20276								297	100%	297	100%
156	45.02	35.49	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	155	373	44.95	20276								297	100%	297	100%
386	11.78	9.02	277.14	DIU_68368	0.00	1099.55	DIU_68368	385	261	11.78	20276								297	100%	297	100%
387	49.03	22.58	544.52	DIU_3WDMed	19.54	1099.55	DIU_4WDMed	386	263	49.03	20276	129.61	78.59	27.57	106.16	74%	26%	297	297	100%	297	100%
151	37.95	13.35	1073.52	DIU_3WDMed	18.06	1099.55	DIU_4WDMed	150	324	37.95	20283								859	200%	859	200%
153	34.01	21.08	277.14	DIU_1WDMed	4.95	1099.55	DIU_4WDMed	152	262	34.01	20283								859	200%	859	200%
154	5.87	4.13	277.14	DIU_68368	0.00	0.00	DIU_4WDMed	153	375	5.87	20283								859	200%	859	200%
158	20.29	15.18	1511.06	DIU_68368	0.00	0.00	DIU_4WDMed	157	372	20.29	20283	98.12	53.74	23.01	76.75	70%	30%	859	859	200%	859	200%
109	9.24	4.98	277.14	DIU_1WDMed	1.34	0.00	DIU_4WDMed	108	392	9.24	70224								1000	180%	1000	180%
126	21.30	13.08	277.14	DIU_1WDMed	1.85	0.00	DIU_4WDMed	125	319	21.29	12332								1000	180%	1000	180%
127	21.68	17.26	277.14	DIU_1WDMed	0.00	0.00	DIU_4WDMed	126	318	21.68	70224								1000	180%	1000	180%
128	43.96	31.30	277.14	DIU_1WDMed	0.08	0.00	DIU_4WDMed	127	282	43.96	70224								1000	180%	1000	180%
428	26.83	19.34	277.14	DIU_1WDMed	3.86	0.00	DIU_4WDMed	427	317	26.83	70224	123.01	85.96	7.13	93.09	92%	8%	1000	1000	180%	1000	180%
Totals:	2859.03	1656.28			505.50					2857.54					2161.78							
Metered:	2699.44	1607.92			432.21					2697.96					2040.13							

Hillsboro East Interceptor 2007 Flow Monitors

Basin	Monitor No.	Residual Area (acres)	Total US Area (acres)	Upstream Monitors (all inclusive)									Upstream Monitor Areas (acres)								
Rock Creek	09877	198.4	2001.6	20276	20283	20238	12424	20206	12383	70224	12323	19882	129.5	98.1	248.0	162.5	294.3	183.1	101.7	320.1	265.9
Rock Creek	12315	696.4	696.4	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	12323	320.1	320.1	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	12383	183.1	1115.5	20276	20283	20238	12424	20206					129.5	98.1	248.0	162.5	294.3	0.0	0.0	0.0	0.0
Rock Creek	12424	162.5	638.1	20276	20283	20238							129.5	98.1	248.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	19882	265.9	265.9	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20206	294.3	294.3	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20238	248.0	248.0	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20276	129.5	129.5	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20283	98.1	227.7	20276									129.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	70224	101.7	1217.2	20276	20283	20238	12424	20206	12383				129.5	98.1	248.0	162.5	294.3	183.1	0.0	0.0	0.0
		2698.0																			

Hillsboro East Interceptor 2007 Flow Monitors - Developed Area

Basin	Monitor No.	Residual Area (acres)	Total US Area (acres)	Upstream Monitors (all inclusive)									Upstream Monitor Areas (acres)								
Rock Creek	09877	128.2	1530.0	20276	20283	20238	12424	20206	12383	70224	12323	19882	106.2	76.8	187.5	120.6	228.3	143.2	93.1	243.3	202.9
Rock Creek	12315	510.1	510.1	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	12323	243.3	243.3	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	12383	143.2	862.5	20276	20283	20238	12424	20206					106.2	76.8	187.5	120.6	228.3	0.0	0.0	0.0	0.0
Rock Creek	12424	120.6	491.1	20276	20283	20238							106.2	76.8	187.5	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	19882	202.9	202.9	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20206	228.3	228.3	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20238	187.5	187.5	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20276	106.2	106.2	None									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	20283	76.8	182.9	20276									106.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Rock Creek	70224	93.1	955.6	20276	20283	20238	12424	20206	12383				106.2	76.8	187.5	120.6	228.3	143.2	0.0	0.0	0.0
		2040.1																			

APPENDIX R

Technical Memorandum dated March 30, 2009
Sanitary Sewer Master Plan Update—Cost Basis for Planning

WEST YOST ASSOCIATES
Consulting Engineers

REGISTERED PROFESSIONAL ENGINEER
73588PE
Corie Peterson
OREGON
Jan. 13, 2004
CORIE PETERSON
EXPIRES: 12/31/10

TECHNICAL MEMORANDUM

DATE: March 30, 2009 Project No.: 517-03-06-14

TO: Andy Braun
Clean Water Services District

FROM: Jeff Pelz
Corie Peterson, R.C.E. #73588 Reviewed By: Ron Berry

SUBJECT: Sanitary Sewer Master Plan Update—Cost Basis for Planning

The purpose of this technical memorandum (TM) is to present the basis of estimating planning-level costs for capital improvements identified in the Sanitary Sewer Master Plan Update. This TM documents the sources of unit costs used for the cost estimates, how the estimates are applied to sewer model output and/or post analysis to estimate construction costs, the level of contingencies and other costs applied to construction costs to estimate total planning-level project costs, and the method of apportioning system development charges (SDC). Finally, this TM conveys a request for the District's review of unit costs used for cost estimating purposes within the Master Plan Update, in light of the District's recent construction experiences as well as the District's long-term budgeting policies and practices. The cost basis for planning and the request for District input are presented under the following headings:

- Gravity Sewer Costs
- Pump Station Costs
- Force Main Costs
- Construction Contingency and Other Markup Costs
- SDC Allocation of Costs
- Requested Feedback

GRAVITY SEWER COSTS

The collection system model generates a peak flow for each link of the modeled system, estimates the hydraulic conditions resulting from that peak flow, and predicts a hydraulic grade line (HGL). The HGL information is used to rank sewers and identify needed capacity improvements. Improvements are based on pipe replacement for existing sewers and construction of new sewers in growth areas. Costs take into effect sewer depth, diameter, manholes and service laterals spaced at typical intervals and typical utility conflicts expected along both collector and arterial roads in urban areas. It is understood that alternative alignments may be evaluated during preliminary design and will be compared with the master plan on the basis of costs and other factors. The purpose of the master plan is to identify the need for a given specific project, define an apparent cost-effective conceptual alignment based on very limited information, and establish a reasonable basis for predicting the project cost.

Construction cost data from the 2000 Sewer Master Plan Update by PMA Engineering is used as the basis of gravity sewer unit costs. The subject report states that the unit costs are "pipe-in-place" costs which include manholes, service laterals, and typical utility conflict avoidance but do not include project contingencies or other costs such as engineering and administration. Cost data from PMA is indexed to the December 1999 Engineering News Record 20-cities Average Construction Cost Index (ENR CCI = 6167). For the current Master Plan Update, the unit costs have been escalated based on the November 2008 index (ENR CCI = 8602). Unit construction costs for gravity sewers are presented in Table 1.

PUMP STATION COSTS

Pump station construction costs for both new pump stations and improvements needed to existing pump stations are discussed below. For design, the most cost effective improvement must be determined on a case-by-case basis at each pump station through a more detailed analysis than that used for planning. However, for the purposes of the master plan, screening criteria were developed to recommend improvements to existing pump stations based on the magnitude of the anticipated flow increase. Where the predicted buildout flow exceeds the pump station firm capacity by up to 200%, the recommended improvement is listed as an upgrade. In these instances, it is assumed that the pump station capacity can be increased by replacing mechanical and electrical equipment without significant structural modifications.

Where the flows are expected to exceed the pump station capacity by more than double the firm capacity, complete replacement is recommended as the improvement. On Figure 1, construction costs are plotted against "firm" pumping capacity for recent pump station projects within Oregon and Northern California. A best-fit curve of the data is shown for reference, but is not recommended for planning-level cost estimates because of the wide variation in data. Rather, for the case of estimating pump station replacement costs, a planning cost curve is plotted to encompass the upper end of the cost data points and is used for planning level cost estimates to prevent underestimation of pump station costs. A minimum construction cost of $500,000 is assumed for the smallest stations.

Table 1. Unit Costs for Gravity Sewers, $/LF

Depth to Invert, ft	Diameter, inches																				
	6	8	10	12	15	18	21	24	27	30	36	42	48	54	60	72	78	84	96	108	120
4	74	86	98	110	127	144	160	177	199	219	257	311	-	-	-	-	-	-	-	-	-
5	81	92	105	117	134	151	168	185	208	228	266	321	382	448	-	-	-	-	-	-	-
6	85	98	110	123	141	158	175	193	216	236	275	331	393	458	529	-	-	-	-	-	-
7	89	102	116	128	147	165	183	201	224	245	285	341	404	469	541	670	-	-	-	-	-
8	96	109	121	134	154	172	190	209	232	253	294	352	415	481	553	683	769	856	-	-	-
9	102	116	128	142	161	179	198	216	240	262	303	362	425	492	565	697	783	873	1,031	-	-
10	109	123	135	149	168	187	205	224	249	270	313	372	436	504	578	711	797	888	1,048	1,218	-
11	114	127	141	155	175	194	213	232	257	279	322	382	447	515	590	725	812	903	1,064	1,236	1,417
12	119	133	146	160	181	201	220	240	265	287	331	392	458	527	602	739	826	918	1,081	1,254	1,435
13	124	138	152	166	188	208	228	248	273	296	341	402	468	538	614	753	841	934	1,097	1,272	1,455
14	130	144	158	173	195	215	235	256	281	304	350	412	479	550	627	766	855	949	1,114	1,290	1,475
15	134	149	163	179	202	222	243	263	290	313	359	422	490	562	639	780	869	964	1,131	1,308	1,494
16	141	155	170	186	209	229	250	271	298	322	369	432	501	573	651	794	884	979	1,147	1,326	1,514
17	146	162	177	191	215	237	258	279	306	330	378	443	512	585	663	808	898	994	1,164	1,344	1,534
18	152	169	184	198	222	244	265	287	314	339	387	453	522	596	676	822	913	1,009	1,180	1,362	1,554
19	159	174	190	205	229	251	273	295	322	347	397	463	533	608	688	836	927	1,024	1,197	1,380	1,573
20	166	181	197	212	236	258	280	303	331	356	406	473	544	619	700	849	942	1,039	1,214	1,398	1,593
21	506	523	538	554	577	601	623	646	675	700	750	817	890	967	1,048	1,198	1,292	1,391	1,565	1,752	1,947
22	529	544	561	576	600	624	646	669	699	724	775	843	916	993	1,075	1,227	1,321	1,421	1,597	1,785	1,982
23	550	566	582	598	622	646	669	692	722	748	800	868	942	1,020	1,103	1,256	1,351	1,451	1,629	1,819	2,017
24	570	587	604	620	644	669	692	716	746	772	824	894	968	1,047	1,130	1,285	1,381	1,482	1,661	1,852	2,052
25	591	608	625	642	667	692	715	739	769	796	849	919	994	1,074	1,158	1,314	1,411	1,512	1,693	1,885	2,087
26	612	630	647	664	689	714	738	762	793	820	874	944	1,020	1,101	1,185	1,343	1,440	1,543	1,725	1,919	2,122
27	635	651	670	686	711	737	761	785	816	843	898	970	1,046	1,127	1,213	1,372	1,470	1,573	1,757	1,952	2,156
28	656	674	690	708	734	760	784	809	840	867	923	995	1,072	1,154	1,241	1,401	1,500	1,603	1,788	1,985	2,191
29	676	695	713	730	756	782	807	832	864	891	948	1,021	1,098	1,181	1,268	1,430	1,530	1,634	1,820	2,018	2,226
30	697	716	734	752	778	805	830	855	887	915	972	1,046	1,124	1,208	1,296	1,459	1,559	1,664	1,852	2,052	2,261

Notes:
1. Costs are for construction only and do not include Engineering & Administration and Contingencies.
2. Costs of manholes and sevice laterals are assumed to be included in unit costs.
3. Source costs are from Clean Water Services' 2000 Sewer Master Plan Update by PMA Engineering, dated August 2001. Costs escalated to November 2008 (ENR CCI = 8602).

Similarly, for estimating pump station upgrade costs, a planning cost curve is plotted on Figure 1 to encompass the upper end of upgrade cost data points and is used to prevent under estimation of pump station upgrade costs.

For reference, Figure 1 includes upper and lower bounds of costs based on those published in "Pumping Station Design", 2nd Ed. by Sanks for new wastewater pump stations with submersible pumps. All historical cost data on Figure 1 is adjusted to current (November 2008) costs using the 20 cities average ENR CCI.

FORCE MAIN COSTS

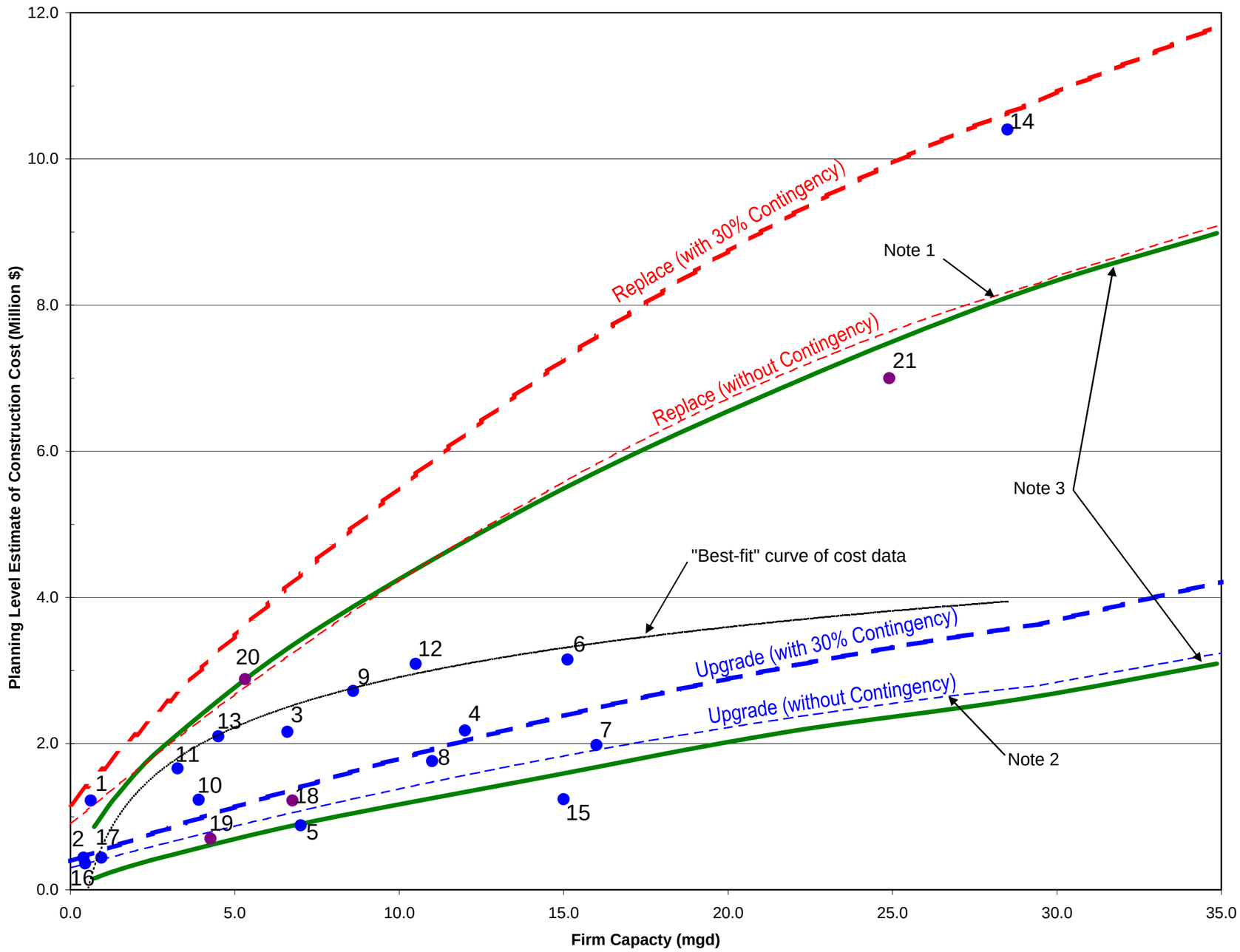
In this master plan, existing force mains are generally recommended for improvement when anticipated flow velocities would exceed 9 feet per second under the predicted peak flow conditions. The type of improvement (replacement versus paralleling) was selected based upon existing force main length, diameter, and the anticipated peak flow in the force main. It should be noted that the type of improvement (replacement versus paralleling) assumed for planning is a preliminary recommendation based upon very limited information. A more detailed comparison of force main alternatives (including a condition assessment) will be completed on a case-by-case basis during the design phase to analyze the interrelation between the characteristics of available pumping equipment and headloss system curves in force mains to determine the optimal combination of pump station and force main improvements.

WYA typically estimates the construction cost of force main improvements to range between $10 and $15 per inch diameter per foot of length (e.g. the unit construction cost for 10 inch diameter force main would range from $100 to $150 per lineal foot). For this cost range, the unit cost value of $10 per inch diameter per foot of length is used for "easy" construction conditions, such as construction in an open field without the need for asphalt patching of trenches, utility conflict avoidance, or traffic control, whereas the value of $15 per inch diameter per foot length is used for "difficult" construction conditions, such as construction with high traffic control requirements and/or with dense utility conflict avoidance needs. For this master plan, a value of $12 per inch diameter per foot of length is used reflecting a typical level of construction difficulty. The unit cost includes typical utility avoidance, sewage air relief valves, repaving saw-cut trench areas in existing streets, and moderate traffic control during construction.

CONSTRUCTION CONTINGENCY AND OTHER MARKUPS

Unit costs are based on limited information appropriate for use in master planning. A variety of factors will affect actual costs, including as yet unidentified field conditions that affect the difficulty of construction. General economic conditions, as well as construction materials, market conditions and bidding climate can also dramatically affect cost.

Total estimated capital costs include a contingency allowance of 30%, which is intended to reflect a "planning level" of project development. As a given project becomes more defined through the design process, this contingency allowance may be appropriately reduced.



	Project	Date	Capacity	Adjusted Cost ($Million)
Completed New or Replacement Pump Stations				
1.	South Airport 63rd (Portland, OR)	2004	0.6	1.22
2.	South Airport 66th (Portland, OR)	2004	0.4	0.44
3.	Mary's River (Corvallis, OR)	2002	6.6	2.16
4.	Brooklane (Corvallis, OR)	2003	12.0	2.18
5.	Creswell WTS (Creswell, OR)	2004	7.0	0.88
6.	Harlow Rd. (Springfield, OR)	2007	15.1	3.15
7.	Westside Interceptor (Lebanon, OR)	2001	16.0	1.98
8.	SSSD WWTF (Klamath Falls, OR)	2001	11.0	1.76
9.	Leisure Town Rd. (Vacaville, CA)	1996	8.6	2.72
10.	Vaca Valley Pkwy (Vacaville, CA)	1998	3.9	1.23
11.	Horse Creek (Vacaville, CA)	1999	3.3	1.66
12.	System 9 Sanguinetti (Stockton, CA)	2004	10.5	3.09
13.	System 9 Origone (Stockton, CA)	2004	4.5	2.10
14.	Lower Tualatin (Tualatin, OR)	2008	28.5	10.40
Completed Upgrades				
15.	Aloha #3 Upgrade (Hillsoboro, OR)	2008	15.0	1.24
16.	Saum Creek Upgrade (Tualatin, OR)	2008	0.5	0.36
17.	RC Ranch Upgrade (Hillsboro, OR)	2008	0.9	0.44
Planning or Predesign Estimates (Future Projects)				
18.	Sherwood Upgrade[1] (Sherwood, OR)	2008	6.8	1.22
19.	River Rd Upgrade[1] (Hillsboro, OR)	2008	4.3	0.70
20.	North Plains[1] (North Plains, OR)	2008	5.3	2.88
21.	Dawson Creek[1] (Hillsboro, OR)	2008	24.9	7.00

[1] Clean Water Services 2008 Cost Estimate

Note 1.
Replacement Costs Curve equations:
Construction Cost, $ = -4,200 x FC ^ 2 + 375,000 x FC + 900,000
(applicable range: 0 mgd < FC <= 30 mgd)
= 140,000 x FC + 4,200,000
(applicable range: FC > 30 mgd)
where, FC means "Firm Capacity" in mgd

Note 2.
Upgrade Costs Curve equations:
Construction Cost, $ = -1,200 x FC ^ 2 + 120,000 x FC + 300,000
(applicable range: 0 mgd < FC <= 30 mgd)
= 80,000 x FC + 450,000
(applicable range: FC > 30 mgd)

Note 3. Range of Costs from Sanks "Pumping Station Design", 2nd Ed., Figure 29-3 ("firm" capacity of submersible pumps)

Note 4. Historical Costs from Completed Pump Stations and Sanks are adjusted to ENR 20 Cities Average CCI for November 2008 (CCI=8602)

Figure 1. Wastewater Pump Station Planning Costs

N:\Clients\517 Clean Water Services\03-06-14 Sanitary Sewer Master Plan\ENG\PS Cost Curve Spreadsheet2.xls

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Other project costs such as engineering, construction management, District administration costs associated with the project, legal costs, and environmental compliance costs are incorporated in an allowance of 25% of the estimated construction cost plus the contingency allowance. Land acquisition and financing costs are not explicitly included in the capital cost estimate and must be accounted for during the budgeting process if expected to be significant.

SDC ALLOCATION OF COSTS

For each gravity sewer replacement that will provide additional capacity to accommodate growth, the construction cost has been apportioned in part to system development charges (SDCs). The allocation to SDCs is proportional to the capacity provided in excess of current peak flows. Where a project is needed, the total gravity flow (un-surcharged) capacity of the replacement sewer, less the modeled existing PWWF, represents the SDC share of capacity.

Example: An existing 10-inch sewer will be replaced with a 12-inch sewer.

The existing modeled PWWF is 1.12 mgd

The capacity of the new 12-inch sewer is 1.44 mgd

The SDC allocation of cost would be 22%, as follows:

$$(1.44 - 1.12) \div 1.44 \times 100\% = 22\%$$

This calculation is performed on a link-by-link basis, and then summed for the given improvement. The overall ratio of total SDC allocation to total cost for the given project may be used to determine the final SDC share once actual final costs are known.

JDP:nmp